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# Magnetic Hyperthermia Experiments with Magnetic Nanoparticles in Clarified Butter Oil and Paraffin: A Thermodynamic Analysis

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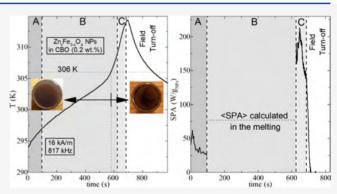
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**ABSTRACT:** In specific power absorption models for magnetic fluid hyperthermia (MFH) experiments, the magnetic relaxation time of nanoparticles (NPs) is known to be a fundamental descriptor of the heating mechanisms. The relaxation time is mainly determined by the interplay between the magnetic properties of NPs and the rheological properties of NPs' environment. Although the role of magnetism in MFH has been extensively studied, the thermal properties of the NP medium and their changes during MFH experiments have been underrated so far. Herein, we show that  $Zn_xFe_{3-x}O_4$  NPs dispersed through different media with phase transition in the temperature range of experiment as clarified butter oil (CBO) and paraffin. These systems show nonlinear behavior of the heating rate within the



temperature range of MFH experiments. For CBO, a fast increase at  $\sim$ 306 K is associated with changes in the viscosity ( $\eta(T)$ ) and specific heat ( $c_p(T)$ ) of the medium at its melting temperature. This increment in the heating rate takes place around 318 K for paraffin. The magnetic and morphological characterization of NPs together with the observed agglomeration of NPs above 306 and 318 K for CBO and paraffin, respectively, indicate that the fast increase in MFH curves could not be associated with the change in the magnetic relaxation mechanism, with Néel relaxation being dominant. In fact, successive experimental runs performed up to temperatures below and above the CBO and paraffin melting points resulted in different MFH curves due to agglomeration of NPs driven by magnetic field inhomogeneity during the experiments. Our results highlight the relevance of the thermodynamic properties of the system NP-medium for an accurate measurement of the heating efficiency for in vitro and in vivo environments, where the thermal properties are largely variable within the temperature window of MFH experiments.

# ■ INTRODUCTION

In a magnetic fluid hyperthermia (MFH) experiment, the relaxation time of the magnetic moment  $(\tau)$  of nanoparticles (NPs) is a key factor for heating mechanisms operating behind specific power absorption (SPA) determination. In a single domain NP, effective heating results from the interplay of two relaxation mechanisms: the Brownian rotation against the viscous forces expressed by  $\tau_{\rm B} = 3\eta V_{\rm hyd}/k_{\rm B}T$ , where  $\eta$  is the viscosity of the medium,  $V_{\rm hyd}$  is the hydrodynamic volume of the NP, and  $k_BT$  is the thermal energy, and the Néel relaxation of the magnetic moment expressed by  $\tau_{\rm N} = \tau_0 \exp(K_{\rm eff}V/k_{\rm B}T)$ , where  $au_0$  is the characteristic attempt time and  $K_{ ext{eff}}V$  is the effective anisotropy energy barrier of the NP given by its effective anisotropy constant  $K_{\text{eff}}$  and volume V. The dominant mechanism will be the one with a shorter relaxation time. For MFH applications, the most adequate systems are those in which  $au_{\rm N}$  dominates  $^{2-5}$  because the heating power depends only on the intrinsic magnetic properties of NPs, and it is independent of the (variable) viscosity of different

biological media. Therefore, the precise heat dose delivered is independent of the specific tissue or organ targeted.  $^{6-10}$  There is a growing consensus on the fact that magnetic NPs for MFH should be fabricated in this way, and optimization is done by adjusting its  $K_{\rm eff}V$ .

Only a few studies have been reported so far, evaluating the variability of SPA expected when the NPs are dispersed in a medium with a viscosity  $[\eta(T)]$  and specific heat  $[c_p(T)]$ , which are temperature-dependent within the temperature range measured. If the medium presents a strong reduction of  $\eta(T)$  in the temperature range of the experiment, for instance, due to melting, it results in a shorter  $\tau_B$ , which may

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lead to a change in the dominant mechanism acting behind the heating process. However, even when the magnetic relaxation  $(\tau_{\rm N})$  is still dominating, changes in the properties of medium may affect the SPA measured for the system. Changes in viscosity may affect the spatial arrangement of the NPs, allowing the alignment of their magnetic easy axis with the external field gradient and yielding the formation of multiparticle structures with a very different SPA response. <sup>12–14</sup> In the case of phase transition such as melting, the latent heat (L) also impacts on the SPA measured.

Paraffin and clarified butter oil (CBO) are both materials that fit our needs for the present study on thermal evolution of the SPA parameter during MFH experiments. Both substances show a phase transition at temperatures within the MFH experimental range. Paraffin is a uncomplicated medium in terms of composition, made of a mixture of linear *n*-alkanes  $(CH_3-(CH_2)_n-CH_3)$  with a phase transition that depends on the number of carbon atoms involved (e.g., 293 K < T < 295 K for  $C_{16}-C_{18}$  and 339 K < T < 341 K for  $C_{21}-C_{50}$ ). 15 It has a latent heat L of 121.9 J/g, a thermal conductivity of  $\sim 0.21$ -0.24 W/mK just below the melting point, 15 and a dynamic viscosity around  $\eta \sim 2.1$  mPa·s at the melting temperature of  $T_{\rm M}$  = 332 K.<sup>16</sup> CBO is a more complex medium obtained by extraction from heated butter oil, which could be interesting when considering how to emulate the potential of NPs candidates for MFH applications. It is composed of 99-99.5% of fatty acids—palmitic, oleic, myristic, and stearic acid. <sup>17</sup> The use of CBO avoids the presence of water droplets that can affect the solidification process of the fat, and consequently, the physicochemical properties of the crystal network. 18 Physical properties of CBO are well known, with  $T_{\rm M} = 305.2~{\rm K}^{19}$ (compared to  $T_{\rm M} = 308.0$  K reported for butter<sup>20</sup>). The viscosity of CBO decreases at the melting point by a factor of 10<sup>3</sup>, from some Pa·s to tens of mPa·s.<sup>21</sup> Also, thermal properties, such as  $c_p$ , vary with temperature, being sensitive to changes in its physical state close to  $T_{\rm M}$ . In fact, there are distinct regions of phase transition related to melting: the lowmelting fraction (LMF), around 280 K, medium-melting fraction (MMF), around 290 K, and a high-melting fraction (HMF), around 310 K, where the temperature range depends on the heating rate.<sup>23</sup> Its thermal conductivity slightly before the melting point is estimated at 0.22 W/m·K.

In this work, we study the SPA of  $Zn_xFe_{3-x}O_4$  NPs dispersed in CBO and paraffin, two media with a strong reduction of viscosity at the phase transition within the temperature range of MFH experiments. In particular, we analyze NPs with different shapes, sizes, and initial heating rates dispersed in these two media, and the effects of particle agglomeration, observed at higher temperatures, on the SPA. For this, we synthesized Zn<sub>x</sub>Fe<sub>3-x</sub>O<sub>4</sub> NPs with different mean diameters  $(\langle d \rangle)$  and dispersions  $(\sigma)$ , as well as different magnetic anisotropy constants  $(K_{\text{eff}})$ . The variations in  $K_{\text{eff}}$ ,  $\langle d \rangle$ , and  $\sigma$  of NPs result in different measured heating rates, and consequently, to different values of SPA. The incorporation of Zn in the ferrite structure reduces the anisotropy of the system, allowing the heating up to lower temperatures, below the transition temperature of the medium, so within the highviscosity range. A nonusual thermal variation of the heating rate is observed in MFH experiments, assigned to changes in the properties of the medium with temperature, together with a spatial rearrangement of the NPs. Finally, irreversibility in the MFH response after successive experiments (runs) is observed

for samples with higher NP concentrations, resulting from agglomeration above the melting point of CBO and paraffin.

## METHODS

 $Zn_xFe_{3-x}O_4$  NPs were produced by the thermal decomposition at high temperatures of Fe(III) and Zn(II) acetylacetonate in different solvents (benzyl ether and trioctylamine) using the surfactants oleic acid and oleylamine. The method was adapted from the procedure described by Lohr et al., <sup>24</sup> trying to avoid the presence of Wüstite phase. The composition of each sample, with general formula  $Zn_xFe_{3-x}O_4$  with x varying in the 0.1–0.2 range, was controlled by the precursor ratio used. The as-prepared NPs are hydrophobic, coated with oleic acid. In order to understand the dominant relaxation mechanisms in MFH experiments, we performed a morphological characterization and correlated the observed magnetic properties with the phase composition of NPs.

The composition of the as-prepared NPs was determined by particle-induced X-ray emission (PIXE)<sup>25</sup> using a 3 MeV H<sup>+</sup> beam from a NEC 5SDH 1.7 MV tandem accelerator with a NEC RC43 end-station. For this, NPs were washed several times with acetone in order to reduce the oleic acid and oleylamine amounts remaining from the synthesis and dried. The resulting powder was conditioned over a carbon tape for PIXE measurements, and the results were analyzed with software GUPIX.<sup>26</sup> As the PIXE technique is very sensitive, the following signals from other elements, arising from sample handling and conditioning, are observed: carbon, aluminum, sodium, calcium, and silicon. Therefore, the composition of each sample was focused only in determining the ratio between zinc and iron amounts ([Zn] and [Fe], respectively), resulting in x = 0.11, 0.12, 0.19, and 0.21 (see Figure S1 in pg. S1 of Supporting Information). Samples were labeled according to

The size and diameter dispersion of as-prepared NPs were determined by transmission electron microscopy (TEM) performed on a Philips CM200 microscope operating at 200 kV. TEM specimens were prepared by dropping a solution of NPs dispersed in toluene onto a copper grid coated with an amorphous carbon layer. The diameter histograms were built up by measuring the diameter of at least 300 NPs, and the mean diameter  $\langle d \rangle$  and dispersion  $\sigma$  were obtained by fitting them with a lognormal distribution. A typical XRD profile (sample x = 0.21) of samples is shown in Figure S2, pg. S2 of Supporting Information. All diffraction peaks observed could be indexed by a cubic magnetite phase (JCPDS card 19-0629). No evidence of ZnO phase was observed within the limit of our background and peak width, as estimated from the absence of most intense peaks of the hexagonal ZnO phase (JCPDS card 36-1451). Thus, we assumed that the Zn contents obtained from PIXE analysis were incorporated into the cubic ferrite structure.

The magnetic properties of systems were measured using a vibrating sample magnetometer (VSM, Lakeshore) and in a commercial superconducting quantum interference device magnetometer (SQUID, MPMS Quantum Design). The saturation magnetization ( $M_{\rm S}$ ) was determined by magnetization measurements as a function of the applied field measured at 300 K using the VSM (see Figure S3 in pg. S3 of Supporting Information). The blocking temperature distribution ( $f(T_{\rm B})$ ) of each sample was obtained from the magnetization curves as a function of temperature measured in the zero-field-cooling (ZFC) and field-cooling (FC)

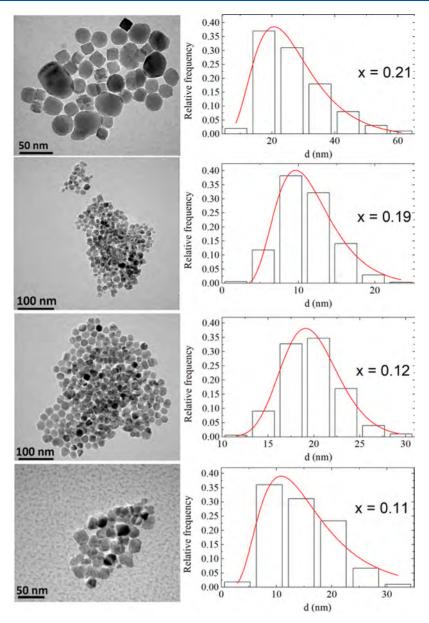


Figure 1. Representative TEM images of the as-prepared  $Zn_xFe_{3-x}O_4$  NPs. The right panel shows the respective diameter histograms fitted with a lognormal distribution, whose parameters are given in Table 1.

protocols ( $M_{ZFC}$  and  $M_{FC}$  curves, respectively) in the SQUID magnetometer with an applied field of 4 kA/m. The blocking temperature distribution  $f(T_B)$  is obtained by the expression  $(1/T)d(M_{ZFC}(T) - M_{FC}(T))/dT$  (see pg. S4 and pg. S5 of Supporting Information), which resulted in good agreement with the blocking temperature distribution obtained from the temperature decay of remanence curve, as shown in a previous work.<sup>27</sup> Other approximations are used in the literature to obtain the blocking temperature, <sup>28-32</sup> and the difference between the  $f(T_B)$  obtained from these expressions depends on the dispersion of size distribution; for comparison, one of them  $[f^{+}(T_{\rm B}) \alpha d(M_{\rm ZFC}(T) - M_{\rm FC}(T))/dT]$  is compared with the expression  $(1/T)d(M_{ZFC}(T) - M_{FC}(T))/dT$  used in this work (see Figure S4 in pg. S6 of Supporting Information). The samples for magnetic measurements were conditioned by dispersing the NPs in epoxy resin in low concentrations (about 0.1 wt %), avoiding the agglomeration and physical rotation of the NPs with the applied field.

In order to avoid the thermal dependence of specific heat  $[c_n(T)]$  of paraffin, CBO and CBO-containing NPs at concentrations of 0.2 wt % (CBO + NPs) were determined by differential scanning calorimetry (DSC) using a TA Instruments Q2000 calorimeter. A three-step procedure<sup>33</sup> has been performed at 10, 5, and 1 K/min, under 50 mL/min N<sub>2</sub> flow in hermetic aluminum crucibles, using sapphire as a calibration substance. DSC results were analyzed in a similar way than used in ref 23 for CBO and in ref 16 for paraffin, reflecting the melting process. For CBO, two peaks were observed, one associated with the unresolved LMF and MMF melting and another peak related to the HMF melting. The last transition is the only one developed within the temperature range of hyperthermia experiments (292-330 K). The enthalpy related to the last peak  $(\Delta H_{\rm M})$  was determined as the area of the measured  $c_p(T)$  curve with respect to the baseline curve  $[c_p^{\text{baseline}}(T)]$  as

$$\Delta H_{\rm M} [{\rm J/g}] = \int_{T_{\rm i}}^{T_{\rm F}} c_p(T) \mathrm{d}T - \int_{T_{\rm i}}^{T_{\rm F}} c_p^{\rm baseline} \, \mathrm{d}T \tag{1}$$

where  $T_{\rm i}$  and  $T_{\rm F}$  are the initial and final temperatures of the HMF, respectively, defined by the linear extrapolation of the increase and decrease in the initial and final steps of the HMF, respectively. For paraffin, without NPs, the melting process is related to a peak between 307.2 K  $(T_{\rm i})$  and 327.4 K  $(T_{\rm F})$ .

The samples used in MFH experiments were prepared by heating CBO and paraffin until 317 and 343 K, respectively, with a small amount of toluene solution containing the amount of NPs necessary to obtain the final concentration being reduced. This mixture was exposed to ultrasound for 30 min at 317 K for CBO and at 343 K for paraffin, both in an open flask. In order to determine the absence of magnetic impurities in the CBO and paraffin used in the experiments, M(H) curves at 300 K of both materials without NPs were measured using a VSM (see Figure S5 in pg. S7 of Supporting Information). In both cases, a diamagnetic component was observed, indicating the absence of magnetic contamination, within the detection limits of the experimental technique.

MFH experiments were performed in two different commercial models (nB Nanoscale Biomagnetics, Spain), operating with a magnetic field amplitude  $(H_0)$  of 16 kA/m: a DM100-model with a working frequencies (f) of 570 and 817 kHz, and a F1-D5 RF-model with f = 570 kHz. These apparatuses present different thermal insulation setups and magnetic field gradients produced by the solenoid, the DM100-model having better insulation and a less field gradient. As calibration, MFH experiments with CBO and paraffin without NPs were performed at room temperature, showing the absence of temperature increment in both cases (see Figure S6 in pg. S8 of Supporting Information). The quantities  $c_p(dT/dt)$  [W/g] and its integral in the corresponding time interval were numerically calculated using an interpolation in the desired range for both curves after an advanced-averaging smoothing procedure for the measured T(t) curves, being labeled as  $\Gamma(t)$ 

$$\Gamma(t) [J/g] = \int_{t_0}^t c_p \left(\frac{\mathrm{d}T}{\mathrm{d}t}\right) \mathrm{d}t \tag{2}$$

# RESULTS AND DISCUSSION

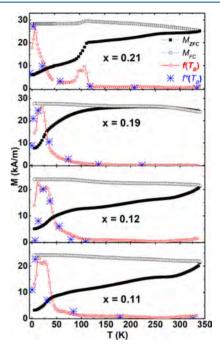
Representative TEM images of synthesized NPs of the four samples are shown in Figure 1, with the respective histograms of diameters presented in the right panel and fitted with a lognormal distribution for all samples. The values of  $\langle d \rangle$  and  $\sigma$  obtained from the fitting are given in Table 1.

Concerning the magnetic properties of our samples, they present a distinct mean blocking temperature  $T_{\rm B}$  (see Table 1) obtained from the  $M_{\rm ZFC}(T)$  and  $M_{\rm FC}(T)$  measurements presented in Figure 2. This is a consequence of the expected changes in the effective magnetic anisotropy  $K_{\rm eff}$  and volume of samples. Figure 2 also shows the corresponding blocking temperature distribution  $f(T_{\rm B})$  of all samples, according to the established results presented in pgs. S4 and S5 of Supporting Information, compared with the blocking temperature distribution  $f^*(T_{\rm B})$  calculated from the diameter histogram obtained from TEM data (Figure 1) by Néel's model assuming a value of  $\tau_0 = 10^{-10}$  s, measuring time  $\tau_{\rm m} = 100$  s and using the amplitude and energy barrier as fitting parameters.  $K_{\rm eff}$  was calculated through the definition of blocking temperature in Néel's model by matching the distribution from TEM results

Table 1. NP Size Distribution and Magnetic Parameters of  $Zn_xFe_{3-x}O_4$  Obtained from TEM Images and Magnetization Measurements

X	$a \langle d \rangle$ (nm)	$a\sigma$	${}^{b}M_{S}^{300K}$ (kA/m)	$^{c}\langle T_{\rm B}\rangle$ (K)	$^{d}K_{\text{eff}}\left(J/\text{m}^{3}\right)$
0.21	24.7	0.41	74	55	$3.0 \times 10^{3}$
0.19	11.0	0.18	75	32	$2.5 \times 10^{3}$
0.12	19.7	0.36	69	72	$5.2 \times 10^{3}$
0.11	14.0	0.50	63	64	$7.5 \times 10^{3}$

 $^a\langle d \rangle$  is the mean particle size and  $\sigma$  is the size dispersion obtained from the fitting of the diameter histogram with a lognormal.  $^bM_{\rm S}^{300{\rm K}}$  is the saturation magnetization at 300 K obtained from the hysteresis cycle.  $^c\langle T_{\rm B} \rangle$  is the mean blocking temperature obtained from the blocking temperature distribution  $f(T_{\rm B})$  calculated from the  $M_{\rm ZFC}$  and  $M_{\rm FC}$  curves.  $^dK_{\rm eff}$  is the effective magnetic anisotropy obtained from the fit of  $f(T_{\rm B})$  with the blocking temperature distribution calculated from the diameter histogram  $f^*(T_{\rm B})$ .



**Figure 2.**  $M_{\rm ZFC}(T)$  and  $M_{\rm FC}(T)$  curves of  ${\rm Zn_xFe_{3-x}O_4}$  NPs (solid and open squares, respectively) measured with an applied field of 4 kA/m. The respective blocking temperature distribution  $f(T_{\rm B})$  (red stars) is also presented together with  $f^*(T_{\rm B})$  (blue crosses), as calculated from the size distributions given in Figure 1.

and the  $f(T_{\rm B})$  distribution from magnetic measurements. The obtained  $K_{\rm eff}$  values are presented in Table 1. A high irreversibility temperature is observed in all curves with the exception of sample x=0.19. These high irreversibility temperatures indicate the contribution of NPs with a large anisotropy but not so relevant in population.

Table 1 also gives the saturation magnetization values  $(M_S)$  measured at 300 K for all samples. Magnetization curves as a function of applied field M(H) are shown in Figure S3, pg. S3 of Supporting Information. Notice that sample x=0.19 presents a composition and morphology resulting in a product  $K_{\rm eff}d^3$  with relatively narrow size dispersion close to a value that results in reasonable SPA values. For the other samples, the product  $K_{\rm eff}d^3$  would result in a reduced SPA value and, in this way, the broader size distributions of these samples result in a SPA that allows performing our MFH experiments in the temperature range of phase transition in both media.

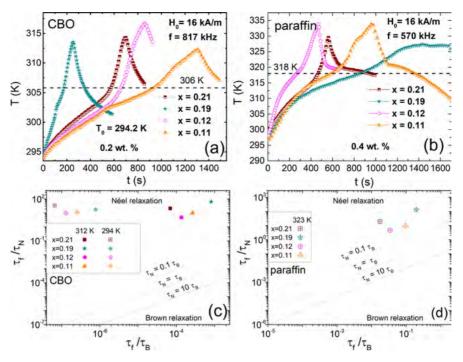


Figure 3. (a,b) Evolution of temperature with time during the MFH experiments performed in the DM100-model for 0.2 wt % of samples x = 0.21, 0.19, 0.12, and 0.11 dispersed in CBO ( $H_0 = 16 \text{ kA/m}$  and f = 817 kHz) and in paraffin ( $H_0 = 16 \text{ kA/m}$  and f = 570 kHz), respectively. Dotted line indicates the temperatures 306 and 318 K, where an increase in the slope is observed for CBO and paraffin, respectively. (c,d) Relaxation time diagram, where the Néel ( $\tau_{\rm N}$ ) and Brown ( $\tau_{\rm B}$ ) relaxation times of different NPs dispersed in CBO and in paraffin, respectively, normalized by the applied field period ( $\tau_{\rm f} = 1/(2\pi f)$ ) are plotted; latter data were calculated for two temperatures 294 and 312 K, where the CBO presents different viscosities, and 323 K, above the melting point of paraffin.

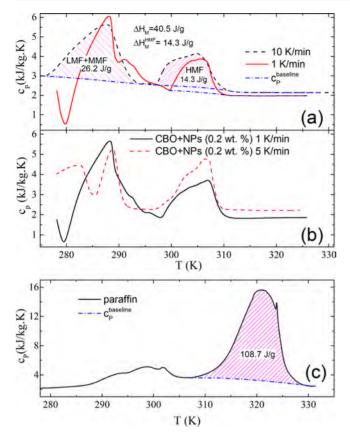
Figure 3a shows the results of the MFH experiment of all samples of NPs dispersed in CBO at a concentration of 0.2 wt % performed with  $H_0=16$  kA/m and f=817 kHz from the initial temperature  $T_0=294.2$  K in the DM100-model. As expected, the samples present a distinct heating rate, which is a consequence of different relaxation times resulting from different morphologies, specifically  $\langle d \rangle$  and  $\sigma$ , and compositions, which is reflected in different  $M_S$  and anisotropy energy barriers proportional to  $\langle T_B \rangle$ . Figure 3b gives the MFH results of the DM100-model ( $H_0=16$  kA/m and f=570 kHz) for the samples x=0.21, 0.19, 0.12, and 0.11 dispersed in paraffin at a concentration of 0.4 wt %, which present similar trends to the samples dispersed in CBO, except that the increment in the heating rate is observed at a higher temperature ( $\sim$ 318 K).

Usually, SPA is obtained from the initial slope of these curves by the simplified relationship SPA =  $(m/m_{\rm NPs})c_p({\rm d}T/{\rm d}t)$ , where  $c_p$  and m are the specific heat and the mass of the media, respectively, and  $m_{\rm NPs}$  is the mass of the NPs. This expression assumes that all energy absorbed by the NPs from the ac applied field is used to increase the temperature, and heat losses are negligible during the first few seconds of heating. After the initial seconds, however, the heating rate  $({\rm d}T/{\rm d}t)$  is observed to depart from the linear behavior due to nonadiabaticity of the system. However, in these systems of NPs dispersed in CBO and in paraffin, the heating curves reveal a complex behavior with regions with different heating rates, which increases around 306 K for all samples in CBO and around 318 K for paraffin, as indicated by the dotted lines in Figure 3a,b.

The increase in the heating rate during the MFH experiment observed in Figure 3a,b could be due to changes in the thermodynamic properties of media or a change in the NP

relaxation mechanism, from Néel to Brown driven by the melting of CBO (or paraffin), and the consequent reduction in the viscosity  $\eta$  of CBO (in the case of paraffin, a change from the solid to liquid state). In order to evaluate the possibility of change in the relaxation mechanism as a consequence of CBO melting, we calculate the Brown  $(\tau_{\rm B})$  and Néel  $(\tau_{\rm N})$  relaxation times of all samples. The characteristic times were calculated as  $\tau_{\rm B} = 3\eta V_{\rm hyd}/k_{\rm B}T$  and  $\tau_{\rm N} = \tau_0 \exp(27\langle T_{\rm B}\rangle/T)$ , using  $\tau_0 = 10^{-10}$ s, the volume obtained from TEM, the CBO viscosity  $\eta = 10$ and 10 mPa·s for T = 294 and 312 K, the lower and higher temperatures than the CBO melting point, respectively. We consider  $V_{\text{hyd}} = (\pi/6)\langle d \rangle^3$ , without including an organic layer usually present in the NPs prepared by this method and, therefore, the value of  $\tau_{\rm B}$  is underestimated. The relationship between  $\tau_{\rm N}$  and  $\tau_{\rm B}$  is plotted in the relaxation time diagrams built according to Lima et al.2 in Figure 3c. From this figure, it is clear that  $\tau_{\rm N} < \tau_{\rm B}$  (even considering an underestimated value of  $\tau_{\rm B}$ ) above and below the melting temperature. In this way, the magnetic relaxation mechanism is the dominant one for all samples and in all the studied temperature range. This result rules out the hypothesis that a change in the NP relaxation mechanism could be responsible for the increase in the heating rate in the MFH experiments during the CBO melting. Figure 3d presents a similar diagram for the NPs in paraffin ( $\eta = 2.1$ mPa·s) for T = 353 K, resulting in  $\tau_{\rm N} < \tau_{\rm B}$  for the four samples and reflecting the Néel relaxation mechanisms as the dominant

Figure 4a presents the  $c_p(T)$  curves of CBO measured at different heating rates: 1 and 10 K/min. As is clearly observed, there are two peaks in both curves, which are better defined for the highest heating rate. The first peak is associated with the unresolved LMF and MMF transitions at lower temperatures,



**Figure 4.** (a) Thermal dependence of specific heat  $[c_p(T)]$  of CBO measured with heating rates of 1 and 10 K/min, as well as of the  $c_p^{\rm baseline}(T)$  curves (dotted-blue line for both heating rates). Dashed zones indicate the difference between  $c_p(T)$  and  $c_p^{\rm baseline}(T)$  associated with the melting of distinct fractions. (b)  $c_p(T)$  curves for CBO containing 0.2 wt % of x=0.19 NPs with heating rates of 1 and 5 K/min. (c)  $c_p(T)$  curves for paraffin with a heating rate of 10 K/min.

and the second peak is associated with the HMF transition of CBO.  $^{23}$  The effect of total melting transition can be observed by the naked eye, as shown in the pictures taken at different temperatures (see Figure S7 in pg. S9 of Supporting Information), where the melting is complete after the HMF transition. As mentioned before, the MFH experiments are performed in the temperature range where the HMF transition develops. The temperature range of the HMF peak  $(\Delta T_{\rm M})$  is well marked for both heating rates and can be calculated from the extrapolated peak onset and offset temperatures in the  $c_p(T)$  curves: 297.1–310.8 K for 10 K/min and 299.8–309.0 K for 1 K/min. For the heating rate of 10 K/min, where the peaks are better defined, a melting enthalpy value of 40.5 J/g is calculated using eq 1 and taking the area of both peaks, that is, for the whole melting process (LMF + MMF and HMF).

Figure 4b gives the  $c_p(T)$  curves measured with heating rates of 1 and 5 K/min for CBO containing x=0.19 NPs at the concentration of 0.2 wt %. As observed, these curves present differences among them and with respect to the curves of pure CBO. Notice that the presence of NPs results in smaller changes in  $\Delta T_{\rm M}$  than those caused by different heating rates in pure CBO. For the heating rates of 1 and 5 K/min,  $\Delta T_{\rm M}$  of the HMF is between 297 and 310 K. For the analysis of MFH experiment, the  $c_p(T)$  curves reported in Figure 4a,b were used for pure CBO and for CBO-containing NPs, respectively.

Finally, Figure 4c gives the  $c_p(T)$  curve for the paraffin measured with a heating rate of 10 K/min.

Independent from the effects of NPs and heating rate, the important changes in the  $c_p(T)$  curve of CBO should be taken into account for the analysis of the MFH results. In particular, the estimation of the SPA of the system should be revised when the specific heat presents a nonmonotonous evolution, and latent heat is stored or released during the phase transition. In this way, the thermal energy of the system when the applied field is turned on and off can be written, respectively, as

$$m_{\text{CBO}}c_p(T)dT = dQ_{\text{SPA}}(T) - dQ_{\text{loss}}(T) \qquad (H_0 > 0)$$
(3)

$$m_{\text{CBO}}c_p(T)dT = -dQ_{\text{loss}}(T)$$
  $(H_0 = 0)$  (4)

where  $m_{\rm CBO}$  is the mass of the medium (CBO),  $Q_{\rm SPA}$  is the heat released by the magnetic losses of NPs for  $H_0 > 0$ , and  $Q_{\rm loss}(T)$  are the heat losses of system due to the nonadiabatic condition of the MFH experimental apparatus.<sup>34</sup> The amount of  $Q_{\rm loss}$  depends on the MFH apparatus used. We remark again that, according to our measurements of cooling down curves (after the applied field is turned off),  $Q_{\rm loss}$  is lower for the DM100-model than for the F1-D5-model. In addition,  $Q_{\rm loss}(T)$  is expected to depend on the temperature difference between the sample and the environment. The melting enthalpy is considered in the thermal variation of  $c_p(T)$  through eq 1.

Taking into account the appropriate  $c_p(T)$  curve together with eqs 3 and 4, the hyperthermia curves could be divided into four regions: A, B, and C, where the applied field is on  $(H_0)$ > 0) and D, where  $H_0 = 0$ . Figure 5a shows these four regions for sample x = 0.21 (at a concentration of 0.2 wt %, f = 817kHz, and  $H_0 = 16 \text{ kA/m}$ ) using the DM100-model. Region A is in the temperature range below the HMF transition (T < 297K), B coincides with the HFM melting (297 K < T < 309 K), and C is for temperatures above the HMF region (T > 309 K). As discussed previously, the increase in the MFH curve above 306 K could not be associated with a change in the dominant relaxation mechanism due to the strong reduction in the viscosity of CBO above the melting point. In fact, a change in the CBO physical state is observed in the pictures at 307 K compared with that at 305 K (see Figure S7 in pg. S9 of Supporting Information). Also, the reduction in the viscosity of CBO, some degrees below  $T_{\rm F}$  = 309 K, may induce some changes in the spatial arrangement of NPs, as discussed below.

Integration of eqs 3 and 4 in the corresponding interval of temperature results in

$$\int_{T_0}^T c_p(T) dT = \int_{t_0}^t c_p(T) \left(\frac{dT}{dt}\right) dt = \frac{(Q_{SPA} - \Delta Q_{loss})}{m_{CBO}}$$

$$(H_0 > 0)$$
(5)

$$\int_{T_0}^T c_p(T) dT = \int_{t_0}^t c_p(T) \left(\frac{dT}{dt}\right) dt = \frac{-\Delta Q_{\text{loss}}}{m_{\text{CBO}}}$$

$$(H_0 = 0)$$
(6)

For eq 5, the integral limits correspond to the starting time  $t_0$  and the final t, where the field is turned off, with the corresponding temperatures  $T_0$  and T, respectively. For eq 6, these integral intervals represent the time and temperature ranges of region D, where  $H_0 = 0$ . Thus, eq 5 gives information

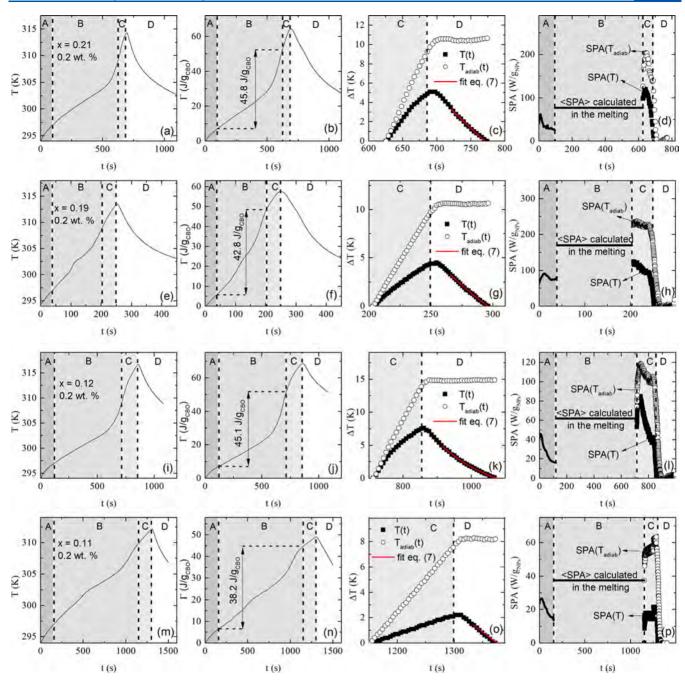


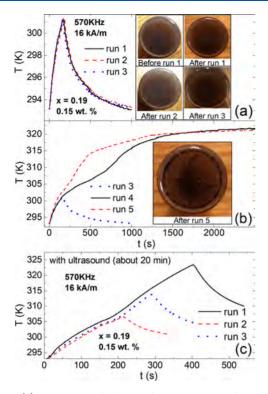
Figure 5. (a) T(t) results of MFH experiments for CBO containing 0.2 wt % of x=0.21 NPs with f=817 kHz and  $H_0=16$  kA/m in the DM100-model. Regions A, B, and C correspond to the temperature range defined below, within, and above the HMF peak in the  $c_p(T)$  curve associated with the melting of CBO + NPs. (b)  $\Gamma(t)$  curves obtained from the MFH results and the line gives the heat variation within the intervals  $T_i$  and  $T_F$ . (c)  $\Delta T(t) = T(t) - T_0$  curve measured for region C fitted with eq 7 and the temperature corrected for adiabatic conditions  $[\Delta T_{\rm adiab}(t) = T_{\rm Adiab}(t) - T_0]$  calculated using eq 8. (d) Estimated SPA values for regions A and C, as well as the mean SPA ( $\langle {\rm SPA} \rangle$ ) estimated for region B. Similar curves for samples x=0.19, x=0.12, and x=0.11 in the same concentration are presented in (e-p), respectively.

about the SPA in regions A, B, and C, while eq 6 provides information on  $\Delta Q_{\rm loss}$ .

Figure 5b gives the corresponding temporal dependence of  $\Gamma(t)$  (eq 2) calculated from the experimental data of MFH (Figure 5a) and  $c_p(T)$  with a heating rate of 5 K/min (see Figure 4b). This graph gives the accumulated thermal energy in CBO, normalized by its mass, due to the magnetic losses from the applied field and the heat loss due to nonadiabatic conditions. This curve is also divided into four regions, taking the corresponding time when the corresponding temperature

of Figure 5a is reached. The increase in the heating rate above 306 K is also observed in these curves.

For region A, it is expected that  $\Delta Q_{\rm loss}$  has a relatively low value in comparison to  $Q_{\rm SPA}$ , as heat losses by the nonadiabatic conditions are small at temperatures close to the ambient temperature ( $T_{\rm e}=293.7$  K). Thus, for region A, the SPA value can be approximated by the quantity  $(m_{\rm CBO}/m_{\rm NPs})c_{\rm p}(T)$  (dT/dt). In fact, a relatively small decrease of the SPA is observed with the increment of time, probably related with a small value  $\Delta Q_{\rm loss}$  that increases with increasing temperature.



**Figure 6.** (a) MFH results for three subsequent runs performed in the D5-F1-model (f = 570 kHz and  $H_0$  = 16 kA/m) for CBO containing 0.15 wt % of x = 0.19 NPs from  $T_0$  to a final temperature below 306 K, followed by cooling to  $T_0$ . (b) Two subsequent runs (4 and 5) measured under the same experimental conditions and performed from  $T_0$  to a final temperature above the melting temperature (T >  $T_{\rm F}$ ). Insets present the picture of samples after the indicated run. (c) Three successive runs of the same sample measured in the D5-F1 model (f = 570 kHz and  $H_0$  = 16 kA/m) with intermediate exposure to ultrasound (about 20 min).

For region C, this approach cannot be used as the temperature of the sample is considerably higher than  $T_{\rm e}$ , and  $Q_{\rm loss}$  should be taken into account. In this way, we propose a correction of the MFH temperature considering the  $Q_{\rm loss}$  obtained from the cooling curve, when the magnetic field is turned off in order to estimate the SPA in region C. The T(t) data in region D were fitted with the following expression that reflects their expected exponential decay with time

$$T(t) = T_{e} + [(T_{t_0} - T_{e})\exp(-\beta(t - t_0))]$$
(7)

where  $T_{t_0}$  is the value of temperature at time  $t_0$  (moment when the field is turned off in this region) and  $\beta$  is the parameter that models the heating loss.  $T_{\rm e}$  is obtained from the low-temperature range of the cooling curve of CBO containing 0.2 wt % of NPs (see Figure S8 in pg. S10 of Supporting Information). The result of this fitting procedure is given in Figure 5c. From this fitting, the corrected temperature, that is, the temperature expected for adiabatic conditions,  $T_{\rm adiab}$ , is calculated from the measured temperature T(t) as

$$T_{\text{adiab}}(t) = T(t) + \beta \left[ \int_{t_0}^t T(t) dT - T_{\text{e}}(t - t_0) \right]$$
 (8)

Both  $\Delta T_{\rm adiab}(t) = T_{\rm adiab}(t) - T_0(t)$  and  $\Delta T(t) = T(t) - T_0(t)$  curves are presented in Figure 5c, together with the fitting of the cooling region. As expected,  $\Delta T_{\rm adiab}(t)$  presents an almost constant value in region D, as is expected for a

system that does not exhibit losses. This result reinforces the fact that our temperature correction procedure is correct. In this way, the corrected value of SPA can be calculated for region C using  $(m_{\rm CBO}/m_{\rm NPS})c_{\rm p}(T)$   $({\rm d}\Delta T_{\rm adiab}(t)/{\rm d}t)$ .

For region B, fitting the SPA dependence with time is not simple because of the HMF melting within this temperature range. Nevertheless, it is possible to estimate a mean SPA value  $(\langle SPA \rangle)$  using eq 5 as follows: (i) the left side of eq 5 in the time interval  $T_i \le T \le T_F$  (see eq 1) could be obtained directly from the data presented in Figure 5b, as indicated, being 45.8  $J/g_{CBO}$ ; (ii) the quantity  $\Delta Q_{loss}$  can be estimated from the equivalent curve from the cooling of CBO + NPs until the temperature attains  $T_e$  (see Figure S8 in pg. S10 of Supporting Information), being  $36.3 \text{ J/g}_{CBO}$ . Therefore, taking these values into account, the mean value of  $\langle SPA \rangle$  is found to be 77 W/  $g_{NPs}$ . This  $\langle SPA \rangle$  value is shown in Figure 5d, together with the values of SPA obtained for regions A and C (here the values obtained for  $\Delta T(t)$  using the same expression are also included, i.e., uncorrected by  $Q_{loss}$ ). Similar analysis was performed for samples x = 0.19 (Figure 5e-h), x = 0.12(Figure 5i–l), and x = 0.11 (Figure 5m–p). Sample x = 0.19presents a higher heating rate in MFH experiments when compared with sample x = 0.21, resulting in the following less evident changes: the decrease of SPA in region A with increasing temperature and a less pronounced decrease in the heating rate between  $T_i = 297$  K. In contrast, samples x = 0.12and x = 0.11 have a smaller heating rate in comparison with sample x = 0.21, making the changes mentioned above more pronounced.

The  $\langle {\rm SPA} \rangle$  values estimated for region B has an intermediate value between those obtained for regions A and C in all samples. Probably, the SPA is not constant along this region, with a probable increment above 306 K. The decrease in the heating rate of MFH curves between 297 and 306 K could be probably associated with two contributions. First, the increase of  $\Delta Q_{\rm loss}$  with respect to  $Q_{\rm SPA}$  with increasing temperature, which could be observed as the decrease of SPA with increasing temperature in region A, is more evident for samples with lower SPA. Second, the latent heat of CBO melting reduces the effects of  $Q_{\rm SPA}$  with temperature increment. It is more evident for samples with smaller  $Q_{\rm SPA}$ .

SPA in region C increases between 2.5 and 3 times for all samples with respect to the values in region A, corresponding to the clearly noticed increment in the heating rate observed in the T(t) curves measured in MFH experiments. This increment in the SPA for region C is reflected in the increased slope of the MFH results above 306 K, some degrees below the ending of the melting and corresponding to a physical change in the CBO, with a strong reduction in the viscosity. Despite the reduction of viscosity with melting,  $\tau_{
m N}$  should be several orders of magnitude smaller than  $\tau_{\rm B}$  (see Figure 3b), which is reinforced by the agglomeration process discussed below. However, the phase transition of CBO with the consequent reduction in the viscosity allows other changes in the sample with consequences in the magnetic response of the system, as discussed below. The SPA in region C remains almost constant until the applied field is turned off for samples x = 0.19 and x = 0.190.11. For samples x = 0.21 and x = 0.12, the increment in the SPA is slightly slower and a decrease in the SPA value is observed before the applied field is turned off. Interestingly, the SPA in region C is almost constant for smaller NPs, and it decreases with time for the two larger ones, which could also be related to an agglomeration or precipitation phenomenon

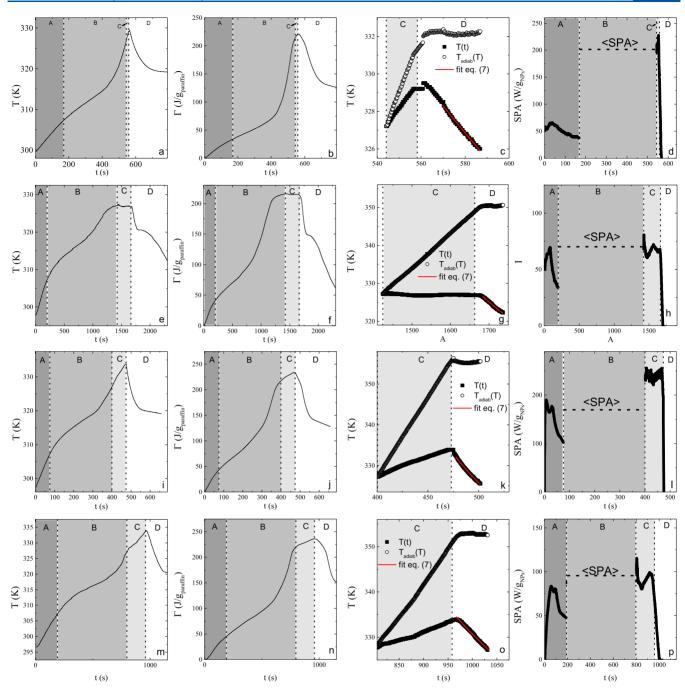


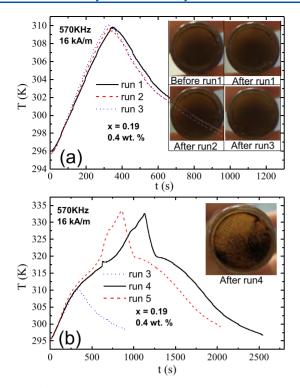
Figure 7. (a) T(t) results of MFH experiments for paraffin containing 0.4 wt % of x=0.21 NPs with f=570 kHz and  $H_0=16$  kA/m in DM100-model. Regions A, B, and C correspond to the temperature range defined below, within, and above the melting peak in the  $c_p(T)$  curve. (b)  $\Gamma(t)$  curves obtained from the MFH results and the line gives the heat variation within the interval  $T_i$  and  $T_F$ . (c)  $\Delta T(t) = T(t) - T_0$  curve measured for region C fitted with eq 7 and the temperature corrected for adiabatic conditions calculated using eq 8. (d) Estimated SPA values for regions A and C, as well as the mean SPA ( $\langle SPA \rangle$ ) estimated for region B. Similar curves for samples x=0.19, x=0.12, and x=0.11 in the same concentration are presented in (e-p).

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with the reduction in the viscosity of CBO above the melting point.

A reproducible behavior was observed in the T(t) curves after three successive heating cycles within  $T_0 < T \le 301$  K, and subsequent cooling (Figure 6a, runs 1, 2, and 3) in the DS-F1-model (f = 570 kHz and  $H_0 = 16$  kA/m) for CBO containing 0.15 wt % of sample x = 0.19. On the other hand, heating the samples above the melting region resulted in a clear nonreproducible data (runs 4 and 5 in Figure 6b). It can be noted that the T(t) curve for run 4 is similar to run 3 up to T

~ 301 K, whereas in run 5, deviations from run 3 are observed even below that temperature. We associate this change in the heating of the system with the agglomeration process of the NP in the melted CBO, being less viscous, probably induced by the magnetic field gradient inside the coil and, to a lesser extent, with gravity. Different spatial configurations and NP aggregation degrees after successive runs could change the SPA, as observed in the analysis presented in Figure 5, and it could also lead to the observation of hysteresis behavior. In fact, the formation of large asymmetric agglomerates (non-



**Figure 8.** (a) MFH results for three subsequent runs performed in the D5-F1-model with  $f=570\,$  kHz and  $H_0=16\,$  kA/m for paraffin containing 0.4 wt % of  $x=0.11\,$  NPs from  $T_0$  to a final temperature below 316 K, followed by cooling to  $T_0$ . (b) Two subsequent runs (4 and 5) measured under the same experimental conditions and performed from  $T_0$  to a final temperature above the melting temperature  $(T>T_{\rm F})$ . Insets present the picture of the samples after the indicated run.

planar or bulk) is clearly observed by the naked eye after successive runs (see Figure 6b), which is not observed after successive runs when the heating temperature is kept below 301 K (see the inset of Figure 6a). The irreversible effect in MFH curves becomes reversible if the particles are dispersed again, for example, with ultrasound exposure, as shown in Figure 6c for three successive runs of the same sample measured in the D5-F1-model (f = 570 kHz and  $H_0 = 16 \text{ kA/m}$ ) with intermediate exposure to ultrasound (about 20 min).

Figure 7a-p presents a similar analysis to that of Figure 5 for samples x = 0.21, 0.19, 0.12, and 0.11 dispersed in paraffin at a concentration of 0.4 wt % with  $H_0 = 16 \text{ kA/m}$  and f = 570 kHz. Here, the quantity  $\Delta Q_{\rm loss}$  can be estimated from the equivalent curve from the cooling of paraffin until the temperature attains  $T_{\rm e}$  (see Figure S9 in pg. S11 of Supporting Information). In general, the graphics present tendencies similar to those ones for the sample dispersed in CBO, except for the higher temperature for the observation of increment in the heating rate and the effects of phase transition. In a similar way to the sample dispersed in CBO, Figure 8a shows the reversibility of hyperthermia results for sample x = 0.11 dispersed in paraffin measured in the D5-F1-model (f = 570 kHz and  $H_0 = 16 \text{ kA/}$ m) when the maximum temperature attained is below 316 K (runs 1-3). Images taken (inset of Figure 8a) before and after each run evidence that no changes are observed in this temperature range. However, when the temperature overcomes the melting point (runs 4 and 5 in Figure 8b), NP agglomeration (see the inset of Figure 8b) and irreversibility are obtained, similarly to that observed for CBO. Interestingly, the increment in the heating rate is not observed when the NPs are dispersed in toluene (see Figure S10 in pg. S12 of Supporting Information), without a phase transition in the temperature range of the MFH experiment, and agglomeration is observed in the beginning of the experiment.

Considering that the change in the MFH curves above the melting temperature can be correlated with this agglomeration process, some speculation can be made with respect to the agglomeration process. There is currently some debate about the effects of particle agglomeration on the heating mechanisms. While some works reported a reduction of the SPA due to the formation of bulk agglomerates, <sup>6,9</sup> there is also experimental evidence that the formation of elongated agglomerates (e.g., needle-like, cylinder, or chain-like structures) increases the SPA compared to that of the welldispersed NPs. 12-14 Recently, some theoretical models and experimental work showed that the actual effects of clustering could be either way, depending on the value of effective magnetic anisotropy and anisotropy energy barrier of NPs. 35,36 Basic considerations from magnetostatics indicate that in the presence of a nonuniform magnetic field, the NPs tend to form elongated structures aligned with the magnetic field gradient. Probably, in our work, the reduction in the viscosity of CBO above the melting point allows the alignment of easy axis of NPs with the applied field at the same time that nonplanar structures, probably elongated ones, are induced by the combination of the magnetic field gradient inside the coil and, to a lesser extent, to gravity. Any real applicator solenoid (even in a perfectly constructed one) will contain a nonuniform magnetic field along the coil axis because of finite size effects. The formation of elongated structures after the first heating cycle, and the consequent increase in SPA in our case, is consistent with this explanation. According to this, the resulting heating curve will therefore depend on the magnetic field gradient (a characteristic of each MFH apparatus) and the NP concentration because of the interparticle interaction strength.

The low anisotropy barrier of the systems studied here could play an important role in the increment of the SPA after agglomeration. A system with a low anisotropy results in an increment in the SPA in the case of agglomeration by two reasons: first, the NPs tend to orient the easy axis with the applied field; second, in the case of formation of agglomerates with axial symmetry.<sup>37</sup>

The results presented in this work call for the attention of the complex heat-transfer process in MFH experiments from the NPs to the medium, where the thermodynamic characteristic of media should be taken into account to evaluate the efficiency of NP systems in MFH treatments when they are applied in a different environment. In particular, CBO and paraffin are used to emulate a high-viscosity environment and evaluate the efficiency of MFH when the Néel relaxation is the dominant mechanism, evidencing how the intrinsic transition of media could affect the heating in an MFH experiment. Several aspects such as the presence of latent heat in a transition, strong variation of specific heat with temperature, and the formation of NP agglomerates when the viscosity diminishes after melting are some of the aspects that should be evaluated in different media with a complex structure or complex thermal response to analyze the MFH results and therapy effectiveness.

## CONCLUSIONS

The SPA of Zn<sub>x</sub>Fe<sub>3-x</sub>O<sub>4</sub> magnetic NPs dispersed in CBO and paraffin presents a complex behavior with temperature related to the melting of these media. Samples present distinct morphology and magnetic properties, specifically distinct anisotropy energy barrier. For all samples, the magnetic relaxation mechanism is dominated by Nèel relaxation, independent of the CBO or paraffin phase, below and above the melting points. The complex SPA behavior with temperature for this system is correlated with the nonlinear thermal response of viscosity and thermodynamic properties of the medium, including a phase transition in the temperature range of MFH experiment. The variation of  $c_p$  of the medium with temperature, as well as the latent heat of melting, is important to analyze the SPA evolution of all samples. The heating rate strongly depends on the variation of these thermodynamic properties.

Despite the change in the viscosity of media with melting being not high enough to change the dominant relaxation mechanism, it allows the NP agglomeration induced by the applied field gradient of the MFH coil, which leads to changes in the SPA when the system is heated above the melting point. This effect in the SPA depends on the NP concentration, and it also results in a hysteresis in MFH experiments for subsequent runs when the melting temperature is attained.

Finally, this work highlights the importance of measuring the thermodynamic properties of media where the NPs would be applied, in order to evaluate the efficiency of MFH treatment, especially in complex media where different transitions could take place.

# ASSOCIATED CONTENT

# Supporting Information

The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acs.jpcc.0c06843.

Compositional analysis by PIXE of the four samples; XRD measurements of sample x = 0.21 as a representative of samples; saturation magnetization (M<sub>s</sub>) determined from magnetic measurements; obtaining the blocking-temperature distribution  $f(T_B)$  from magnetization measurements as a function of temperature; magnetization measurements of CBO and paraffin without NPs at 300 K; MFH measurements of CBO and paraffin without NPs; changes in the physical aspects of CBO with temperature; cooling curve of CBO + NPs heated in a hot plate up to a temperature above the melting point and its analysis with respect to quantity  $\Gamma(t)$ ; cooling curve of paraffin with NPs heated in a hot plate up to a temperature above the melting point and its analysis with respect to quantity  $\Gamma(t)$ ; and MFH of the four samples dispersed in toluene (PDF)

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### Notes

The authors declare no competing financial interest.

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