

Quantification of the interfacial and bulk contributions to the longitudinal spin Seebeck effect

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(Dated: 12 February 2021)

We report the disentanglement of bulk and interfacial contributions to the thermally excited magnon spin current in the spin Seebeck effect under static heating. For this purpose, we have studied the dependence of the inverse Spin Hall voltage and the thermal conductivity on the magnetic layer thickness. Knowledge of these quantities allows us to take into account the influence of both sources of thermal spin current in the analysis of the voltage dependence. The magnetic layer thickness modulates the relative magnitude of the involved thermal drops for a fixed total thermal difference throughout the sample. In the end, we attain the separate contributions of both sources of thermal spin current—bulk and interfacial—and obtain the value of the thermal magnon accumulation length scale in maghemite, which we find to be 29(1) nm. According to our results, bulk magnon accumulation dominates the spin Seebeck effect in our studied range of thicknesses, but the interfacial component is by no means negligible.

PACS numbers: 72.15.Jf, 72.25.b, 81.15.-z

The spin Seebeck effect (SSE) is a complex phenomenon that lies at the intersection between several spintronics subfields. It is defined as the generation of a spin current in a magnetic material (FM) subjected to a thermal gradient, standing as one of the major spin-caloritronics topics¹. However, the detection of the SSE makes use of tools from spin-orbitronics, since it is commonly achieved by spin current to charge current conversion by means of the inverse spin Hall effect (ISHE) observed in a nonmagnetic heavy metal (NM) adjacent to the magnetic material (FM)². Furthermore, these thermal spin currents have been proved to be of magnonic origin, which means that magnonics are also involved in SSE^{3,4}. This complexity affects both theoretical and experimental aspects and is evidenced, e.g., by the difficulties found in the definition of a standard SSE coefficient^{5,6}.

Part of this intricacy comes from the fact that there are different physical mechanisms contributing to the SSE⁷. Two main theories have been developed so far which describe two different sources for a magnon spin current in a FM/NM system subjected to a thermal gradient. The first one points to the temperature difference between the metal electrons and the magnetic magnons at the interface, such that the excited spin current is given by^{4,8}:

$$J_s^i \propto \Delta T_i^{\text{NM/FM}}, \quad (1)$$

where $\Delta T_i^{\text{NM/FM}}$ denotes the interfacial thermal drop.

The second origin of the thermal spin current lies on the thermal gradient present in the bulk of the FM layer itself,

rather than the temperature difference at the interface^{9–12}. This gradient creates a magnon accumulation which acts as a spin potential for the spin current. In this case, the spin current is determined by a finite magnon propagation length scale (Λ_m) and follows the expression^{10,12}:

$$J_s^b \propto \frac{\cosh(t_{\text{FM}}/\Lambda_m) - 1}{\sinh(t_{\text{FM}}/\Lambda_m)} \nabla T_{\text{FM}}, \quad (2)$$

where ∇T_{FM} is the temperature gradient across the FM layer and t_{FM} denotes its thickness.

We emphasize that both mechanisms arise in the presence of a thermal gradient and thus meet the definition of the SSE, but they actually represent different physical sources for thermally excited magnon spin currents.

Nowadays the longitudinal spin Seebeck effect (LSSE) is widely used because of experimental simplicity, and most theoretical efforts have focused on it¹³. In the LSSE an out-of-plane thermal gradient is applied perpendicularly to a magnetic field. The excited spin current is parallel to the thermal gradient and according to the ISHE phenomenology, the generated voltage can be measured in the transverse direction (perpendicular to both thermal gradient and magnetic field).

Whilst time-resolved optical approaches of SSE measurements have been able to selectively excite only interfacial LSSE (*i*LSSE)^{14,15} and the *b*LSSE has been unambiguously detected using a magnon-valve structure¹⁶, the relative contributions in a standard DC measurement in which the whole sample is subjected to a thermal gradient have not been addressed. In these conditions, both thermal spin current sources coexist and contribute to the signal. Notwithstanding, in most of previous works one of the existing models is chosen, as-

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suming that only one of the mechanisms is present or relevant. Therefore, a relative quantification of both contributions is still lacking. This is however an important issue, required for a deeper understanding of the LSSE. In addition, it is also desirable from a practical point of view as it will give hints concerning the design of materials and devices to be used in potential applications.

In this work, we disentangle the contributions of *i*LSSE and *b*LSSE (bulk LSSE) within a static SSE experiment. We make use of following definitions for the corresponding coefficients (S^i and S^b):

$$S^i = \frac{\Delta V_{\text{ISHE}}^i}{d_y \Delta T^{\text{NM/FM}}} \quad \text{and} \quad S^b = \frac{\Delta V_{\text{ISHE}}^b}{d_y \Delta T_{\text{FM}}}, \quad (3)$$

where d_y is the distance between the transverse contacts to measure the transverse ISHE voltage (ΔV_{ISHE}). These definitions make use of the actual temperature difference driving each effect, rather than the overall temperature difference. This normalization is favored by the SSE measurement method known as heat flux method^{6,17,18}, which measures the heat current flowing through the sample instead of the total temperature difference (used in the temperature difference method).

Our approach to the quantification of *i*LSSE and *b*LSSE contributions is based on the study of the LSSE as a function of t_{FM} . Under a fixed total thermal difference across the whole sample ΔT (typical experimental condition in LSSE static experiments), the thermal drops across the FM layer thickness and at the NM/FM interface change upon changing t_{FM} . Consequently, J_s^b and J_s^i change accordingly, since they are driven by those thermal differences (recall Eqs. 1 and 2). However, this issue has been omitted in previous studies on the t_{FM} dependence of LSSE employing the temperature difference approach, although it represents a source of modulation of the contribution of both LSSE mechanisms. Typically, only the dependence related to the Λ_m (prefactor in equation 2) is addressed, whereas the influence of t_{FM} in the temperature drop in FM, ΔT_{FM} , has not been considered so far. To evaluate this, knowledge on the cross-plane thermal conductivities is needed to quantify the gradients. Therefore, a key point in our work is the assessment of the thermal conductivities for thin films of different thicknesses. An alternative to circumvent the thickness variation of ΔT_{FM} is offered by the heat flux method¹⁹. However, to separate the contributions to the LSSE, knowledge of the thermal conductivities is necessary.

In sum, in a typical experiment of LSSE as a function of t_{FM} in which ΔT is fixed to the same value for all t_{FM} , we consider the modulation of the thermally excited spin current J_s by three different means: (1) the existence of a magnon propagation length scale Λ_m comparable to the dimensions of our samples, (2) the change of the involved thermal drops due to the variation of the FM layer thickness in relation to the rest of the stacked layers, and (3) the dependence of the thermal conductivity of the FM layer on its thickness.

The studied samples consisted of epitaxial thin films of insulating ferrimagnetic $\gamma\text{-Fe}_2\text{O}_3$ (maghemite) deposited on (001) oriented MgO substrates of 0.5 mm of thickness, and an additional layer of Pt on top of maghemite for spin-to-charge

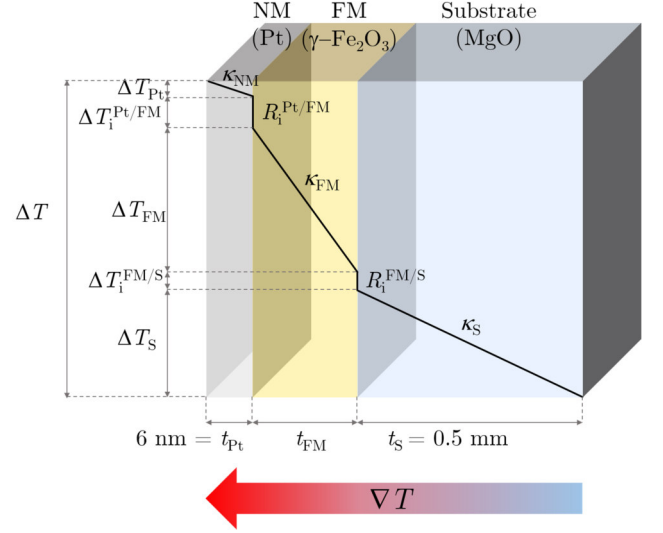


FIG. 1. Depiction of the thermal differences established in the LSSE experiment through the studied sample, as expressed in Eq. 4. The graded arrow shows the direction of the thermal gradient.

current conversion. The thickness of the Pt layer is held at 6 nm through all studied samples. Maghemite is an ideal material to study LSSE because of its insulating behavior ruling Anomalous Nernst Effect contribution to the voltage^{20–22}. However, proximity magnetism induced in the Pt layer by interdiffusion of Fe may originate an ANE contribution. To avoid this effect, Pt was deposited at room temperature^{23,24}. Details about the fabrication of the samples can be found elsewhere, along with the description of the experimental setup for the LSSE measurements²⁵. Moreover, the quality of interfaces affects the magnitude of the LSSE²⁶; therefore, we assessed the interfacial roughness by X-ray reflectivity, finding comparable values < 1 nm for every t_{FM} (supplementary material).

In our setup the temperature difference between the hot and cold baths (i.e. the temperature drop ΔT across the whole sample including MgO substrate) is controlled and measured. The temperature profile will show two main features: (1) a change in its slope from layer to layer because of the different thermal conductivities and (2) a discontinuity at the interfaces due to the interfacial thermal resistance, also known as Kapitza resistance. Therefore, as illustrated in Fig. 1, we can split the total temperature difference into thermal drops along the sample:

$$\Delta T = \Delta T_{\text{Pt}} + \Delta T_i^{\text{Pt/FM}} + \Delta T_{\text{FM}} + \Delta T_i^{\text{FM/S}} + \Delta T_s \quad (4)$$

which accounts for the temperature drop in the Pt layer, at the Pt/FM interface, in the FM layer, at the FM/substrate interface, and across the substrate. In this equation, the thermal drops originated by the thermal contacts of the sample with the baths²⁷ are disregarded, thus the values obtained in the determination of S^i and S^b are underestimated. However, the quantification of the relative contributions to ΔV_{ISHE} should be unaffected by this systematic error. The heat flux

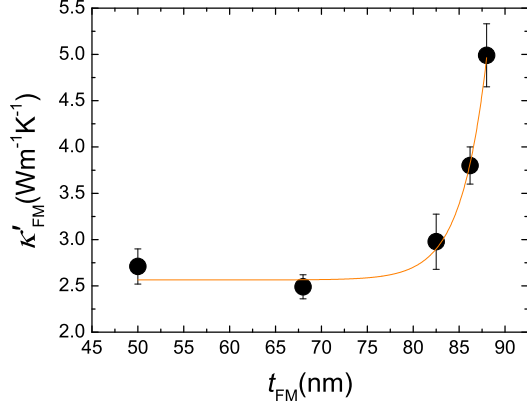


FIG. 2. Effective thermal conductivity of maghemite epitaxial thin films as a function of the thickness. Solid line represents an experimental fit to a sigmoid function used for interpolation of κ'_{FM} at the desired t_{FM} .

method^{6,17,18} offers another possibility to circumvent this error.

According to a simple thermal model the heat flux is constant through the whole sample:

$$J_Q = \left(\frac{t_{\text{Pt}}}{\kappa_{\text{Pt}}} + \frac{t_{\text{FM}}}{\kappa_{\text{FM}}} + \frac{t_{\text{S}}}{\kappa_{\text{S}}} + R_i^{\text{Pt/FM}} + R_i^{\text{FM/S}} \right)^{-1} \Delta T = \frac{1}{R_T} \Delta T = \frac{\kappa_{\text{FM}}}{t_{\text{FM}}} \Delta T_{\text{FM}} = \frac{1}{R_i^{\text{Pt/FM}}} \Delta T_i^{\text{Pt/FM}} \quad (5)$$

t 's denote thicknesses and κ 's denote thermal conductivities; $R_i^{\text{Pt/FM}}$ ($R_i^{\text{FM/S}}$) is the thermal resistance coming from the Pt/FM (FM/substrate) interface; and R_T represents the thermal resistance of the system as a whole, i.e., the composition of the thermal resistances of each layer and interface.

As pointed above, the first step is establishing the actual thermal drop across the magnetic layer as well as through the FM/Pt interface. This is especially troublesome when dealing with thin films in which thermal transport properties differ from those of the bulk materials and are not handily characterizable²⁸. However, the knowledge of these quantities is paramount for the quantitative analysis of the LSSE. This means that measurement of the thermal conductivity of the thin film is mandatory, since its value must be included into even the simplest thermal model along with that of the substrate.

In this work, the cross-plane thermal conductivity of maghemite thin films as well as MgO substrate were determined by the 3ω method²⁹ (supplementary material). It is important to note that the determined thin film conductivity is not the intrinsic κ_{FM} but an effective κ'_{FM} which also accounts for the thermal loss at the $\gamma\text{-Fe}_2\text{O}_3/\text{MgO}$ interface $R_i^{\text{FM/S}}$ ³⁰.

$$\kappa'_{\text{FM}} = \frac{\kappa_{\text{FM}}}{1 + R_i^{\text{FM/S}} \kappa_{\text{FM}}/t_{\text{FM}}} \quad (6)$$

We will use this effective κ'_{FM} to calculate ΔT_{FM} . This means that hereafter, $\Delta T_i^{\text{FM/S}}$ will be contained in ΔT_{FM} .

We measure κ'_{FM} at $T = 300$ K for different t_{FM} up to the thickness range of the samples we studied in the LSSE experiments. The thereby obtained values of the thermal conductivities at 300 K are depicted in Fig. 2. They follow a rather complex dependence, which may be attributed to the presence of defects rapidly changing with the film thickness; a possible candidate are the antiphase boundaries (APBs) which are usually shown by spinel structures (such as maghemite) and whose density decrease on increasing thickness³¹. A detailed analysis of this dependence is however beyond the scope of this work. From this experimental curve, we interpolate the values of κ'_{FM} at the t_{FM} of the samples studied in the LSSE experiments. Concerning MgO substrate, we measured $\kappa_{\text{S}} = 44.2(5) \text{ Wm}^{-1}\text{K}^{-1}$ at $T = 300$ K, in agreement with reported values for MgO single crystals^{32,33}.

The thermal resistance of the Pt layer is lower than the rest of the terms by two orders of magnitude, due to its small thickness $t_{\text{Pt}} = 6$ nm and large thermal conductivity $\kappa_{\text{Pt}} = 64 \text{ Wm}^{-1}\text{K}^{-1}$ ³⁴. The thermal resistances of the stacked layers are $R_{\text{MgO}} \sim 10^{-5} \text{ W}^{-1}\text{m}^2\text{K}$, R_{FM} ranges from $\sim 10^{-9}$ to $10^{-8} \text{ W}^{-1}\text{m}^2\text{K}$, and from literature $R_i \sim 10^{-9} \text{ W}^{-1}\text{m}^2\text{K}$ ^{34,35}; all of them exceed $R_{\text{Pt}} \sim 10^{-11} \text{ W}^{-1}\text{m}^2\text{K}$ by at least two orders of magnitude. This means that we can hence neglect the temperature drop in the Pt layer in Eq. 4 and its resistance contribution to Eq. 5.

Eq. 5 allows us to write every temperature drop in terms of the known ΔT :

$$\begin{aligned} \Delta T_{\text{FM}} &\approx \frac{\kappa_{\text{S}} t_{\text{FM}}}{\kappa_{\text{S}} t_{\text{FM}} + \kappa'_{\text{FM}} t_{\text{S}}} \Delta T \\ \Delta T_i^{\text{Pt/FM}} &\approx \frac{\kappa_{\text{S}} \kappa'_{\text{FM}} R_i^{\text{Pt/FM}}}{\kappa_{\text{S}} t_{\text{FM}} + \kappa'_{\text{FM}} t_{\text{S}}} \Delta T \end{aligned} \quad (7)$$

where we have taken a second approximation: $\kappa_{\text{S}} \kappa_{\text{FM}} R_i^{\text{Pt/FM}} \ll \kappa_{\text{FM}} t_{\text{S}}$, which is reasonable, given the substrate thickness as well as the typical values of R_i .

Once the thermal conductivities κ'_{FM} and κ_{S} have been estimated in this way, we proceed to the LSSE experiments for different t_{FM} . It has been shown that variations in the thermal contacts between the sample and the baths are source of error^{17,27}; care was taken to minimize these errors by ensuring that the same heat power sustained a similar ΔT for all samples. Alternatively, other approaches measure the heat flux instead^{6,17,36}.

In Fig. 3 the measured dependence of transverse voltage ΔV_{ISHE} on t_{FM} is shown. Following a widespread practice, these quantities have been normalized by the total thermal difference ΔT ^{13,37}, using the slopes of the linear fits of ΔV_{ISHE} as a function of different ΔT (see the inset of Fig. 3).

However, this means that, according to Eq. 7, ΔT_{FM} and ΔT_i depend on t_{FM} in Fig. 3. Hence, the observed behavior comprises not only the effect of Λ_{m} (as assumed by previous works) but also the variation of the thermal differences driving the LSSE (bulk and interfacial). To rigorously take into account both effects, the scaling with the corresponding thermal drops should be used instead^{17,18}, as proposed in Eq. 3. For this, we rewrite the spin Seebeck coefficients as a function

of the measured total ΔT , using Eq. 7:

$$\begin{aligned}\Delta V_{\text{ISHE}}^i &\approx S^i \cdot d_y \cdot \frac{\kappa_S \kappa'_{\text{FM}} R_i^{\text{Pt/FM}}}{\kappa_S t_{\text{FM}} + \kappa'_{\text{FM}} t_S} \Delta T \\ \Delta V_{\text{ISHE}}^b &\approx S^b \cdot d_y \cdot \frac{\kappa_S t_{\text{FM}}}{\kappa_S t_{\text{FM}} + \kappa'_{\text{FM}} t_S} \Delta T\end{aligned}\quad (8)$$

According to ISHE phenomenology, ISHE transverse voltage ΔV_{ISHE} and the exciting spin current density J_s are related by $\Delta V_{\text{ISHE}} \propto \theta_{\text{SH}} \rho_c J_s$ ³⁸, where θ_{SH} is the so-called spin Hall angle accounting for the efficiency of the spin-to-charge conversion, and ρ_c is the longitudinal electrical resistivity of the NM ISHE medium (here, Pt). Depending on the mechanism

governing ISHE, θ_{SH} may depend on ρ_c ^{39–41}. However, in this experiment, Pt layer thickness is the same for all samples, resulting in constant ρ_c . Therefore, $\Delta V_{\text{ISHE}} \propto J_s$. In sight of this fact and Eqs. 1, 2 and 8, we note that, unlike S^i , S^b depends on t_{FM} and can be expressed as:

$$S^b = A \cdot \frac{1}{t_{\text{FM}}} \frac{\cosh(t_{\text{FM}}/\Lambda_m) - 1}{\sinh(t_{\text{FM}}/\Lambda_m)} \quad (9)$$

where the coefficient A describes the thickness-independent term.

Altogether, the measured transverse voltage ΔV_{ISHE} will be

$$\begin{aligned}\Delta V_{\text{ISHE}} &= \Delta V_{\text{ISHE}}^i + \Delta V_{\text{ISHE}}^b = S^i \cdot d_y \cdot \Delta T_i^{\text{Pt/FM}} + S^b \cdot d_y \cdot \Delta T_{\text{FM}} \approx \\ &\approx \left(S^i \cdot d_y \cdot \frac{\kappa_S \kappa'_{\text{FM}} R_i^{\text{Pt/FM}}}{\kappa_S t_{\text{FM}} + \kappa'_{\text{FM}} t_S} + A \cdot d_y \cdot \frac{\cosh(t_{\text{FM}}/\Lambda_m) - 1}{\sinh(t_{\text{FM}}/\Lambda_m)} \frac{\kappa_S}{\kappa_S t_{\text{FM}} + \kappa'_{\text{FM}} t_S} \right) \Delta T\end{aligned}\quad (10)$$

A fit of this expression to the experimental data, shown in Fig. 3, provides (supplementary material) $\Lambda_m = 29(1)$ nm, $S^i R_i^{\text{Pt/FM}} = 1.83(6) \times 10^{-9}$ ($\text{Vm}^{-1}\text{K}^{-1}) \cdot (\text{W}^{-1}\text{m}^2\text{K})$ and $A = 40.8(9) \times 10^{-9}$ $\text{V} \cdot \text{K}^{-1}$. Given the reported order of magnitude of interfacial thermal resistances $R_i \sim 10^{-9} - 10^{-8}$ $\text{W}^{-1}\text{m}^2\text{K}$, we can also establish that S^i order of magnitude must lie between 0.1 and 1 $\text{Vm}^{-1}\text{K}^{-1}$, in agreement with previous estimations in other systems^{7,15,26}. Concerning S^b , the value of A provides from $S^b = 0.65(6)$ $\text{Vm}^{-1}\text{K}^{-1}$ for the thinnest sample down to $S^b = 0.46(4)$ $\text{Vm}^{-1}\text{K}^{-1}$ for the thickest one.

We can now compute the relative contribution of each source — b LSSE and i LSSE— to the total ΔV_{ISHE} output in our t_{FM} range for an experiment in which a total ΔT is estab-

lished. For this, we calculate ΔV_{ISHE}^i and ΔV_{ISHE}^b generated per Kelvin of total thermal drop ΔT from Eqs. 3 and 7 (i.e., the two addends between brackets in Eq. 10). The result is shown in Fig. 4. As one could expect, the influence of $R_i^{\text{Pt/FM}}$ is greater for thinner samples and consequently i LSSE contribution to the overall signal reduces as t_{FM} is increased, and reversely for b LSSE.

In summary, we have experimentally separated the bulk magnon accumulation and purely interfacial contributions to the LSSE in static heating conditions. We have done so by studying the LSSE as a function of the FM layer thickness in γ - $\text{Fe}_2\text{O}_3/\text{Pt}$ bilayers, and taking into account the relative change of the present thermal drops along the sample on vary-

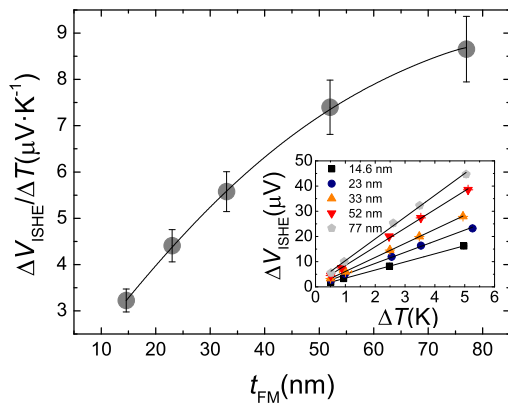


FIG. 3. Transverse voltage $\Delta V_{\text{ISHE}}/\Delta T$ measured for every different t_{FM} and fit of Eq. 10 to the experimental data. Inset: linear fits of ΔV_{ISHE} as a function of ΔT .

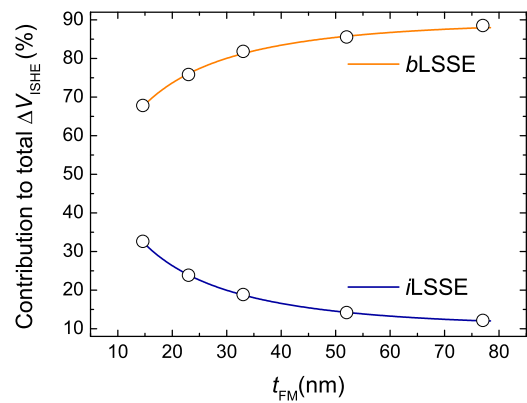


FIG. 4. Relative contribution ΔV_{ISHE}^i and ΔV_{ISHE}^b to the total ΔV_{ISHE} . Note that these percentages cannot be directly extended to S^i and S^b , given that they do not share the voltage dependences on t_{FM} (see Eq. 8).

ing the FM thickness. To that end, we have also measured the thickness dependence of the thermal conductivity of γ -Fe₂O₃ thin films by means of the 3ω method. With this, we managed to fit the addition of theoretical models for both sources to our experimental data. This allowed us to in the end compute the separate contribution of each source of thermal spin current. We found that although bulk component dominates in the range of thickness of our samples, the interfacial contribution is not negligible against it, as it represents from $\approx 33\%$ to $\approx 12\%$ of the total voltage. Besides, b LSSE coefficient values were determined: it varies between $S^b = 0.68(6) \text{ Vm}^{-1}\text{K}^{-1}$ for the thinnest sample ($t_{\text{FM}} = 14.5 \text{ nm}$) and $S^b = 0.46(4) \text{ Vm}^{-1}\text{K}^{-1}$ for the thickest one ($t_{\text{FM}} = 77 \text{ nm}$). i LSSE coefficient order of magnitude was estimated to lie between $S^i \sim 0.1$ and $1 \text{ Vm}^{-1}\text{K}^{-1}$, in agreement with the values reported in literature for other systems^{7,15,26}. The fit also provided a thermal magnon accumulation length in γ -Fe₂O₃ of $\Lambda_m = 29(1) \text{ nm}$. In literature, Λ_m at room temperature corresponding to other ferrimagnetic oxides can be found: $\Lambda_m = 17 \text{ nm}$ for half-metal Fe₃O₄⁴² or $\Lambda_m \sim 100 \text{ nm}$ for insulating YIG²⁶ were reported using the temperature difference method. However, one must be cautious before comparing our result, because those works only considered the influence of the thermally excited magnon propagation length on the thickness dependence of LSSE. More recent works using different approaches to investigate this dependence circumvent the change of ΔT_{FM} . For example, Noack *et al.* studied the LSSE time evolution in YIG thin films heating with microwave pulses, finding $\Lambda_m \sim 425 \text{ nm}$ ⁴³; and Venkat *et al.*, using the heat flux method, reported $\Lambda_m = 19(2) \text{ nm}$ for Fe₃O₄ thin films¹⁹. Still, only the bulk effect is considered to explain the results.

These results reassure maghemite's potential in spin-caloritronic devices and bring insight into the global picture of the LSSE. In particular, the relative quantification of bulk and interfacial contributions improves the precision of its description, therefore assisting a deeper understanding of the effect.

SUPPLEMENTARY MATERIAL

See supplementary material for details of the 3ω method, the structural characterization of samples, and the fit parameters initialization.

ACKNOWLEDGMENTS

This work was supported by the Spanish Ministry of Science (through Projects No. MAT2014-51982-C2-R, MAT2016-80762-R, MAT2017-82970-C2-R and PID2019-104150RB-I00 (including FEDER funding) and the Aragón Regional government (Project No. E26). P. J.-C. acknowledges Spanish MECD for support through FPU program (reference FPU014/02546). D.B. acknowledges support from MINECO (Spain) through an FPI program (BES-2017-079688). Authors acknowledge the Advanced Microscopy Laboratory-INA University of Zaragoza for offering access to their instruments.

DATA AVAILABILITY

The data that support the findings of this study are available from the corresponding author upon reasonable request.

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SUPPLEMENTARY MATERIAL FOR

Quantification of the interfacial and bulk contributions to the
longitudinal spin Seebeck effect

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I. The 3ω method

The cross-plane thermal conductivity of the samples were measured by the 3ω method.^{1,2} In this method a thin metal resistor serves as a heater and a thermometer simultaneously. By applying an AC current at frequency ω and amplitude I_0 through the resistor, a temperature oscillation at 2ω ($\Delta T_{2\omega}$) is produced due to conventional Joule heating. The amplitude of this oscillation is indirectly measured through the third harmonic voltage, $V_{3\omega}$, from the formula given below (a detailed description can be found on Ref. 3,4):

$$V_{3\omega} = \frac{I_0}{2} \left(\frac{dR}{dT} \right) \Delta T_{2\omega}.$$

The heating produced at frequency 2ω , which depends on the frequency, ω , of the applied ac current, is related to the thermal properties of the medium underneath the resistor. Specifically, by solving the one-dimensional heat equation, the following expression is obtained:⁵

$$\Delta T_{2\omega} = \frac{I_0^2 R}{\pi l \kappa} \left[\frac{1}{2} \ln \left(\frac{D}{\left(\frac{w}{2}\right)^2} \right) - \frac{1}{2} \ln(2\omega) + \eta - \frac{i\pi}{4} \right],$$

where $I_0^2 R$ is the power dissipated through the resistor (R is the electrical resistance of the metal line), l is its length, κ and D are, respectively, the thermal conductivity and thermal diffusivity of the material on top of which the resistance is placed, w is the width of the resistor, and η is a parameter that depends on the material used,^{2,3,6,7} Note that in order to consider the heat flow as being one-dimensional, the width of the resistor, w , should be much smaller than the penetration length of the thermal wave.⁵

When the sample underneath the resistor consists of a thin film and a substrate, the solution of the heat equation is slightly different. As long as the thickness of the film is much smaller than the width of the resistor ($t \ll w$), which is our case, the transmission of heat through the film can be considered one-dimensional. In this scenario, the following expression is deduced (Ref. 2):

$$\Delta T_{2\omega} = \frac{P}{\pi l \kappa} \left[\frac{1}{2} \ln \left(\frac{D}{\left(\frac{w}{2}\right)^2} \right) - \frac{1}{2} \ln(2\omega) + \eta - \frac{i\pi}{4} \right] + \frac{P}{\kappa_{film}} \frac{t}{wl} = \Delta T_{substrate} + \Delta T_{film},$$

where the second term in the equation is the temperature increase produced by the film. At each frequency, this contribution of the film appears as an offset in comparison with the heating produced when just the substrate is present (Fig. S1) Then by subtraction of the heating produced

in the substrate ($\Delta T_{\text{substrate}}$) to that obtained when measuring the film + substrate ($\Delta T_{\text{film+substrate}}$) the thermal conductivity of the thin film can be obtained from:

$$\kappa_{\text{film}} = \frac{P}{\Delta T_{\text{film}}} \frac{t}{wl}.$$

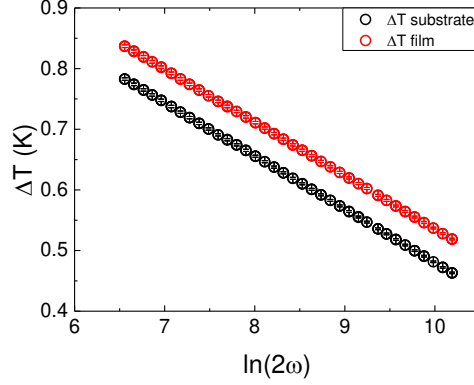


Fig S1. Temperature rise on a sample 50 nm thick and the MgO substrate.

The resistors used were made of Au or Pt (100 nm thick, 10 μm width, 1 mm length with 10 nm of Cr for adhesion), by evaporation and optical lithography. The measurements were performed by applying current with a Keithley 6221 AC source at frequencies from 56 to 2120 Hz to produce a heat dissipation of 30 mW for all samples. These samples were grown on half the substrate, leaving space on the other half to have a reference resistor on the bare substrate. The voltage drop at 3ω was measured with a Stanford Research Systems SR830 lock-in amplifier. As the ratio $V_{1\omega}/V_{3\omega}$ is around 10^3 , a circuit was used to cancel out the voltage at 1ω , which is described in Ref. 3.

II. Structural characterization

X-ray characterization was performed *Bruker D8 Advance* high-resolution diffractometer using Cu $K\alpha_1$ radiation. X-ray reflectivity (XRR) measurements were performed to assess the thicknesses and interfaces quality, and X-ray diffraction (XRD) patterns were recorded to ascertain the crystal quality of maghemite films.

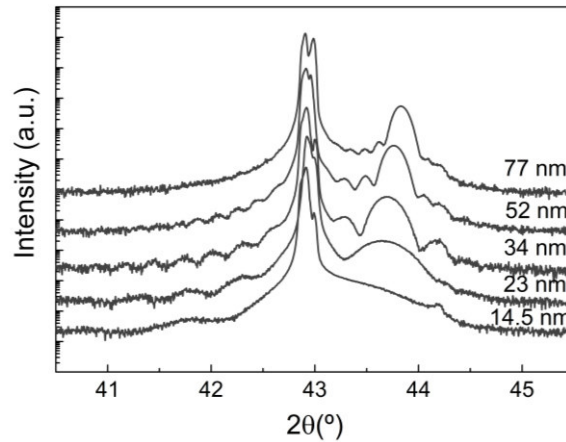


Fig S2. XRD spectra of the MgO// γ -Fe₂O₃/Pt samples for different γ -Fe₂O₃ thickness measured around the (002) MgO substrate Bragg peak.

XRD patterns around the (002) MgO substrate Bragg peak are shown in Fig. S2. We observe the narrowing of the (004) maghemite peak as thickness increased, as expected from the Scherrer's formula⁸. Additionally, Laue oscillations are visible for all samples, indicating the existence of crystal coherence along the whole thickness of the sample.

The XRR measurements performed for every sample are shown in Fig. S3(a). The raw data are analyzed using the software *Leptos* from Bruker, by means of which the sample structure is simulated and fitted to the data using a simulated annealing algorithm which uses thicknesses and roughnesses as fitting parameters.

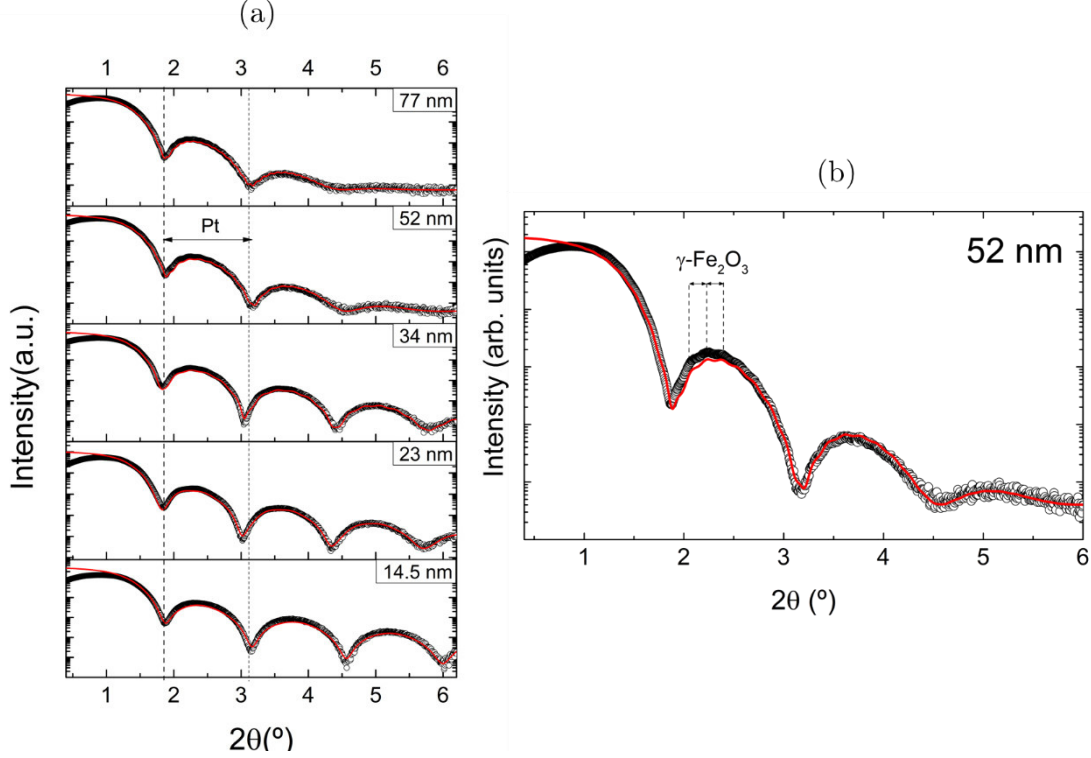


Fig S3. XRR spectra of the MgO// γ -Fe₂O₃/Pt samples for different γ -Fe₂O₃ thickness: data and fit to a simulated sample using the *Leptos* software.

The long-period Kiessig fringes correspond to the Pt layer and allow the extraction of its thickness, while the short-period fringes (highlighted in Fig. S3 for one of the samples) correspond to the γ -Fe₂O₃ layer. The obtained interface and surface roughness remains <1 nm for all samples, ensuring the quality of interfaces. This was expected given that both layers (γ -Fe₂O₃ and Pt) were deposited *in situ*. As it influences the efficiency in the spin transmission across the γ -Fe₂O₃/Pt interface⁹, interfaces with similar quality are required to enable the reliable comparison between the results obtained for all samples.

III. Initial value of the parameters in the fit of $\Delta V_{\text{ISHE}}/\Delta T$

The fit of Eq. 10 of the main text to the data plotted in Fig. 3 was performed using as fitting parameters Λ_m , A , and the product $S^i R_i$. The respective expected order of magnitude was assigned as initial value of each parameter, as indicated in Table S1.

No lower or upper bounds to these parameters were set.

Parameter	Initial value
Λ_m	10×10^{-9} m
A	1×10^{-9} V K ⁻¹
$S R_i$	1×10^{-9} (Vm ⁻¹ K ⁻¹)(m ² KW ⁻¹)

Table S1. Values employed for the initialization of the parameters in the fit of Eq. 10 of the main text to $\Delta V_{\text{ISHE}}/\Delta T$ data.

The contact distance to measure ΔV_{ISHE} is $d_y = 6.5$ mm. The electrical connections were made using 0.025 mm Al wire bonded with silver paste at the sample edges. It was shown in Ref.¹⁰ that the uncontrolled size of these connections was source of experimental error responsible for data dispersion. Consequently, an error of ± 0.5 mm (half the resolution of a ruler) has been assigned to d_y and propagated to ΔV_{ISHE} in order to address this uncertainty.

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