

# Historical Developments of Pyrolysis Reactors: A Review

J.A. Garcia-Nunez<sup>1</sup>, M.R. Pelaez-Samaniego<sup>2</sup>, M.E. Garcia-Perez<sup>3</sup>, I. Fonts<sup>4,5</sup>, J. Abrego<sup>5</sup>,  
R.J.M. Westerhof<sup>6</sup>, M. Garcia-Perez<sup>7\*</sup>

<sup>1</sup>*Colombian Oil Palm Research Centre, Cenipalma, Bogotá, Colombia*

<sup>2</sup>*Faculty of Chemical Sciences, Universidad de Cuenca, Cuenca, Ecuador*

<sup>3</sup>*Facultad de Quimico Farmacobiologia, Universidad Michoacana de San Nicolas de Hidalgo,  
Morelia, Mich., Mexico*

<sup>4</sup>*Centro Universitario de la Defensa-AGM, Zaragoza, Spain*

<sup>5</sup>*Grupo de Procesos, Termoquímicos - Universidad de Zaragoza, Spain*

<sup>6</sup>*Sustainable Process Technology Group, University of Twente, Netherlands*

<sup>7</sup>*Department of Biological Systems Engineering Department, Washington State University,  
Pullman, WA, USA*

**Abstract:** This paper provides a review on pyrolysis technologies, focusing on reactor designs and companies commercializing this technology. The renewed interest on pyrolysis is driven by the potential to convert lignocellulosic materials into bio-oil and biochar and the use of these intermediates for the production bio-fuels, biochemicals and engineered biochars for environmental services. This review presents slow, intermediate, fast and microwave pyrolysis as complementary technologies that share some commonalities in their designs. While slow pyrolysis technologies (traditional carbonization kilns) use wood trunks to produce char chunks for cooking, fast pyrolysis systems process small particles to maximize bio-oil yield. The realization of the environmental issues associated with the use of carbonization technologies and the technical difficulties to operate fast pyrolysis reactors using sand as heating media and large volumes of carrier gas, as well as the problems to refine resulting highly oxygenated oils, are forcing the thermochemical conversion community to rethink the design and use of these reactors. Intermediate pyrolysis reactors (also known as converters) offer opportunities for the large scale balanced production of char and biooil. The capacity of these reactors to process forest and agricultural wastes without much preprocessing is a clear advantage. Microwave pyrolysis is an option for modular small autonomous devices for solid waste management.

1  
2  
3  
4  
5 Herein, the evolution of the pyrolysis technology is presented from a historical perspective; thus,  
6  
7 old and new innovative designs are discussed together.  
8  
9

10 **Keywords:** Pyrolysis reactors, carbonization reactors, thermochemical reactors, bio-oil, char  
11

12  
13 *\*Corresponding Author*  
14

15 Manuel Garcia-Perez  
16

17 Department of Biological Systems Engineering  
18

19 Washington State University  
20

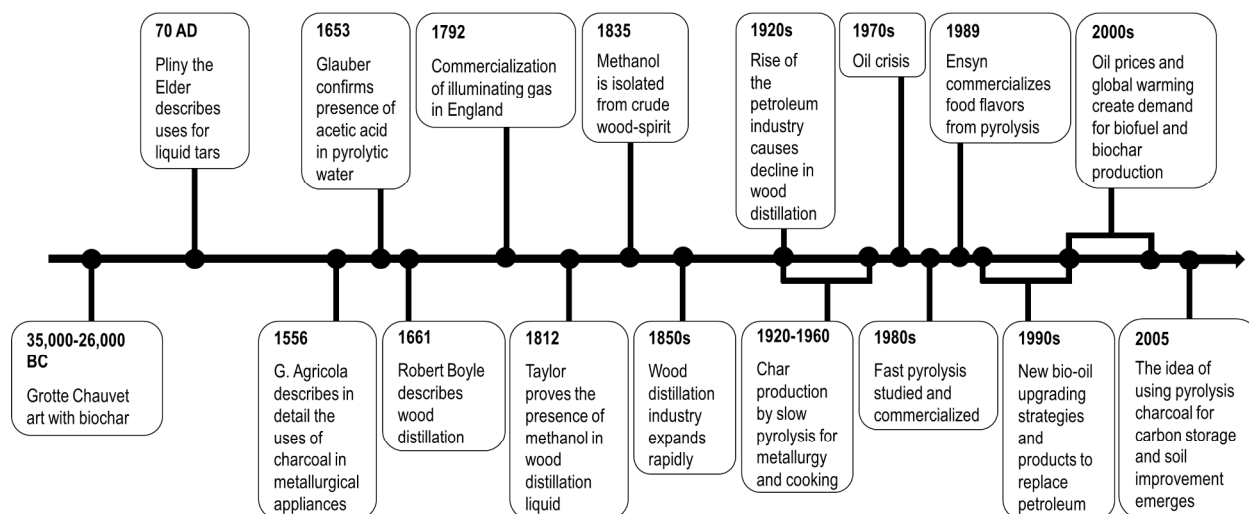
21 Pullman, WA, 99164  
22

23 Phone number: 509-335-7758  
24

25 e-mail: [mgarcia-perez@wsu.edu](mailto:mgarcia-perez@wsu.edu)  
26  
27  
28  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

## 1. Introduction

The practice of carbonizing wood to manufacture char has existed for as long as human history has been recorded<sup>1-5</sup>. Initially, producing char was the sole objective of wood carbonization<sup>2,4,5</sup>. In fact, char is the first synthetic material produced by mankind<sup>6, 7</sup>. However, new byproducts (tars, acetic acid, methanol, acetone) were obtained from wood as the civilization progressed and new reactors and bio-oil recovery systems were designed. The ancient Egyptians used pyrolytic liquid products such as fluid wood-tar and pyroligneous acid to embalm their deads<sup>5</sup>. According to the writings of Theophrastus, the Macedonians obtained wood tar from burning biomass in pits<sup>4</sup>. At the end of the eighteenth century, technologies to recover and utilize the condensable pyrolysis products were relatively well developed<sup>3,4,8</sup>. This resulted in brick kilns to recover the condensable gases that were normally lost in the pits. Iron retorts (vessels) followed brick kilns. In the 19<sup>th</sup> century the “acid-wood industry”, also known as the “wood distillation industry” was established<sup>9</sup> to produce charcoal and liquid by-products (e.g. acetic acid, methanol and acetone). The historical development of carbonization industry is one of the most fascinating in the annals of the Industrial Chemistry<sup>1,4</sup>. The hardwood distillation industry is frequently considered the precursor of the modern petrochemical industry<sup>10</sup>. The rise of the petroleum industry at the beginning of the twentieth century, with cheaper products, caused the decline of the pyrolysis industry. However, the oil crisis during the 1970’s forced to reconsider biomass pyrolysis as a technology that could contribute to reduce our dependency on fossil oil. The “fast” pyrolysis reactors were introduced at that time, aiming at maximizing liquid products<sup>11-19</sup>. Recent advances in bio-oil hydrotreatment<sup>20,21</sup>, bio-oil fractionation<sup>22-25</sup> and new bio-oil derived products (e.g., transportation fuels, phenol formaldehyde resins, carbon fibers) are catalyzing the development of bio-oil refineries. Figure 1 shows important developmental milestones of pyrolysis technology.



**Figure 1.** Some important milestones in the development and use of pyrolysis (Adapted from:<sup>2,4,5</sup>)

The social and economic impact of wood carbonization in today's world is significant<sup>26</sup>. The wood used as fuelwood and charcoal is about half of the wood extracted from forest, generating income for 40 million people worldwide<sup>26</sup>. The world's top producers of charcoal are (in descendent order): Brazil, Nigeria, Ethiopia, India, the Democratic Republic of Congo, Ghana, Tanzania, China, Madagascar and Thailand<sup>26</sup>. Today this industry contributes with an estimated \$ 650 million to Tanzania's economy (300 000 people involved in production and trade)<sup>26</sup>. The Food and Agriculture Organization (FAO) of the United Nations, estimated that 2.4 billion people in developing nations use charcoal as domestic fuel<sup>26-31</sup>. Approximately, 3 billion people still lack access to clean fuels and technologies for cooking<sup>26</sup>. According to the FAO<sup>32</sup> more than 52 Mt of charcoal were produced worldwide in 2015 (Africa 62 %, Americas: 19.6 % and Asia: 17 %)<sup>26</sup>, showing an increase of close to 20 % since 2005. Since current char yields a mere 20 wt. % of the original biomass, it can be estimated that more than 260 Mt of wood are currently processed worldwide to produce charcoal. Between 1 and 2.4 GT CO<sub>2eq</sub> of greenhouse gases are emitted annually in the production and use of fuelwood and charcoal which represents 2-7 % of global anthropogenic emissions<sup>26,33</sup>. Charcoal produced using sustainable managed resources and improved pyrolysis technologies has the potential to reduce emissions by 80 %<sup>26</sup>. Therefore, there are huge opportunities to improve the environmental performance of current carbonization

1  
2  
3  
4  
5 units<sup>34-36</sup>. The potential use of char as a means to fight global warming is also attracting renewed  
6 interest on pyrolysis<sup>37</sup>. Char has the capacity to increase soil fertility and sequester carbon<sup>38-41</sup>.  
7  
8 Sustainable char technology could offset up to 130 Gt CO<sub>2</sub><sub>eq</sub> emissions during the first century of  
9 adoption<sup>39</sup>. Greening the pyrolysis value supply chain (with sustainable sourcing, production,  
10 transport, and distribution) is critical to supporting livelihoods and providing energy security in  
11 developing nations<sup>26</sup>. The International Energy Agency forecasted that by 2030 charcoal will  
12 become a \$ 12 billion industry<sup>27</sup>.  
13  
14  
15  
16  
17  
18

19 According to Scopus, the number of research papers with the keyword “carbonization reactors  
20 (CR)” and “fast pyrolysis reactors (FP)” have been steadily growing: 1980-1990 (CR:59 and  
21 FP:63 papers), 1990-2000 (CR:86 and FP:88 papers), 2000-2010 (CR:306 and FP:371 papers),  
22 2010-2017 (CR:340 and FP:840 papers). Despite the growing interest to produce bio-oil and  
23 char, the disperse information on pyrolysis technologies and manufacturers hinders the  
24 development of this industry. There is a vast diversity of factors affecting the pyrolysis process  
25 (different feedstocks, scale, capacity, use of mobile or stationary units) which makes it very  
26 difficult to find an exclusive design that is sustainable across all the potential feedstocks and  
27 applications.  
28  
29  
30  
31  
32  
33  
34  
35

36 Although there are excellent reviews on fast pyrolysis technologies<sup>13-19,42</sup>, on conventional  
37 carbonization reactors<sup>5, 6,41,43</sup>, and microwave pyrolysis<sup>44, 45</sup> there are only few reviews on the  
38 converters and retorts<sup>1,4,9,46</sup>. Lynch and Joseph<sup>47</sup>, published a guideline for the development and  
39 testing of pyrolysis plants for char production. Interestingly, some companies are reproducing  
40 old concepts to design new pyrolysis reactors. Thus, the main goal for this paper is to provide a  
41 comprehensive overview of pyrolysis reactors. Herein, we describe designs, operating  
42 conditions, scale, and yields to help those involved in the development of pyrolysis projects  
43 identifying robust flexible designs for their business models. This work is an attempt to present  
44 all pyrolysis reactors in a single document within a historical perspective intending that the  
45 knowledge and experience generated through centuries could serve as inspiration for the  
46 development of new designs.  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

## 2. Fundamentals of biomass pyrolysis

The main factors on the operation of pyrolysis reactors affecting the yield and composition of products are: (1) Biomass pyrolysis temperature<sup>48</sup>, (2) Particle size<sup>49-51</sup>, (3) Alkali content<sup>52-54</sup>, (4) Residence time in vapor phase<sup>55-57</sup>, (5) Pressure<sup>58-60</sup>, (6) Pretreatment temperature<sup>61, 62</sup> and (7) Heating rate<sup>55,56,63</sup>. Other factors such as feedstock composition, use of additives, and condensation conditions are outside the scope of this review.

Thermochemical depolymerization reactions are important between 250 and 600 °C<sup>63</sup>. When biomass is heated, thermal cracking of bonds in biomass constituents (cellulose, hemicellulose and lignin) happens. These primary thermal depolymerization reactions happen in the solid. When biomass macromolecules are heated, some fractions can crosslink and form a solid product<sup>63, 64</sup> and others can depolymerize into light oxygenates that can be easily evaporated<sup>65</sup> or into oligomeric products that can form a liquid intermediate<sup>66-68</sup>. This liquid intermediate is acidic which enhances dehydration and polycondensation reactions<sup>69</sup>. Most of the pyrolytic water is formed in the liquid intermediate<sup>69</sup>. The oligomeric molecules in the liquid intermediate may be removed from the hot reaction environment in the form of aerosols by thermal ejection<sup>66, 67</sup>.

Biomass particle size has a direct impact on heating rate and the release of aerosols, and ultimately on the product distribution of pyrolysis. Indeed, the evacuation of the aerosols formed during the pyrolysis reaction can proceed in two distinct ways depending on the particle size. When very small particles (mostly formed by cell walls) are used, aerosols formed in the pyrolysis reaction can be easily ejected and pyrolysis vapors can be removed without travelling inside the cell cavities<sup>50,51</sup>. Mass transfer limitations increase with particle size. The second regime involves aerosol formation inside cell walls. An important part of these aerosols is retained from escaping through the cell walls and will eventually contribute to the formation of extra char through secondary reactions. Volatile pyrolysis products are also formed inside the particles and will react on their way out of the biomass particle and of the reactor<sup>49,50</sup>. Secondary reactions are typically called intra- and extra- particle homogeneous and heterogeneous reactions<sup>49,57,70,71</sup>.

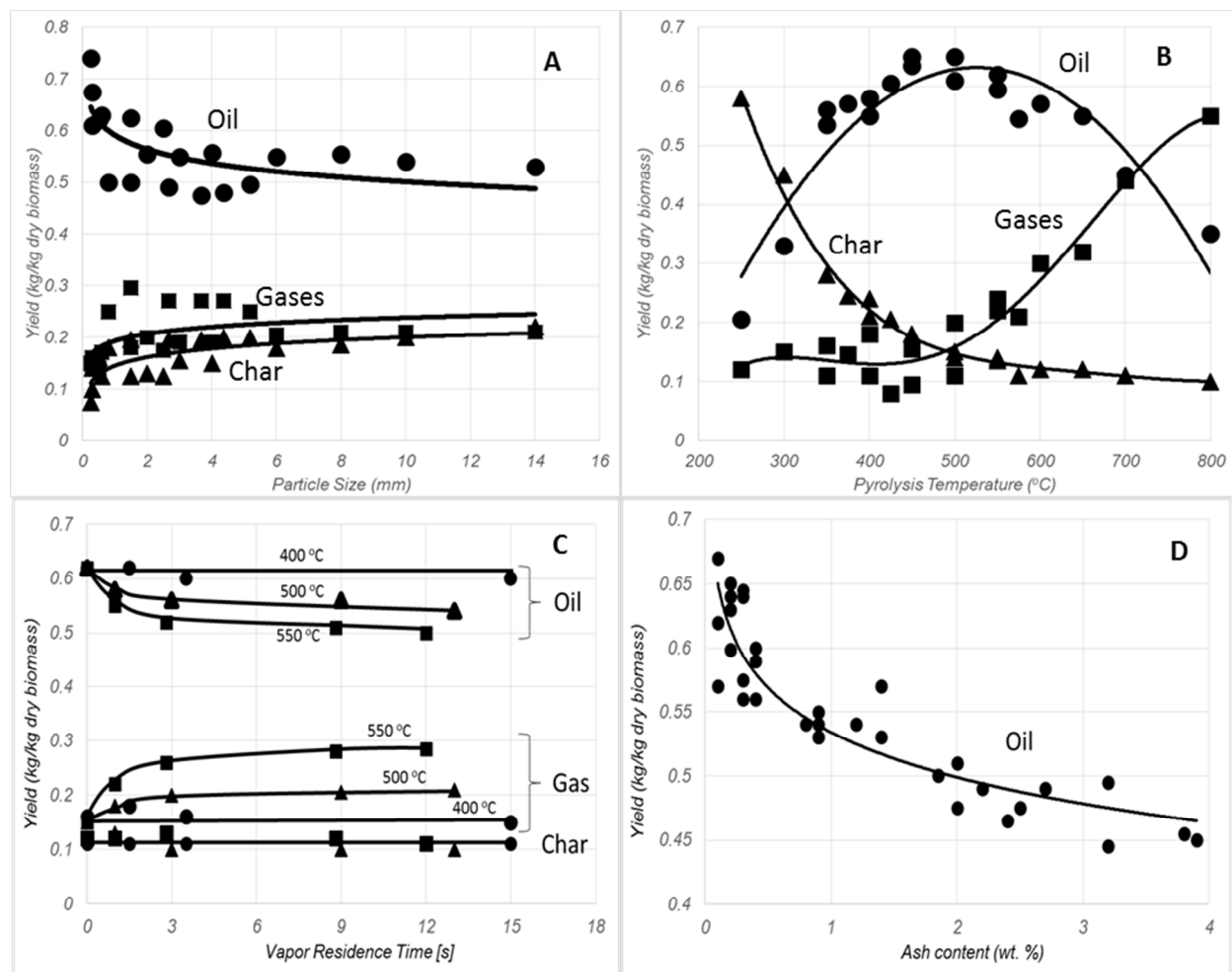
1  
2  
3  
4  
5 The temperature and hydrodynamics of the gaseous reaction environment, the presence of a  
6 secondary heating medium (e.g. sand, steel balls, reactor walls, heating tubes) and the size of the  
7 biomass particle determine the total conversion time by controlling internal particle heat transfer  
8 and reaction kinetics<sup>72</sup>. External heat transfer is determined by the reactor type and its heating  
9 method. These factors together define the traditional distinction between slow and fast pyrolysis  
10 reactors. The heat transfer in carbonization units operating with logs is controlled by the heat  
11 transfer rate inside the wood pile (bed) and inside the logs (typically low heating rates are  
12 achieved: less than 100 °C/min). Fast pyrolysis reactors typically operate with very small  
13 particles to achieve high heating rates (>1000°C/s) inside the particles and high bio-oil yields.  
14  
15  
16  
17  
18  
19  
20  
21

22 Although there are few studies on the effect of these parameters for all the reactors covered in  
23 this review, a discussion for the specific case of fluidized bed reactors is instructive to gain  
24 insights on their potential impact in other reactors. Fluidized beds are designed to maximize bio-  
25 oil yields; thus, in order to obtain an adequate gas-solid heat transfer for this purpose, the  
26 biomass particles should be very small. This is due to the poor thermal conductivity of biomass  
27 (typically around 0.1 W/mK along the grain and around 0.05 W/mK across the grain). A thin  
28 reaction layer may achieve a temperature increase of 10,000 °C/s, but the low thermal  
29 conductivity of wood will prevent this heating rate to occur throughout the entire particle. As the  
30 size of the particle increases, secondary reactions within the particle become increasingly  
31 significant, leading to the reduction of liquid yields<sup>11</sup>.  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41

42 Figure 2 shows the effect of some operational parameters on the yield of pyrolysis products in  
43 fluidized beds. These studies clearly show that to achieve high bio-oil yields: (i) the pyrolysis  
44 temperature should be between 450 and 550 °C, (ii) very small particle sizes should be used, (iii)  
45 the residence time of pyrolysis vapors inside the reactor should be minimized, and (iv) alkaline  
46 content in biomass should be low<sup>48-50, 54, 55, 73, 74</sup>. Data from this figure also suggest that: a) the  
47 type of reactor is only one of the several factors controlling product yields, and b) a careful  
48 control of the operating conditions (temperature, particle size, ash content) of systems that are  
49 not traditionally considered fast pyrolysis reactors could dramatically improve the yield of  
50 desirable products. This is especially relevant since most of the literature on fast pyrolysis from  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

1  
2  
3  
4 the 1980s and 90s focused on identifying the very stringent operational conditions that maximize  
5 bio-oil yields, while assuming that char should be combusted to provide the energy needed for  
6 the process. Instead, currently there is a growing research interest towards the design and use of  
7 simpler systems for combined production of bio-oil and char, both presently regarded as valuable  
8 products <sup>20,75</sup>. The design of reactors resulting in oils with lower oxygen content and higher  
9 yields of gases by taking advantage of the secondary homogeneous reactions in gas phase  
10 warrant further investigation.  
11  
12  
13  
14  
15  
16  
17  
18  
19  
20  
21  
22  
23  
24  
25  
26  
27  
28  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

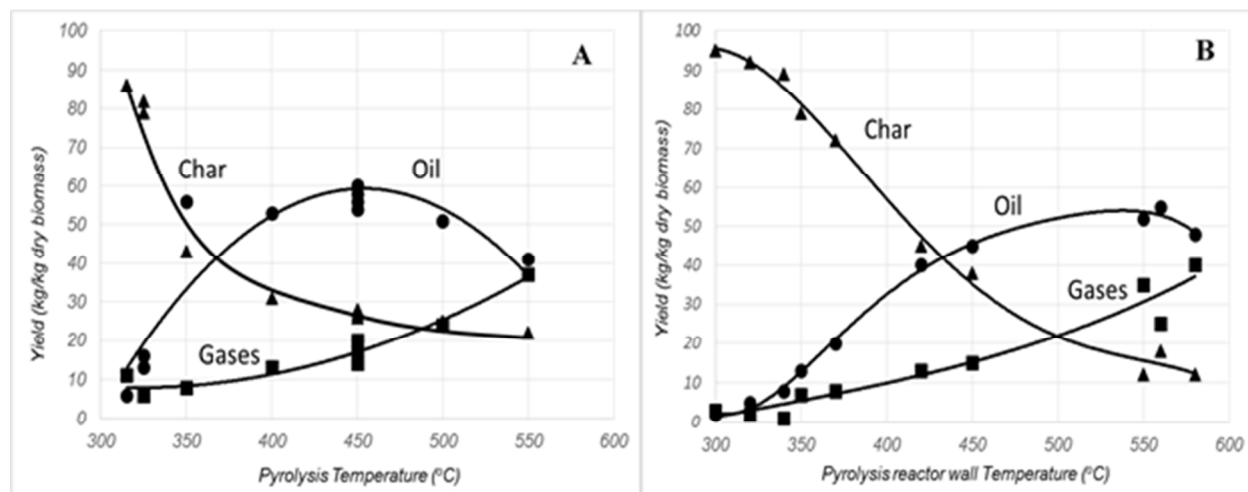




**Figure 2.** Effect of operational parameters on the yield of products during fast pyrolysis: **A:** Effect of particle size (Adapted from:<sup>49, 50</sup>) (Feedstock: Mallee wood<sup>49</sup>, Beech wood<sup>50</sup>), **B:** Effect of Pyrolysis temperature (Adapted from <sup>48, 74</sup>) (Feedstock: Pine, Beech, Bamboo, Demolition wood<sup>48</sup>, Malee Wood<sup>74</sup>), **C:** Effect of vapor residence time (Adapted from<sup>55</sup>) (Feedstock: Pine wood<sup>55</sup>), **D:** Effect of ash content (Adapted from<sup>54</sup>).

The interest in reactors capable of producing both char and bio-oil, has resulted in a growing number of designs for the balanced production of both products<sup>76, 77</sup>. Figure 3 shows the effect of the temperature on the yield of products obtained when pellets and small particles are processed in a rotary drum and in an auger pyrolysis reactor respectively<sup>76, 77</sup>. Although, bio-oil yields in the auger and rotary drum reactors were lower than for fluidized beds (see Figure 2), these

reactors are easier to operate (use less carrier gas and do not use sand) and do not consume the charcoal for their energy needs. The higher gas yields could help to satisfy an important fraction of the energy needs of these systems. Moreover, pyrolysis gas produced in Auger and rotary drums is less diluted in the carrier gas than in bubbling or circulating fluidized beds, making it more plausible their combustion in conventional boilers and gas engines.



**Figure 3.** Yield of products in (A) rotary drum (Feedstock: Arbor Pellet<sup>76</sup>) and (B) an auger pyrolysis reactor (Feedstock: Douglas Fir Wood<sup>77</sup>)

### 3. Types of pyrolysis reactors

There are hundreds of pyrolysis reactors designs<sup>78</sup>. Reviewing all of them is out of the scope of this review. Therefore, in this paper we will focus on the reactors most commonly employed. Bridgwater<sup>16</sup> classified the pyrolysis reactors based on the vapors residence time (VRT) inside the reactor and the time the biomass particle takes to reach final temperature (or heating rate) into: fast (final temperature: 500 °C, particle diameter below 2 mm, VRT: 1 s), Intermediate (final temperature: 500 °C, small particles, VRT: 1 s), Slow (final temperature: 500 °C, logs or chips, VRT: days). The term “*fast pyrolysis reactors*” refers to reactors designed to maximize the yields of bio-oil and typically use powdery biomass as feedstock. Emrich<sup>5</sup> sub-classified the slow pyrolysis (carbonization) reactors as: kilns, retorts, and converters. The term “*kiln*” is used to

1  
2  
3  
4 describe traditional char making equipment, solely employed to produce char from wood logs.  
5  
6 Industrial reactors capable of recovering char and products from volatile fractions (liquid  
7  
8 condensates and syngas) are herein referred to as “retorts or converters.” The term “retort”  
9  
10 refers to a reactor able to pyrolyze pile-wood, or wood logs over 30 cm long and over 18 cm in  
11  
12 diameter<sup>5</sup>. “Converters” produce char by carbonizing small particles of biomass such as chipped  
13  
14 or pelletized wood. The converters using small particles, operate at conditions comparable to the  
15  
16 intermediate pyrolysis reactors described by Bridgwater<sup>16</sup>. In this review we use the heating  
17  
18 mechanism to group the pyrolysis reactors into: Slow pyrolysis (Kiln, retort), intermediate  
19  
20 pyrolysis (converters), fast pyrolysis and microwave pyrolysis reactors<sup>5, 16, 44, 45</sup>. Classification of  
21  
22 reactors can also be based on: (1) the final products targeted (oil, char, heat, electricity, gases),  
23  
24 (2) the reactor’s mode of operation (batch or continuous), (3) the manner in which it is heated  
25  
26 (direct or indirect heating, auto-thermal, microwave), (4) the heat source used (electric, gas  
27  
28 heater, biomass combustion), (5) the method used to load the reactor (by hand, mechanical), (6)  
29  
30 the pressure at which the unit operates (vacuum, atmospheric, pressurized), (7) the material used  
31  
32 for the construction of the reactor (soil, brick, concrete, steel), (8) reactor portability (stationary,  
33  
34 mobile) and (9) the reactor’s position. More information on the classification of pyrolysis  
35  
36 reactors can be found elsewhere<sup>79</sup>.

37  
38 Although the type of pyrolysis reactor and its operating conditions greatly determine the quality  
39  
40 of the final targeted products, there is limited information on the open literature linking reactor  
41  
42 type, operating conditions and product quality. For charcoal, proximate analysis gives a good  
43  
44 indication of its quality. According to Antal and Gronli<sup>6</sup>, fixed carbon content of charcoal for  
45  
46 domestic cooking should have volatile matter contents of less than 30%, whereas those of  
47  
48 metallurgical charcoal should be <15%. Ash contents should be between 0.5 and 5%. These  
49  
50 values correspond to calorific values between 28 and 33 MJ/kg. For the use of charcoal as  
51  
52 biochar (soil amendment), the International Biochar Initiative provides a standardized definition  
53  
54 of its characteristics<sup>80</sup>. A common issue in carbonization reactors, especially in batch systems, is  
55  
56 the inhomogeneous quality of charcoal due to temperature gradients inside the reactor, uneven  
57  
58 gas circulation, partial combustion and heterogeneous wood particle sizes. Thus, in terms of  
59  
60 product quality, a good temperature control is a key factor for well-designed retorts or

1  
2  
3  
4  
5  
6  
7  
8  
9  
10  
11  
12  
13  
14  
15  
16  
17  
18  
19  
20  
21  
22  
23  
24  
25  
26  
27  
28  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

converters<sup>5</sup>. The type of reactor is also one of the factors that define bio-oil quality, together with biomass feedstock composition, particle size and condensation system<sup>81</sup>. The desired bio-oil characteristics will differ depending on the targeted final use, i.e, use as a fuel, further upgrading, or use as a product source. From the point of view of bio-oil as a fuel, the multiphase nature of bio-oil is a critical issue<sup>81</sup>. The bio-oil obtained by the fast pyrolysis of relatively dry materials is a homogeneous single-phase oil. The liquid obtained from intermediate, slow and microwave pyrolysis processes is typically formed by a decanted oil and an aqueous phase<sup>16</sup>. The formation of separated phases depends on the relative quantities of the polar compounds (water, sugars, pyrolytic humins), the non-polar compounds (pyrolytic lignin) and the solvents (organic compounds of low molecular weight, such as: methanol, hydroxyacetaldehyde and acetol)<sup>54, 81</sup>. Most of the research on bio-oil properties has focused on fast pyrolysis. Thus, more studies are needed to understand how the type of intermediate and slow pyrolysis reactor and their operational conditions affect bio-oil composition<sup>81-85</sup> and its multiphase behavior<sup>54, 81, 86</sup>.

#### 4. Kilns (Carbonization methods)

This section covers examples of the main groups of “kilns”: earth (mound, pit) and brick/concrete/metal (Brazilian, Argentine, Missouri, TPI) (Figure 4). There are excellent reviews and books covering these reactors<sup>5,87, 88</sup>. Therefore, this section will focus on the generalities and recent publications related with these reactors. Since, the number of recent publications on these reactors is limited, the information herein reported relates mostly with operating conditions of reactors in real settings.

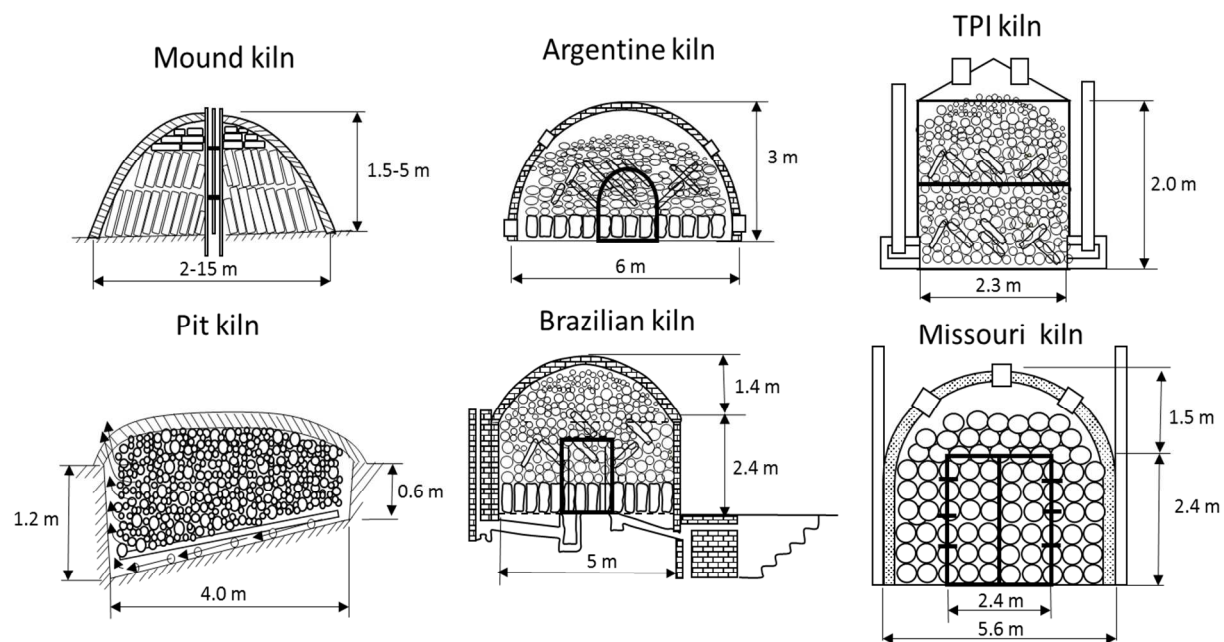
*Earth kilns* (mound pit) have been used for centuries; and are still very popular in some developing countries<sup>41</sup>. Soil is used as a barrier for oxygen attack to prevent high levels of oxidation. The liquids (condensates) released during carbonization on the soil and the vapors released to the atmosphere are important sources of pollution. Two types of earth kilns are distinguished: pit kilns and mound kilns (sometimes referred to as earth-mound kiln) (Figure 4). When the soil is well drained, deep and easy to excavate pit kilns are preferred<sup>89</sup>. The main advantage of these kilns is their low capital investment. However, the circulation of air is

1  
2  
3  
4  
5 difficult to control and are harmful to the environment with the emission of vapors to the  
6 atmosphere and the condensation of oils in soils<sup>89</sup>.  
7  
8  
9

10 *Mound kilns* can be classified into three types: vertical mound kiln, horizontal mound kiln, and  
11 improved mound kiln designs (the Casamance mound kiln)<sup>90</sup>. Casamance-type kilns, which use  
12 oil drums as chimneys, are the result of improvements made during the 1970's and 1980's. The  
13 Casamance kiln can typically produce up to 1.7 times more charcoal than a traditional earth kiln  
14 (i.e., reaching efficiencies from 20 wt. % in pit kilns to 34 wt. %)<sup>27, 29, 90, 91</sup>. A number of factors,  
15 such as location of kilns, conditions and type of wood, as well as qualification of operators,  
16 greatly affect the carbonization efficiency of earth mound kilns. This explains why some  
17 publications present different yields for similar types of kilns operating in different places. For  
18 example, Mangue<sup>27</sup> reports efficiencies from 12 to 16 % in Mozambique. Schenkel et al.<sup>90</sup> show  
19 tables comparing efficiencies of similar kilns operated in other latitudes, with efficiencies  
20 varying from 12 to 34%. Kammen and Lew<sup>29</sup> show the charcoal energy yield as a function of the  
21 kiln size for traditional kilns and the Casamance kiln, noticing a better efficiency of the latter.  
22 The average energy efficiency is around 18 % for the traditional kiln and 32% for the Casamance  
23 kiln<sup>29</sup>. Menemencioglu<sup>92</sup> reported data on wood charcoal production in Turkey. The author  
24 collected data from 44 kilns ranging from 25 to 45 m<sup>3</sup>, which were built by 23 adults. Typically,  
25 1 kg of charcoal was obtained from every 5 to 6 kg of biomass, using 1350 tons oak and having  
26 255 tons of charcoal. The average productivity was 11 t of charcoal per adult for the 7 month  
27 production season. The wholesale price was \$0.7 kg<sup>-1</sup> resulting in an average income of \$7,761  
28 per season (7 months)<sup>92</sup>.  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44

45 The main advantage of earth mound kilns is that they are simple, made of earth and can be built  
46 in the same area that the biomass is available. This technology is well suited to operate with logs.  
47 Its final product (charcoal chunks) can be easily commercialized as domestic fuel in some  
48 developing nations. No special equipment is required and the initial investment is low (\$ 27/t<sup>87</sup>).  
49 This kiln is easy to operate and very flexible with regards to capacity<sup>89</sup>. Its main disadvantages  
50 are: high labor demand, char is dirtied by the covering, sensitiveness to weather conditions, very  
51 poor control of carbonization, low efficiency, difficulty to carbonize small size agricultural  
52  
53  
54  
55  
56  
57  
58  
59  
60

wastes and the release of very large quantities of organic pollutants<sup>89</sup>. A detailed description on the construction and operation of earth kilns can be found elsewhere<sup>10, 88, 89</sup>. Some of the main characteristics of these kilns are presented in Table 1.



**Figure 4.** Schematic representation of typical kilns. Dimensions are presented for reference only (Adapted from<sup>5, 88, 89</sup>).

**Table 1.** Characteristics of kilns for charcoal production

	Earth kiln	Cinder block, brick and metal kilns
Types/Representative kilns	Pit kilns and Mound kilns	Brazilian beehive and Half orange kiln, Argentine beehive kiln, Adam retort, TPI kiln, New Hampshire, Connecticut kiln, Missouri kiln
Construction materials	Earth	Cinder/brick/concrete/Iron bands <sup>44</sup>
Portability	Built in place	Stationary
Carbonization duration	1-5 weeks <sup>89</sup>	10-30 days <sup>43, 89</sup>
Capacity*****	Mound: 50-32,000 kg (3-330 m <sup>3</sup> ) <sup>93</sup> Casamance: 50-1,000 kg <sup>87</sup>	Brazilian: 20 t <sup>87</sup> Argentine: 30 t <sup>87</sup> Missouri: 80 t <sup>87</sup>
Charcoal yields reported	Pit kiln: 12–30 wt. % <sup>29</sup> ; 12–16 wt. % <sup>28</sup> Mound: 2 – 42 wt. % <sup>29</sup> Casamance: 30 wt. % <sup>87</sup>	Brick: 12-33 wt. % <sup>29</sup> Portable Steel (TPI): 19-31 wt. % <sup>29</sup> Missouri: 33 % <sup>29</sup>
Loading and discharge methods	Manual	Manual/Mechanical
Dimension of reactor	Pit kiln: depth 0.6-1.2; length: 4.0 m, capacity: 1-30 m <sup>3</sup> Mound kiln: diameter: 2-15 m; height: 1-5 m (volumes: 8-156 m <sup>3</sup> )	Brazilian/Argentine: diameter: 5-7 m, high: 2-3 m producing Missouri kiln: wide: 7 m, length: 11-13 m, height: 3.5-4 m, TPI kiln: diameter: 2.3 m, high: 2 m
Reactor capital cost	Mound: \$27/t charcoal <sup>87</sup> Casamance: \$ 200 <sup>87</sup>	Brazilian: \$ 150-1,500 <sup>87</sup> Missouri: \$ 15,000 <sup>87</sup>
Charge ignition method	Small kindled wood at midpoint	Small kindle wood/burning oil/gas fired torch
Process control	Observing color of produced vapors	Observing color of produced vapors or temperature measurements
Raw material used	Cordwood	
Final product targeted	Char	
Heat transfer rate achieved	Slow Pyrolysis	
Mode of operation	Batch operation	
Heating method	Partial combustion of foliage (auto-thermal process)	
Pressure	Atmospheric	

*Brick/concrete/metal:* The four main kilns reviewed in this section are: Brazilian, Argentine, Missouri and the TPI kilns (Figure 4). In the US, during the 19<sup>th</sup> century, earth kilns were replaced by the so called “beehive kilns”<sup>8, 94</sup>. The basic difference between earth kilns and cinder block and brick kilns is the construction material (Table 1). These kilns have a long lifespan and several types have proved their economic viability. Cinder block and brick kilns can be differentiated by their shape: hangar kilns, with rectangular or square shape, and round brick kilns<sup>5</sup>. The main advantages of brick kilns are the use of local materials, higher yields than mound and pit kilns, good quality charcoal, good thermal isolation, easy operation, lifespan of 6 to 10 years and they are not sensitive to climate conditions<sup>89</sup>. These kilns can operate with logs and the final products (charcoal chunks) can be easily commercialized as domestic fuel. The

1  
2  
3  
4  
5  
6  
7  
8  
9  
10  
11  
12  
13  
14  
15  
16  
17  
18  
19  
20  
21  
22  
23  
24  
25  
26  
27  
28  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

main disadvantages of brick kilns are associated with the need of skilled workers for their construction, fixed location, long production cycle (on average 15 days, the cooling process is slow), and higher construction and operating costs than mound and pit kilns. These kilns are also responsible for important air pollution<sup>5</sup>. The most commonly used round brick kilns are: the Argentinean half-orange kiln and the Brazilian beehive kiln (see Figure 4). The most commonly used hangar kilns is the Missouri kiln (See Figure 4). All these kilns are auto-thermal and operate by burning part of the charge within the kiln.

The *Brazilian brick* kiln is an internally heated, fixed, batch-type kiln widely operated in Brazil, especially in the state of Minas Gerais and in the Amazonian region, with a typical capacity of 45 m<sup>3</sup><sup>43</sup>. Thousands of them are used to produce charcoal for the Brazilian iron and steel industry<sup>5,95</sup>. A detailed description of the methods to build and operate these kilns can be found elsewhere<sup>88,96</sup>. A typical operational cycle consists of 8 hours for loading/discharging, 80 hours for carbonization and 70 hours for cooling<sup>43</sup>. Some of the most advanced modifications to the Brazilian kilns are the attachment of an external heating chamber and the reduction of the number of smoke stacks<sup>5</sup>. Branches, brushwood, and other residual materials, which are not suitable for charcoal production and would be otherwise wasted, are used to heat the kiln. The raw material used for carbonization is typically cordwood, obtained from dedicated plantations or from forest clear cutting<sup>5,96</sup>. These kilns can be modified to recover pyroligneous water and decanted oil. Only few research papers describe the operation and yield of products from Brazilian kilns<sup>97</sup>.

The *Argentine kiln* is also generally referred to as the “half-orange-kiln” due to its hemispherical shape. This kiln, like many others, can be built in various sizes. Unlike the Brazilian kiln, Argentine kilns are built completely out of bricks with no iron parts<sup>5</sup>. A detailed description on how to build and operate a half-orange kiln can be found elsewhere<sup>88</sup>.

*Missouri-type kilns* are sometimes referred to as concrete kilns<sup>38</sup> or batch-type charcoal kilns<sup>98</sup>. They can be built with volumes up to 350 m<sup>3</sup> (typically between 150 and 200 m<sup>3</sup>)<sup>27,31,43,98</sup>, thus, requiring mechanized loading and unloading<sup>10,31</sup>. The operational cycle consists of 4 days of



1  
2  
3  
4 loading/discharging, 6 days of carbonization and 20 days of cooling<sup>43</sup>. The Missouri charcoal  
5 kiln, which was developed at the beginnings of the 1950s by V. Wulff in the Ozark County  
6 (Missouri)<sup>27</sup>, is a well proven kiln<sup>5,10, 38, 99</sup>. Missouri-type kilns are still used in Missouri, United  
7 States<sup>41, 98, 99</sup> and are responsible for an important fraction of the charcoal produced in the USA<sup>98,</sup>  
8 <sup>100, 101</sup>. Several improvements have been made to the original design. For instance, using  
9 thermocouples within the kiln contributes to the identification of cold ports and controlling  
10 airflow<sup>38</sup>. Additionally, the environmental impact of these kilns can be reduced by using  
11 afterburners<sup>78, 98, 100, 102</sup>. More information on the design and operation of this kiln can be found  
12 elsewhere<sup>5, 10, 31</sup>.  
13  
14  
15  
16  
17  
18  
19  
20  
21

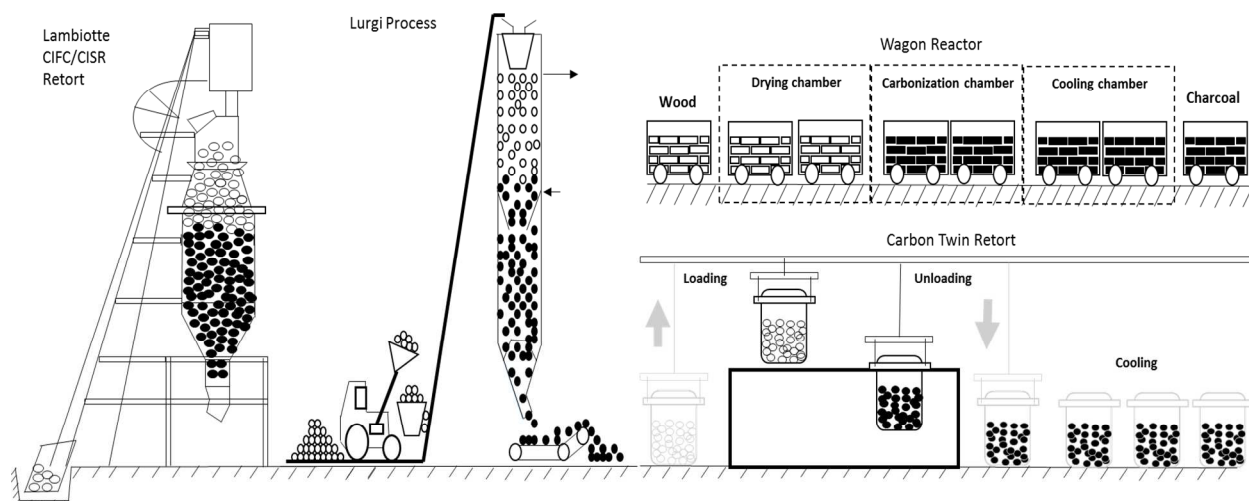
22 The *TPI kiln* is a small size kiln developed by the Tropical Products Institute (TPI) (Figure 4).  
23 This kiln is built with two interlocking cylindrical sections and a conical cover with ports to  
24 release vapors<sup>38, 88</sup>. Eight channels located at the perimeter of the base section support the kilns  
25 and serve as air inlets or smoke stacks. Compared to earth kilns, air inlet and gas outlet are easy  
26 to control, with less supervision needed. All the carbon produced can be recovered. These  
27 reactors can be transported to the place the feedstock is collected. They produce high charcoal  
28 yields with relatively short carbonization times (around three days). These kilns can be easily  
29 operated in high rainfall regions. However, they have important air pollution issues<sup>38,88</sup>. Other  
30 disadvantages include: higher capital costs compared with earth kilns, the need to cut and split  
31 biomass to fit inside the kiln, difficult transportation in hilly terrain, and a relatively short  
32 lifespan (only 2-3 years)<sup>89</sup>.  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42

43 The emission of gases and particulates from charcoal production in rural areas using medium-  
44 sized traditional and improved kilns has been studied by Sparrevik et al<sup>103</sup>. They reported the  
45 following average emission levels: 1,950 g CO<sub>2</sub>/kg charcoal, 157 g CO/kg charcoal, 6.1 g non-  
46 methane organic volatile compounds/kg charcoal, 24 g CH<sub>4</sub>/kg charcoal, 24 g solid particles/kg  
47 charcoal and 1.8 g NO<sub>x</sub>/kg charcoal<sup>103</sup>.  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

Other important kilns reported in the literature not discussed in this section include: *New Hampshire kiln*<sup>104,105</sup>, *Connecticut kiln*<sup>10,104,106;107</sup>, *Black Rock Forest kiln*,<sup>5,10,106,107</sup>, *Rima Contained kiln (RCK)*<sup>93</sup>, the *Adam retort*<sup>103, 108, 109</sup>, and the *European Schwartz kiln*<sup>5</sup>.

## 5. Retorts

While kilns are typically closed containers releasing gas and vapor to the atmosphere, the retorts condense the vapors and make good use of the energy content of gases<sup>89, 110</sup>. The main reactors discussed in this section are: the wagon reactor, Lambiotte French SIFIC (<http://www.lambiotte.com/>), the Lurgi Process<sup>111</sup> and the Carbon Twin Retort<sup>112</sup> (Figure 5). All these systems operate with logs. Their main characteristics are listed in Table 2. The main advantages of these systems are associated with the high charcoal yield and high charcoal quality. Additionally, the by-products from the vapors can be recovered. The main disadvantages are related with the high capital costs, attrition problems, the need of external sources of energy and the fact that most of these systems are not portable and require a concentrated supply of raw materials<sup>89</sup>.



**Figure 5.** Schematics of Retorts (Adapted from<sup>88, 110-112</sup>)

**Table 2.** Characteristics and operational details of some retorts operating with logs

	Lurgi	Lambiotte French SIFIC	The wagon retort	Carbo Twin Retort
Final product targeted	Char			
Heat transfer rate achieved	Slow pyrolysis			
Capacity	6.2 t wood/h <sup>111</sup> (per unit) 13,000 t charcoal/year (per unit)	2,000-6,000 t/year (per unit) <sup>87</sup>	6,000 t/year <sup>87</sup>	900 t/year per furnace <sup>112</sup>
Production per unit reaction volume	10 t/year/m <sup>3</sup>	16 t/year/m <sup>3</sup>		70 t/year/m <sup>3</sup>
Carbonization time	n/a	n/a	25-35 h	8 h (carbonization), 24-48 h (cooling)
Heating method	Contact with heat gases		External heat & volatile combustion, an oil burner (or LPG) is used to provide heat for the initial start-up	
Dimensions	Height: 27 m Diameter: 3 m Woodfeed size: 150 mm x 150 mm x 250 mm	Height: 16.3 – 18 m <sup>110</sup> D= 3-4.3 m <sup>43</sup> Volume: 600 m <sup>3</sup> <sup>110</sup>	Trolleys: 12 m <sup>3</sup> Length: 8-16 m Diameter: 2.5 m Tunnel capacity: 35-60 m <sup>3</sup> Length: 45 m long	Volume per Vessel: 5 m <sup>3</sup> Six vessels are needed to keep the system running
Construction materials	Steel			
Portability	Stationary			
Reactor Position	Vertical	Vertical	Horizontal	Vertical
Raw material used	Cordwood	Cordwood	Cordwood	
Loading and discharge methods	Mechanical	Mechanical	Use of wagons	
Process control	Direct measurement of temperature			
Mode of operation	Continuous			Semi-continuous
Pressure	Atmospheric			
Efficiency	30-40 %	35 %		30 %
Pretreatment needed	Pre-dried			
Cost	Capital cost: \$ 10 million (1989) Operating cost: EUR 320/t charcoal	Capital cost: 0.5-2 million dollars Capital cost: EUR 360/t charcoal		Capital cost: 480,000 EUR <sup>112</sup> Char sales price: 250 EUR/t <sup>112</sup> Operating cost: EUR 380/t charcoal
Yields reported		Char: 30-35 wt. %	Char: 30 – 33 wt. % Pyroligneous acid: 20 – 25%	Char: 33 wt. % <sup>112</sup>

1  
2  
3  
4  
5  
6  
7  
8  
9  
10  
11  
12  
13  
14  
15  
16  
17  
18  
19  
20  
21  
22  
23  
24  
25  
26  
27  
28  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

*The Wagon Retort:* These retorts consist of the following components: (a) a steel horizontal carbonizing chamber fitted with either a fixed cover at one end and a door at the other, or doors at both ends<sup>4</sup>. One or two vapor outlets provided on the side, top, or at one end of the chamber and a rail-track for running retort cars through, (b) a furnace for the heating process, (c) a condenser connected to the retort, (d) a steel chamber with a door at each end for cooling char placed in front of the retort and fitted with a similar rail-track, (e) a section of rail that connects the retort with the char cooler that can be moved as needed, (f) mechanical equipment for moving the cars, and (g) retort-cars. A length of 8 to 9 m with a diameter up to 2.5 m is standard for retorts<sup>113</sup>. Retorts usually require gradual cooling of the carbonization products, generally by heat release to the surroundings at room temperature<sup>2</sup>. Compared to other methods, the wagon retort required a substantial amount of manpower<sup>5,114</sup>. This retort commonly used raw material made up of round wood and split round wood with an average length between 1.0 and 1.2 m. A limited quantity of shorter pieces was also charged<sup>5, 114</sup>. These reactors were able to produce charcoal with efficiencies up to 36%, tar and oils with efficiency varying from 5 to 20%, crude pyroligneous water varying from 30 to 50%, and non-condensable gases varying from 20 to 30%, depending on the composition of wood<sup>4,8</sup>. According to Klar<sup>4</sup>, these units were able to obtain between 2.3 and 10.5 wt. % of acetate of lime (80 % purity), between 0.6 and 2.5 wt. % crude naphtha, between 5 and 20 wt. % tars, and between 0.4 and 8 wt. % pine-oil. Charcoal was mainly used in the iron industry. Burning of gases and tar in boilers was a common practice<sup>8</sup>.

A wagon retort system was recently in operation by Impianti Trattamento Biomasse (an Italian company). In 2010, this company had plants in Milazzo and Mortera (Italy) producing up to 6,000 t/y of charcoal<sup>115</sup>. The process was called O.E.T. Calusco (former Carbolisi) but it does not seem in operation currently<sup>115</sup>. Alterna Biocarbon, a company with head office in Prince George, BC, Canada, recently commercialized an upgraded design of the wagon retort<sup>87</sup> (the company is not currently in operation). The main products targeted by this company were energy pellets, activated carbon, products for mercury recovery and chars for soil applications.

*The Lambiotte Retort* has proven to be a successful technology for the production of char. As a result of several attempts to simplify the SIFIC process, the CISR Lambiotte Retort was

1  
2  
3  
4 developed (See Figure 6)<sup>43</sup>. The pre-dried wood enters by the top of the retort through a lock  
5 controlled electronically to keep the retort always full. The retort has four zones (cooling zone,  
6 carbonization, drying and torch)<sup>110</sup>. The charring wood section is where the wood decomposes  
7 into char, vapors and gases. Carbonization usually proceeds at a narrow temperature range (547-  
8 560 °C). The gases released from this section are drawn upward by a fan. The energy needed for  
9 carbonization is provided by the hot flue gases coming from combustion of part of the pyrolysis  
10 vapors in an external chamber<sup>5, 93</sup>. Once the char is discharged, it is loaded on the converter  
11 plenum and carried away for storing. Since the lower segment of the retort acts as the first step in  
12 the cooling process, there is no need for separating char in the cooler<sup>5</sup>. The surplus combustible  
13 vapors can easily be used for steam or electricity generation (Table 2). These plants have been  
14 running commercially for several years. Balt Carbon Ltd. is the supplier of Lambiotte retorts for  
15 Russia and other East European and Central Asian Countries. The company has built a 2,000 t  
16 charcoal per year unit in Kaplava (Eastern Latvia) and an 8,000 t charcoal per year in Ugale  
17 (Western Latvia)<sup>27</sup>. Char Solutions Inc (<http://www.biocharsolutions.com/>), from Colorado, has  
18 built a reactor using similar principles (continuous downdraft pyrolysis reactor) but using chips  
19 or pellets. This system is a mobile downdraft auto-thermal gasifier able to convert up to 225 kg/h  
20 of biomass into synthesis gas and char. The main advantages of the Lambiotte system compared  
21 with other retorts are: (1) high labor efficiency due to high level of automation, (2) higher  
22 charcoal yield, (3) good product quality, (4) it is possible to use the vapors produced for co-  
23 generation<sup>27</sup>. A disadvantage of the system is its sensitivity to biomass moisture content.  
24 Biomass with high moisture content reduces the capacity and in some cases may it require  
25 burning auxiliary (oil) fuel. Attrition with the consequent production of fines happens due to the  
26 vertical movement of the load. These retorts are also prone to corrosion by acetic acid<sup>27</sup>.

27  
28  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47 The operation of the *Lurgi reactor* is similar to the Lambiotte reactor. The Lurgi reactor (Figure  
48 5) also has an upper carbonization zone and a lower cooling zone, each one with its own re-  
49 cycling gases<sup>43, 111</sup>. The reactor has an air-lock hopper fed with a skip hoist that elevates dry  
50 wood blocks to the top of the reactor<sup>111</sup>. The combustion of pyrolytic vapors and gases in a  
51 staged external incinerator provides the heat for carbonization. In the first stage, the retort gas is  
52 burnt at near stoichiometric conditions. In the second stage, more air is added to ensure complete  
53  
54  
55  
56  
57  
58  
59  
60

1  
2  
3  
4  
5  
6  
7  
8  
9  
10  
11  
12  
13  
14  
15  
16  
17  
18  
19  
20  
21  
22  
23  
24  
25  
26  
27  
28  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

combustion before releasing to the atmosphere. Up to 6,000 Nm<sup>3</sup>/h of gas at 600 °C is used for heating the retort<sup>111</sup>. The largest Lurgi charcoal plant forms part of the Silicon Metal Complex (SIMCOA) in Bunbury, (<http://simcoa.com.au>), Western Australia, and produces 27,000 t of charcoal every year in two retorts from local hardwood<sup>43, 111</sup>.

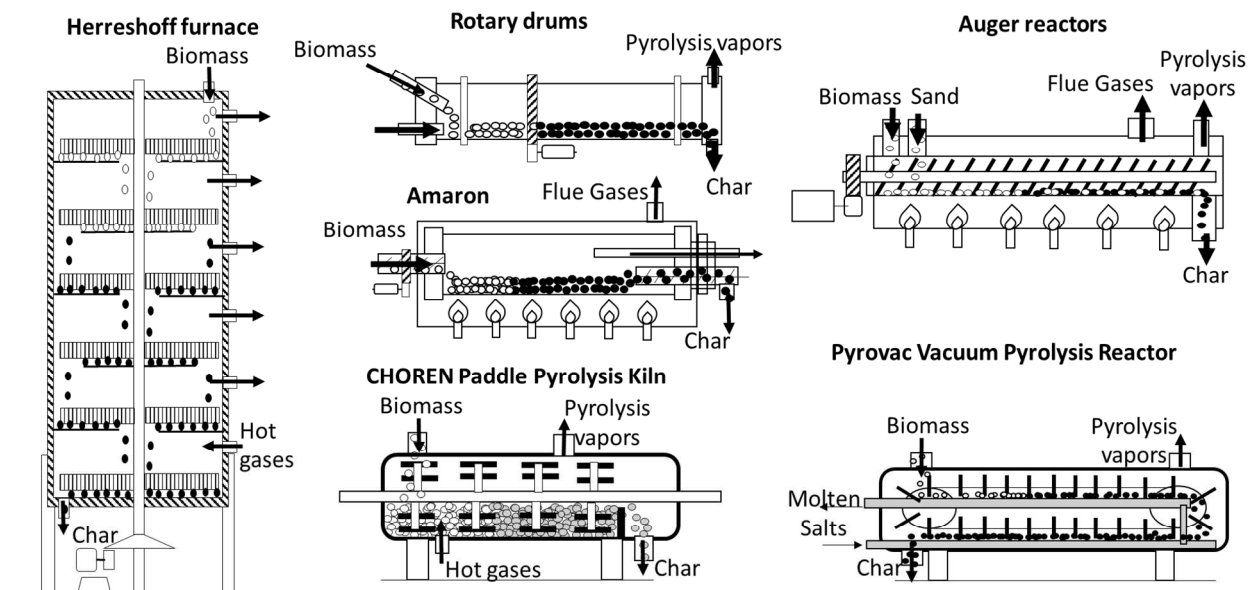
The *Carbo Twin Retort* was initially developed in the 1990's in the Netherlands. The twin system was formed by two retorts placed in an insulated oven, with a monorail and overhead crane that enables the placement of retort vessels into and out the carbonization unit. The pyrolysis vapors released by the pyrolysis reactions taking place inside the vessel are combusted outside to provide the heat supply needed for heating up the system<sup>112</sup>. The system is equipped with an internal afterburner furnace with an excess of air to burn all the organic compounds<sup>27</sup>. One of the main advantages of this system is the low labor requirements: one worker per shift can operate (load and discharge) and supervise a battery of ten twin retorts<sup>27</sup>. Other advantages of this system are: high energy efficiency, high char yield, superior product quality, straight forward operation, easy scaling up with modular designs, low emissions, flexible operation and control, and continuous operation<sup>112</sup>. Carbo Twin Retorts have been installed in Almelo (The Netherlands), Parnu (Estonia), Manso Amenfi (Ghana) and Hailin (China)<sup>27</sup>. Similar twin reactor concepts have been developed also in The Netherlands by VMR Systems<sup>43</sup>, Charbon Engineering and Clean Fuels BV and also in Portugal by Ibero Massa Florestal.

Other important retorts not reviewed in detail in this section are: *the Reichert Converter*<sup>5,114</sup>, *the Rima Container Kiln (RCK)*<sup>93</sup>, and the *CML France Batteries*<sup>43,93</sup>. Although not commercialized, the innovative concept of the Flash Carbonization process developed by Antal<sup>7</sup> (*in situ* partial burning of the pyrolysis vapors inside the reactor with air at high pressure) is worth mentioning.

## 6. Converters (also known as intermediary pyrolysis reactors)

The carbonization techniques described in the previous section are used for logs and are not suitable for the small particles and chips found in agricultural and forest logging residues. If one of the large kilns is charged with small waste particles such as sawdust, the particles will tend to

1  
2  
3  
4  
5 pack much more tightly, thus promoting insufficient penetration of gases unless the cargo is  
6 continuously rotated or moved<sup>4,5</sup>. This section reviews reactors able to handle chips and pellets,  
7 as well as deliberately crushed or chopped material such as sugarcane bagasse, bark, twiglets,  
8 olive stones or coconut shells. The reactors herein reviewed are: *the Herreshoff furnaces, rotary*  
9 *drums, auger reactors, paddle kiln* and *moving beds* (Figure 6). The main operational features of  
10 these reactors are shown in Table 3.  
11  
12  
13  
14



35  
36 **Figure 6.** Scheme of common converters for processing wood chips and other small biomass  
37 particles (Adapted from:<sup>5, 76, 88, 116</sup>)  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

**Table 3.** Characteristics of converters for wood chips processing.

	Herreshoff furnace	Rotary drums	Auger reactor	Moving agitated bed	Paddle pyrolysis kiln
Final product targeted	Char/bio-oil/heat				
Heat transfer rate achieved	Commonly slow/medium heating rates depending on particle size				
Mode of operation	Continuous				
Capacity	Up to 96 t/d	Up to 288 t/d	Up to 50 t/d <sup>42</sup>	84 t/d <sup>16</sup>	-
Heating method	Direct contact with hot gases	Direct contact with hot gases or indirect heating	Direct contact with hot gases/using a hot heat carrier/ indirect heating	Indirect heating	
Construction materials	Metal				
Portability	Stationary	Stationary/Portable	Stationary/Portable	Stationary	
Reactor Position	Vertical	Horizontal			
Raw material used	Chips/shells/fine particles				
Loading and discharge methods	Mechanical				
Size of the reactor	Large	Large/Medium/Small	Small/Medium	Medium/Large	Small/Medium
Charge ignition method	Combustion of pyrolysis gases and/or of auxiliary fuels	Combustion of auxiliary fuels and direct or indirect contact of combustion gases		External oven heating a hot sand heat carrier	External heater
Process control	Direct measurement of temperature				
Pressure	Atmospheric/Vacuum			Atmospheric / Vacuum	Atmospheric
Yield of carbon	25-30 wt. % <sup>87</sup>	-	-	-	-
Pretreatment needed	Ground in chips/ fine particles				

The Herreshoff multiple hearth furnace was patented in 1921 by R.D. Pike. It consists of 4-10 circular hearths or plates located one above another inside a refractory lined steel shell<sup>27</sup>. A vertical rotating shaft (1-2 rpm) with radial arms located in the center of the shell moves the feed from the top of the hearth to the bottom using a spiral of teeth across each hearth. The shaft in the center rotates at 1-2 rpm. This converter was designed for converting raw materials in the form of sawdust, shavings, or milled wood and bark into charcoal. The system is typically heated up to 500-600 °C using external gas or oil burners<sup>27</sup>. The yield of dry char for this process is about 25 wt.%. Automatic oxygen monitoring is used to minimize power draw and fuel demand. The first carbonization Herreshoff furnace was used in 1984, and by 1985 there were about 16 Herreshoff furnaces in use in the South of US, producing over half of the total char produced



1  
2  
3  
4 from wood and bark<sup>27</sup>. This type of reactor has also been used in vacuum conditions<sup>117, 118</sup>.  
5  
6 Currently, a mobile Herreshoff pyrolysis reactor is commercialized by BIG Char, a company  
7  
8 with headquarters in Queensland, Australia. This company is commercializing a patented mobile  
9  
10 multiple heart furnace, producing char and heat with capacities up to 1 t/h of biomass. The char  
11  
12 produced is available in a briquetted form (<http://www.bigchar.com.au>). The major advantage of  
13  
14 a Herreshoff furnace is its ability to efficiently and flexibly use fine-grained materials of little  
15  
16 economic value. One disadvantage is the need for briquetting of charcoal powder before it can be  
17  
18 commercialized. The capital cost is high.  
19

20  
21 The *rotary drum* reactor is a very reliable system for carbonizing biomass. Figure 6 presents the  
22  
23 two main types of rotary drum designs (directly heated and indirectly heated). The residence  
24  
25 time of the biomass particles in these systems are controlled by the angle of the drum and the  
26  
27 rotation speed. A converter of this type consists of: (1) an internal concentric steel tube and a  
28  
29 cylindrical internally insulated mantle that makes up the rotary part. A sequence of radial steel  
30  
31 fins is supported by the mantle which has a solid connection to the steel tube, (2) the solid and  
32  
33 gaseous products are charged and discharged by two fixed parts at the end of the rotary. This  
34  
35 furnace provides the heat required for the carbonization process by burning gases and pyrolysis  
36  
37 vapors. Table 4 shows the yield of liquid, char and gases reported for tests with rotary drums.  
38  
39 This type of reactor is able to achieve a good balance between oil (between 37 and 62 wt. % of  
40  
41 liquid product) and char yield (19-38 wt. %).  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

The European Union<sup>119</sup> and Japan<sup>120</sup> have extensively used these reactors for tires, sewage sludge, municipal solid waste, and plastics. Examples of these systems are: a 2.2 MW<sub>el</sub> pyrolysis plant operating since 1983 in Burgau-Unterknöringen, Germany, a 100,000 t/year pyrolysis plant at the VEW Energie AG (VEW) power station Westfalen in Hamm-Uentrop, Germany, and other systems that combine gasification with pyrolysis or pyrolysis with combustion<sup>119</sup>. Specific concepts of interest are: the ConTherm® technology by RWE Energie AG (RWE), the Serpac technology, the EDDITH process, The PYROPLEQ® process, Gibros PEC Process or PKA technology, SIEMENS Schwel-Brenn technology, THERMOSELECT process<sup>119</sup>. Most of those reactors could be easily adapted to work with biomass.

In 2009 Amaron Energy designed, constructed and began testing a unique indirectly-heated rotary kiln for pyrolysis of biomass to produce bio-oil and char<sup>121, 122</sup>. Amaron has achieved char yields and bio oil yields close to those from fast pyrolysis fluid beds (Figure 6). The Amaron rotary reactor consists of: (1) a cylindrical reaction section heated by multiple high intensity gaseous fueled burners located and controlled to optimize heat transfer into the materials being heated, (2) a feed section with an auger arrangement that suppresses heating of the material until the particles reach the area where optimized heat transfer begins, (3) a withdrawal section with a char outlet below the end of the rotating reaction section, (4) a stationary end closure supporting a withdrawal pipe for vapors and gases. The vapors are condensed in multiple units designed to operate without problems caused by condensation of tars in the interconnecting piping.

**Table 4.** Yield of products obtained from rotary kilns

Biomass specie and reactor	Capacity	T (°C)	Char (wt. %)	Bio-oil (wt. %)	Gas (wt. %)	References
Olive stones		500	26	38	35	[123]
Pinon-Juniper wood	0.5 t/h	500	30	59	11	[122]
Black liquor	0.5 t/h	500	38	37	25	[122]
Fir pellets	0.5 t/h	500	23	62	16	[122]
Fir fines	0.5 t/h	500	19	59	22	[122]
Lemna	0.5 t/h	500	28	44	28	[122]
Pine shredded	0.5 t/h	500	30	58	12	[122]
Pine bark	0.5 t/h	500	34	36	30	[122]
Aspen	0.5 t/h	500	28	43	29	[122]

1  
2  
3  
4 The *auger reactor* is typically fed at one end through a hopper or a feeding screw<sup>116, 124</sup>. A screw  
5 then gradually carries the biomass to the hot zone of the reactor where it is carbonized, and the  
6 gases and vapors are extracted and led to a condenser<sup>46</sup>. The residence time of the hot vapors in  
7 these reactors can vary, in average from 5 to 30 s<sup>16</sup>. These reactors can be operated with and  
8 without using hot sand, steel or ceramic balls as heat carriers<sup>124, 42</sup>. The discharging of char and  
9 heat carriers happen by gravity<sup>94</sup>. Table 5 shows the yield of products obtained under different  
10 operational conditions using auger pyrolysis reactors. Experimental studies with woody biomass  
11 show yields of char between 17 and 30 wt. % and yields of oil between 48 and 62 wt. %<sup>42</sup>. The  
12 bio-oil yield is slightly lower than that of fluidized bed reactors and contains more water 30-55  
13 %<sup>42</sup>. As expected, the oil yield of agricultural residues was much lower due to the high ash  
14 content of this feedstock. Although difficult to compare, it seems that the yields obtained with  
15 sand heat carrier is slightly higher than those obtained without. ABRI-Tech in Canada has sold  
16 several 1 t/day units<sup>42</sup>. Auburn University (USA), KIT (FZK) (Germany), Mississippi State  
17 University (USA), Michigan State University (USA), Texas A&M (USA) and Washington State  
18 University (USA)<sup>61</sup> have active research programs on this technology<sup>16</sup>.  
19  
20  
21  
22  
23  
24  
25  
26  
27  
28  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

**Table 5.** Auger pyrolysis results

Biomass specie	Capacity.	T (°C)	Char (wt. %)	Bio-oil (wt. %)	Gas (wt.%)	Reference
Without heat carrier						
Oak	1 kg/h	450	18-20	50-56		[125]
Pinewood sawdust	1 kg/h	450	18-20	49-55		[125]
Pinewood chips	1.5 kg/h	500	30	58	12	[61]
Pinewood chips	15 kg/h	500	20	57	25	[126]
Miscanthus	7 kg/h	425		60		[127]
Pinewood sawdust	7 kg/h	450	19	54		[128]
Douglas fir wood	1 kg/h	400	12	48	40	[77]
Corn stover	7 kg/h	450		35		[130]
Switchgrass	7 kg/h	450		33		[130]
Cassawa stalk		450		32		[130]
Peanut shell		450		33		[130]
Rice husk				35		[130]
Rice straw	60 g/h	500	45	26	13	[131]
With heat carrier						
Eucalyptus grandis	10 kg/h	500		60.3		[129]
Wheat straw (twin screw, Biolq)	500 kg/h	500	23-28	50-55	22	[132]
Wheat straw (twin screw, Biolq)	10 kg/h	500	24	51	24	[133]
Wheat bran (twin screw, Biolq)	10 kg/h	500	18	60	22	[133]
Softwood (twin screw, Biolq)	10 kg/h	500	15	69	16	[133]
Hardwood (twin screw, Biolq)	10 kg/h	500	15	66	18	[133]

In *moving agitated bed* reactors biomass is conveyed by patented mixers over a horizontal surface heated by molten salts. These reactors have been used in vacuum conditions<sup>134, 135</sup>. The molten salt used is a mixture of potassium nitrate, sodium nitrate, and sodium nitrite<sup>136</sup>. The size (height) of an industrial moving bed (few cm) is comparable with the height of fixed bed of most of the laboratory tests (also few cm). In fact, the scaling up of this reactor was typically conducted with the aid of fixed bed reactors operating in vacuum. In this section, we report results obtained with fixed bed at laboratory scale (Table 6). Bio-oil yields over 50 wt. % are obtained with woody biomass in most vacuum tests.

**Table 6.** Fixed bed reactor

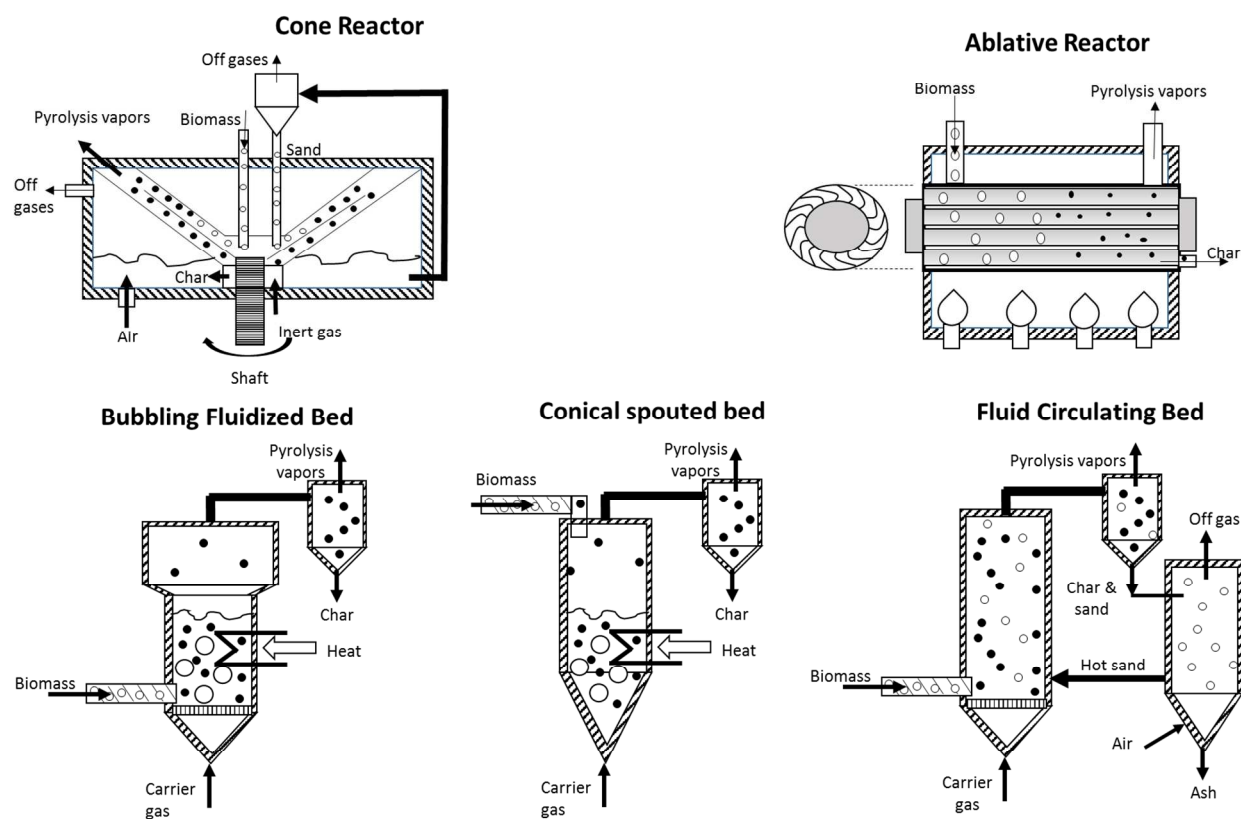
Biomass specie and reactor	Capacity	T (°C)	Char (wt. %)	Bio-oil (wt. %)	Gas (wt. %)	References
Rice husk and fixed bed	180 g	100 - 500 °C/min	42-48	28-35		[137]
Switch grass and 100 psi (fixed bed)			42	27	10	[138]
Pine chips	1.4 kg	500	31	50	18	[60]
Hardwood rich in fiber (Aspen poplar, white birch) (vacuum in fixed bed)	4.2 kg (15 dm <sup>3</sup> reactor)	500	26	54	20	[60]
Softwood bark residue (white spruce, balsam fir, larch) (vacuum in moving bed)	15 kg/h (total 1050 kg pyrolyzed)	500	28	45	27	[60]
Sugarcane bagasse and vacuum pyrolysis	Pilot (20 kg) Laboratory (80 g)	530 500	26 19	51 62	22 18	[59]
Rape straw and vacuum reactor		500		43		[139]
Palm oil decanter cake and vacuum reactor		500	39	41	20	[140]
Rice husk and vacuum reactor	10 g	500	38	49	13	[141]
Rice straw and vacuum reactor	10 g	500	35	47	18	[141]
Empty fruit bunch and vacuum reactor	10 g	500	26	54	20	[141]
Douglas fir (fixed bed)	800 mg	500	22	66	8	[142]
Pine and vacuum	500 g	500		52	25	[143]
Pine sawdust and vacuum reactor		500	20	50	30	[143]
Red oak	800 mg	500	24	67	8	[142]
Camphorwood sawdust and vacuum		474	20	50	30	[144]
Eucalyptus and vacuum	10 g	500	26	62	17	[144]
Teng wood and vacuum	10 g	500	30	58	12	[144]
Rubberwood and vacuum	10 g	500	30	51	19	[144]

The *Paddle Pyrolysis reactor* (See Figure 6)<sup>145</sup> are characterized by the use of internal mechanisms to move and mix the biomass and thus to increase heat transfer. This kind of reactors have been used by companies such as BEST Energies, currently part of Pacific Pyrolysis Inc., (<http://pacificpyrolysis.com/technology.html>), and was also part of the design of Choren<sup>146</sup>.

Other important reactors in this category not included in this review are the *Shelf reactors*<sup>4, 46</sup> and the *Stafford-Badger retort*<sup>10</sup>. The converters are the reactors with more potential for the balanced production of char and oil. However, more research is needed to understand the potential of these reactors.

## 7. Fast pyrolysis reactors for high yields of bio-oil production

This section reviews the most common fast pyrolysis reactors (rotating cone, ablative, conical spouted bed, bubbling fluidized bed and circulating bed) (Figure 7) that have been developed intending to optimize the yields of bio-oil. There are very good literature reviews in fast pyrolysis reactors<sup>15, 16, 19, 136, 147</sup>. Thus, this section will only focus on recent developments. The main characteristics of the reactors studied in this section are discussed in Table 7.



**Figure 7.** Schemes of Fast Pyrolysis Reactors (Adapted from<sup>136</sup>)

**Table 7.** Characteristics of some fast pyrolysis reactors

	Bubbling fluidized bed reactor	Circulating bed reactor	Ablative pyrolysis	Rotating cone
Final product targeted	Bio-oil		Bio-oil/char	Bio-oil
Heat transfer rate achieved	Fast pyrolysis			
Mode of operation	Continuous			
Heating method	Direct and indirect heat/sand		Indirect heating	Direct and Indirect heating
Construction materials	Metal			
Portability	Stationary			
Reactor Position	Vertical		Horizontal	Vertical
Raw material used	Fine particles (less than 2 mm)		Chips	Fine Particles
Loading and discharge methods	Mechanical			
Ind. reactor capacity built	0.5-200 t/day <sup>16</sup>	9.6-96 t/day <sup>16</sup>	6 t/day <sup>16</sup>	50 t/day <sup>16</sup>
Charge ignition method	External combustion chamber to heat the carrier gases			
Process control	Direct measurement of temperature			
Complexity*	Medium		High	High
Status*	Demonstration	Commercial	Pilot	Demonstration
Industrial companies	Agritherm Canada <sup>16</sup> , Biomass Engineering Ltd <sup>16</sup> , UK, Dynamotive, Canada <sup>16</sup> , RTI, Canada <sup>16</sup> , Avello Bioenergy, USA	Ensyn, Canada <sup>16</sup> , Metso/UPM Finland <sup>16</sup>	PyTec, Germany <sup>16</sup>	BTG, Netherland <sup>16</sup>
Pressure	Atmospheric			
Pretreatment needed	Particle milling and pre-drying		None	Particle milling
Yields reported (wt. %)	Up to 70% of bio-oil <sup>147</sup>			

The bubbling fluidized bed reactors use a mixture of convection and conduction to transfer heat from a heat source (hot sand) to the biomass particle. Although most of the literature suggest that fast pyrolysis should be operated with particles with diameters 2-3 mm<sup>16</sup> to obtain high liquid yields (over 65 %), the particles must be smaller (typically below 0.5 mm)<sup>49, 50</sup> to avoid the retention of aerosols inside the particle and to achieve high heat transfer rates. One of the best-known examples of using a fluidized bed reactor was Dynamotive, company that was a result of the pioneering job conducted by the University of Waterloo<sup>11, 12, 148</sup>. In the design of most fluidized bed reactors in operation the char is entrained by carefully controlling the difference between the sizes and densities between biomass particles and the sand. Char particles obtained

1  
2  
3  
4  
5 from the pyrolysis of raw materials with very high ash content such as, sewage sludge, usually  
6 abandons the bubbling fluidized beds by overflow. The heat used in bubbling fluidized beds is  
7 generated from the combustion of pyrolysis gases and chars and is typically transferred to the  
8 fluidized bed by heating coils and by heating the carrier gas (in industrial conditions typically a  
9 recirculated pyrolytic gas). Given the low heat transfer rates between combustion gases and the  
10 bed (100-200 W/m<sup>2</sup>K) at least 10 to 20 m<sup>2</sup> of surface area is required to transfer the heat required  
11 to pyrolyze 1 t/h of biomass. These heat transfer surfaces are very susceptible to attrition from  
12 the sand<sup>136</sup>. Several main features of this type of reactors are: the ability to accurately control  
13 temperature, the use of entrainment for the separation of the char, the use of cyclone separation,  
14 the easy scaling, the technology is well known and understood, small particles are required, and  
15 there must be a large scale heat transfer to the bed. Dynamotive developed bench-scale plants, a  
16 15 t/day pilot plant, a 130 t/day plant in West Lorne, and a 200 t/day plant in Guelph, Ontario,  
17 Canada<sup>149</sup> that are currently not operating. Tables 8-10 show the yield of products obtained from  
18 the pyrolysis of grass and agricultural residues, softwood, and hardwood species in fluidized  
19 beds. When processing grasses and other agricultural wastes the conversion yield to liquid bio-  
20 oil, solid char and non-condensable gas are in the ranges of 35-68.7 wt. %, 12.9-45.7 wt. % and  
21 3-25.7 wt. %, respectively, on an as fed basis (Table 8). This broad range of values is mostly due  
22 to the wide range of ash contents in these materials. When processing of softwoods result in 59-  
23 78.1 wt. % bio-oil, 10-15.7 wt. % char and 7.8-28 wt. % non-condensable gas. Comparable  
24 yields were also obtained for hardwood species (char: 9.8-20.7 wt. %, bio-oil: 59-77 wt. %,   
25 gases: 9.3-24.6 wt. %). Lower oil yields (35-73 wt. %) and higher char yields (13.4-45.7 wt. %)  
26 are obtained with some grasses, likely due to higher ash content in some of these materials.  
27  
28  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60



**Table 8.** Pyrolysis of grasses and agricultural residues using fluidized bed reactors.

Biomass specie	Capacity	T (°C)	Char (wt %)	Bio-oil (wt %)	Gas (wt. %)	Reference
Corn stover	100 g/h	450	46	35	11	[12]
Corn stover	100 g/h	550	34	50	14	[12]
Corn stover	100 g/h	600	28	50	13	[12]
Rice husk	120 kg/h	475	-	50		[150]
Rice husk	<150 kg/h	450	30	50	20	[151]
Rice husk	7.32 kg/h	450	29	56	15	[152]
Rice husk	60 g/h	500		55		[153]
Rice straw	300 g/h	500	27	43	23	[131]
Rice straw	60 g/h	500	31	53	15	[153]
Corn cob	60 g/h	500	20	62	17	[153]
Sugarcane bagasse	60 g/h	500		67		[153]
Sugarcane bagasse	2 – 5.3 kg/h	500	23	73	4	[154]
Sugarcane bagasse	100 g/h	510	19	69	12	[148]
Barley straw	1 kg/h	525		54		[155]
Timothy	1 kg/h	525		61		[155]
Switchgrass	1 kg/h	510	19	60	16	[156]
Switchgrass	2.5 kg/h	480	13	61	11	[157]
Switchgrass			20	58		[158]
Miscanthus	1 kg/h	505	29	51	12	[156]
Wheat straw	1 kg/h	525	27	38	26	[156]
Wheat straw	1.5 kg/h	525	22	61	17	[158]
Wheat straw	100 g/h	550	24	54	24	[148]
Wheat chaff	100 g/h	515	18	67	16	[148]
Sorghum bagasse	100 g/h	510	13	69	12	[148]
Sunflower hulls	100 g/h	500	23	57	20	[148]

**Table 9.** Pyrolysis of softwood species using fluidized bed

Biomass specie	Capacity	T (°C)	Char (wt.%)	Bio-oil (wt.%)	Gas (wt%)	References
Pine-wood chip and pellets	1 kg/h	530	10	59	28	[159]
Pitch pine (debarked, dp< 5 mm)	Non-cont. feed	500	16	64	21	[160]
Pine sawdust	1 kg/h	525		67-71		[155]
Douglas - fir	220 g/h	500		52		[161]
Douglas - fir	3-5 kg/h	480	12	64	24	[162]
Spruce	300 g/h	465-470	14	61	27	[163]
Japanese Cedar (debarked, dp<0.5 mm)	Non-cont. feed	500	13	66	22	[160]
Pine sawdust	1 kg/h	525		67-71		[155]
Spruce sawdust	100 g/h	500	12	78	8	[148]

**Table 10.** Pyrolysis of hardwood species using fluidized bed reactors

Biomass specie	Capacity	T (°C)	Char (wt. %)	Bio-oil (wt. %)	Gas (wt. %)	References
Red oak	6 kg/h	400	21	67	13	[164]
Red oak	6 kg/h	500	19	63	18	[164]
Red oak	1.5 kg/h	450-500	25	62	13	[165]
Eucalyptus grandis	700 g/h	500		69		[166]
Eucalyptus grandis	0.1 kg/h	500		69		[129]
Eucalyptus grandis woodchips	1 kg/h	500		62		[129]
Eucalyptus (debarked)	0.85 kg/h	500		62		[167]
Eucalyptus loxophleba wood	0.15 kg/h	500	14	61	25	[160]
Eucalyptus loxophleba wood	2 kg/h	500	14	62	12	[49]
Eucalyptus wood	1 kg/h	450	17	64		[168]
Eucalyptus grandis woodchips	1 kg/h	500	18	59	23	[169]
Eucalyptus loxophleba wood	0.1 kg/h	450	14	71	14	[170]
Beech	1 kg/h	510	13	72	9	[171]
Beech	1 kg/h	512	13	67	12	[156]
Beech	300 g/h	465-470	10	70	23	[163]
Beech	1 kg/h	500	10	71	15	[50, 62]
Poplar sawdust	100 g/h	504	12	77	11	[148]

10 t/day mobile pyrolysis units with a fluidized bed reactor have been developed by Agritherm at the University of Western Ontario (<http://agri-therm.com>)<sup>16, 42</sup>. An important feature of the design proposed by this company is a compact design in which the pyrolysis reactor is built using an annulus with a burner at the core providing the energy needed for the pyrolysis process. Avello Bioenergy in the State of Iowa (US) is another company commercializing fast pyrolysis technologies (<http://www.avellobioenergy.com>). This company specializes in the development of fractionation strategies to obtain different products from bio-oils. Bioware is a Brazilian company commercializing auto-thermal fluidized bed reactors<sup>172</sup> to produce bio-oil, char and phenolic resins (<https://www.bioware.com.br>). Nettenergy BV is a private company from the Netherlands (<http://www.nettenergy.com/index.php/en/>) that built a 100 kg/h mobile unit with a unique multi-stage compact separation design<sup>42</sup>.

*Circulating fluidized beds:* Research performed by the University of Western Ontario in the late 1970s and early 1980s spawned the Rapid Thermal Processing (RTP)<sup>TM</sup> technology commercialized and developed by Ensyn. Before feeding this system's reactor, the biomass is comminuted to approximately 6 mm, and then dried to a moisture content of 10% or less. The hot recirculated biomass and sand enter in an up-flowing transported bed reactor. Once the

products have passed through two cyclones that separate both solids from the produced vapors, they experience a rapid cooling and quenching in multiple stages<sup>14</sup>. The residence time of the solids and vapors in these reactors is almost the same<sup>16</sup>. The recirculation of gases from secondary char combustion is the main heat source<sup>16</sup>. RTP is the only pyrolysis technology in the world that has operated on a long-term commercial basis (<http://www.ensyn.com>, <https://www.envergenttech.com>). Larger scale units include: ENEL plant build by Ensyn in Italy (15.6 t/day), several 40 t/day units at Red Arrow (USA) operating for the production of smoke aromas and the Ensyn 50 t/day unit at their R&D center in Renfrew Canada<sup>16</sup>. Some features of the transported bed reactor include: precise temperature control within the reactor, the ability to use large size particles, suitability for very large throughputs, and well understood technology<sup>16</sup>. Some of the main disadvantages of these technologies are: (1) use of large volumes of inert carrier gases causes a dilution of the pyrolytic gases making bio-oil recovery very difficult (2) many fast pyrolysis reactors use sand as a heat carrier, (3) complex hydrodynamics, (4) high velocities lead to higher levels of attrition, and the separation of the char and the sand from the vapors with a “cyclone”, (5) careful control is needed for the closely integrated combustion, and a large scale heat transfer to the bed is required (6) Char and sand attrition is an important issue. Table 11 shows the yield of bio-oil reported in the literature for different feedstocks. Bio-oil yields between 54 and 71 wt. % have been reported.

**Table 11.** Pyrolysis of biomass using circulating fluidized bed reactors.

Biomass specie	Capacity	T (°C)	Bio-oil (wt. %)	References
Timothy	20 kg/h	520	54	[155]
Rapeseed straw	20 kg/h	520	60	[155]
Pine saw dust	20 kg/h	520	74	[155]
Green forest residue (86% spruce, 9% pine, 5% birch)	20 kg/h	520	64	[155]
Brown forest residue (80% spruce, 10% pine, 10% birch)	20 kg/h	520	58	[155]
Eucalyptus chips	20 kg/h	520	71	[155]

A similar technology, with the use of catalysts instead of inert sand is being developed by KIOR, now Inaeris Tech (<http://www.inaeristech.com/>), a company located in Houston, Texas. The company uses a proprietary catalyst system to produce a deoxygenated bio-oil in a Fluid Catalytic Cracking (FCC) reactor. Metso, UPM and Fortum constructed and has operated since

1  
2  
3  
4  
5 2013 a 400 kg/h circulating bed pyrolysis reactor coupled with a condensation system in Joensuu  
6 (Finland). The bio-oil produced is combusted in a fluidized bed power boiler<sup>16</sup>. CPERI (Greece),  
7  
8 Guangzhou Inst. Energy Conversion (China), U. Birmingham and U. Nottingham (UK) and VTT  
9 (Finland) have active research programs on this technology<sup>16</sup>.  
10  
11

12  
13 *Rotating Cone:* This technology was developed by the University of Twente and is  
14 commercialized by BTG-BTL (Biomass Technology Group-Biomass to Liquid, Netherlands)  
15 (<http://www.btgworld.com/en/>)<sup>16</sup>. The centrifugal force effectively develops a transported bed  
16 without the need for large volumes of carrier gas<sup>16</sup>. The hot sand and the biomass are transported  
17 up in a conical bed by the centrifugal forces created by rotation of the cone<sup>16</sup>. This process has  
18 been successfully applied in Malaysia for the conversion of empty fruit bunches from palm oil  
19 trees in a demonstration plant of 50 t/day capacity<sup>165</sup>. This technology has been also used by  
20 Empyro for the construction of a plant that operates from 2015 in Hengelo (The Netherlands).  
21 This plant converts 5 t/h of wood residues into pyrolysis oil, process steam and electricity. In  
22 both plants, gas and char are burned to heat the sand, which is recycled back to the pyrolysis  
23 reactor<sup>16</sup>.  
24  
25  
26  
27  
28  
29  
30  
31  
32

33  
34  
35 *Ablative pyrolysis:* This process entails a heated surface in which wood is pressed against and  
36 moved rapidly leaving an oily film that then evaporates<sup>16</sup>. Larger particles of wood can be used  
37 for this process and the limiting factor is typically the rate of heat supplied to the reactor. These  
38 reactors can process large amounts of biomass in a little volume, are compact and do not require  
39 carrier gases or recirculation<sup>70, 71</sup>. The rate of reaction is proportional to the force exerted on the  
40 biomass in contact with the wall and the available heat transfer surface<sup>16</sup>. An important feature of  
41 ablative heat transfer is that when the biomass contacts the hot solid, ablation occurs and  
42 subsequently exposes new fresh biomass to the hot surface. This, in theory, allows for no  
43 limitations in particle size. NREL (Golden, Colorado, USA) and CNRS laboratories (France)  
44 conducted most of the pioneering studies on ablative reactors<sup>16</sup>. In the 90s, BBC from Canada  
45 built and operated an ablative reactor with a capacity between 10-25 kg/h<sup>136</sup> (this company is not  
46 in operation today). The University of Hamburg built three plants using ablative reactors. The  
47 first plant was conceived for research and has a capacity of 20 kg/h; the second one, is a pilot  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

1  
2  
3  
4  
5  
6  
7  
8  
9  
10  
11  
12  
13  
14  
15  
16  
17  
18  
19  
20  
21  
22  
23  
24  
25  
26  
27  
28  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

plant of 250 kg/h and the third is a demonstration unit with capacity of 2 t/h<sup>16, 136</sup>. Reed and Cowdrey constructed an ablative pyrolysis reactor testing bone dry wood at a feeding rate of 0.2 kg/h<sup>14</sup>. Biomass-to-oil (BTO) process was developed by PYTEC, Germany. The process is based on the ablative pyrolysis principle. Biomass wood (including chips of 60x40x5 mm) is put in direct contact with a rotating hot metal surface that melts the wood and produces oil<sup>173</sup>. The crude bio-oil produced is combusted in a CHP unit running on a 300 MW<sub>e</sub> diesel engine<sup>173</sup>. Compared with the fluidized bed, the main advantages of ablative reactors are: (1) no milling efforts needed for biomass, (2) compact design because of ideal heat transfer with high heating rates at relatively small contact surfaces, (3) energy and cost efficiency as no heating and cooling of fluidized bed is required, (4) condensation units with small volume can be installed, requiring less space and lower cost<sup>174</sup>. The main downsides are that these reactors require a heated surface area control system, operates with moving parts at high temperatures increasing their complexity, and induces an inevitable wear and tear on the moving components<sup>175</sup>. Table 12 reports the yields obtained in ablative reactors using wood and wheat straw. The yields of char, oil and gases are comparable with those obtained with similar feedstock with fluidized bed reactors. Aston University (UK), Institute of Engineering Thermophysics (Ukraine), Latvian State Institute (Latvia) and the Technical University of Denmark have active programs on this technology<sup>16, 42</sup>.

**Table 12.** Experiences on biomass fast pyrolysis using ablative pyrolysis reactors

Biomass specie	Capacity	T (°C)	Char (wt. %)	Bio-oil (wt. %)	Gas (wt. %)	Reference
Barley or wheat straw	10 kg/h	549	32	50	12	[176]
Wheat straw	Lab-scale pyrolysis centrifuge reactor	525	23-32	40-47	27-30	[177]
Wood	250 kg/h	650	6	60	34	[174]

*Spouted fluid bed reactor:* The viability of the spouted bed technology for pyrolysis was studied by the Chemical Engineering Department of the University of the Basque Country (Spain). A pilot plant at Ikerlan-IK4 facility with capacity to process up to 25 kg/h of biomass is now operational<sup>16, 178</sup>. The yield of products shown in Table 13 is comparable and even higher to those reported for fluidized bed reactors for similar feedstocks. The Anhui University of Science & Technology is also developing this technology<sup>16</sup>.

**Table 13.** Biomass pyrolysis results using a conical spouted bed

Biomass specie	Capacity	T (°C)	Char (wt.%)	Biooil (wt.%)	Gas (wt. %)	Reference
Rice husk	60 g/h	450	26	70	4	[179]
50% <i>Cytisus multiflorus</i> and 50% <i>Spartium junceum</i>	200 g/h	500	17	80	4	[180]
<i>Pterospartum tridentatum</i>	200 g/h	500	20	75	5	[180]
<i>Miscanthus</i>	Lab-scale	500	38	40	20	[181]
Pine saw dust	200 g/h	500	17	75	8	[182]
Pine saw dust	5 kg/h	480	14	73	13	[183]
<i>Acacia dealbata</i> (Silver wattle)	200 g/h	500	23	72	5	[180]
<i>Eucalyptus</i>	200 g/h	500	18	75	6	[184]

## 8. Microwave Pyrolysis

There are excellent reviews on microwave pyrolysis<sup>44,45, 185, 186</sup>. Von Hippel developed the basic understanding of the macroscopic microwave-matter interactions<sup>44</sup>. Microwave wavelengths falls between infrared and radio regions (from 0.3 to 300 GHz)<sup>44, 45</sup>. Heating is due to molecular friction during dipolar molecules rotation induced by the electromagnetic radiation. Conversely to conventional heating, microwave heating is a volumetric heating, so an opposite temperature gradient is established<sup>44</sup>. Tech-En Ltd in Hainault (UK) developed microwave pyrolysis in the mid-nineties<sup>185, 187, 188</sup>. In this process, the feedstock is thoroughly mixed with a highly microwave-adsorbent material (often char), which absorbs enough microwave energy (typically at 915 MHz or 2.45 GHz)<sup>185</sup>. Although microwave penetration is typically 1-2 cm, penetration depth varies depending on the properties of the materials and radiation frequency (oil palm fiber: 10.2 cm (at 5.8 GHz), oil palm shell: 5.5 cm (5.8 GHz), biochar: 8.5 cm (5.8 GHz), paper and cardboard: 20-60 cm (2.54 GHz), wood: 8-350 cm (2.54 GHz))<sup>44</sup>. While, microwave heating favors solid phase reactions, or heterogeneous reactions, conventional heating has higher effect on gas-phase reactions<sup>44</sup>. Table 14 shows product yields obtained with these reactors.

**Table 14.** Results of Biomass microwave pyrolysis.

Biomass specie	Reactor	T (°C)	Char (wt. %)	Bio-oil (wt. %)	Gas (wt. %)	Reference
Wheat straw	Mass: 5-30 g, N <sub>2</sub> : 3 L/min, 3 kW at 2.45 GHz	400-600			17-22	[189]
Larch ( <i>Lalix leptolepis</i> GORDON) Cylindrical blocks (d: 60–300 mm; weight: 80–12000 g)	1.5-3 kW at 2.45 GHz, exposition time: 3-12.5 min		18-50	15-30		[190]
Microalgae ( <i>Chlorella vulgaris</i> ) particle size < 200µm	Mass:30 g, power: 0.75-2.25 kW at 2.45 GHz, N <sub>2</sub> : 300 mL/min, catalysts: activated carbon, CaO, SiC	200 600 775	90 30 25	0 36 22	10 34 52	[191]
Douglas fir sawdust pellet (diameter: 6 mm, length: 10 mm)	Mass:400 g, 0.7 kW, reaction time: 10–20 min	350-450	31-61	31-54	8-15	[192]
Sewage sludge	Mass: 100 g, 25 g of graphite (1x1 mm) as microwave absorber, N <sub>2</sub> : 100 mL/min, Power 0.4-0.6 kW at 2.45 GHz	490-570	39-40	48-50	11-12	[193]
Rice straw	Mass: 3-5 g, N <sub>2</sub> : 50 mL/min, 0.2-0.5 kW	280-500			< 70	[194]
Oil palm fiber (OPF) (0.3–0.6 mm), and oil palm shell (OPS) (0.001 to 0.1 m)	Ratio sample: microwave absorber (1:0.25, 1:0.5, and 1:1), power 0.45 kW at 2.45 GHz, exposure time: 25 min	400-1300	OPS 45-70 OPF 50-80	OPS 10-20 OPF 5-25	OPS 20-30 OPF 10-28	[195]
Microalgae ( <i>Chlorella sp</i> )	Mass: 30 g, 6 g of char as microwave absorber, N <sub>2</sub> : 500 mL/min, Power 0.5-1.25 kW at 2.45 GHz, exposition time: 20 min	460-630	25-28	Oil 18-28 Water 20-22	24-35	[196]
Sewage sludge	Mass: 3.5 kg, N <sub>2</sub> : 5-20 L/min, power: 6.4-8.0 kW at 2.45 GHz, time: 120 min	350-500		30.4% of organic fraction		[197]
Rice straw (0.425-0.850 mm)	3-5 g sample, N <sub>2</sub> flow: 50 mL/min, 0.2-0.5 kW	400	28	23	49	[198]
Oil palm shell (OPS) < 0.850 mm)	Mass: 150 g, ratio sample: microwave absorber (1:0.25, 1:0.5, and 1:1), power 0.45 kW at 2.45 GHz, exposition time: 25 min	450-925	40-65	10-17	25-47	[199]
Corn stover	Mass:50 g, power: 0.3-0.9 kW at 2.45 GHz			30 (0.9 kW)	47 (0.9 kW)	[200]
Rice husk (RH) (0.149–0.297 mm, 0.149–0.074 mm and < 0.074 mm) Sugar cane residues (SCR)	Mass: 7-10 g , 0.15-0.4 kW at 2.45 GHz, exposition time: 4-30 min	280-600	RH: 33-50 SCR:s 25-67			[201]



1  
2  
3  
4  
5 The main advantages of microwave pyrolysis compared to conventional technologies are: (1)  
6 it provides rapid heating<sup>185</sup> (2) it is much cleaner and easier to control<sup>195</sup> (3) it can be easily  
7 modularized for small applications (these processes can be developed for on-site processing  
8 reducing transportation cost) (4) heat is generated within the material (the particles are heated  
9 from the center), allowing the surface of the reactor to operate at lower temperatures, (5) high  
10 conversion efficiencies of energy to heat (80-85 %) are obtained and (6) higher power  
11 densities are used<sup>185</sup>.  
12  
13  
14  
15  
16  
17

18  
19 The main challenges and barrier for microwave pyrolysis are: (1) limited information is  
20 available on waste materials microwave relevant properties<sup>185</sup> (2) uneven heating can lead to  
21 poor product quality control, (3) electricity is expensive and often produced from fossil fuels  
22 by Rankine cycles (with efficiency typically between 20 and 30 %), (4) electrical hazard that  
23 should be contained with an appropriate Faraday cage, (5) the presence of metals generate  
24 arcing that may damage the equipment, (6) the microwave heating systems are more  
25 expensive than traditional heating systems<sup>185</sup>. Some of the institutions with active programs in  
26 microwave pyrolysis are: The Chinese Academic of Sciences, the National Institute of  
27 Advanced Industrial Science and Technology of Japan, the Shandong University of China, the  
28 Technical University of Vienna (Austria), the University of Malaysia Sarawak (Malaysia), the  
29 University of Minnesota (USA), Washington State University (Tri-cities), the University of  
30 Mississippi (USA), the University of Nottingham (UK), the University of York (UK) and the  
31 Ecole Polytechnique de Montreal (Canada)<sup>16, 42</sup>.  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42

## 43 44 **9. Design and scale up of Pyrolysis units**

45  
46  
47 *Business models:* There are very few reports with information on the development of business  
48 models, technical design and techno-economic evaluation of pyrolysis units<sup>47, 202, 203</sup>. The  
49 technical design of the pyrolysis unit will depend on the business model selected<sup>203</sup>. The  
50 International Biochar Initiative (<http://www.biochar-international.org/commercialization>) has  
51 identified a number of business models for bio-char production including the characteristics of  
52 the feedstock, sustainability issues, associated production technology, potential co-products,  
53  
54  
55  
56  
57  
58  
59  
60



1  
2  
3  
4  
5 economic and social challenges. The main business models discussed by the IBI and the  
6 technologies associated were: (1) Restoration site (e.g. forest, wetland) (mobile pyrolysis,  
7 charring piles in situ), (2) Managed forest (mobile pyrolysis, hog fuel for co-generation,  
8 feedstock for pellets and briquettes), (3) Forest product processing waste (Co-gen pyrolysis or  
9 gasification, feedstock for pellet or briquettes), (4) Biomass plantation (Co-gen pyrolysis or  
10 gasification, feedstock for pellets or briquettes), (5) Urban forestry and landscaping (Biochar,  
11 process heat, electricity, home heat), (6) Agricultural Waste-Industrial (Mobile pyrolysis, co-gen,  
12 pyrolysis or gasification), (7) Agricultural waste subsistence (Stoves, kilns feedstock for  
13 briquettes), (8) Municipal Solid Waste (MSW) (Co-gen pyrolysis or gasification)<sup>203</sup>.

20  
21 *Reactor Sizing:* Although companies designing and building pyrolysis reactors may have  
22 developed scale up criteria and methodologies for sizing these equipment, the authors were not  
23 able to find systematic methodologies for the design of pyrolysis reactors in the open literature.  
24 Therefore, the design of pyrolysis reactors is still an art. For this reason, in this section we will  
25 briefly present a strategy based on our own experience. The design of pyrolysis reactors can be  
26 conducted following these steps: (1) Select throughput capacity, (2) Determine the biomass  
27 particle size to be used, (3) In the case of fluidized bed reactors select the appropriate  
28 sand/biomass particles size ratio, (4) Select the carrier gas to be used and quantify the carrier gas  
29 to be used (for fluidized bed reactors it is recommended 2.75 kg carrier gas/kg dry biomass<sup>204</sup>);  
30 (5) Specify reaction temperature (in the case of fast pyrolysis typically 500 °C) and conduct  
31 pyrolysis tests at lab or pilot facilities (6) Conduct a mass balance with the yield of products  
32 obtained experimentally (see information in tables 5, 6, 7, 8, 10); (7) Conduct energy balances to  
33 calculate how much heat has to be removed or supplied to the reactor. Thermodynamic  
34 information for the overall energy balance of pyrolysis reactors can be found elsewhere<sup>205-208</sup>. (8)  
35 Calculate the residence time of the biomass particle to achieve a targeted conversion.  
36 Information on experimental and modeling strategies (single particle models) to calculate  
37 conversion as a function of residence time can be found elsewhere<sup>72, 75, 209-211</sup>. (9) Calculate the  
38 solid hold up in the reactor. The residence time of the solid in the reactor depend on the  
39 hydrodynamic and the mechanic design of these reactors. In the case of rotary drums, it depends  
40 on the slope of the reactor, kiln rotational speed and the length and diameter of the reactor<sup>212</sup>. For  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

1  
2  
3  
4  
5 fluidized beds, the retention of the solid is controlled by the terminal velocity of the converted  
6 biomass particle in the free board, (10) In the case of fluidized bed calculate or determine  
7 experimentally the minimum fluidization velocity (typically use 2 to 3 times the minimum  
8 fluidization velocity)<sup>213, 214</sup>, (11) Calculate the cross sectional area and diameter of the reactor<sup>213</sup>,  
9 (12) In the case of fluidized bed reactors calculate volume of expanded fluidized bed (sand and  
10 char particles)<sup>213, 215</sup>, (13) If designing fluidized bed reactors calculate the length and the  
11 diameter of the free board<sup>213</sup>, (14) Select the heating or cooling method to be used (e.g. indirect,  
12 direct or microwave heating) and calculate the heat transfer area needed to supply or remove the  
13 heat calculated in the energy balances<sup>213</sup>, (15) In the case of the fluidized bed reactors size the  
14 distribution grate<sup>213</sup>.  
15  
16  
17  
18  
19  
20  
21  
22  
23

## 24 **10. Challenges for the implementation of pyrolysis**

25  
26  
27 The development of pyrolysis technologies must overcome two major hurdles. The first one is  
28 associated with the lack of markets for pyrolysis oils and the second one with the lack of biochar  
29 derived products with well-defined performance characteristics. Consequently, it is imperative to  
30 accelerate the development and deployment of bio-oil refineries and the development and  
31 commercialization of engineered bio-char for environmental services. Developing flexible  
32 designs for pyrolysis units to produce high yields of both bio-oil and char is a technological  
33 challenge facing the thermochemical community.  
34  
35  
36  
37  
38  
39  
40  
41

42 The selection of pyrolysis technologies, their operational conditions, and the feedstocks to be  
43 used will depend mostly on economic tradeoffs<sup>216</sup>. The results presented in this review clearly  
44 show that there are multiple operational conditions and designs to obtain a wide range of  
45 products yields. Most of fast pyrolysis reactors reviewed are operated at conditions (500 °C,  
46 small particles (below than 2 mm), use of heat carrier (sand) and residence time of vapors below  
47 2 s (use of a carrier gas)) for maximizing bio-oil yields with little regard for the quality of the  
48 product. The use of high volumes of carrier gas and the heat carrier reduce the energy efficiency  
49 of these processes, create important sand attrition problems, and makes it very difficult to  
50 condense the diluted vapors, requiring very large surface areas and considerable cooling power.  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

1  
2  
3  
4  
5 Most of fast pyrolysis designs combust the char to satisfy the energy needs of the process. The  
6 difficulties to refine fast pyrolysis oils with high oxygen content is the main reason for the  
7 growing interest in catalytic pyrolysis for the production of bio-oils with lower oxygen content.  
8  
9 The catalytic cracking strategies to reduce bio-oil oxygen content typically result in an increase  
10 in gas yield and coke formation. The converters reviewed are flexible enough to operate in  
11 conditions where bio-oil and biochar production is possible. More studies are needed to explore  
12 designs that take advantage of homogeneous secondary reactions in gas phase for oxygen  
13 removal from pyrolysis oils.  
14  
15  
16  
17  
18  
19

20  
21 There is a vast diversity of situations in which pyrolysis can be applied (different feedstocks,  
22 scale, capacity, use of mobile or stationary units) as well as the diversity of products that can be  
23 obtained. This makes it very difficult to find an exclusive design that is sustainable across all the  
24 potential applications. Table 15 is an attempt to summarize the type of reactor suitable for a  
25 specific cases. A balanced investment in the creation of new knowledge (i.e., Science), in the  
26 design, testing and scale up of new technologies (for pyrolysis reactors and for rural bio-oil  
27 refineries) (i.e., Technology) and in the development of new products (from bio-oil and char)  
28 (i.e., Market) to build a shared vision that take advantage of existing infrastructure and is  
29 achievable in small steps are all critical for the deployment of a viable biomass based economy  
30 on pyrolysis technologies.  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

**Table 15.** Summary of the technology status of pyrolysis reactors

Type of reactor	Companies/Institutions <sup>a</sup>	Technology status	Remarks	References
<b>Kilns using Trunks of cordwood of Logs</b>				
Earth kiln, traditional methods	Families for household income, farmers, communities	Commercial	Widely used in developing nations	[115, 217]
Cinder block, brick and metal kilns (Brazilian and Brazilian beehive and Half orange, TPI kiln, New Hampshire, Connecticut, Missouri kiln)	Families for household income, farmers, communities, multiple small companies -	Commercial	Widely used in developing nations	[87, 115]
<b>Retorts using trunks of cordwood or Logs</b>				
Small metal kilns and retorts	Applied Gaia Corporation (US) Carbon Compost Co. Ltd (UK) Pressvess (UK) CarbonZero, (Switzerland) Ithaka Institut (Switzerland)	Commercial	Multiple designs, Some can include liquid recovery	<a href="http://appliedgaia.com">http://appliedgaia.com</a> <a href="http://www.carboncompost.co.uk">http://www.carboncompost.co.uk</a> <a href="http://www.pressvess.co.uk">http://www.pressvess.co.uk</a> <a href="http://www.carbonzero.ch">http://www.carbonzero.ch</a> <a href="http://www.ithaka-institut.org/en/kon-tiki">http://www.ithaka-institut.org/en/kon-tiki</a>
Adam retort	Adam + Partner (Ethiopia)	Commercial		[108, 109]
Wagon retorts	O.E.T. Calusco (Imperianti Trattamento Biomass) Alterna Biocarbon	Commercial	No operating units <sup>b</sup>	[4, 5, 43, 115]
Reichert converter	Evonik (Germany, formerly Degussa)	Commercial		[5, 218]
French SIFIC Process (CISR Lambiotte retort)	Lambiotte (France) Balt Carbon (Latvia)	Commercial		<a href="http://www.lambiotte.com">http://www.lambiotte.com</a> [43, 115]
Lurgi carbonization retort (Lurgi Umwelt GmbH)	Simcoa (Australia) Lurgi LR (Germany)	Commercial		<a href="http://www.simcoa.com.au">http://www.simcoa.com.au</a> [43, 16]
Twin type retorts	Charbon Engineering (Carbon-Twin) (Netherlands) Clean Fuels (Netherlands) VMR Systems (Netherlands) CG2000 Carboniser Ibero Massa Florestal (Portugal)	Commercial	Some designs can include liquid recovery	<a href="http://www.charbon-engineering.eu">http://www.charbon-engineering.eu</a> <a href="http://www.cleanfuels.nl">http://www.cleanfuels.nl</a> , <a href="http://www.vmrsystems.com">http://www.vmrsystems.com</a> , <a href="http://www.imflorestal.com">http://www.imflorestal.com</a> [43, 112, 115, 219]]
Flash Carbonization	University of Hawai'i	Pilot Plant		[6, 43]

**Table 15.** Summary of the technology status (Continuation....)

Type of reactor	Companies/Institutions <sup>a</sup>	Technology status	Remarks	References
<b>Converters using chips and pellets</b>				
Herreshoff multiple hearth furnaces	(BigChar) Pyrocal Pty Ltd (Australia) CSE Hankin Environmental System (USA)	Commercial		<a href="http://www.bigchar.com.au">http://www.bigchar.com.au</a> , <a href="http://hankines.com">http://hankines.com</a> [115, 119]
Autogenous pyrolysis reactor	CSIRO (Australia)	Pilot Plant		[220]
Auger reactors	BioGreen Spirajoule (France) Genesis Industries (USA) BioMaCon GmbH (Germany) Karr Group (USA) Polvax (Ukraine) Pro-Natura (France)	Commercial	Multiple designs and companies offering auger reactors	<a href="http://www.biogreen-energy.com">http://www.biogreen-energy.com</a> , <a href="http://egenindustries.com">http://egenindustries.com</a> <a href="http://www.biomacon.com">http://www.biomacon.com</a> <a href="http://karrgroupco.com">http://karrgroupco.com</a> <a href="http://www.pyrolys.net">http://www.pyrolys.net</a> <a href="http://www.pronatura.org/?page_id=521&amp;lang=en">http://www.pronatura.org/?page_id=521&amp;lang=en</a> , [115]
	Bioliq, Karlsruher Institute für Technologie (Germany), Energy Farmers (Australia) ABRITech (Canada) Renewable Oil International LLC (USA)	Demonstration		<a href="http://www.energyfarmers.com.au">http://www.energyfarmers.com.au</a> <a href="http://www.abritechinc.com">http://www.abritechinc.com</a> , <a href="http://demoplants21.bioenergy2020.eu/projects/displaymap/twhWVt">http://demoplants21.bioenergy2020.eu/projects/displaymap/twhWVt</a> <a href="http://www.renewableoil.com">www.renewableoil.com</a> [221, 16]
	Thermo-catalytic reforming (Fraunhofer UMSICHT & Susteen Technologies, Germany), Alternative Energy Solutions Ltd (New Zealand) Renewable Oil Int, (USA)	Pilot Plant		<a href="http://www.susteen-tech.com">http://www.susteen-tech.com</a> [16,222]
Indirectly heated Rotary kilns	Amaron Energy (USA) Mitsubishi Heavy Industries (Japan) Ansac Energy Ltd 3R Environmental Technologies Group Mitsui R21 ITC	Commercial	Multiple plants for waste treatment (MSW, sludge) are adaptable to biomass pyrolysis.	<a href="http://www.amaronenergy.com">http://www.amaronenergy.com</a> , <a href="http://www.mhiec.co.jp/en/products/water/sludge/contents/sludge_carbonization_facility.html">http://www.mhiec.co.jp/en/products/water/sludge/contents/sludge_carbonization_facility.html</a> [222]
	University of Perugia (Italy)	Pilot Plant		[223]

**Table 15.** Summary of the technology status of pyrolysis reactors (Continuation...)

Type of reactor	Companies/Institutions <sup>a</sup>	Technology status	Remarks	References
<b>Fast/intermediate Pyrolysis Reactors using chips</b>				
Moving Agitated bed (Pyrovac)	Pyrovac	Demonstration		[134, 135]
Shelf reactors		Commercial	No operating units <sup>b</sup>	[4, 46]
Paddle pyrolysis kiln	BEST	Demonstration	-	BEST website not working
Ablative pyrolysis Pytec, German	Pytec	Demonstration	Web site is not working-	[16]
Rotating cone	BTG-BTL, Netherlands	Commercial		<a href="http://www.empyroproject.eu">http://www.empyroproject.eu</a> <a href="http://www.btgworld.com/en/">http://www.btgworld.com/en/</a> [16]
<b>Fast Pyrolysis using fine particles (catalytic and non-catalytic processes)</b>				
Bubbling Fluidized bed reactors.	Anellotech (USA) Valmet - Fortum (Finland) Agritherm (Canada) RTI (USA) Avello Bioenergy (USA) Bioware, (Brasil) Biomass Engineering Ltd (BEL), UK Nettenergy BV (Netherlands)	Commercial / Demonstration	Static/Mobile	<a href="http://anellotech.com">http://anellotech.com</a> <a href="http://www.fortum.com">http://www.fortum.com</a> <a href="http://agri-therm.com">http://agri-therm.com</a> <a href="http://www.rti.org/energy">www.rti.org/energy</a> <a href="http://www.avellobioenergy.com">http://www.avellobioenergy.com</a> <a href="https://www.bioware.com.br">https://www.bioware.com.br</a> <a href="http://www.nettenergy.com/index.php/en/">http://www.nettenergy.com/index.php/en/</a> [16, 42]
Circulating bed reactors	Rapid Thermal Processing: Ensyn, (USA), Envergent Technologies (USA) Metso (Finland) Anaeris Technology (former Kior)	Commercial / Demonstration		<a href="http://www.ensyn.com">http://www.ensyn.com</a> , <a href="https://www.envergenttech.com">https://www.envergenttech.com</a> <a href="http://www.inaeristech.com/">http://www.inaeristech.com/</a> [149, 16]
Spouted bed	Ikerlan (Spain)	Pilot Plant		[16, 178]
<b>Microwave pyrolysis</b>				
Microwave pyrolysis	Carbonscape (New Zealand) Beijing Sino-Green Technology Co., Ltd (China) Bioenergy 2020 + gmbh (Austria)	Pilot Plant		<a href="http://carbonscape.com">http://carbonscape.com</a> , [186, 16]

## 11. Conclusions

The number of publications on slow and fast pyrolysis reactors has been growing steadily in the last thirty years. The community interested in these reactors is formed by researchers interested on char production and those interested on bio-oil production. This paper reviews slow, intermediate, fast and microwave pyrolysis intending that companies and academic institutions, researching, designing and commercializing pyrolysis/carbonization reactors can take advantage of the technological solutions shown. Very little progress has been made in the last century in the design of kilns. The release of large quantities of pyrolysis vapors to the atmosphere and/or their condensation in soils are major sources of pollution that need to be urgently addressed. Several of the *retorts* used today were developed and commercialized by the “wood distillation industry”. These units were designed for the carbonization of logs. However, deforestation issues and the limited availability of logs for carbonization are major hurdles for their widespread deployment in today’s world. The *converters* are receiving growing attention for their capacity to convert forest and agricultural residues in the form of chips and shredded materials into bio-oil and charcoal. These systems do not require the use of large volumes of carrier gas or a heat carrier (sand). Nevertheless, the lack of commercial interest for fine chars produced by these systems has been a major hurdle for the commercialization of this technology. The growing interest on using char as soil amendments and the development of technologies for the production of char pellets and briquettes from these fines are catalyzing new companies commercializing these designs. The current design and operation of *fast pyrolysis reactors* is based on conditions maximizing bio-oil yields with little regard for the quality of the bio-oil produced. High bio-oil yield is achieved at 500 °C, using small particles (less than 1 mm) a heat carrier (sand) and using high volumes of carrier gas to reduce the residence time of vapors below 2 s. The energy need of these reactors is typically satisfied by char combustion. Consequently, most of these processes do not commercialize char as one of their products. The lack of commercial bio-oil refineries is the main barrier for the commercialization of these reactors. Problems with fast pyrolysis oil refining are catalyzing interest on strategies to produce oils with lower oxygen content. Most of these strategies result in high gas yield, which is an opportunity to explore the use of the gases to satisfy part of the energy needed of the system, without scarifying

1  
2  
3  
4 char production. Microwave pyrolysis is a promising technology for the development of small  
5 convenient systems for waste management.  
6  
7  
8

9  
10 **Acknowledgements:** M.G-P acknowledges the Waste to Fuel program from the Washington  
11 State Department of Ecology, Washington State Agricultural Research Center (NIFA-Hatch-  
12 WNP00701) and the National Science Foundation (CBET-1434073, CAREER CBET-1150430)  
13 for their financial support.  
14  
15  
16

17  
18  
19 **References:**

- 20  
21 1. Withrow J: The Chemical Engineering of the Hardwood Distillation Industry. *Ind. Eng. Chem.*  
22 *Res.* (1915), Vol. 7, No II, p. 912  
23  
24 2. Brown N.C: The hardwood distillation industry in New York. The New York State College of  
25 Forestry at Syracuse University. January 1917.  
26  
27 3. Bunbury, H. M., The destructive distillation of wood, Benn Brothers, Ltd., London, 1923.  
28  
29 4. Klar M, Rule A: The Technology of Wood Distillation. London Chapman & Hall LTD, 1925.  
30  
31 5. Emrich W., Handbook of charcoal Making. The Traditional and Industrial Methods, D. Reidel  
32 Publishing Company, 1985  
33  
34 6. Antal, MJ, Grønli M., The Art, Science, and Technology of Charcoal Production, *Ind. Eng.*  
35 *Chem. Res.* 2003, 42, 1619–1640.  
36  
37 7. Antal MJ, Mochidzuki K, Paredes LS: Flash Carbonization of Biomass. *Ind. Eng. Chem. Res.*,  
38 2003, 42 (16), 3690-3699.  
39  
40 8. Veitch, F.P., Chemical Methods for Utilizing Wood. Including destructive distillation,  
41 recovery of Turpentin, rosin and pulp, and the preparation of alcohols and oxalic acid.  
42 USDA, 1907  
43  
44 9. Canham, H. O., The wood chemical industry in the Northeast: An old industry with new  
45 possibilities, Northern Woodlands, February 8th 2010, [http://www.faqs.org/photo-](http://www.faqs.org/photo-dict/phrase/10393/kilns.html)  
46 [dict/phrase/10393/kilns.html](http://www.faqs.org/photo-dict/phrase/10393/kilns.html)  
47  
48 10. Massengale R, Black gold:A history of charcoal in Missouri, Author House, Bloomington,  
49 2006  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60



11. Scott DS, Piskorz J, The Continuous Flash Pyrolysis of Biomass. *Can. J. Chem. Eng.* 1984, 62 (3), 404-412.
12. Scot DS, Piskorz J, Radlein D. Liquid products from the continuous flash pyrolysis of biomass. *Ind. Eng Chem Process Des Dev.*, 1985, 24, 581-888.
13. Bridgwater AV, Czernik S, Piskorz J: The status of biomass fast pyrolysis. In: Bridgwater AV, editor. *Fast pyrolysis of biomass a handbook*, Vol. 2. Newbury, UK, CPL Press, 2002, p. 1-22.
14. Bridgwater AV, Peacocke GVC, *Fast Pyrolysis Processes for Biomass. Renewable and Sustainable Energy Reviews*, 2000, 4, 1-73
15. Czernik S, Bridgwater A.V., Overview of Applications of Biomass Fast Pyrolysis Oil. *Energy & Fuel*, 2004, 18, 2, 977-997
16. Bridgwater AV, Review of fast pyrolysis of biomass and product upgrading. *Biomass and Bioenergy*, 38, 2012, 68-94
17. Diebold J.P., Bridgwater A.V., Overview of Fast Pyrolysis of Biomass for the Production of Liquid Fuels. *Fast Pyrolysis of Biomass. A Handbook*, Eds. Bridgwater A et al. CPL press, 1999, 14-32.
18. Kersten SRA, Wang X, Prins W, van Swaaij WPM: Biomass pyrolysis in a fluidized bed reactor. Part 1: literature review and model simulations. *Ind Eng Chem Res.*, 2005, 44: 8773-85.
19. Mohan D, Pittman CU, Steele PH: Pyrolysis of Wood/Biomass: A critical review. *Energy & Fuels*, 2006, 20 (3), 848-889.
20. Elliott DC: Historical developments in hydroprocessing bio-oils. *Energy & Fuels*, 2007, 21: 1792-1815
21. Elliott D: Advancement of Bio-oil Utilization for Refinery Feedstock. Presented at the Washington Bioenergy Research Symposium. November 8, 2010, Seattle, Washington State ([http://www.pacificbiomass.org/documents/Elliott%20\(C1\).pdf](http://www.pacificbiomass.org/documents/Elliott%20(C1).pdf)).
22. Kumar S, Lange J-P, Van Rossum G, Kersten SRA: Bio-oil fractionation by temperature-swing extraction: Principle and Application. *Biomass and Bioenergy*, 2015, 83, 96-104

- 1  
2  
3  
4  
5  
6  
7  
8  
9  
10  
11  
12  
13  
14  
15  
16  
17  
18  
19  
20  
21  
22  
23  
24  
25  
26  
27  
28  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60
23. Ijmker HM, Gramblicka M, Kersten SRA, van der Ham AGJ, Schuur B: Acetic Acid extraction from aqueous solutions using fatty acids. *Separation and Purification technology* 125, 2014, 256-263.
  24. Li X, Luque-Moreno LC, Oudenhoven SRC, Rehmann L, Kersten SRA, Schuur B: Aromatics extraction from pyrolytic sugars using ionic liquid to enhance sugar fermentability. *Bioresource Technology*, 2016, 216, 12-18.
  25. Li X, Kersten SRA, Schuur B: Extraction of acetic acid, glycoaldehyde and acetol from aqueous solutions mimicking pyrolysis oil cuts using ionic liquid. *Separation and Purification technology*. 175, 2017, 24, 498-505
  26. FAO 2017. The charcoal transition: greening the charcoal value chain to mitigate climate change and improve local livelihoods, by J. van Dam. Rome, Food and Agricultural Organization of the United Nations. <http://www.fao.org/3/a-i6935e.pdf>
  27. Stassen HE: Chapter 14: Current Issues in Charcoal Production and Use. In: Biomass power for the world. Edited Wim PM van Swaij, Kersten SRA, Palz W, 2015.
  28. Mangué, P. D., Review of the existing studies related to fuelwood and/or charcoal in Mozambique, Project GCP/INT/679/EC, EC-FAO Partnership Programme, 2000
  29. Kammen DM, Lew DJ: Review of Technologies for the Production and Use of Char. Energy and Resources Group & Goldman School of Public Policy. UC Berkley and NREL, 2005
  30. Seidel A, Charcoal in Africa. Importance, Problems and Possible Strategies. Eschborn, 2008.
  31. FAO, Simple technologies for Charcoal Making, FAO Forestry paper 41, 1983. Available at: <http://www.fao.org/docrep/X5328e/X5328e00.htm>
  32. FAO (2017), FAOSTAT, Forestry Production and Trade, Retrieved February 17<sup>th</sup>, 2017, from: <http://www.fao.org/faostat/en/#data/FO>
  33. Chidumayo EN, Gumbo DJ: The environmental impacts of charcoal production in tropical ecosystems of the world: A synthesis, 2013, 17, 2, 86-94
  34. Bailis R, Rujanavech C, Dwivedi P, de Oliveire Vilela A, Chang H, Carneiro de Miranda R: Innovation in charcoal production: A comparative life-cycle assessment of two kiln technologies in Brazil. *Energy for Sustainable Development*, 2013, 17, 2, 189-200

- 1  
2  
3  
4  
5 35. Kituyi E: Towards sustainable production and use of charcoal in Kenya: exploring the  
6 potential in life cycle management approach. *Journal of Cleaner Production*, 2004, 12,  
7 1047-1057  
8  
9  
10 36. Norgate T, Langberg D: Environmental and Economic Aspects of Charcoal Use in  
11 Steelmaking. *ISIJ International*, 2009, 49, 4, 587-595  
12  
13 37. Amonette J: Biochar and Bioenergy: What Can they Do to Help Mitigate Climate Change.  
14 Washington State Bioenergy Research Symposium, Seattle, WA, 8 November 2010.  
15 [http://www.pacificbiomass.org/documents/Amonette%20\(C1\).pdf](http://www.pacificbiomass.org/documents/Amonette%20(C1).pdf)  
16  
17  
18 38. Lehmann, J., Stephen, J., Char for Environmental Management: An Introduction, In: Biochar  
19 for Environmental Management. Science and Technology, Earthscan Publishers Ltd, 2009  
20  
21 39. Woolf D, Amonette J, Stree-Perrot A, Lehmann J, Joseph S: Sustainable biochar to mitigate  
22 global change. *Nature Communications*, August 2010 OPEN ACCESS online at:  
23 [www.nature.com/naturecommunications](http://www.nature.com/naturecommunications)  
24  
25  
26 40. Ogawa, M., Okimori, Y., Pioneering works in biochar research, Japan, *Australian Journal of*  
27 *Soil Research*, 2010, 48, 489–500  
28  
29 41. Trossero M, Domac J, Siemons R: Industrial Char Production. TCP/CRO/3101 (A)  
30 Development of a sustainable char industry. FAO, June 2008, Zagreb, Croatia  
31  
32 42. Meier D, van de Beld B, Bridgwater AV, Elliott D, Oasmaa A, Preto F: State of the art of fast  
33 pyrolysis in IEA bioenergy member countries. *Renewable and Sustainable Energy Reviews*  
34 20 (2013) 619-641  
35  
36 43. Grønli, M., 2010, Pyrolysis and Charcoal,  
37 <http://www.bioforsk.no/ikbViewer/Content/71499/Biokarbonseminar%20%20%C5s%2011-03-2010%20Morten%20Gr%F8nli.pdf>, Retrieved February 26, 2017,  
38  
39 44. Motasemi F, Afzal MT: A review on the microwave-assisted pyrolysis technique. *Renewable*  
40 *and Sustainable Energy Reviews*, 2013, 28, 317-330  
41  
42 45. Mushtaq F, Mat R, Nasir-Ani F: A review on microwave assisted pyrolysis of coal and  
43 biomass for fuel production. *Renewable and Sustainable Energy Reviews* 39, 2014, 555-  
44 574  
45  
46 46. Dumesny P, Noyer J Wood Products. Distillates and Extracts. Part I. The Chemical Products  
47 of Wood distillation. Part II. Dyeing and tanning extracts from wood. London, Scott,  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

- 1  
2  
3  
4  
5 Greenwood & Son. "The oil and colour Trades Journal "Offices & Broadway, Ludgate Hill,  
6 E.C.1908.  
7
- 8  
9  
10 47. Lynch J, Joseph S: Guidelines for the Development and Testing of Pyrolysis Plants to  
11 Produce Char. International Biochar Initiative, IBI 2010. [http://www.biochar-](http://www.biochar-international.org/sites/default/files/IBI_Pyrolysis_Plant_Guidelines.pdf)  
12 [international.org/sites/default/files/IBI\\_Pyrolysis\\_Plant\\_Guidelines.pdf](http://www.biochar-international.org/sites/default/files/IBI_Pyrolysis_Plant_Guidelines.pdf) Retrieved February  
13 26, 2017,  
14
- 15  
16 48. Wang X, Kersten SRA, Prins W, van Swaaij WPM: Biomass Pyrolysis in a Fluidized bed  
17 reactor. Part 2: Experimental Validation of Model results. *Ind. Eng. Chem. Res.* 2005, 44,  
18 8786-8795  
19
- 20  
21 49. Shen J, Wang X-S, Garcia-Perez M, Mourant D, Rhodes MJ, Li C-Z: Effects of particle size  
22 on the fast pyrolysis of oil mallee woody biomass. *Fuel*, 2009, 88, 1810-1817  
23
- 24  
25 50. Westerhof RJM, Nygard HS, van Swaaij WPM, Kersten SRA, Brilman DWF. Effect of  
26 Particle Geometry and Microstructure on Fast Pyrolysis of Beech Wood. *Energy & Fuels*,  
27 2012; 26, 4, 2274  
28
- 29  
30 51. Zhou S, Garcia-Perez M, Pecha B, McDonald AG, Westerhof RJM: Effect of particle size on  
31 the composition of lignin derived oligomers obtained by the fast pyrolysis of beech wood.  
32 *Fuel*, 2014, 125, 15-19  
33
- 34  
35 52. Patwardhan PR, Satrio J, Brown RC, Shanks BH: Influence of inorganic salts on the  
36 primary pyrolysis products of cellulose. *Bioresource Technology*, 2010, 101, 4646-4655  
37
- 38  
39 53. Mourant D, Wang Z, He M, Wang XS, Garcia-Perez M, Ling K, :Li C-Z: Mallee wood fast  
40 pyrolysis: Effects of alkali and alkaline earth metallic species on the yield and composition  
41 of bio-oil. *Fuel*, 2011, 90, 2915-2922  
42
- 43  
44 54. Oasmaa A, Sundqvist T, Kuoppala E, Garcia-Perez M, Solantausta Y, Lindfors C:  
45 Controlling Phase Stability of Biomass Fast Pyrolysis Bio-oils. *Energy&Fuels*, 2015, 29, 7,  
46 4373–4381  
47
- 48  
49 55. Hoekstra E, Westerhof RJM, Brikman W, Van Swaaij WPM, Kersten SRA, Hogendoorn  
50 KJA: Heterogeneous and Homogeneous Reactions of Pyrolysis Vapors from Pine Wood.  
51 *AiChE Journal*, 2012, 58, 9, 2830-2842  
52  
53  
54  
55  
56  
57  
58  
59  
60

- 1  
2  
3  
4  
5 56. Hoekstra E, Van Swaaij WPM, Kersten SRA, Hogendoorn KJA: Fast Pyrolysis in a novel  
6 wire-mesh reactor: Decomposition of pine wood and model compounds. *Chemical*  
7 *Engineering Journal*, 2012, 187, 172-184  
8  
9  
10 57. Zhou S, Garcia-Perez M, Pecha B, McDonald A, Kersten SRA, Westerhof RJM: Secondary  
11 Vapor Phase Reactions of Lignin-Derived Oligomers Obtained by Fast Pyrolysis of Pine  
12 Wood. *Energy&Fuels*, 2013, 27, 3, 1428-1438  
13  
14  
15 58. Mok S. W., Antal, M. J., Szabo, P., Varhegyi, G., Zelei, B., Formation of Charcoal from  
16 Biomass in a Sealed Reactor, *Ind. Eng. Chem. Res.* 1992, 31, 1162-1166.  
17  
18  
19 59. Garcia-Perez M, Chaala A, Roy C: Vacuum pyrolysis of sugarcane bagasse. *J. Anal. Appl.*  
20 *Pyrolysis*, 2002, 65, 111-136  
21  
22  
23 60. Garcia-Perez M, Chaala A, Pakdel H, Kretchmer D, Roy C: Vacuum pyrolysis of softwood  
24 and hardwood biomass. Comparison between product yields and bio-oil properties. *J. Anal.*  
25 *Appl. Pyrolysis*, 2007, 78, 104-116  
26  
27  
28 61. Liaw S-S, Zhou S, Wu H, Garcia-Perez: Effect of Pretreatment Temperature on the Yield and  
29 Properties of Bio-Oils obtained from the Auger Pyrolysis of Douglas Fir Wood. *Fuel*, 2013,  
30 103, 672-682  
31  
32  
33 62. Westerhof RJM, Brillman DWF, Garcia-Perez M, Wang Z, Oudenhoven SRG, Kersten SRA.  
34 Stepwise fast pyrolysis of pine wood. *Energy&Fuels*, 2012; 26, 12, 7263.  
35  
36  
37 63. Montoya J, Pecha B, Roman D, Chejna-Janna F, Garcia-Perez M: Effect of temperature and  
38 heating rate on product distribution from the pyrolysis of sugarcane bagasse in a hot plate  
39 reactor. *J. Anal. Appl. Pyrolysis* 123, 2017, 347-362  
40  
41  
42 64. Wooten J.B., Seeman J.I., Hajaligol M.R. 2004. Observation and Characterization of  
43 Cellulose Pyrolysis Intermediates by C CP MAS NMR. A New Mechanistic Model<sup>13</sup> *Energy*  
44 *& Fuels*, 2003, 18, 1.  
45  
46  
47 65. Westerhof RJM, Oudenhoven SRG, Marathe PS, Englen M, Garcia-Perez M, Wang Z,  
48 Kersten SRA: The Interplay between Chemistry and Heat/Mass Transfer during Fast  
49 Pyrolysis of Cellulose. *Reaction Chemistry & Engineering*, 2016, 1, 555.  
50  
51  
52 66. Dauenhauer PJ, Colby JL, Balonek CM, Suszynski WJ, Schmidt LD: Reactive boiling of  
53 cellulose for integrated catalysis through an intermediate liquid. *Green Chem.* 2009, 11,  
54 1555-1561  
55  
56  
57  
58  
59  
60

- 1  
2  
3  
4  
5 67. Montoya J, Pecha B, Chejne-Janna F, Garcia-Perez M: Micro-explosion of liquid  
6 intermediates during the fast pyrolysis of sucrose and organosolv lignin. *J. Anal. Appl.*  
7 *Pyrolysis*, 2016, 122, 106-121  
8  
9  
10 68. Pelaez-Samaniego MR, Yadama V, Garcia-Perez M, Lowell E, McDonald AG: Effect of  
11 temperature during wood torrefaction on the formation of lignin liquid intermediates. *J.*  
12 *Anal. Appl. Pyrolysis*. 2014, 109, 222-233  
13  
14  
15 69. Mamleev V, Bourigot S, Le Bras M, Yvon J: The facts and hypotheses relating to the  
16 phenomenological model of cellulose pyrolysis: Interdependence of the steps. *J. Anal. Appl.*  
17 *Pyrolysis*, 2009, 84, 1-17.  
18  
19  
20 70. Graham RG, Bergougnou MA, Overend RP: Fast Pyrolysis of Biomass. *J. of Anal. Appl.*  
21 *Pyrolysis*, 6, 1984, 95-135.  
22  
23  
24 71. Graham R.G., Bergougnou M.A., Freel B.A. The kinetics of vapor phase cellulose fast  
25 pyrolysis reactions. *Biomass and Bioenergy*, 1994, 7, 1-6, 33-47  
26  
27  
28 72. Pyle DL, Zaror CA: Heat transfer and kinetics in the low temperature pyrolysis of solids.  
29 *Chemical Engineering Science*, 1984, 36, 1, 147-158,  
30  
31  
32 73. Di Blasi C, Galgano A, Branca C: Effects of Potassium Hydroxide Impregnation on Wood  
33 Pyrolysis. *Energy & Fuels*, 2009, 23, 1045-1054  
34  
35 74. Garcia-Perez, M., Xiao Shan Wang, Jun Shen, Martin J. Rhodes, Fujun Tian, Woo-Jin Lee,  
36 Hongwei Wu, and Chun-Zhu Li, Fast Pyrolysis of Oil Mallee Woody Biomass: Effect of  
37 Temperature on the Yield and Quality of Pyrolysis Products, *Ind. Eng. Chem. Res.* 2008, 47,  
38 1846-1854  
39  
40  
41 75. Kersten SRA, Garcia-Perez M: Recent developments in fast pyrolysis of lingo-cellulosic  
42 materials. *Current Opinion in Biotechnology*, 2013, 24: 414-420  
43  
44  
45 76. Coates R, Gardner T: Mobile Pyrolysis Process for Conversion of Biomass into Energy  
46 Products. Amaron Energy. Presentation at the 2014 Washington Demonstration.  
47 <http://www.pacificbiomass.org/documents/Amaron.pdf>. Accessed on Feb 26, 2017  
48  
49  
50 77. Liaw S-S, Wang Z, Ndegwa P, Frear C, Ha S, Li C-Z, et al. Effect of pyrolysis temperature  
51 on the yield and properties of bio-oils obtained from the auger pyrolysis of Douglas Fir  
52 wood. *J. Anal. Appl. Pyrolysis*, 2012;93, 52.  
53  
54  
55  
56  
57  
58  
59  
60

- 1  
2  
3  
4  
5 78. Rousset P: From biomass to fuel, power and chemicals. Brazilian charcoal-based pig iron.  
6 Cirad. Presentation at the Department of Aeronautics and Astronautics, National Cheng  
7 Kung University, Taiwan, ROC, November, 6<sup>th</sup>, 2014  
8 <http://agritrop.cirad.fr/578836/1/taiwan%20nov%202014%20ver2%20OK.pdf> Accessed on  
9 Feb. 26, 2017  
10  
11  
12  
13 79. Boateng AA, Garcia-Perez M, Masek O, Brown R, del Campo B: Chapter 4: Biochar  
14 production technology. In: Biochar for Environmental Management. Science, Technology,  
15 and implementation. Edited by Johannes Lehmann and Stephen Joseph. Second Edition  
16 2015, 63  
17  
18  
19  
20 80. International Biochar Initiative. Standardized Product Definition and Product Testing  
21 Guidelines for Biochar That Is Used in Soil. 2015 [http://www.biochar-](http://www.biochar-international.org/characterizationstandard)  
22 [international.org/characterizationstandard](http://www.biochar-international.org/characterizationstandard)  
23  
24  
25  
26 81. Oasmaa A, Fonts I, Pelaez-Samaniego MR, Garcia-Perez ME, Garcia-Perez M: Pyrolysis Oil  
27 Multiphase behavior and Phase Stability: A Review. *Energy & Fuels* 2016, 30, 6179-6200  
28  
29 82. Garcia-Perez M, Chaala A, Pakdel H, Kretschmer D, Roy C: Characterization of bio-oils in  
30 Chemical families. *Biomass and Bioenergy* 2007, 31, 222-242  
31  
32 83. Stankovikj F, Garcia-Perez M: TG-FTIR Method for the Characterization of Bio-oils in  
33 Chemical Families. *Energy and Fuels*, 2017, 31, 1689-1701.  
34  
35 84. Stankovikj F, McDonald A, Helms GL, Olarte MV, Garcia-Perez M: Characterization of the  
36 Water Soluble Fraction of Biomass Pyrolysis Oils. *Energy Fuels*, 31, 2017, 1650-1664  
37  
38 85. Stankovikj F, McDonald A, Helms GL, Garcia-Perez M: Quantification of Bio-oil Functional  
39 Groups and Evidence of the Presence of Pyrolytic Humins *Energy & Fuels*, 2016, 30, 6505-  
40 6524  
41  
42 86. Garcia-Perez M, Chaala A, Pakdel H, Kretschmer D, Rodrigue D, Roy C: Multiphase  
43 Structure of Bio-oils. *Energy & Fuels*, 2006, 20 (1), 364-375  
44  
45 87. Riuji Lohri C, Mtoro Rajabu H, Sweeney DJ, Zurbrugg C: Char fuel production in  
46 developing countries- A review of urban biowaste carbonization. *Renewable and*  
47 *Sustainable Energy Reviews*, 2016, 59, 1514-1530  
48  
49 88. FAO, Simple technologies for charcoal making, FAO Forestry paper 41, 1987. Retrieved  
50 November 20<sup>th</sup>, 2010, from: <http://www.fao.org/docrep/x5328e/x5328e00.htm#Contents>  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60



- 1  
2  
3  
4  
5 89. Seboka Y: Chapter 6. Charcoal Production: Opportunities and barriers for improving  
6 efficiency and sustainability. In: Bio-carbon opportunities in eastern & southern Africa.  
7 Harnessing Carbon, Finance to Promote Sustainable Forestry, agro-forestry and Bio-energy.  
8 UNDP 2009. [http://www.environmentportal.in/files/Bio-](http://www.environmentportal.in/files/Bio-carbon%20in%20Africa.pdf#page=113)  
9 [carbon%20in%20Africa.pdf#page=113](http://www.environmentportal.in/files/Bio-carbon%20in%20Africa.pdf#page=113)  
10  
11  
12  
13 90. Schenkel, Y., Bertaux, P., Vanwijnbergh, S., Carre, J., An evaluation of the mound kiln  
14 carbonization technique, *Biomass and Bioenergy*, 1998, 14, 5/6, 505-516.  
15  
16 91. Nahayo A, Ekise I, Mukarugwiza A: Comparative Study on Charcoal Yield Produced by  
17 Traditional and Improved kilns: A study of Nyaruguru and Nyamagabe Districts in Southern  
18 Province of Rwanda. *Energy and Environment Research*, 2013, 3, 1.  
19  
20 92. Menemencioglu K: Traditional wood charcoal production labor in Turkish forestry (Cankiri  
21 sample). *Journal of Food, Agriculture & Environment*, 2013, 11, 2, 1136-1142  
22  
23 93. De Oliveira Vilela A, Silva Lora E, Roman-Quintero Q, Antonio-Vicintin R, da Silva e  
24 Souza TP: A new Technology for the combined production of charcoal and electricity  
25 through cogeneration. *Biomass and Bioenergy*, 2014, 69, 222-240  
26  
27 94. Toole AW, Lane PH, Arbogast C, Smith WR, Peter R, Locke E, Beglinger E, Erickson  
28 E.C.O.: Char Production, Marketing and Use. Forest Products Laboratory, Madison  
29 Wisconsin. USDA-Forest Service, University of Wisconsin. Report 1961, July 1961.  
30  
31 95. Pelaez-Samaniego M.R., Garcia-Perez M, Cortez LB, Rosillo-Calle F, Mesa J: Improvements  
32 of Brazilian carbonization industry as part of the creation of a global biomass economy.  
33 *Renewable and Sustainable Energy Reviews*, 2008, 12 1063-1086.  
34  
35 96. Brito, J. O., Princípios de produção e utilização de carvão vegetal de madeira, Documentos  
36 florestais, Piracicaba (9): 1 –19, mai. 1990  
37  
38 97. Bustamante-Garcia V, Carrillo-Parra A, Gonzalez-Rodriguez H, Ramirez-Lozano RG,  
39 Corral-Rivas JJ, Garza-Ocanas F: Evaluation of a charcoal production process from forest  
40 residues of *Quercus sideroxyla* hum, & Bpnpl. In a Brazilian beehive kiln. *Industrial Crops*  
41 *and products*, 2013, 42, 169-174.  
42  
43 98. Yronwode, P., From the hills to the grills, *Missouri Resources Magazine*, Spring 2000  
44  
45 99. Lemieux, P. M., Emissions of Air Toxics from a Simulated Charcoal Kiln Equipped with an  
46 Afterburner (Project Summary), EPA, March 2001  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60



- 1  
2  
3  
4  
5 100. Braun S., Missouri Charcoal-Makers Agree to Clean Their Kilns, August 14 1997, Los  
6 Angeles Times, Retrieved January 27<sup>th</sup>, 2011, from:  
7 <http://articles.latimes.com/1997/aug/14/news/mn-22314>  
8  
9  
10 101. Campbell R.R., A revolution in the heartland: Changes in rural culture, family and  
11 communities 1900-2000, Columbia (MO), 2004, Retrieved January 27, 2011, from:  
12 <http://web.missouri.edu/~campbellr/Book/Chapter28.htm#E11>  
13  
14  
15 102. Fink, R. J., Fink, R. L., An assessment of biomass feedstock availability in Missouri, Final  
16 Report, Contract No. SEBSRP-SSEB-2004XX-KLP-001, April, 2005  
17  
18  
19 103. Sparrevik M, Adam C, Martinsen V, Jubaedah, Cornelissen G: Emissions of gases and  
20 particles from charcoal/biochar production in rural areas using medium-sized traditional and  
21 improved “retort” kilns. *Biomass and Bioenergy*, 2015, 72, 65-73  
22  
23  
24 104. Baldwin, H I., The New Hampshire charcoal kiln, Concord, New Hampshire, 1958.  
25  
26 105. VT, 2010, Design and instructions for making a New Hampshire-style metal charcoal kiln  
27 from readily-available materials, Adaptation of New Hampshire kilns, at:  
28 <http://www.forestry.vt.edu/charcoal/documents/kiln-design.pdf>  
29  
30  
31 106. Skok, R.A., Beazley, R., Small kiln charcoal production possibilities in Minnesota,  
32 Minnesota Forestry Notes, April 15, 1955  
33  
34  
35 107. Simmons, F. C., Charcoal from portable kilns and fixed installations, An international  
36 journal of forestry and forest industries, Vol. 17, 1963, Retrieved January 27<sup>th</sup>, 2011, from:  
37 <http://www.fao.org/docrep/00950e/00950e07.htm#TopOfPage>  
38  
39  
40 108. Adam+Partner, 2010, Accessed November 15<sup>th</sup>, 2010, from:  
41 <http://www.biocoal.org/index.html>  
42  
43  
44 109. Adam JC: Improved and more environmentally friendly charcoal production system using a  
45 low cost retort-kiln (Eco-charcoal). *Renewable Energy*, 2009, 34, 1923-1925  
46  
47  
48 110. Klavina K, Klavins J, Veidenbergs I, Blumberga D: Charcoal production in a continuous  
49 operation retort. Experimental data processing. *Energy Procedia*, 2016, 95, 208-215  
50  
51  
52 111. Szymkowski CJ, Bultitude-Paull JM: The Production of High quality Silicon Metal at  
53 Simcoa. INFACON 6, Proceedings of the 6<sup>th</sup> International Ferroalloys Congress, Cape  
54 Town, Volume 1. Johannesburg, SAIMM, 1992, 185-191.  
55  
56  
57  
58  
59  
60

- 1  
2  
3  
4  
5 112. Reumerman PJ, Frederiks B: Carbon Production with Reduced Emissions. 12<sup>th</sup> European  
6 Conference on Biomass for Energy, Industry and Climate Protection, Amsterdam, 2002,  
7 [http://www.cleanfuels.nl/Sitepdfs/Charcoal%20Production%20with%20Reduced%20Emissions%20\(paper\).pdf](http://www.cleanfuels.nl/Sitepdfs/Charcoal%20Production%20with%20Reduced%20Emissions%20(paper).pdf)  
8  
9  
10  
11  
12 113. Bates JS: Distillation of hardwoods in Canada. Forestry Branch-Bulletin # 74, Department  
13 of the Interior, Canada. 1922.  
14  
15 114. FAO, Industrial Technologies for Charcoal Making, FAO Forestry paper 63, 1985.  
16 Available at: <http://www.fao.org/docrep/x5555e/x5555e00.htm#Contents>  
17  
18 115. Siemons R. Industrial Charcoal production, 2008, FAO TCP/CRO/3101 (A) Development  
19 of a sustainable Charcoal industry.  
20  
21  
22 116. Mura E, Debono O, Villot A, Paviet F: Pyrolysis of biomass in a semi-industrial scale  
23 reactor: Study of the fuel-nitrogen oxidation during combustion of volatiles. *Biomass and*  
24 *Bioenergy*, 2013, 59, 187-194  
25  
26  
27 117. Pakdel H, Roy C: Chemical Characterization of Wood Pyrolysis oils obtained in a Vacuum-  
28 Pyrolysis Multiple-Hearth Reactor. In: ACS Symposium Series, Vol. 376, Pyrolysis Oils  
29 from Biomass. Chapter 19, 1988, 203-219  
30  
31  
32 118. Lemieux R, Roy C, de Caumia B, Blanchette D: Preliminary Engineering Data for Scale up  
33 of a Biomass vacuum pyrolysis reactor. ACS Division of Fuel Chemistry, Reprints, 1987,  
34 32, 2, 12-20.  
35  
36  
37 119. Malkow, T., Novel and innovative pyrolysis and gasification technologies for energy  
38 efficient and environmentally sound MSW disposal, *Waste Management*, 2004, 24, 53–79  
39  
40 120. Fukushima, M., Wu, B., Ibe, H., Wakai, K., Sugiyama, E., Abe, H., Kitagawa, K., et al.,  
41 Study on dechlorination technology for municipal waste plastics containing polyvinyl  
42 chloride and polyethylene terephthalate, *J Mater Cycles Waste Manag*, 2010, 12, 108–122.  
43  
44  
45 121. Coates R.L., Eddings E.G., Coates B.R. Bio-oil yields from pyrolysis in a novel rotary  
46 reactor. Symposium on Thermal and Catalytic Sciences for Biofuels and Biobased Products.  
47 Iowa State University, September 21-23, 2010  
48  
49 122. Coates R, Gardner T, Eddings E: Mobile Pyrolysis Process for Conversion of Biomass Into  
50 Energy products. Presentation at the 2013 North American Biochar Symposium, October  
51 13-16, 2013. <file:///C:/Users/mgarcia-perez/Downloads/F&P%20Amaron%20Energy.pdf>  
52  
53  
54  
55  
56  
57  
58  
59  
60

- 1  
2  
3  
4  
5 123. Sangines P, Dominguez MP, Sznchez F, San Miguel G. Slow pyrolysis of olive stones in a  
6 rotary kiln: Chemical and energy characterization of solid, gas, and condensable products.  
7 *Journal of Renewable and Sustainable Energy*, 2015;7,4, 043103.  
8  
9  
10 124. Brown, J.N., Brown, R.C.. Process optimization of an auger pyrolyzer with heat carrier  
11 using response surface methodology. *Bio resource Technology*, 2012, 103, 405-414  
12  
13 125. Ingram L, Mohan D, Bricka M, Steele P, Strobel D, Crocker D, et al. Pyrolysis of wood and  
14 bark in an auger reactor: Physical properties and chemical analysis of the produced bio-oils.  
15 *Energy&Fuels*, 2008;22, 1, 614-625.  
16  
17 126. Puy N, Murillo R, Navarro MV, López JM, Rieradevall J, Fowler G, et al. Valorisation of  
18 forestry waste by pyrolysis in an auger reactor. *Waste Management* 2011;31, 6, 1339.  
19  
20 127. Gajjela SK, Mitchell B, Li Q, Hassan EBM, Steele PH. Production of bio-fuels from giant  
21 miscanthus. 11AIChE - 2011 AIChE Spring Meeting and 7th Global Congress on Process  
22 Safety, Conference Proceedings; 2011  
23  
24 128. Wang H, Srinivasan R, Yu F, Steele P, Li Q, Mitchell B. Effect of acid, alkali, and steam  
25 explosion pretreatments on characteristics of bio-oil produced from pinewood. *Energy&*  
26 *Fuels*, 2011, 25, 8, 3758.  
27  
28 129. Joubert JE, Carrier M, Dahmen N, Stahl R, Knoetze JH. Inherent process variations  
29 between fast pyrolysis technologies: A case study on Eucalyptus grandis. *Fuel Processing*  
30 *Technology* 2015, 131, 389.  
31  
32 130. Wang H, Srinivasan R, Yu F, Steele P, Li Q, Mitchell B, et al. Effect of Acid, Steam  
33 Explosion, and Size Reduction Pretreatments on Bio-oil Production from Sweetgum,  
34 Switchgrass, and Corn Stover. *Applied Biochemistry and Biotechnology*, 2012;167, 2, 285-  
35 297.  
36  
37 131. Nam H, Capareda SC, Ashwath N, Kongkasawan J. Experimental investigation of pyrolysis  
38 of rice straw using bench-scale auger, batch and fluidized bed reactors. *Energy* 2015, 93,  
39 2384-2394.  
40  
41 132. Pfitzer C, Dahmen N, Troger N, Weirich F, Sauer J, Gunther A, et al. Fast Pyrolysis of  
42 Wheat Straw in the Bioliq Pilot Plant. *Energy & Fuels*, 2016;30, 10, 8047-8054.  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

- 1  
2  
3  
4  
5  
6  
7  
8  
9  
10  
11  
12  
13  
14  
15  
16  
17  
18  
19  
20  
21  
22  
23  
24  
25  
26  
27  
28  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60
133. Henrich E, Dahmen N, Weirich F, Reimert R, Kornmayer C. Fast pyrolysis of lignocellulosics in a twin screw mixer reactor. *Fuel Processing Technology*, 2016;143, 151-161.
134. Roy C., Blanchette D., korving L., Yang J., de Caumia B., Development of a Novel Vacuum Pyrolysis Reactor with improved heat transfer Potential. In: Developments in: Thermochemical Biomass Conversion. A.V. Bridgwater and D.G.B. Boocock, Eds., Blackie Academic and Professional, London, UK, 1997, 351-367.
135. Roy C., Lemieux S., de Caumia B., Pakdel H., Vacuum Pyrolysis of Biomass in a Multiple Heat Furnace. *Biotechnology and Bioenergy*, Sym. No 15, 1985, 107.
136. Venderbosch RH, Prins W., Fast Pyrolysis technology development. *Biofuels, Bio-products and Biorefining*, 2010, 4, 178-208
137. Tsai WT, Lee MK, Chang YM. Fast pyrolysis of rice husk: Product yields and compositions. *Bioresource Technology*, 2007;98, 1,:22.
138. Imam T, Capareda S. Characterization of bio-oil, syn-gas and char from switchgrass pyrolysis at various temperatures. *J. Anal. Appl. Pyrolysis* 2012;93, 170.
139. Fan Y, Cai Y, Li X, Yin H, Yu N, Zhang R, et al. Rape straw as a source of bio-oil via vacuum pyrolysis: Optimization of bio-oil yield using orthogonal design method and characterization of bio-oil. *J. Anal. Appl. Pyrolysis*, 2014;106, 63.
140. Dewayanto N, Isha R, Nordin MR. Use of palm oil decanter cake as a new substrate for the production of bio-oil by vacuum pyrolysis. *Energy Conversion and Management* 2014, 86, 226.
141. Fukuda S. Pyrolysis investigation for bio-oil production from various biomass feedstocks in Thailand. *International Journal of Green Energy*, 2015, 12, 3, 215.
142. Le Brech Y, Jia L, Cissé S, Mauviel G, Brosse N, Dufour A. Mechanisms of biomass pyrolysis studied by combining a fixed bed reactor with advanced gas analysis. *J. Anal. Appl. Pyrolysis*, 2016, 117, 334.
143. Xu Y, Wang T, Ma L, Zhang Q, Chen G. Technology of bio-oil preparation by vacuum pyrolysis of pine straw. *Nongye Gongcheng Xuebao/Transactions of the Chinese Society of Agricultural Engineering*, 2013, 29, 1, 196.

- 1  
2  
3  
4  
5 144. Fan YS, Cai YX, Li XH, Yu N, Chen L. Comparison of the products in vacuum pyrolysis  
6 vapors derived from non-catalytic and catalytic upgrading of camphorwood sawdust.  
7 *Chemistry and Industry of Forest Products*, 2015, 35, 1, 70.  
8  
9  
10 145. Li R., Deng X. S., Gou J. S., Lv Z. L.: Vacuum Paddle Fast Pyrolysis Reactor Design and  
11 Internal Heat Transfer Investigation, *Materials Science Forum*, 2012, Vols. 704-705, 468-  
12 474  
13  
14  
15 146. Rudloff M. Biomass to Liquid Fuels (BtL) Presentation made by Choren. Process,  
16 Environmental Impact and Latest Developments. Automobile & Environment at Beograd  
17 Congress, May 2005.  
18  
19  
20 147. Meier D, Faix O: State of the art of applied fast pyrolysis of lignocellulosic materials—a  
21 review. *Bioresour Technol* 1999, 68, 71–77.  
22  
23  
24 148. Scott, D., Majerski, P., Piskorz, J., Radlein, D., A second look at fast pyrolysis of biomass—  
25 the RTI process, *J. Anal. Appl. Pyrolysis*, 1999, 51, 23–37  
26  
27  
28 149. DynaMotive Energy \_ Systems Corporation, BioTherm™, A System for Continuous  
29 Quality, Fast Pyrolysis BioOil, Fourth Biomass Conference of the Americas, Oakland,  
30 California, September 1, 1999  
31  
32  
33 150. Lu Q, Yang X-l, Zhu X-f. Analysis on chemical and physical properties of bio-oil pyrolyzed  
34 from rice husk. *J. Anal. Appl. Pyrolysis*, 2008;82, 2, 191.  
35  
36  
37 151. Heo HS, Park HJ, Dong J-I, Park SH, Kim S, Suh DJ, et al. Fast pyrolysis of rice husk  
38 under different reaction conditions. *Journal of Industrial and Engineering Chemistry*,  
39 2010;16, 1, 27  
40  
41  
42 152. Ji-lu Z. Bio-oil from fast pyrolysis of rice husk: Yields and related properties and  
43 improvement of the pyrolysis system. *J. Anal. Appl. Pyrolysis*, 2007;80, 1, 30.  
44  
45  
46 153. Phan BMQ, Duong LT, Nguyen VD, Tran TB, Nguyen MHH, Nguyen LH, et al.  
47 Evaluation of the production potential of bio-oil from Vietnamese biomass resources by fast  
48 pyrolysis. *Biomass and Bioenergy*, 2014;62, 74.  
49  
50  
51 154. Montoya JL, Valdes C, Chejne F, Gomez CA, Blanco A, Marrugo G, Osorio J, Castillo E,  
52 Aristobulo J, Acero J: Bio-oil production from Colombian bagasse by fast pyrolysis in a  
53 fluidized bed: An experimental study. *J. Anal. Appl. Pyrolysis*, 2015, 112, 379-387  
54  
55  
56  
57  
58  
59  
60

- 1  
2  
3  
4  
5 155. Oasmaa A, Solantausta Y, Arpiainen V, Kuoppala E, Sipilä K. Fast pyrolysis bio-oils from  
6 wood and agricultural residues. *Energy & Fuels*, 2010; 24, 2, 1380.  
7  
8  
9 156. Greenhalf CE, Nowakowski DJ, Harms AB, Titiloye JO, Bridgwater AV. A comparative  
10 study of straw, perennial grasses and hardwoods in terms of fast pyrolysis products. *Fuel*,  
11 2013;108, 216.  
12  
13 157. Boateng, A.A., Daugaard, D.E., Goldberg, N.M., Hicks, K.B., Bench-Scale Fluidized-Bed  
14 Pyrolysis of Switchgrass for Bio-Oil Production. *Ind. Eng. Chem. Res.* 2007, 46, 1891-1897  
15  
16 158. Jendoubi N, Broust F, Commandre JM, Mauviel G, Sardin M, Lédé J. Inorganics  
17 distribution in bio oils and char produced by biomass fast pyrolysis: The key role of  
18 aerosols. *J. Anal. Appl. Pyrolysis*, 2011;92, 1, 59.  
19  
20 159. Westerhof RJM, Brilman DWF, van Swaaij WPM, Kersten SRA: Effect of temperature in  
21 fluidized bed fast pyrolysis of biomass: oil quality assessment in tests units. *Ind. Eng. Chem*  
22 *Res*, 2010, 49, 1160-1168  
23  
24 160. Kim KH, Kim T-S, Lee S-M, Choi D, Yeo H, Choi I-G, et al. Comparison of  
25 physicochemical features of biooils and biochars produced from various woody biomasses  
26 by fast pyrolysis. *Renewable Energy* 2013;50, 188.  
27  
28 161. Soysa R, Choi SK, Jeong YW, Kim SJ, Choi YS. Pyrolysis of Douglas fir and coffee  
29 ground and product biocrude-oil characteristics. *J. Anal. Appl. Pyrolysis*, 2015;115, 51.  
30  
31 162. Wu S-R, Chang C-C, Chang Y-H, Wan H-P. Comparison of oil-tea shell and Douglas-fir  
32 sawdust for the production of bio-oils and chars in a fluidized-bed fast pyrolysis system.  
33 *Fuel*, 2016;175, 57.  
34  
35 163. Azeez AM, Meier D, Odermatt J, Willner T. Fast pyrolysis of African and European  
36 lignocellulosic biomasses using Py-GC/MS and fluidized bed reactor. *Energy&Fuels*  
37 2010;24, 3, 2078.  
38  
39 164. Rover MR, Johnston PA, Whitmer LE, Smith RG, Brown RC. The effect of pyrolysis  
40 temperature on recovery of bio-oil as distinctive stage fractions. *J. Anal. Appl. Pyrolysis*  
41 2014;105, 262.  
42  
43 165. Mullen CA, Boateng AA, Goldberg NM. Production of deoxygenated biomass fast  
44 pyrolysis oils via product gas recycling. *Energy&Fuels*, 2013;27, 7, 3867.  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

- 1  
2  
3  
4  
5 166. Torri IDV, Paasikallio V, Faccini CS, Huff R, Caramão EB, Sacon V, et al. Bio-oil  
6 production of softwood and hardwood forest industry residues through fast and intermediate  
7 pyrolysis and its chromatographic characterization. *Bioresource Technology*, 2016;200, 680.  
8  
9  
10 167. Carrier M, Joubert JE, Danje S, Hugo T, Görgens J, Knoetze JH. Impact of the  
11 lignocellulosic material on fast pyrolysis yields and product quality. *Bioresource*  
12 *Technology*, 2013;150, 129.  
13  
14  
15 168. He M, Mourant D, Gunawan R, Lievens C, Wang XS, Ling K, et al. Yield and properties of  
16 bio-oil from the pyrolysis of mallee leaves in a fluidised-bed reactor. *Fuel*, 2012;102, 506.  
17  
18 169. Chang S, Zhao Z, Zheng A, Li X, Wang X, Huang Z, et al. Effect of hydrothermal  
19 pretreatment on properties of bio-oil produced from fast pyrolysis of eucalyptus wood in a  
20 fluidized bed reactor. *Bioresource Technology*, 2013;138, 321.  
21  
22  
23 170. Heidari A, Stahl R, Younesi H, Rashidi A, Troeger N, Ghoreyshi AA. Effect of process  
24 conditions on product yield and composition of fast pyrolysis of *Eucalyptus grandis* in  
25 fluidized bed reactor. *Journal of Industrial and Engineering Chemistry*, 2014;20, 4,2594.  
26  
27  
28 171. Atsonios K, Panopoulos KD, Bridgwater AV, Kakaras E. Biomass fast pyrolysis energy  
29 balance of a 1kg/h test rig. *International Journal of Thermodynamics*, 2015;18, 4, 267.  
30  
31  
32 172. Mesa-Pérez JM, Cortez LAB, Marín-Mesa HR, Rocha JD, Pelaez-Samaniego MR,  
33 Cascarosa E. A statistical analysis of the auto thermal fast pyrolysis of elephant grass in  
34 fluidized bed reactor based on produced charcoal. *Applied Thermal Engineering*, 2014, 65,  
35 1-2, 322–329.  
36  
37  
38 173. Faix, A., Schweinle, J., Schöll, S., Becker, G., Meier, D., (GTI-tcbiomass) Life-Cycle  
39 Assessment of the BTO\_-Process (Biomass-to-Oil) with Combined Heat and Power  
40 Generation, *Environmental Progress & Sustainable Energy*, 29, 2, 2010.  
41  
42  
43 174. Meier, D., Schöll, S., Klaubert, H., Markgraf, J., (n.d.), Practical results from Pytec's  
44 biomass to-oil (BTO) process with ablative pyrolyser and diesel CHP plant, Success &  
45 Visions for Bioenergy, [http://www.pytecsite.de/pytec\\_eng/publikationen.htm](http://www.pytecsite.de/pytec_eng/publikationen.htm)  
46  
47  
48 175. Bridgwater AV, Meier D, Radlein D: An overview of fast pyrolysis of biomass. *Organic*  
49 *Geochemistry*, 30, 1999, 1479-1493.  
50  
51  
52 176. Schulzke T, Conrad S, Westermeyer J. Fractionation of flash pyrolysis condensates by  
53 staged condensation. *Biomass and Bioenergy*, 2016, 95, 287-295  
54  
55  
56  
57  
58  
59  
60

- 1  
2  
3  
4  
5 177. Bech N, Larsen MB, Jensen PA, Dam-Johansen K. Modelling solid-convective flash  
6 pyrolysis of straw and wood in the Pyrolysis Centrifuge Reactor. *Biomass and Bioenergy*,  
7 2009; 33, 6–7, 999.  
8  
9  
10 178. Makibar J, Fernandez-Akarregi AR, Amutio M, Lopez G, Olazar M. Performance of a  
11 conical spouted bed pilot plant for bio-oil production by poplar flash pyrolysis. *Fuel*  
12 *Processing Technology*, 2015;137, 283.  
13  
14  
15 179. Alvarez J, Lopez G, Amutio M, Bilbao J, Olazar M. Bio-oil production from rice husk fast  
16 pyrolysis in a conical spouted bed reactor. *Fuel*, 2014;128, 162.  
17  
18  
19 180. Amutio M, Lopez G, Alvarez J, Moreira R, Duarte G, Nunes J, et al. Flash pyrolysis of  
20 forestry residues from the Portuguese Central Inland Region within the framework of the  
21 BioREFINA-Ter project. *Bioresource Technology*, 2013;129, 512.  
22  
23  
24 181. Du S, Sun Y, Gamliel DP, Valla JA, Bollas GM. Catalytic pyrolysis of miscanthus ×  
25 giganteus in a spouted bed reactor. *Bioresource Technology*, 2014;169, 188.  
26  
27  
28 182. Amutio M, Lopez G, Artetxe M, Elordi G, Olazar M, Bilbao J. Influence of temperature on  
29 biomass pyrolysis in a conical spouted bed reactor. *Resources, Conservation and Recycling*  
30 2012;59, 23.  
31  
32  
33 183. Chen M, Yao Y, Ren Z, Li T, Guo X, Yan Y. Preparation of liquid fuel through pyrolysis of  
34 biomass in a conduit-spouting fluidized reactor. Proceedings of the 2003 5th International  
35 Symposium on Coal Combustion; 2003, 272.  
36  
37  
38 184. Amutio M, Lopez G, Alvarez J, Olazar M, Bilbao J. Fast pyrolysis of eucalyptus waste in a  
39 conical spouted bed reactor. *Bioresource Technology*, 2015; 194, 225.  
40  
41  
42 185. Lam SS, Chase HA: A review on Waste to Energy Processes using Microwave Pyrolysis.  
43 *Energies*, 2012, 5, 4209-4232  
44  
45 186. Li J, Dai J, Liu G, Zhang H, Gao Z, Fu J, He Y, Huang Y: Biochar from microwave  
46 pyrolysis of biomass: A review. *Biomass and Bioenergy*, 94 (2016), 228-244  
47  
48  
49 187. Holland KM, Apparatus for Waste Pyrolysis, US Patent 5,387,321, 7 February 1995  
50  
51 188. Holland KM, Process for Destructive Distillation of Organic Materials. U.S. Patent  
52 5,330,623, May 1994  
53  
54 189. Zhao X, Wang M, Liu H, Li L, Ma C, Song Z: A microwave reactor for characterization  
55 of pyrolyzed biomass. *Bioresource Technology*, 2012, 104, 673-678  
56  
57  
58  
59  
60



- 1  
2  
3  
4  
5 190. Miura M, Kaga H, Sakurai A, Kakuchi T, Rapid pyrolysis of woof block by microwave  
6 heating. *J. Analytical and applied Pyrolysis*. 71, 2004, 187-199  
7  
8 191. Hu Z, Ma X, Chen C. A study on experimental characteristic of microwave assisted  
9 pyrolysis of microalgae. *Bioresource Technology*, 2012, 107, 487-493  
10  
11 192. Ren S, Lei H, Wang L, Bu Q, Chen S, Wu J, et al. Biofuel production and kinetics analysis  
12 for microwave pyrolysis of Douglas fir sawdust pellet. *Journal of Analytical and Applied*  
13 *Pyrolysis* 2012; 94: 163–169  
14  
15 193. Tian Y, Zuo W, Ren Z, Chen D. Estimation of a novel method to produce biooil from  
16 sewage sludge by microwave pyrolysis with the consideration of efficiency and safety.  
17 *Bioresource Technology* 2011;102:2053–61  
18  
19 194. Huang YF, Kuan WH, Lo SL, Lin CF. Hydrogen-rich fuel gas from rice straw via  
20 microwave-induced pyrolysis. *Bioresource Technology* 2010;101: 1968–73  
21  
22 195. Salema AA, Ani FN. Microwave induced pyrolysis of oil palm biomass. *Bioresource*  
23 *Technology* 2011;102: 3388–3395.  
24  
25 196. Du Z, Li Y, Wang X, Wan Y, Chen Q, Wang C, et al. Microwave-assisted pyrolysis of  
26 microalgae for biofuel production. *Bioresource Technology* 2011;102: 4890–4896  
27  
28 197. Lin Q, Chen G, Liu Y. Scale-up of microwave heating process for the production of bio-oil  
29 from sewage sludge. *Journal of Analytical and Applied Pyrolysis* 2012;94: 114–119.  
30  
31 198. Huang YF, Kuan WH, Lo SL, Lin CF. Total recovery of resources and energy from rice  
32 straw using microwave-induced pyrolysis. *Bioresource Technology* 2008; 99: 8252–8258  
33  
34 199. Salema AA, Ani FN. Microwave-assisted pyrolysis of oil palm shell biomass using an  
35 overhead stirrer. *Journal of Analytical and Applied Pyrolysis* 2012; 96: 162–72  
36  
37 200. Yu F, Ruan R, Steele P. Microwave pyrolysis of corn stover. *Transactions of the American*  
38 *Society of Agricultural and Biological Engineers* 2009; 52: 1595–601  
39  
40 201. Wang MJ, Huang YF, Chiueh PT, Kuan WH, Lo SL. Microwave-induced torrefaction of  
41 rice husk and sugarcane residues. *Energy* 2012; 37: 177–84  
42  
43 202. Mesa-Perez JM, Fonseca-Felfli: Chapter 9: Technical and Marketing Criteria for the  
44 Development of Fast Pyrolysis technologies. In: *Innovative Solutions and Fluid-Particle*  
45 *Systems and Renewable energy Management*. Editor: Katia Tannous (Unicamp Brazil),  
46 **2015**

- 1  
2  
3  
4  
5 203. Garcia-Perez M, Garcia-Nunez JA, Pelaez-Samaniego MR, Kruger C, Fuchs MR, Flora G:  
6 Sustainability, Chapter 10. Business Models and Techno-economic Analysis of Biomass  
7 Pyrolysis Technologies. In: Innovative Solutions and Fluid-Particle Systems and Renewable  
8 energy Management. Editor: Katia Tannous (Unicamp Brazil), **2015**  
9  
10  
11 204. Jones SB, Valkenburg C, Walton C, Elliott DC, Holladay JE, Stevens DJ, Kinchin C,  
12 Czernik S: Production of gasoline and Diesel from biomass via fast pyrolysis, hydrotreating  
13 and hydrocracking: A design case. Prepared for the U.S. Department of Energy under  
14 Contract DE-AC05-76RL01830. PNNL-18284 Rev. 1, June 2009  
15  
16  
17 205. Daugaard DE, Brown RC: Enthalpy of pyrolysis for several types of biomass. *Energy &*  
18 *Fuels*, 2003, 17, 934-939  
19  
20  
21 206. Catoire L, Yahyaouo M, Osmont A, Gokalp I: Thermochemistry of Compounds Formed  
22 during Fast Pyrolysis of Lignocellulosic Biomass. *Energy & Fuels* 2008, 22, 4265-4273  
23  
24  
25 207. Auber M: Effect catalytique de certains inorganiques sur la selectivite des reactions de  
26 pyrolyse rapide de biomasses et de leurs constituants. PhD thesis. Institut National  
27 Polytechnique de Lorraine. 2009  
28  
29  
30 208. Yang H, Kudo S, Huo H-P, Norinaga K, Mori A, Masek O, Hayashi J-I: Estimation of  
31 Enthalpy of Bio-oil Vapor and Heat Required for Pyrolysis of Biomass. *Energy & Fuels*  
32 2013, 27, 2675-2686  
33  
34  
35 209. Janse AMC, Westerhout RWJ, Prins W: Modelling of fast pyrolysis of a single wood  
36 particle. *Chemical Engineering and Processing* 39 (2000), 239-252  
37  
38  
39 210. Wang X, Kersten S.R.A., Prins W, van Swaaij W.P.M: Biomass Pyrolysis in a Fluidized  
40 Bed Reactor. Part 2: Experimental Validation of Model Results. *Ind. Eng. Chem. Res.* 2005,  
41 44, 8786-8795  
42  
43  
44 211. Thunman H, Lecker B: Thermal conductivity of wood-models for different stages of  
45 combustion. *Biomass and Bioenergy* 23 (2002) 47-54  
46  
47  
48 212. Boateng AA: Rotary Kilns. *Transport Phenomena and Transport Processes*. Butterworth-  
49 Heinemann, 2008  
50  
51  
52 213. Basu P: *Combustion and Gasification in Fluidized beds*. Taylor & Francis. 2006.  
53  
54  
55 214. Zhong W, Jin B, Wang X, Xiao R: Fluidization of Biomass Particles in a Gas-Solid Fluid  
56 Bed. *Energy & Fuel* 2008, 22 (6), 4170-4176  
57  
58  
59  
60

- 1  
2  
3  
4  
5 215. Bruni G, Solimene R, Marzocchella A, Salatino P, Yates JG, Lettieri P, Fiorentino M: Self-  
6 segregation of high-volatile fuel particle devolatilization in a fluidized bed reactor. *Powder*  
7 *Technology* 128 (2002) 11-21  
8  
9  
10 216. Yoder J, Galinato S, Granatstein D, Garcia-Perez M: Economic treadoff between biochar  
11 and bio-oil production via pyrolysis. *Biomass and Bioenergy*, 2011, 35, 5, 1851-1862  
12  
13 217. Bailis R: Modeling climate change mitigation from alternative methods of charcoal  
14 production in Kenya. *Biomass and Bioenergy*, 2009, 33, 11, 1491-1502  
15  
16  
17 218. Ronsse F, Nachenius R, Prins W: Carbonization of Biomass. In: Recent advances in  
18 thermochemical conversion of biomass. Edited by: Pandey A, Bashkar T, Stocker M,  
19 Sukumaran R, 2015, 293-324  
20  
21  
22 219. Siemons, R., Baaijens, L. An Innovative Carbonisation Retort: Technology and  
23 Environmental Impact. *Termotehnika*, 2012, 38, 2, 131-138.  
24  
25  
26 220. Jahanshaki S, Mathieson JG, Somerville MA, Haque N, Norgate TE, Deev A, Pan Y, Xie  
27 D, Ridgeway P, Zulli P: Development of low-emission Integrated Steelmaking Process.  
28 *Journal of Sustainable Metallurgy*, 2015, 1, 1, 94-114  
29  
30  
31 221. N. Dahmen, E. Dinjus, E. Heinrich, The Karlsruhe Process bioliq®: Synthetic Fuels from  
32 the Biomass. In: Renewable Energy: Sustainable Energy Concepts for the Future, R.  
33 Wengenmayr (Editor), T. Buhrke (Editor). Wiley, 2008. ISBN: 978-3-527-40804-7  
34  
35  
36 222. Jager N, Conti R, Neumann J, Apfelbacher A, Daschner R, Binder S, Hornung A: Thermo-  
37 Catalytic Reforming of Wood Biomass. *Energy&Fuels*, 2016, 30, 10, 7923-7929  
38  
39  
40 223. Moriconi N, Laranci P, D'Amico M, Bartocci P, D'Alessandro B, Cinto G, Baldinelli A,  
41 Discepoli G, Bidini G, Desideri U, Cotana F, Fantozzi F: Design and preliminary operation  
42 of a Gasification Plant for Micro-CHP with Internal Combustion engine and SOFC. *Energy*  
43 *Procedia*, Vol. 81, 2015, 298-308, 69<sup>th</sup> Conference of the Italian Thermal Engineering  
44 Association, ATI 2014.  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60

Graphical abstract

