

# Experimental determination of the critical loci for $\{n\text{-C}_6\text{H}_{14}$ or $\text{CO}_2$ + alkan-1-ol} mixtures. Evaluation of their critical and subcritical behavior using PC-SAFT EoS.

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## ■ ABSTRACT

Vapor-liquid critical locus ( $x$ ,  $T_c$ ,  $P_c$ ) has been determined, in the whole range of mole fractions, for the systems  $\{n\text{-hexane} + \text{methanol, or } + \text{ethanol, or } + \text{propan-1-ol, or } + \text{butan-1-ol}\}$  and  $\{\text{CO}_2 + \text{methanol, or } + \text{ethanol, or } + \text{propan-1-ol, or } + \text{butan-1-ol}\}$ .

A comprehensive bibliographic review for the vapor-liquid equilibrium (VLE) and the critical locus of these systems has been performed, and they have been modelled with PC-SAFT EoS. The three parameters that characterize the segments of pure compounds have been rescaled from their critical point values. In all cases, the classical mixing rules and temperature-dependent binary interaction parameters  $k_{ij}(T) = k_{ij}^0 + k_{ij}^1 T$  have been used.

The average deviations obtained for the  $n\text{-hexane} + \text{alkan-1-ol}$  binary mixtures are: for critical loci, mean relative deviation in critical temperature  $MRD(T_c) = 0.47\%$  and in critical pressure  $MRD(P_c) = 3.38\%$ ; for VLE, mean relative deviation in bubble pressure  $MRD(P) = 2.90\%$  and absolute deviation for the solvent mole fraction in the vapor phase  $\Delta y_{\text{C}_6\text{H}_{14}} = 0.031$ .

The average deviations obtained for the  $\text{CO}_2 + \text{alkan-1-ol}$  binary mixtures are:  $MRD(T_c) = 1.91\%$  and  $MRD(P_c) = 5.93\%$ ;  $MRD(P) = 7.07\%$  and  $\Delta y_{\text{CO}_2} = 0.022$ .

**Keywords:** Critical points; alkan-1-ol;  $n\text{-hexane}$ ; carbon dioxide; PC-SAFT.

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## 1. Introduction

Supercritical media exhibit two important and interesting properties as opposed to simple liquid solvents: (i) The values of densities can vary continuously from those typical of liquids to those typical of gases. By working at temperatures slightly higher than the critical temperature, it is possible to reach a broad range of densities by simply changing temperature and pressure conditions. (ii) The second property of supercritical fluids (SCF) is also related to the very high compressibility of the fluid near the critical point region. In this “compressible regime”, the very high susceptibility of the solvent density to small variations of pressure generates strong density fluctuations at the microscopic level [1-3]. The presence of such microscopic density fluctuations in the solvent is therefore expected to have significant effects on the molecular arrangement and dynamics of the solute in such compressible SCF solutions. In particular, attractive solutes are expected to induce a region of local solvent density that can be greater than the density of the bulk solvent [4,5]. Additionally, the extent of this density enhancement is, at least partly, driven by the relative strength of solute-solvent versus solvent-solvent interactions.

Supercritical carbon dioxide (scCO<sub>2</sub>) is often regarded as a “green” solvent because it is recyclable, has low toxicity, and is a nonflammable fluid. It can be used in the control of reaction rates, in the developing of efficient separation processes, and in the manufacturing of various kinds of special materials due to its easy tunability of solvent properties. However, although CO<sub>2</sub> is the most commonly used supercritical fluid, it is not the only one. In recent years, several industrial processes that use other types of fluids in the supercritical state have been developed. For example, supercritical hexane has been used as a reaction media in several processes such as hydrodeoxygenation of biocrude [6], Fischer-Tropsch (FT) synthesis [7,8], SynGas process [9,10], etc.

However, these fluids are only capable of dissolving polar and ionic materials to a very small extent, a fact which greatly limits their industrial use. To circumvent this disadvantage, some other polar compounds, such as small-chain alcohols, can be added as cosolvents to enhance the capacity of these fluids to dissolve this type of materials. Therefore, in order to understand this behavior it is essential to determine the exact type of molecular interactions present in non polar SCF - alcohol (cosolvent) systems. This study can be approached from a thermodynamic point of view through the experimental determination of the critical loci of these systems, and by means of modelling the behavior of these fluids in the upper limit of the gas-liquid phase equilibrium.

When using an alkane as a SCF together with an alcohol, the only non-dispersive interaction present in the mixture is the alcohol - alcohol hydrogen bonding, which can lead to different types of molecular aggregates. On the other hand, those interactions emerging when alcohols act as cosolvents in the scCO<sub>2</sub> media are much more complex. In addition to the non-dispersive interactions and the hydrogen bonds among alcohol molecules, there exist some other specific interactions: carbon atom of CO<sub>2</sub> - oxygen atom of alcohol and CO<sub>2</sub> - alcohol hydrogen bonding (between an oxygen atom of CO<sub>2</sub> and the hydrogen atom of the hydroxyl group). To develop this study, it is necessary to take into account the nature of CO<sub>2</sub>.

Although CO<sub>2</sub> was originally considered to be a non-polar solvent comparable to alkanes because of its low dielectric constant and zero dipole moment, this view is slowly changing. The charge separation and electronic structure of CO<sub>2</sub> (the carbon atom in a CO<sub>2</sub> molecule is electron deficient, whereas the oxygen has two lone pairs of electrons) generate a significant quadrupole moment and allow it to act, depending on its environment, either as a Lewis acid (LA) or as a Lewis base (LB). These conditions can induce a dipole moment in the CO<sub>2</sub> molecule. In the above situation, the carbon atom behaves as an electron acceptor from a neighboring molecule, whereas the oxygen atom plays as an electron donor. The miscibility of cosolvents such as alcohols in CO<sub>2</sub> is closely linked to this aspect of the carbon dioxide molecule. In general, sp<sup>3</sup> oxygen atoms are better electron donors than sp<sup>2</sup> oxygen atoms. Therefore, in CO<sub>2</sub> - alcohol mixtures, oxygen atoms from an alcohol are also expected to participate in a LA - LB interaction (electron donor - acceptor, EDA, complex) similar to that of the CO<sub>2</sub> - carbonyl group. Danten et al. [11] and van Ginderen et al. [12] show how the interaction between CO<sub>2</sub> and sp<sup>3</sup> oxygen of methanol is energetically almost as favorable as those calculated by Raavendran and Wallen [13] for the CO<sub>2</sub> - acetaldehyde or methyl acetate mixtures.

As mentioned above, the CO<sub>2</sub> oxygen atoms could participate in hydrogen bonding with molecular systems carrying electron-deficient hydrogen atoms: Raavendran and Wallen's ab initio calculations [13,14] revealed that in CO<sub>2</sub> + acetaldehyde or + methyl acetate systems, the CO<sub>2</sub> oxygen participates in a cooperative C-H...O hydrogen bond, apart from the EDA interaction.

Raman spectroscopic studies of acetaldehyde and CO<sub>2</sub> mixtures [15] showed the presence of both interactions: EDA complex, corresponding to the carbonyl stretching band red-shifting, and a blue-shifting attributed

to the cooperative C-H...O hydrogen bond between the aldehyde C-H and the CO<sub>2</sub> oxygen. Fujii et al. [16] used IR spectroscopy to reveal the formation of conventional hydrogen bonds between an oxygen atom of CO<sub>2</sub> and hydroxyl (OH) groups. Saharay and Balasubramanian [17] carried out Car-Parrinello molecular dynamics simulation studies of a system containing ethanol (EtOH) and CO<sub>2</sub>. They concluded that carbon dioxide and ethanol can interact with each other by forming an EDA complex or through the formation of a hydrogen bond. Xu et al. [18] analyzed and compared, using Monte Carlo simulations, the following three interactions in some EtOH + CO<sub>2</sub> mixtures: EtOH - EtOH hydrogen bonding, EtOH - CO<sub>2</sub> hydrogen bonding and EtOH - CO<sub>2</sub> EDA bonding.

In our current investigation, the critical loci of mixtures containing *n*-hexane or carbon dioxide + alkan-1-ols have been determined experimentally along the whole composition range. Likewise, an exhaustive review of the critical locus and vapor-liquid equilibrium of these systems has been carried out with the aim of modelling its thermodynamic behavior, both in critical and subcritical conditions.

## 2. Model

In this work, the PC-SAFT model, developed by Gross and Sadowski [19,20] has been used. In this model, molecules are conceived to be chains composed of spherical segments in which the pair potential for the segment of a chain is given by a modified square-well potential. When the molecules exhibit various attractive interactions, the equation of state is given as the sum of the ideal-gas contribution, a hard-chain term, a contribution for the dispersive attraction and several terms for associating, dipolar and quadrupolar interactions. The form of the PC-SAFT equation of state written in terms of the Helmholtz energy,  $a$ , is:

$$a = a^{id} + a^{hc} + a^{dis} + a^{assoc} + a^{polar} \quad (1)$$

$$a = a^{id} + a^{hc} + a^{dis} + a^{assoc} + (a^{QQ} + a^{DD} + a^{QD})$$

For the pure compounds a maximum of 5 parameters are needed: the segment number,  $m$ , the segment diameter,  $\sigma$ , the segment energy parameter,  $\varepsilon$ , the volume of association,  $\kappa^{A_i B_i}$ , and the energy of association,  $\varepsilon^{A_i B_i}$ .  $m$ ,  $\sigma$  and  $\varepsilon$  (“geometric parameters”) are needed for every molecule.  $\kappa^{A_i B_i}$  and  $\varepsilon^{A_i B_i}$  (“association parameters”) are only needed if the molecule is self-associated and therefore the association scheme of the compound should be established. Due to their physical meaning, the association parameters ( $\kappa^{A_i B_i}$ ,  $\varepsilon^{A_i B_i}$ ) could be

estimated from molecular orbital calculations or based on experimental values of the enthalpy and entropy of hydrogen bonding [21-23]. Thus, only three parameters ( $m$ ,  $\sigma$ ,  $\varepsilon$ ) remain to be fit to vapor pressures and liquid densities. These parameters provide an accurate representation for both volumetric and vapor-liquid equilibrium properties, but they always overestimate the values for the critical properties. Other SAFT versions have been proposed to describe the critical area at the expense of using more adjustable parameters [24,25]. On the other hand, Cismondi et al. [26] present a rescaling of PC-SAFT pure-compounds parameters from critical temperature and pressure ( $T_c$  and  $P_c$ ), for which the critical point is matched. We also rescaled the PC-SAFT pure-compounds parameters for the CO<sub>2</sub> + alkane mixtures in previous works [27,28], and we were able to represent the volumetric and critical mixture properties without major deviation.

Following this approach, both properties, VLE phase equilibria and critical locus of each studied mixture, are going to be represented through a single set of pure-compounds parameters. We calculated the pure CO<sub>2</sub> geometric parameters ( $m$ ,  $\sigma$ ,  $\varepsilon$ ) in a previous work [27]. For pure *n*-hexane and pure alkan-1-ols these parameters ( $m$ ,  $\sigma$ ,  $\varepsilon$ ) have been rescaled from their critical points using the method described by Heidemann et al. [29], employing the objective function:

$$OF = \left[ \left( \frac{T_c^{\text{exp}} - T_c^{\text{cal}}}{T_c^{\text{exp}}} \right)^2 + \left( \frac{P_c^{\text{exp}} - P_c^{\text{cal}}}{P_c^{\text{exp}}} \right)^2 \right] \quad (2)$$

where “exp” and “cal” superscripts refer to the experimental and calculated values, respectively.

The association parameters ( $\kappa^{A_i B_i}$  and  $\varepsilon^{A_i B_i}$ ) for the pure alcohols have been extracted from Gross and Sadowski [20], where the association scheme 2B (molecule with two association sites, 1-electron donor and 1-electron acceptor) [30] was used. CO<sub>2</sub> has been considered as a non self-associated molecule [27,28].

When dealing with mixtures, classical mixing rules have been used and temperature-dependent binary interaction parameters  $k_{ij}(T) = k_{ij}^0 + k_{ij}^1 T$  have been introduced. Several authors [31-35] have shown that the use of a temperature-dependent binary interaction parameter is justified if the modelling temperature range is wide or the mixtures are very asymmetric, either in size or interactions. Critical loci calculations were carried out using the method described by Heidemann et al. [29]. For VLE we have used bubble point calculations, which obtain bubble

pressure and vapor-phase composition from liquid-phase composition at a given temperature. The estimation of the  $k_{ij}(T)$  parameters from VLE data has been performed using the objective function:

$$OF = \sum_{i=1}^N \left( \frac{P_i^{\text{exp}} - P_i^{\text{cal}}}{P_i^{\text{exp}}} \right)^2 \quad (3)$$

### 3. Experimental Section

#### 3.1. Materials.

The compounds were used as received without further purification. Table 1 shows their purity, their water content, the suppliers and our experimental values for  $T_c$  and  $P_c$ , as well as those recommended by the National Institute of Standards and Technology (NIST) [36].

#### 3.2. Apparatus and procedures.

The experimental setup used in this work is the same as that described in previous studies [37]. The flow apparatus was designed by ARMINES at the École Nationale Supérieure des Mines de Paris (France) and manufactured by TOP-INDUSTRIE. The apparatus allows critical property measurements ( $P_c$  and  $T_c$ ) of pure compounds and mixtures up to 700 K and 20 MPa. These measurements are carried out by observing the critical opalescence (a video is available in the online version) in a sapphire transparent cell. Similar facilities have been used in previous works of Soo et al. [38], Horstman et al. [39-42], Guilbot et al. [43], and Juntarachat et al. [44,45]. The uncertainties in the critical temperature and the critical pressure for pure compounds are [37]: repeatability in the critical temperature  $\leq 0.14$  K, repeatability in the critical pressure  $\leq 0.011$  MPa, and the confidence intervals are  $c.i.(T_c) < 0.1$  K and  $c.i.(P_c) < 0.01$  MPa. For the mixtures, the repeatabilities in critical temperature and pressure are  $\leq 0.15$  K and  $\leq 0.013$  MPa, and the confidence intervals calculated are  $c.i.(T_c) < 0.32$  K and  $c.i.(P_c) < 0.034$  MPa. Finally, for the mixtures studied in this work a mean value uncertainty in the mole fraction,  $u(x_j) = \pm 0.0015$  has been obtained.

### 3.3. Experimental results.

#### *n*-hexane + alkan-1-ol systems

Experimental results ( $x$ ,  $T_c$ ,  $P_c$ ) for the critical locus of the systems *n*-hexane + alkan-1-ol (methanol, ethanol, propan-1-ol, butan-1-ol) are given in Table 2 and Figures 1a, 1b, 1c. Each mixture was studied over the whole range of compositions, with at least twenty-one experimental points (including pure compounds ones) at mole fraction intervals of approximately 0.05.

All the systems display an uninterrupted (gas + liquid) critical locus which connects the critical points of the pure components. This indicates that the fluids belong either to Type I or Type II fluid phase behavior, according to the classification of van Konynenburg and Scott [46]. Several authors [47-50] report partial miscibility for *n*-hexane + methanol mixtures, a fact which implies that they are Type II fluids. For the rest of the systems, no indication of partial miscibility has been found in the literature. *n*-hexane + methanol, or + ethanol or + propan-1-ol present a minimum temperature point in the critical locus curve. This is characteristic of systems whose components have small differences in  $T_c$  and form positive (minimum boiling) azeotropes extending up to their critical region [51]. The lower the number of carbon atoms in the alkan-1-ol (the closer its  $T_c$  to that of the *n*-hexane) the deeper the minimum is. Simultaneously, as the number of carbon atoms in the alkan-1-ol increases (and with it, its  $T_c$ ), the minima in critical temperature points shift to richer compositions in *n*-hexane. The mixture containing butan-1-ol, whose  $T_c$  is the highest, does not present a temperature minimum. The  $P_c$ - $x$  projections of the systems are monotonic functions.

In the literature there exist few data on the critical points of *n*-hexane + alkan-1-ol studied mixtures [38,50,52-63], and more than half of the references do not provide the three variables  $x$ ,  $P_c$  and  $T_c$ , or do not cover the whole range of compositions or neither of them. The whole set of experimental data (from this work and literature) is represented in Figures SF1 - SF6. These figures and the comparison between our experimental results and those from literature are included in the Supplementary Data.

The experimental results ( $x$ ,  $T_c$ ,  $P_c$ ) for the critical locus of the systems CO<sub>2</sub> + alkan-1-ol (methanol, ethanol, propan-1-ol and butan-1-ol) are given in Table 3 and Figures 2a, 2b, 2c. Each mixture was studied over the whole range of compositions, with at least twenty-one experimental points (including pure compounds ones) at mole fraction intervals of approximately 0.05.

From our results we deduce a fluid phase behavior of Type I or Type II for these mixtures, according to the classification of van Konynenburg and Scott [46], although many discrepancies have been found in the literature about the exact corresponding type. Lam et al. [64] indicate that the lightest alkan-1-ol exhibiting LLV immiscibility with CO<sub>2</sub> is propan-1-ol. Likewise, Polishuk et al. [65], from experimental results of several authors, assign CO<sub>2</sub> + methanol and CO<sub>2</sub> + ethanol to Type I and CO<sub>2</sub> + butan-1-ol to Type II. Secuianu et al. [66-68] attribute the mixtures containing methanol and ethanol to Type I as well, and include CO<sub>2</sub> + propan-1-ol in Type III. Nevertheless, Roman-Ramírez et al. [31] report that CO<sub>2</sub> + methanol or + ethanol or + propan-1-ol belong to Type II while Peters and Gauter [69] state that the four systems (CO<sub>2</sub> + methanol, or + ethanol, or + propan-1-ol, or + butan-1-ol) are Type II.

The critical loci curves have neither maxima nor minima in temperature, although all of them present a point of maximum critical pressure. This behavior is typical of those systems whose components differ greatly in physical and chemical properties but do not form azeotropes [51]. Ethanol, propan-1-ol and butan-1-ol have lower  $P_c$  than CO<sub>2</sub> and such  $P_c$  values reduce as the number of C atoms in the alkan-1-ol increases. This results in these mixtures exhibiting higher critical pressure values the higher the number of carbon atoms present in the alkan-1-ol.  $P_c$  of methanol is higher than that of CO<sub>2</sub> and the maximum critical pressure value for the mixture lays between CO<sub>2</sub> + propan-1-ol and CO<sub>2</sub> + butan-1-ol ones. The compositions at the maximum critical pressure points are located in the CO<sub>2</sub>-rich zone, and they shift to regions richer in CO<sub>2</sub> as the number of carbon atoms in the alkan-1-ol increases.

Critical point data of CO<sub>2</sub> + methanol [54,70-81] and CO<sub>2</sub> + ethanol [73,75-78,82-93] mixtures are abundant in the literature, but they are scarcer for mixtures with propan-1-ol [68,73,75,78,88,94] or butan-1-ol [73,75,78,95,96]. 90% of the references do not give the three variables  $x$ ,  $P_c$  and  $T_c$ , or do not cover the whole range of compositions or neither of them. The whole set of experimental data (this work and literature) is represented in Figures SF7 - SF10.



These figures and the comparison between our experimental results and those from literature are included in the Supplementary Data.

The agreement between the authors is in general better in the  $P_c$ - $T_c$  projection than in the  $T_c$ - $x$  and  $P_c$ - $x$  planes. This fact becomes much more evident for the  $\text{CO}_2$  + methanol or + ethanol systems. Errors in the determination of the real composition of the critical mixtures could be attributed to the difficulty in achieving a homogeneous mixture. To overcome this problem in our current investigation, we have carried out all our experimental measurements by paying special attention to several aspects of the setup: the pump flows have been adjusted according to the viscosities and densities of the chemicals, and the length of the tubing conducting the mixture to the cell has been increased. Another contribution to the aforementioned disagreements could also be found in the different sources, purities and water contents of the chemicals used by the different authors.

## 4. Discussion

### 4.1. *n*-hexane + alkan-1-ol systems

Mixtures that contain a polar component and an alkane show a transitional behavior between non-associating and associating mixtures. The specific interactions (polar and hydrogen bonding) exhibited between alcohol molecules are strongly affected when surrounded even by a single alkane molecule in their proximity. As a result, modelling of *n*-hexane + alcohol mixtures should be based preferentially on theories with strong molecular origin that contain a quantitative account of the pertinent intermolecular forces between like and unlike molecules such as PC-SAFT EoS. In this work, *n*-hexane + alkan-1-ol systems have been modelled over the whole composition range and over the temperature and pressure ranges which are reported in Table 4.

Table 5 shows the geometric pure-compounds parameters for *n*-hexane + alkan-1-ol mixtures rescaled in this work, as well as the association parameters for pure alkan-1-ols with a 2B association scheme, taken from reference [20].

For the mixtures, classical mixing rules have been used and only one temperature dependent binary interaction parameter  $k_{ij}(T) = k_{ij}^0 + k_{ij}^1 T$  has been introduced to model both VLE and critical locus of each system.

We have used for modelling about 1970 VLE experimental values from the literature [48,50,52,55-57,97-130] and 245 critical experimental values from this work and other literature data [38,50,52-63]. Unpublished data from Laga [63], determined with the same apparatus that we used in our investigation, are included. Tables 6 and 7 show the number of experimental points and the corresponding authors for both critical loci and VLE, as well as the comparison of PC-SAFT results with experimental data by means of the values of the mean relative deviations,  $MRD$ , for critical temperature, critical pressure and bubble pressure, obtained from equation 4,

$$MRD(X) = \frac{100}{N} \sum_{n=1}^N \left| \frac{X_n^{\text{exp}} - X_n^{\text{calc}}}{X_n^{\text{exp}}} \right| \quad (4)$$

where  $X$  refers to a generic variable and  $N$  is the number of experimental points. For VLE, the absolute deviations for the solvent mole fraction in the vapor phase  $\Delta y_{\text{C}_6\text{H}_{14}}$  (eq. 5) are also included.

$$\Delta y = \frac{1}{N} \sum_{n=1}^N |y_n^{\text{exp}} - y_n^{\text{cal}}| \quad (5)$$

Figures 1a, 1b and 1c show the experimental and calculated critical loci for these systems and Figures 3 and 4 show VLE (experimental and calculated) for *n*-hexane + methanol or + ethanol mixtures. The corresponding figures for the rest of the VLE systems are included in the Supplementary Data (Figures SF11 - SF14).

As it can be seen, there is a good agreement between experimental values and those calculated by using a single set of pure-compounds parameters and only one temperature-dependent binary interaction parameter for the two kind of properties of each mixture. The mean values of the deviations are:  $MRD(T_c) = 0.47\%$  and  $MRD(P_c) = 3.38\%$  for the critical locus and  $MRD(P) = 2.90\%$  and  $\Delta y_{\text{C}_6\text{H}_{14}} = 0.031$  for the VLE.

The modelling has been carried out using temperature-independent binary interaction parameters  $k_{ij}$  as well. Tables ST1 and ST2 (Supplementary Data) show values for  $k_{ij}(T)$  and  $k_{ij}$  as well as  $MRD$  and  $\Delta y$  for each system in both calculations. As it can be observed, the values obtained for critical loci do not differ greatly from those calculated with  $k_{ij}(T)$  as expected due to the fact that critical temperatures of both components are similar. However, the results for VLE are worse than those obtained with  $k_{ij}(T)$ .

Some studies of the performance of different SAFT types in alkane - alkanols mixtures have been published

[32,33,131-137]. None of the authors carried out their studies in a wide range of temperatures, neither do they calculate simultaneously the VLE and the critical locus of the systems. Table ST3 (Supplementary Data) shows the deviations obtained by the preceding authors and those obtained by us. As it can be observed, our deviations are similar to those obtained by other authors even though we have modelled with only one binary interaction parameter both the critical locus and the VLE over the whole composition range and over a wide range of temperature.

#### 4.2. $\text{CO}_2$ + alkan-1-ol systems

We have used PC-SAFT EoS to model the systems  $\text{CO}_2$  + alkan-1-ol as well, but the scheme to represent these mixtures has to differ from that used to represent *n*-hexane + alkan-1-ol mixtures, since these systems present different types of interactions and thus very different behavior from the preceding mixtures (Figures 1a, 1b, 1c and 2a, 2b, 2c).

In these systems, beside the dispersive interactions and alcohol - alcohol hydrogen bonding, there are other specific interactions: carbon atom of  $\text{CO}_2$  - oxygen atom of alcohol and  $\text{CO}_2$  - alcohol hydrogen bonding (between an oxygen atom of  $\text{CO}_2$  and the hydrogen atom of the hydroxyl group). The association theories belonging to the SAFT family explicitly account for self- and cross-association, or solvation phenomena, due to the Lewis acid - Lewis base interaction. When modeling systems containing  $\text{CO}_2$  and alcohols, the important question of what model to choose arises. There are many studies in the literature on this topic. Some of them [34,138] conclude that the solvation/association effect for  $\text{CO}_2$  must be included, whereas others [31] remark that the introduction of polar contributions in the model (PCSAFT-Q, PCSAFT-D, PCSAFT-QD) do not improve it substantially. Finally, other authors [33,94,95,133,139,140,143] utilize other models from which some of them obtain better results, but at the expense of increasing the number of parameters. None of these studies performs an exhaustive correlation from bibliographic VLE and critical data. Table ST4 (Supplementary Data) shows the deviations obtained by the preceding authors (when numeric values are available) and those obtained by us. As it can be observed, our deviations are similar to those obtained by other authors even though we have modelled the critical locus and the VLE over the whole composition range and over a wide range of temperature.

On the other hand, simulation studies show the influence of temperature, pressure and composition on the interactions in these mixtures. Xu et al. [18] have studied the microscopic structure and molecular interactions of mixtures containing supercritical carbon dioxide and ethanol (EtOH) using Monte Carlo simulations and they have calculated the average number of bonding for each type of present interaction (EtOH – EtOH hydrogen bonding, EtOH - CO<sub>2</sub> hydrogen bonding and EtOH - CO<sub>2</sub> EDA bonding) as a function of temperature, pressure and mole fraction. The average number of EtOH - EtOH hydrogen bonding (which is the highest) increases significantly with ethanol mole fraction, however it also decreases significantly with temperature and pressure; the average number of EtOH - CO<sub>2</sub> hydrogen bonding (the lowest), decreases slightly with ethanol mole fraction, does not vary with temperature and increases slightly with pressure; finally, for EtOH - CO<sub>2</sub> EDA bonding, the average number of these interactions shows a similar behavior to the average number of EtOH - CO<sub>2</sub> hydrogen bonding though its values are slightly higher.

Fulton et al. [144] use Fourier transform infrared (FTIR) spectroscopy to study the aggregation of a series of small alcohols in supercritical CO<sub>2</sub> and supercritical ethane; they conclude that the specific interaction CO<sub>2</sub> quadrupole - alcohol dipole is not present in the alkane-alcohol system and that the solubility of the alcohol in CO<sub>2</sub> greatly increases. Likewise, they affirm that this interaction also perturbs the monomer-aggregate equilibria towards the monomer form of the alcohol. Thus, at a temperature of 313 K, 20 MPa pressure and an alcohol (methanol, ethanol and butan-1-ol) mole fraction from 0.03 to 0.15, the monomeric alcohol concentration in CO<sub>2</sub> is around three times of that in ethane.

In this work, the systems have been studied over the whole composition range and over the temperature and pressure ranges which are reported in Table 4. The number of experimental points from the literature as well as the corresponding authors for both critical loci [54,68,70-92,94-96] and VLE [66-68,71,74-77,79,85-92,95,96,145-195] are shown in Tables 8 and 9. All the experimental data (around 2250 VLE and 350 critical values) were used in the modelling, except those for VLE marked with an asterisk in Table 9 (46 values), due to their very high deviations.

Table 10 shows the rescaled geometric pure-compounds parameters for CO<sub>2</sub> (previous work [27]) and alkan-1-ols (this work) as well as the utilized association scheme and the pure-compounds association parameters.

In these systems classical mixing rules have been used and due to their complexity (different types of specific interactions), the wide range of temperatures studied and the different behavior of the supercritical systems, it has been necessary to adjust one temperature-dependent binary interaction parameter  $k_{ij}(T) = k_{ij}^0 + k_{ij}^1 T$  for each of the two properties studied, VLE and critical locus, for a given system. These values, together with the mean deviations obtained,  $MRD$  (eq. 4), for the critical temperature, critical pressure and bubble pressure are collected in Tables 8 and 9. For VLE, the absolute deviations for the solvent mole fraction in the vapor phase  $\Delta y_{CO_2}$  (eq. 5) are also included.

Regarding the association, we find a similar behavior to that observed by Fulton et al. [144]. When modeling  $CO_2 + n - C_m H_{2m+1} OH$  ( $m \neq 1$ ) mixtures with a given association scheme for the alcohols (2B for instance) results are unsatisfactory, either for VLE or for the critical locus. The net balance of the three types of specific interactions that appear competing in these systems, in addition to the occasionally opposed effects of temperature, pressure and composition, has led us to choose a scheme without association of hydrogen bonding and without cross-association to represent  $CO_2 +$  ethanol or + propan-1-ol or + butan-1-ol systems.

Nevertheless,  $CO_2 +$  methanol behavior is different. The critical locus of this system could be represented without great deviations with the same scheme as above ( $MRD(T_c) = 1.9\%$  and  $MRD(P_c) = 6.1\%$ ), but the representation of its VLE is unsatisfactory. Since methanol has higher self-association energy (Table 5) and dielectric constant than any of the other three alcohols (methanol: 33.0; ethanol: 25.3; propan-1-ol: 20.8; butan-1-ol: 17.8) [196], we have to take into account all the present interactions in this mixture. For this reason we have chosen a scheme where the molecule of methanol is considered both as a donor and as an acceptor centre (2B scheme), and the  $CO_2$  as a two-electron donor (with two negative sites which are only active when mixed with a molecule with at least one positive or neutral site), 2C scheme [197].

As we have considered pure  $CO_2$  as a non self-associated molecule, it is not possible to calculate its volume and energy of association. The Dortmund approximation based on the Kleiner and Sadowski method has been chosen [198] to calculate the mixture association parameters:

$$\varepsilon^{A_i B_j} = \frac{\varepsilon^{assoc}}{2} \quad \kappa^{A_i B_j} = \kappa^{assoc} \quad (6)$$

where  $\varepsilon^{assoc}$  and  $\kappa^{assoc}$  are respectively the energy of association and the volume of association of the associated compound, in our case methanol.

With this association scheme it is only necessary one temperature-dependent binary interaction parameter  $k_{ij}(T) = k_{ij}^0 + k_{ij}^1 T$  to represent both VLE and critical locus. These values, together with the mean deviations obtained,  $MRD$  (eq. 4), for the critical temperature, critical pressure and bubble pressure are collected in Tables 8 and 9. For VLE, the absolute deviations for the solvent mole fraction in the vapor phase  $\Delta y_{CO_2}$  (eq. 5) are also included.

Figures 2a, 2b and 2c show the experimental and calculated critical loci for these systems and Figures 5 and 6 the VLE (experimental and calculated) for  $CO_2$  + methanol or + ethanol mixtures. The corresponding figures for the rest of the VLE systems are included in the Supplementary Data (Figures SF15 - SF16).

There is a good agreement between experimental and calculated values of these properties. The obtained deviations are:  $MRD(T_c) = 1.91\%$  and  $MRD(P_c) = 5.93\%$ ,  $MRD(P) = 7.07\%$  and  $\Delta y_{CO_2} = 0.022$ .

The modelling has been carried out using temperature-independent binary interaction parameters  $k_{ij}$  as well. Tables ST1 and ST2 (Supplementary Data) show values for  $k_{ij}(T)$  and  $k_{ij}$  as well as  $MRD$  and  $\Delta y$  for each system in both calculations. As it can be seen, the improvement is noticeable when using temperature-dependent binary interaction parameters, as expected due to the different values of the critical temperatures of the pure components (asymmetric mixtures).

Finally, we have represented the ternary critical locus [54] and VLE [199] for  $n\text{-}C_6H_{14} + CO_2 + CH_3OH$ , both found in the literature. For this purpose, we have used the parameters obtained in this work for the binary interactions  $CO_2 - CH_3OH$  and  $n\text{-}C_6H_{14} - CH_3OH$ , and for the interaction  $CO_2 - \text{alkane}$  we have used those parameters obtained by us in earlier reports [27],  $k_{ij} = 0.09$ . The calculated deviations for the critical locus of the ternary mixture ( $MRD(T_c) = 3.5\%$  and  $MRD(P_c) = 7.1\%$ ) are similar to those obtained for the corresponding binary mixtures determined by the same author, a fact that indicates that the presence of a third component does not modify the binary interaction between the other two, and that significant ternary interactions do not exist in the mixture. The calculated deviation for the VLE of the ternary mixture is  $MRD(P) = 8.26\%$ .

## 5. Conclusions

In this work, the critical locus of the mixtures  $n - C_6H_{14} + n - C_mH_{2m+1}OH$  and  $CO_2 + n - C_mH_{2m+1}OH$  ( $m = 1 - 4$ ), has been determined experimentally over the entire range of compositions. The measurements were carried out using an experimental setup that includes a flow apparatus for the determination of critical temperature and pressure ( $P_c$ ,  $T_c$ ), using a critical opalescence method. All the systems display an uninterrupted (gas + liquid) critical locus connecting the critical points of the pure components.

$n - C_6H_{14} + n - C_mH_{2m+1}OH$  ( $m = 1 - 3$ ) systems present a minimum in the  $T_c$ - $x$  projection, which is more pronounced the lower the number of carbon atoms in the alcohol is. Simultaneously, we observed that the minimum shifts to richer compositions in  $n$ -hexane as the number of carbon atoms in the alcohol (and thus its  $T_c$ ) increases. In the  $P_c$ - $x$  projection, all the lines are monotonic.

In  $CO_2 + n - C_mH_{2m+1}OH$  ( $m = 1 - 4$ ) systems, the critical locus curves have neither maximum nor minimum points in temperature and all of them present a point of maximum critical pressure located in the  $CO_2$ -rich zone, shifting to regions richer in  $CO_2$  as the number of carbon atoms of the alcohol increases.

In this work, a comprehensive bibliographic review of the phase equilibrium of the systems containing  $n$ -hexane + alkan-1-ol (methanol, ethanol, propan-1-ol, butan-1-ol, pentan-1-ol and hexan-1-ol) and  $CO_2$  + alkan-1-ol (methanol, ethanol, propan-1-ol and butan-1-ol) has been undertaken with the aim of modelling their thermodynamic behavior under critical and subcritical conditions. For this, PC-SAFT EoS has been used. The geometrical parameters for the pure compounds have been rescaled from the values of their critical points. In all cases, classical mixing rules and temperature-dependent binary interaction parameters  $k_{ij}(T) = k_{ij}^0 + k_{ij}^1T$  have been used.

In this manner, approximately 2215 points (VLE and critical loci) have been modelled for the  $n - C_6H_{14} + n - C_mH_{2m+1}OH$  ( $m = 1 - 6$ ) systems in a temperature range from 263 to 588 K. The results show that these systems are well represented by PC-SAFT EoS when using a 2B association scheme for the alcohols and only one temperature-dependent binary interaction parameter for both VLE and critical locus of each system. The deviations obtained are  $MRD(T_c) = 0.47\%$  and  $MRD(P_c) = 3.38\%$  for the critical locus and  $MRD(P) = 2.90\%$  and  $\Delta y_{C_6H_{14}} = 0.031$  for the VLE.

Additionally, we have analyzed the behavior of  $\text{CO}_2 + n - \text{C}_m\text{H}_{2m+1}\text{OH}$  ( $m = 1 - 4$ ) mixtures for approximately 2600 points (VLE and critical loci) in a range from 213 to 563 K. In these systems, besides the dispersive interactions and alcohol - alcohol hydrogen bonding, some other specific interactions exist: carbon atom of  $\text{CO}_2$  - oxygen atom of alcohol and  $\text{CO}_2$  - alcohol hydrogen bonding, between an oxygen atom of  $\text{CO}_2$  and the hydrogen atom of the hydroxyl group. Association theories like those of the SAFT family account explicitly for self- and cross-association or solvation phenomena due to the Lewis acid - Lewis base interaction. Thus, we have obtained good results for the  $\text{CO}_2$  + methanol mixtures when including solvation phenomena (2C scheme) in  $\text{CO}_2$  and association (2B scheme) in methanol, and only one temperature-dependent binary interaction parameter for both VLE and critical locus. For the rest of the alcohols, the net balance of the three types of specific interactions that seem to compete in these systems, in addition to the occasionally opposed effects of temperature, pressure and composition, has lead us to choose a scheme without association; nevertheless, in this case, the temperature-dependent binary interaction parameters when representing the VLE and critical locus are different. For the  $\text{CO}_2$  + alkan-1-ol systems the deviations obtained are:  $MRD(T_c) = 1.91 \%$ ,  $MRD(P_c) = 5.93 \%$ ,  $MRD(P) = 7.07 \%$  and  $\Delta y_{\text{CO}_2} = 0.022$ .

Finally, we have represented the ternary critical locus and VLE for  $n\text{-C}_6\text{H}_{14} + \text{CO}_2 + \text{CH}_3\text{OH}$ , both found in the literature. To do this, we have used the parameters obtained in this work for the binary interactions  $\text{CO}_2$  -  $\text{CH}_3\text{OH}$  and  $n\text{-C}_6\text{H}_{14}$  -  $\text{CH}_3\text{OH}$ , and for the  $\text{CO}_2$  - alkane interaction those parameters obtained by us in earlier studies. The calculated deviation for the ternary mixture ( $MRD(T_c) = 3.5 \%$  and  $MRD(P_c) = 7.1 \%$ ) is similar to that obtained for the corresponding binary mixtures determined by the same authors, which indicates that the presence of a third component does not modify the binary interaction between the other two and that a significant ternary interaction does not exist in the mixture.

In this work, the computations were performed using the VLXE software [200] for the PC-SAFT EoS calculations.



## Supplementary data

Supplementary data include:

\* $P_c$ - $T_c$ ,  $P_c$ - $x$  and  $T_c$ - $x$  representations of experimental data from this work and literature for  $n$ -hexane + methanol, or + ethanol, or + propan-1-ol, or + butan-1-ol, or + pentan-1-ol, or + hexan-1-ol mixtures (Figures SF1, SF2, SF3, SF4, SF5 and SF6, respectively).

\* A comparison between this work experimental data and those from literature for the critical loci of  $n$ -hexane + alkan-1-ol systems.

\* $P_c$ - $T_c$ ,  $P_c$ - $x$  and  $T_c$ - $x$  representations of experimental data from this work and literature for CO<sub>2</sub> + methanol, or + ethanol, or + propan-1-ol, or + butan-1-ol mixtures (Figures SF7, SF8, SF9 and SF10, respectively).

\*A comparison between this work experimental data and those from literature for the critical loci of CO<sub>2</sub> + alkan-1-ol systems.

\*VLE representations for  $n$ -hexane + propan-1-ol, or + butan-1-ol, or + pentan-1-ol, or + hexan-1-ol mixtures (Figures SF11, SF12, SF13 and SF14, respectively).

\*VLE representations for CO<sub>2</sub> + propan-1-ol and + butan-1-ol mixtures (Figures SF15 and SF16, respectively).

\*Table ST1 including values for the temperature-dependent,  $k_{ij}(T)$ , or temperature-independent,  $k_{ij}$ , binary interaction parameters of the studied systems.

\*Table ST2 including results from the modelling carried out using either temperature-dependent,  $k_{ij}(T)$ , or temperature-independent,  $k_{ij}$ , binary interaction parameters for the studied systems.

\*Table ST3 including deviations obtained in this work and by other authors when modelling the VLE or the critical loci for the  $n$ -hexane + alkan-1-ol systems.

\*Table ST4 including deviations obtained in this work and by other authors when modelling the VLE or the critical loci for the CO<sub>2</sub> + alkan-1-ol systems.

\*A video is available in the online version.

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## Nomenclature

### Abbreviations

<i>c.i.</i>	confidence interval
CO <sub>2</sub>	carbon dioxide
EDA	electron donor - acceptor
EoS	equation of state
EtOH	ethanol
LA	Lewis acid
LB	Lewis base

$$MRD(X) = \frac{100}{N} \sum_{n=1}^N \left| \frac{X_n^{\text{exp}} - X_n^{\text{cal}}}{X_n^{\text{exp}}} \right| \quad \text{mean relative deviation in } X \text{ (generic variable)}$$

$n - \text{C}_6\text{H}_{14}$        $n$ -hexane

$n - \text{C}_m\text{H}_{2m+1}\text{OH}$       alkan-1-ol

*OF*      objective function

PC-SAFT      Perturbed-Chain Statistical Associating Fluid Theory

scCO<sub>2</sub>      supercritical carbon dioxide

SCF      supercritical fluid

*u*      uncertainty

VLE      vapor-liquid equilibria

$$\Delta y = \frac{1}{N} \sum_{n=1}^N |y_n^{\text{exp}} - y_n^{\text{cal}}| \quad \text{absolute deviation for the solvent mole fraction}$$

in the vapor phase

### List of symbols

$k_{ij}$	binary interaction parameter
$m$	chain length number
$P$	pressure
$T$	temperature
$x$	liquid-phase mole fraction
$y$	vapor-phase mole fraction

### Greek symbols

$\varepsilon$	segment energy parameter
$\sigma$	segment diameter
$\varepsilon^{A_i B_i}$	energy of association
$\kappa^{A_i B_i}$	volume of association

### Subscripts

$i, j$	pure component indexes
$c$	critical

### Superscripts

assoc	association
cal	calculated
DD	dipole-dipole
dis	dispersive
exp	experimental
hc	hard chain
id	ideal
QD	quadrupole-dipole
QQ	quadrupole-quadrupole

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## FIGURE CAPTIONS

**FIGURE 1.** (a),  $(P_c, T_c)$ ; (b),  $(P_c, x)$  and (c),  $(T_c, x)$  projection for *n*-hexane + alkan-1-ol critical loci. Symbols, experimental values:  $\oplus$ , methanol (this work);  $\blacksquare$ , ethanol (this work);  $\blacktriangle$ , propan-1-ol (this work);  $\blackstar$ , butan-1-ol (this work);  $\bullet$ , pentan-1-ol (ref. [63]);  $\blacklozenge$ , hexan-1-ol (ref. [63]). Lines, calculated with PC-SAFT EoS using the parameters from Tables 5 and 6.

**FIGURE 2.** (a),  $(P_c, T_c)$ ; (b),  $(P_c, x)$  and (c),  $(T_c, x)$  projection for CO<sub>2</sub> + alkan-1-ol critical loci. Symbols, experimental values:  $\oplus$ , methanol (this work);  $\blacksquare$ , ethanol (this work);  $\blacktriangle$ , propan-1-ol (this work);  $\blackstar$ , butan-1-ol (this work). Lines, calculated with PC-SAFT EoS using the parameters from Tables 8 and 10.

**FIGURE 3.** Pressure–mole fraction diagram for *n* – C<sub>6</sub>H<sub>14</sub> + CH<sub>3</sub>OH VLE. Symbols, experimental values:  $\circ$ ,  $T = 298.15$  K (ref. [98]);  $\blackstar$ ,  $T = 313.15$  K (ref. [102]);  $\blacklozenge$ ,  $T = 333.15$  K (ref. [105]);  $\blacktriangle$ ,  $T = 348.15$  K (ref. [100]);  $\triangleleft$ ,  $T = 423.15$  K (ref. [55]);  $\blacksquare$ ,  $T = 448.15$  K (ref. [55]). Lines, calculated with PC-SAFT EoS using the parameters from Tables 5 and 7.

**FIGURE 4.** Pressure–mole fraction diagram for *n* – C<sub>6</sub>H<sub>14</sub> + C<sub>2</sub>H<sub>5</sub>OH VLE. Symbols, experimental values:  $\circ$ ,  $T = 263.15$  K (ref. [106]);  $\blacksquare$ ,  $T = 293.15$  K (ref. [106]);  $\blacklozenge$ ,  $T = 328.15$  K (ref. [115]);  $\blacktriangle$ ,  $T = 413.15$  K (ref. [117]);  $\blackstar$ ,  $T = 443.15$  K (ref. [117]);  $\triangleleft$ ,  $T = 473.15$  K (ref. [117]). Lines, calculated with PC-SAFT EoS using the parameters from Tables 5 and 7.

**FIGURE 5.** Pressure–mole fraction diagram for CO<sub>2</sub> + CH<sub>3</sub>OH VLE. Symbols, experimental values:  $\circ$ ,  $T = 273.15$  K (ref. [145]);  $\blacklozenge$ ,  $T = 298.15$  K (ref. [155]);  $\triangleleft$ ,  $T = 308.15$  K (ref. [151]);  $\blacktriangle$ ,  $T = 323.15$  K (ref. [146]);  $\triangleleft$ ,  $T = 348$  K (ref. [74]);  $\square$ ,  $T = 373$  K (ref. [74]);  $\blacksquare$ ,  $T = 423.15$  K (ref. [146]);  $\blackstar$ ,  $T = 477.6$  K (ref. [79]). Lines, calculated with PC-SAFT EoS using the parameters from Tables 9 and 10.

**FIGURE 6.** Pressure–mole fraction diagram for CO<sub>2</sub> + C<sub>2</sub>H<sub>5</sub>OH VLE. Symbols, experimental values:  $\circ$ ,  $T = 291.15$  K (ref. [168]);  $\blackstar$ ,  $T = 304.2$  K (ref. [171]).  $\blacklozenge$ ,  $T = 313.0$  K (ref. [89]);  $\triangleleft$ ,  $T = 337.2$  K (ref. [179]);  $\blacksquare$ ,  $T = 348.40$  K (ref. [89]);  $\square$ ,  $T = 391.96$  K (ref. [88]). Lines, calculated with PC-SAFT EoS using the parameters from Tables 9 and 10.

**Table 1.** Purity, water content (% wt) and supplier of the compounds used in this work. Values of the critical temperatures,  $T_c$ , and critical pressures,  $P_c$ , obtained in this work for pure compounds and those recommended by the National Institute of Standards and Technology, NIST, ref. [36].

Compound	Purity (%)	% wt water	Supplier	This Work		NIST	
				$T_c$ / K	$P_c$ / MPa	$T_c$ / K	$P_c$ / MPa
CO <sub>2</sub>	99.98	≤ 0.0003	Air Liquide	304.21	7.383	304.20 ±0.02	7.3825 ±0.0005
<i>n</i> -C <sub>6</sub> H <sub>14</sub>	99.5	< 0.01	Fluka	507.64	3.044	507.6 ±0.5	3.02 ±0.04
CH <sub>3</sub> OH	99.8	< 0.02	Fluka	512.90	8.094	513 ±1	8.1 ±0.1
C <sub>2</sub> H <sub>5</sub> OH	99.8	< 0.2	Scharlau	514.25	6.168	514 ±7	6.3 ±0.4
C <sub>3</sub> H <sub>7</sub> OH	99.5	< 0.15	Fluka	537.06	5.179	536.9 ±0.8	5.2 ±0.1
C <sub>4</sub> H <sub>9</sub> OH	99.8	< 0.005	Aldrich	563.42	4.425	562 ±2	4.5 ±0.4

**Table 2.** Experimental critical temperatures,  $T_c$ , and critical pressures,  $P_c$ , for the  $\{n - C_6H_{14} + n - C_mH_{2m+1}OH\}$  mixtures as a function of the  $n - C_6H_{14}$  mole fraction.

$x_{C_6H_{14}}$	$T_c / K$	$P_c / MPa$	$x_{C_6H_{14}}$	$T_c / K$	$P_c / MPa$
<b><math>n-C_6H_{14} + CH_3OH</math></b>					
0.0000	512.90	8.094	0.5502	483.79	5.028
0.0499	505.84	7.577	0.6001	486.31	4.876
0.1000	498.87	7.034	0.6496	487.67	4.763
0.1500	493.72	6.682	0.6999	490.40	4.572
0.2000	489.17	6.301	0.7496	493.86	4.321
0.2501	485.92	6.001	0.8001	496.26	4.131
0.2999	483.56	5.767	0.8499	499.99	3.804
0.3499	482.22	5.571	0.8996	502.72	3.556
0.3998	481.85	5.388	0.9502	506.01	3.331
0.4498	481.72	5.282	1.0000	507.64	3.044
0.5000	482.54	5.163			
<b><math>n-C_6H_{14} + C_2H_5OH</math></b>					
0.0000	514.25	6.168	0.5501	490.68	4.242
0.0501	511.13	5.921	0.6002	491.09	4.154
0.0999	505.80	5.691	0.6503	492.18	4.048
0.1500	501.43	5.431	0.6999	493.53	3.945
0.2000	498.29	5.230	0.7497	495.45	3.821
0.2499	495.18	5.024	0.7999	498.17	3.696
0.2999	492.49	4.861	0.8497	499.92	3.552
0.3500	491.63	4.700	0.9001	503.41	3.418
0.4001	490.15	4.573	0.9500	505.50	3.256
0.4500	489.89	4.460	1.0000	507.64	3.044
0.4999	489.77	4.349			

<b><i>n</i>-C<sub>6</sub>H<sub>14</sub> + C<sub>3</sub>H<sub>7</sub>OH</b>					
0.0000	537.06	5.179	0.5506	502.90	3.612
0.0500	530.79	4.955	0.6001	502.81	3.541
0.0999	525.23	4.756	0.6497	502.87	3.473
0.1501	520.83	4.562	0.7001	503.64	3.412
0.2000	516.21	4.384	0.7497	503.82	3.346
0.2500	512.88	4.245	0.7998	504.58	3.287
0.3001	509.56	4.092	0.8501	505.24	3.226
0.3498	507.59	3.975	0.9002	506.11	3.163
0.4000	505.50	3.867	0.9498	507.02	3.105
0.4501	504.28	3.764	1.0000	507.64	3.044
0.4999	503.52	3.689			
<b><i>n</i>-C<sub>6</sub>H<sub>14</sub> + C<sub>4</sub>H<sub>9</sub>OH</b>					
0.0000	563.42	4.425	0.5499	520.81	3.568
0.0500	559.37	4.360	0.5999	518.32	3.495
0.1001	554.84	4.301	0.6501	515.74	3.426
0.1500	550.30	4.227	0.7000	513.59	3.362
0.1999	546.28	4.147	0.7500	511.64	3.301
0.2499	542.06	4.059	0.8000	510.25	3.241
0.3001	538.18	3.976	0.8499	509.19	3.192
0.3501	535.08	3.895	0.9000	508.72	3.142
0.4001	530.76	3.808	0.9500	508.30	3.093
0.4503	526.79	3.725	1.0000	507.64	3.044
0.4999	523.57	3.644			



**Table 3.** Experimental critical temperatures,  $T_c$ , and critical pressures,  $P_c$ , for the  $\{\text{CO}_2 + n - \text{C}_m\text{H}_{2m+1}\text{OH}\}$  mixtures as a function of the  $\text{CO}_2$  mole fraction.

$x_{\text{CO}_2}$	$T_c / \text{K}$	$P_c / \text{MPa}$	$x_{\text{CO}_2}$	$T_c / \text{K}$	$P_c / \text{MPa}$
<b>CO<sub>2</sub> + CH<sub>3</sub>OH</b>					
0.0000	512.90	8.094	0.7101	371.44	15.169
0.0501	508.63	8.807	0.7301	363.32	14.487
0.0995	501.64	9.582	0.7502	350.96	13.439
0.1351	495.95	10.133	0.7695	346.18	12.964
0.1997	491.70	10.830	0.7853	339.82	12.112
0.2501	484.72	11.712	0.7998	336.81	11.614
0.3000	480.24	12.249	0.8144	333.74	11.286
0.3505	471.87	13.058	0.8503	328.42	10.345
0.4001	465.25	13.614	0.8701	324.92	10.016
0.4494	455.58	14.389	0.8989	320.75	9.419
0.4999	438.84	15.480	0.9198	317.10	8.878
0.5503	424.25	16.096	0.9601	311.86	8.009
0.6006	408.98	16.388	0.9901	306.25	7.503
0.6505	393.20	16.266	0.9949	305.06	7.402
0.7000	377.29	15.623	1.0000	304.21	7.383
<b>CO<sub>2</sub> + C<sub>2</sub>H<sub>5</sub>OH</b>					
0.0000	514.25	6.168	0.5505	428.65	14.439
0.0500	507.29	7.309	0.6001	413.32	14.929
0.1000	501.54	8.064	0.6504	400.57	15.077
0.1500	493.23	9.052	0.7199	374.38	14.400
0.1998	486.84	9.579	0.7506	368.18	13.842
0.2504	480.48	10.509	0.8002	348.47	12.429
0.3000	474.58	11.056	0.8504	336.96	11.088

0.3496	466.35	11.865	0.9000	326.90	9.817
0.3999	458.40	12.578	0.9501	319.07	8.605
0.4496	451.14	13.390	1.0000	304.21	7.383
0.5002	436.22	14.086			
<b>CO<sub>2</sub> + C<sub>3</sub>H<sub>7</sub>OH</b>					
0.0000	537.06	5.179	0.5495	447.10	14.602
0.0498	529.39	6.122	0.5998	435.29	15.268
0.0997	523.59	6.862	0.6495	422.60	15.928
0.1495	517.40	7.712	0.6994	398.97	15.975
0.2002	510.88	8.538	0.7498	383.17	15.446
0.2501	502.93	9.383	0.7999	362.07	14.114
0.3000	496.88	10.198	0.8502	344.49	12.177
0.3497	488.68	11.062	0.8999	327.97	10.203
0.4000	480.52	11.901	0.9500	315.45	8.660
0.4494	471.87	12.743	1.0000	304.21	7.383
0.4993	459.09	13.786			
<b>CO<sub>2</sub> + C<sub>4</sub>H<sub>9</sub>OH</b>					
0.0000	563.42	4.425	0.6999	430.26	17.084
0.0496	554.67	5.445	0.7299	419.43	17.271
0.0996	546.59	6.597	0.7501	410.86	17.254
0.1504	538.62	7.800	0.7795	393.78	16.879
0.1995	528.69	8.813	0.8004	384.44	16.538
0.2488	521.54	9.634	0.8099	377.56	16.136
0.3001	513.06	10.826	0.8298	362.32	15.163
0.3500	504.08	11.576	0.8498	351.71	13.885
0.3999	495.90	12.556	0.8601	343.05	12.843
0.4498	487.11	13.338	0.8799	335.74	11.531

0.4994	478.73	13.987	0.9248	323.96	9.868
0.5495	470.59	14.819	0.9599	314.07	8.800
0.5999	458.87	15.596	1.0000	304.21	7.383
0.6495	445.27	16.448			

**Table 4.** Temperature and pressure ranges of the experimental data (this work and literature critical loci and VLE) used in the modellization with the PC-SAFT model. All the systems have been studied over the whole composition range.

System	Critical locus		VLE	
	$T_c / K$	$P_c / MPa$	$T / K$	$P / MPa$
<i>n</i> -hexane + methanol	480 - 513	3.02 - 8.09	293 - 507	0.013 - 7.40
<i>n</i> -hexane + ethanol	488 - 515	3.01 - 6.17	263 - 514	0.0023 - 6.14
<i>n</i> -hexane + propan-1-ol	502 - 537	3.04 - 5.18	298 - 513	0.0028 - 4.34
<i>n</i> -hexane + butan-1-ol	507 - 563	3.04 - 4.42	288 - 332	0.00041 - 0.076
<i>n</i> -hexane + pentan-1-ol	507 - 588	3.04 - 3.88	303 - 323	0.00044 - 0.054
<i>n</i> -hexane + hexan-1-ol	507 - 545	3.04 - 3.40	293 - 373	0.00006 - 0.245
CO <sub>2</sub> + methanol	304 - 513	7.38 - 18.50	213 - 478	0.10 - 16.46
CO <sub>2</sub> + ethanol	304 - 514	6.15 - 15.30	283 - 494	0.51 - 15.16
CO <sub>2</sub> + propan-1-ol	304 - 537	5.18 - 16.00	293 - 427	0.47 - 16.03
CO <sub>2</sub> + butan-1-ol	304 - 563	4.42 - 17.37	293 - 430	0.52 - 17.35

**Table 5.-** Association scheme and PC-SAFT EoS pure-compounds parameters used in the *n*-hexane + alkan-1-ol modellization.  $m$ ,  $\sigma$ ,  $\varepsilon$ : geometric parameters, rescaled in this work from  $T_c$  and  $P_c$ .  $\kappa^{A_i B_i}$  and  $\varepsilon^{A_i B_i}$ : association parameters taken from reference [20].

Compound	Association scheme	$m / M$ (mol g <sup>-1</sup> )	$\sigma$ (Å)	$\varepsilon$ (K)	$\kappa^{A_i B_i}$	$\varepsilon^{A_i B_i}$ (K)
<i>n</i> -C <sub>6</sub> H <sub>14</sub>	Non	0.03760	3.8823	225.88		
CH <sub>3</sub> OH	2B	0.05273	3.3264	175.20	0.035176	2899.5
C <sub>2</sub> H <sub>5</sub> OH	2B	0.04924	3.4895	187.51	0.032384	2653.4
C <sub>3</sub> H <sub>7</sub> OH	2B	0.05560	3.3722	216.80	0.015268	2276.8
C <sub>4</sub> H <sub>9</sub> OH	2B	0.04079	3.7307	242.47	0.006692	2544.6
C <sub>5</sub> H <sub>11</sub> OH	2B	0.04486	3.5439	233.83	0.010319	2252.1
C <sub>6</sub> H <sub>13</sub> OH	2B	0.03745	3.7817	247.04	0.005747	2538.9

**Table 6.-** PC-SAFT EoS temperature-dependent binary interaction parameters,  $k_{ij}(T)$ , and mean relative deviations in critical temperature and pressure,  $MRD(T_c)$  and  $MRD(P_c)$ , for  $\{n - C_6H_{14} + n - C_mH_{2m+1}OH (m = 1 - 6)\}$  systems obtained using the parameters from Table 5. Average deviations for each system are also included.

System	$k_{ij}(T)$	Range T/ K	Nº Points	Range P/ MPa	Range $x_{C_6H_{14}}$	$MRD(T_c)/\%$	$MRD(P_c)/\%$	Ref.
$n-C_6H_{14} +$								
CH <sub>3</sub> OH	$0.00234 + 1.40 \times 10^{-4} T$	481-513	21	3.04-8.09	0-1	0.96	6.82	This work
		481-513	10	3.02-8.06	0-1	0.83	6.92	[52]
		481-513	18	3.02-8.07			4.48	[53]
		480-513	18	3.02-8.12	0-1	1.07	7.37	[54]
		481-507	4	3.05-5.38	0.41-1	0.46	4.65	[55]
		$MRD(T_c) = 0.94\% ; MRD(P_c) = 6.26\%$						
C <sub>2</sub> H <sub>5</sub> OH	$0.00187 + 3.70 \times 10^{-5} T$	489-515	21	3.04-6.17	0-1	0.42	3.02	This work
		489-514	10	3.03-6.12	0-1	0.43	1.47	[38]
		489-514	11	3.01-6.14	0-1	0.35	2.49	[56]
		493-503	2	3.31-3.93	0.68-0.91	0.59	1.39	[57]
		499-514	6		0-0.8	0.99		[58]
		488-514	8		0-1	0.60		[59]
$MRD(T_c) = 0.50\% ; MRD(P_c) = 2.46\%$								
C <sub>3</sub> H <sub>7</sub> OH	$0.00153 + 6.54 \times 10^{-5} T$	502-537	20	3.04-5.18	0-1	0.34	1.21	This work
		503-513	3	3.41-4.34	0.31-0.79	0.10	3.30	[50]
		502-537	10		0-1	0.12		[60]
		502-528	8		0.1-0.89	0.13		[61]
$MRD(T_c) = 0.23\% ; MRD(P_c) = 1.48\%$								
C <sub>4</sub> H <sub>9</sub> OH	$0.00153 + 2.73 \times 10^{-5} T$	507-563	21	3.04-4.42	0-1	0.22	0.97	This work
		507-562	10		0-1	0.14		[60]
		508-548	8		0.19-0.93	0.15		[61]
$MRD(T_c) = 0.19\% ; MRD(P_c) = 0.97\%$								
C <sub>5</sub> H <sub>11</sub> OH	$0.00153 + 1.63 \times 10^{-5} T$	507-588	8		0-1	0.85		[59]
		507-588	7		0-1	0.50		[62]
		507-588	21	3.04-3.88	0-1	0.23	1.07	[63]
$MRD(T_c) = 0.42\% ; MRD(P_c) = 1.07\%$								
C <sub>6</sub> H <sub>13</sub> OH	$0.00153 + 2.12 \times 10^{-5} T$	507-545	9	3.04-3.40	0.65-1	0.21	1.12	[63]
		$MRD(T_c) = 0.21\% ; MRD(P_c) = 1.12\%$						

**Table 7.-** PC-SAFT EoS temperature-dependent binary interaction parameters,  $k_{ij}(T)$ , mean relative deviations in bubble pressure,  $MRD(P)$ , and absolute deviations for the solvent mole fraction in the vapor phase,  $\Delta y_{C_6H_{14}}$ , for  $\{n - C_6H_{14} + n - C_mH_{2m+1}OH (m = 1 - 6)\}$  systems obtained using the parameters from Table 5. Average deviations for each system are also included.

<b><math>n-C_6H_{14} + CH_3OH ; k_{ij}(T) = 0.00234 + 1.40 \times 10^{-4}T</math></b>													
<b><math>T/K</math></b>	<b>Nº Points</b>	<b>Range <math>P/10^{-3}MPa</math></b>	<b>Range <math>x_{C_6H_{14}}</math></b>	<b><math>MRD(P)/\%</math></b>	<b><math>\Delta y_{C_6H_{14}}</math></b>	<b>Ref.</b>	<b><math>T/K</math></b>	<b>Nº Points</b>	<b>Range <math>P/10^{-3}MPa</math></b>	<b>Range <math>x_{C_6H_{14}}</math></b>	<b><math>MRD(P)/\%</math></b>	<b><math>\Delta y_{C_6H_{14}}</math></b>	<b>Ref.</b>
293.15	24	13-28	0-1	4.40	0.019	[97]	318.15	13	44-84	0-1	1.88	0.020	[104]
298.15	21	16-35	0-1	4.48		[48]	323.15	24	54-103	0-1	2.02		[100]
298.15	26	31-36	0.06-0.93	2.47	0.011	[98]	333.15	24	76-149	0-1	1.75		[100]
298.15	7	32-35	0.05-0.95	3.43	0.020	[99]	333.15	30	76-194	0-1	1.98	0.026	[105]
303.15	20	22-45	0-1	7.25	0.041	[130]	343.15	25	104-212	0-1	1.68		[100]
308.15	24	28-55	0-1	6.64		[100]	348.15	25	129-251	0-1	1.80		[100]
313.15	25	35-69	0-1	2.52		[100]	398.15	6	450-1040	0-1	0.87		[55]
313.15	55	35-69	0-1	5.73	0.036	[101]	423.15	6	750-1840	0-1	1.42		[55]
313.15	32	35-69	0-1	1.75	0.010	[102]	448.15	6	1200-3100	0-1	1.23		[55]
313.15	14	35-69	0-1	3.78		[103]	402-507	79	500-7400	0-1	1.83		[52]
318.15	25	44-84	0-1	2.22		[100]							
<b><math>MRD(P) = 3.20\% ; \Delta y_{C_6H_{14}} = 0.010</math></b>													
<b><math>n-C_6H_{14} + C_2H_5OH ; k_{ij}(T) = 0.0187 + 3.70 \times 10^{-5}T</math></b>													
<b><math>T/K</math></b>	<b>Nº Points</b>	<b>Range <math>P/10^{-3}MPa</math></b>	<b>Range <math>x_{C_6H_{14}}</math></b>	<b><math>MRD(P)/\%</math></b>	<b><math>\Delta y_{C_6H_{14}}</math></b>	<b>Ref.</b>	<b><math>T/K</math></b>	<b>Nº Points</b>	<b>Range <math>P/10^{-3}MPa</math></b>	<b>Range <math>x_{C_6H_{14}}</math></b>	<b><math>MRD(P)/\%</math></b>	<b><math>\Delta y_{C_6H_{14}}</math></b>	<b>Ref.</b>
263.15	19	2.3-4.2	0.05-0.95	4.58	0.058	[106]	323.15	26	29-73	0-1	3.82		[109]
273.15	15	3.8-7.5	0.05-0.95	3.69	0.076	[106]	323.15	20	29-73	0-1	5.59	0.055	[114]
283.15	19	7.2-13	0.05-0.95	2.74	0.067	[106]	328.15	11	37-89	0-1	4.28	0.049	[110]
293.15	19	10-21	0.05-0.95	2.44	0.078	[106]	328.15	17	46-90	0-0.96	2.15	0.038	[115]
298.15	27	7.8-25	0-1	6.49		[48]	333.15	26	47-107	0-1	3.15		[109]
298.15	17	15-27	0.04-0.96	4.19	0.069	[98]	333.15	8	90-110	0.13-0.88	2.35	0.057	[116]
298.15	9	20-25	0.10-0.90	5.18	0.055	[99]	343.15	26	72-152	0-1	2.63		[109]
298.15	9	7.8-25	0-1	4.62	0.055	[107]	353.15	26	108-211	0-1	2.18		[109]
298.15	9	19-26	0.10-0.90	3.72	0.056	[108]	413.15	11	617-1067	0-1	2.32	0.017	[117]

303.15	19	17-33	0.05-0.95	4.37	0.075	[106]	443.15	11	1095-2006	0-1	1.44	0.013	[117]
303.15	26	10-32	0-1	5.48		[109]	473.15	14	1811-3479	0-1	2.46	0.007	[57]
308.15	11	14-40	0-1	6.20	0.046	[110]	473.15	11	1811-3485	0-1	0.79	0.019	[117]
313.15	26	18-49	0-1	4.56		[109]	483.15	12	2109-4130	0-1	1.26	0.015	[57]
313.15	19	18-50	0-1	4.54	0.041	[111]	493.15	7	2334-4885	0-1	1.29	0.008	[57]
313.15	15	18-49	0-1	5.01	0.043	[112]	503.15	5	2838-5561	0-1	0.85	0.001	[57]
318.15	11	22-61	0-1	4.57	0.048	[110]	382-514	127	435-6140	0-1	1.65		[56]
318.15	40	23-60	0-1	5.47	0.049	[113]							

$$MRD(P) = 3.43\% ; \Delta y_{C_6H_{14}} = 0.026$$

$$n-C_6H_{14} + C_3H_7OH ; k_{ij}(T) = 0.00153 + 6.54 \times 10^{-5} T$$

$T/K$	Nº Points	Range $P/10^{-3}MPa$	Range $x_{C_6H_{14}}$	$MRD(P)/\%$	$\Delta y_{C_6H_{14}}$	Ref.	$T/K$	Nº Points	Range $P/10^{-3}MPa$	Range $x_{C_6H_{14}}$	$MRD(P)/\%$	$\Delta y_{C_6H_{14}}$	Ref.
298.15	27	2.8-21	0-1	2.70		[48]	318.15	5	41-48	0.26-0.71	1.04	0.010	[122]
298.15	9	13-21	0.10-0.90	1.77	0.004	[99]	323.15	22	12-58	0-1	2.00	0.008	[123]
298.15	11	2.8-21	0-1	3.12		[118]	483.15	13	2088-2771	0-1	1.79	0.010	[50]
298.15	11	2.8-21	0-1	2.43	0.011	[119]	493.15	14	2451-3215	0-1	1.53	0.015	[50]
308.15	9	5.6-32	0-1	2.56		[120]	503.15	8	2824-3788	0-1	1.04	0.010	[50]
313.15	22	7.0-40	0-1	1.37	0.009	[121]	513.15	4	3554-4340	0-0.24	1.40	0.013	[50]

$$MRD(P) = 2.01\% ; \Delta y_{C_6H_{14}} = 0.007$$

$$n-C_6H_{14} + C_4H_9OH ; k_{ij}(T) = 0.00153 + 2.73 \times 10^{-5} T$$

$T/K$	Nº Points	Range $P/10^{-3}MPa$	Range $x_{C_6H_{14}}$	$MRD(P)/\%$	$\Delta y_{C_6H_{14}}$	Ref.	$T/K$	Nº Points	Range $P/10^{-3}MPa$	Range $x_{C_6H_{14}}$	$MRD(P)/\%$	$\Delta y_{C_6H_{14}}$	Ref.
288.15	15	0.41-13	0-1	2.80	0.006	[124]	313.15	15	2.5-37	0-1	2.41	0.009	[124]
298.15	17	0.82-20	0-1	4.51	0.009	[125]	332.53	26	8.1-76	0-1	3.14	0.010	[126]

$$MRD(P) = 3.25\% ; \Delta y_{C_6H_{14}} = 0.009$$

$$n-C_6H_{14} + C_5H_{11}OH ; k_{ij}(T) = 0.00153 + 1.63 \times 10^{-5} T$$

$T/K$	Nº Points	Range $P/10^{-3}MPa$	Range $x_{C_6H_{14}}$	$MRD(P)/\%$	$\Delta y_{C_6H_{14}}$	Ref.	$T/K$	Nº Points	Range $P/10^{-3}MPa$	Range $x_{C_6H_{14}}$	$MRD(P)/\%$	$\Delta y_{C_6H_{14}}$	Ref.
303.15	15	0.44-24	0-1	2.35	0.004	[127]	323.15	15	1.8-54	0-1	3.02	0.007	[127]

$$MRD(P) = 2.68\% ; \Delta y_{C_6H_{14}} = 0.005$$

$$n-C_6H_{14} + C_6H_{13}OH ; k_{ij}(T) = 0.00153 + 2.12 \times 10^{-5} T$$



<i>T</i> / <i>K</i>	Nº Points	Range <i>P</i> / 10 <sup>-3</sup> MPa	Range <i>x</i> <sub>C<sub>6</sub>H<sub>14</sub></sub>	<i>MRD</i> ( <i>P</i> )/%	$\Delta y_{C_6H_{14}}$	Ref.	<i>T</i> / <i>K</i>	Nº Points	Range <i>P</i> / 10 <sup>-3</sup> MPa	Range <i>x</i> <sub>C<sub>6</sub>H<sub>14</sub></sub>	<i>MRD</i> ( <i>P</i> )/%	$\Delta y_{C_6H_{14}}$	Ref.
293.15	23	0.06-16	0-1	3.70		[128]	328.21	11	0.95-65	0-1	1.17		[129]
298.23	11	0.11-20	0-1	2.42	0.000	[129]	333.15	23	1.3-76	0-1	1.51		[128]
303.15	23	0.14-25	0-1	2.82		[128]	333.16	11	1.3-76	0-1	1.58		[129]
303.15	11	0.16-25	0-1	2.11		[129]	338.18	11	1.8-90	0-1	1.94		[129]
308.15	11	0.23-31	0-1	2.56		[129]	342.82	11	2.3-104	0-1	2.28	0.004	[129]
313.15	23	0.32-37	0-1	1.68		[128]	343.15	23	2.3-105	0-1	1.86		[128]
313.22	11	0.33-37	0-1	0.82		[129]	353.15	23	4.1-142	0-1	2.18		[128]
318.21	11	0.48-45	0-1	0.31		[129]	363.15	22	6.9-188	0-1	2.38		[128]
323.15	23	0.65-54	0-1	1.40		[128]	373.15	23	11-245	0-1	2.46		[128]
323.16	11	0.68-54	0-1	0.67	0.001	[129]							
<i>MRD</i> ( <i>P</i> ) = 1.81% ; $\Delta y_{C_6H_{14}}$ = 0.002													

**Table 8.-** PC-SAFT EoS temperature-dependent binary interaction parameters,  $k_{ij}(T)$ , and mean relative deviations in critical temperature and pressure,  $MRD(T_c)$  and  $MRD(P_c)$ , for  $\{CO_2 + n - C_mH_{2m+1}OH (m = 1 - 4)\}$  systems obtained using the parameters from Table 10. Average deviations for each system are also included.

System	$k_{ij}(T)$	Range T/ K	Nº Points	Range P/ MPa	Range $x_{CO_2}$	$MRD(T_c)/\%$	$MRD(P_c)/\%$	Ref.
CO <sub>2</sub> +								
CH <sub>3</sub> OH	$-0.0323 + 2.88 \times 10^{-4} T$	304-513	30	7.38-16.39	0-1	1.17	5.97	This work
		304-513	18	7.42-16.34	0-1	2.86	6.30	[54]
		304-492	20	7.39-16.41			3.45	[70]
		323-473	4	9.55-16.13	0.27-0.84	3.10	11.0	[71]
		321-473	19	9.5-16.5			2.90	[72], [73]
		323-408	4	9.80-18.50	0.42-0.75	12.5	28.2	[74]
		307-422	11	7.35-16.41	0.49-0.98	5.49	15.7	[75]
		313.2	1	8.21	0.968	2.97	0.49	[76]
		313-343	5	8.15-12.40	0.76-0.94	2.53	15.0	[77]
		305-320	8	7.62-9.35	0.93-0.99	0.69	2.04	[78]
		323-478	4	9.50-16.50	0.25-0.85	2.54	7.17	[79]
		304-317	4	7.38-9.24	0.96-1	0.72	7.53	[80]
		304-328	6	7.38-10.49	0.79-1	1.78	10.8	[81]
		$MRD(T_c) = 2.67\% ; MRD(P_c) = 7.17\%$						
C <sub>2</sub> H <sub>5</sub> OH	$2.60 \times 10^{-4} T$	304-514	21	6.17-15.08	0-1	0.77	3.93	This work
		323-483	15	9.6-15.4			4.25	[73]
		310-410	7	7.77-15.17	0.60-0.96	1.16	2.62	[75]
		313.2	1	8.15	0.970	1.70	4.30	[76]
		313-345	5	8.16-11.97	0.80-0.96	0.87	5.06	[77]
		306-325	8	7.65-9.74	0.93-0.99	0.54	4.41	[78]
		304-514	6	6.15-15.30	0-1	5.63	15.5	[82]
		321-364	10	9.10-13.86	0.83-0.93	2.06	14.1	[83]
		304-321	5	7.38-9.27	0.93-1	0.31	3.49	[84]
		313-333	2	8.03-10.71	0.89-0.97	0.74	9.27	[85]
		313-343	4	8.1-11.9			7.68	[86]
		308.15	1	7.794	0.9940	0.80	4.60	[87]
		333.53	1	10.75	0.850	0.60	8.80	[88]
		313-373	5	8.15-14.34	0.72-0.97	1.19	4.70	[89]
		308.15	1	7.702	0.9797	0.60	0.38	[90]
		318.15	1	8.80	0.9649	1.60	11.4	[91]
383-493	2	8.87-14.72	0.20-0.70	1.18	3.85	[92]		

		$MRD(T_c) = 1.37\% ; MRD(P_c) = 6.17\%$						
$C_3H_7OH$	$2.65 \times 10^{-4} T$	304-537	21	5.18-15.97	0-1	0.97	3.48	This work
		313-353	3	8.19-13.40	0.87-0.98	1.46	13.4	[68]
		323-513	18	8.4-16.0			2.62	[73]
		314-424	9	8.44-16.00	0.64-0.97	1.53	2.08	[75]
		307-320	6	7.58-9.00	0.96-0.99	0.27	2.35	[78]
		352.83	1	13.33	0.833	1.50	10.8	[88]
		426.68	1	15.335	0.540	5.78	4.28	[94]
		$MRD(T_c) = 1.16\% ; MRD(P_c) = 3.53\%$						
$C_4H_9OH$	$2.90 \times 10^{-4} T$	304-563	27	4.42-17.27	0-1	1.88	6.92	This work
		323-533	17	8.5-17.4			2.58	[73]
		315-427	6	8.71-17.37	0.71-0.97	2.78	5.00	[75]
		305-329	8	7.58-10.81	0.967-0.997	0.43	5.19	[78]
		324-427	5	9.80-17.03	0.75-0.93	3.74	5.06	[95]
		313.15	1	8.23	0.987	0.78	3.40	[96]
		$MRD(T_c) = 1.92\% ; MRD(P_c) = 5.17\%$						

**Table 9.-** PC-SAFT EoS temperature-dependent binary interaction parameters,  $k_{ij}(T)$ , mean relative deviations in bubble pressure,  $MRD (P)$ , and absolute deviations for the solvent mole fraction in the vapor phase,  $\Delta y_{CO_2}$ , for  $\{CO_2 + n - C_m H_{2m+1} OH (m = 1 - 4)\}$  systems obtained using the parameters from Table 10. Average deviations for each system are also included.

<b>CO<sub>2</sub> + CH<sub>3</sub>OH ; <math>k_{ij}(T) = -0.0323 + 2.88 \times 10^{-4} T</math></b>													
<b>T / K</b>	<b>Nº Points</b>	<b>Range P / MPa</b>	<b>Range <math>x_{CO_2}</math></b>	<b>MRD (P) / %</b>	<b><math>\Delta y_{CO_2}</math></b>	<b>Ref.</b>	<b>T / K</b>	<b>Nº Points</b>	<b>Range P / MPa</b>	<b>Range <math>x_{CO_2}</math></b>	<b>MRD (P) / %</b>	<b><math>\Delta y_{CO_2}</math></b>	<b>Ref.</b>
213.15	4	0.10-0.43	0.09-0.58	16.9	0.001	[145]	313.14	17	1.32-8.03	0.07-0.88	4.62	0.002	[152]
228.15	7	0.10-0.71	0.05-0.45	11.7	0.001	[145]	313.14	17	1.32-7.72	0.07-0.88	4.97	0.002	[153]
230.00	6	0.69-0.88	0.38-0.96	9.37	0.000	[146]	313.14	16	0.57-7.78	0.03-0.74	2.69	0.007	[139]
233.15	6	0.30-0.89	0.11-0.54	8.53		[147]	313.15	11	0.69-8.12	0.04-0.94	4.16	0.010	[77]
237.15	9	0.10-1.01	0.03-0.47	8.78	0.001	[145]	313.15	8	1.29-6.76	0.07-0.47	6.9	0.004	[150]
243.15	6	0.20-1.33	0.06-0.71	11.0		[148]	313.15	9	0.58-8.06	0.03-0.90	4.07	0.002	[154]
247.15	10	0.10-1.16	0.02-0.62	5.42	0.001	[145]	313.15	5	4.20-7.82	0.24-0.87	4.65		[158]
248.15	7	0.33-1.69	0.08-1	5.61		[147]	313.15	5	4.20-7.82	0.24-0.87	4.65		[159]
250.00	7	0.69-1.75	0.16-0.93	4.52	0.000	[146]	313.2	13	0.70-8.07	0.04-0.87	2.81	0.003	[76]
253.15	6	0.55-1.52	0.11-0.49	10.2		[147]	313.2	7	0.93-7.93	0.05-0.79	4.04		[162]
258.15	6	0.22-2.13	0.04-0.72	5.55		[148]	313.4	8	0.68-7.71	0.03-0.62	9.31	0.006	[163]
258.15	4	0.51-1.65	0.09-0.35	1.20	0.042	[149]	320.15	10	0.60-8.93	0.03-0.88	5.22	0.004	[77]
263.15	4	0.79-2.53	0.12-0.67	2.10	0.003	[150]	323	14	0.50-9.00	0.02-0.64	11.5	0.009	[74]
273.15	10	0.69-3.45	0.08-0.99	2.57	0.000	[146]	323.15	10	1.03-9.51	0.04-0.81	8.55	0.015	[66]
273.15	9	0.45-3.30	0.06-0.76	3.54		[147]	323.15	13	0.99-9.53	0.04-0.82	5.14		[71]
273.15	20	0.66-3.49	0.08-1	1.55		[147]	323.15	13	0.99-9.53	0.04-0.82	5.77	0.010	[146]
273.15	6	0.19-3.19	0.02-0.65	1.74		[148]	323.15	5	5.06-9.24	0.24-0.87	6.73		[159]
273.15	4	0.89-3.27	0.11-0.67	1.22	0.002	[150]	323.2	10	0.06-9.42	0-0.79	7.83	0.008	[79]
278.15	8	1.50-3.93	0.12-0.82	10.3	0.001	[151]	330.00	11	0.78-10.57	0.03-0.82	4.94	0.014	[77]
288.15	7	1.50-4.95	0.11-0.83	10.3	0.001	[151]	330.00	13	0.69-10.65	0.02-0.85	5.57	0.009	[146]
290.00	9	0.69-5.16	0.05-0.97	2.96	0.001	[146]	333	12	9.51-10.90	0.78-0.96	7.08		[164]
291.1	12	0.56-4.93	0.06-0.88	23.6	0.005	[152]	333.15	5	5.70-10.78	0.24-0.87	6.08		[159]
291.2	11	0.56-4.33	0.06-0.76	25.5	0.004	[153]	335.65	11	0.84-11.45	0.03-0.79	5.61	0.022	[77]
293.15	6	0.79-5.03	0.06-0.61	5.54	0.003	[66]	342.8	13	0.67-12.39	0.02-0.76	5.38	0.030	[77]
298.1	6	1.30-5.42	0.09-0.54	3.25	0.003	[156]	343	12	9.45-12.58	0.80-0.95	5.75		[164]
298.15	30	0.50-5.99	0.03-0.83	6.38	0.001	[66]	343.15	5	6.44-12.16	0.24-0.87	6.49		[159]

298.15	17	1.73-6.23	0.12-0.97	4.05		[71]	348	16	0.05-11.00	0.01-0.43	7.44	0.007	[74]
298.15	13	1.73-5.75	0.12-0.65	4.95	0.001	[146]	352.6	9	0.82-13.53	0.02-0.65	8.09	0.021	[79]
298.15	11	0.78-5.08	0.06-0.56	5.41		[147]	353	10	8.11-13.89	0.80-0.95	2.55		[164]
298.15	8	0.26-5.38	0.02-0.57	2.94		[148]	363	10	11.74-14.78	0.77-0.93	6.22		[164]
298.15	9	1.50-6.08	0.10-0.88	8.00	0.002	[151]	363.15	8	0.97-8.56	0.03-0.27	8.20	0.013	[150]
298.15	8	0.79-5.95	0.06-0.90	2.59	0.001	[154]	373	16	0.50-11.00	0.005-0.32	7.95	0.027	[74]
298.15	13	0.22-6.13	0.01-0.96	1.41	0.002	[155]	373	10	10.79-15.28	0.77-0.91	7.16		[164]
298.16	17	0.92-5.71	0.07-0.88	3.85	0.004	[152]	373.15	11	2.01-15.42	0.04-0.67	10.6		[71]
298.16	17	0.92-5.71	0.07-0.88	3.98	0.004	[153]	373.15	10	3.81-15.42	0.09-0.67	9.85	0.023	[146]
303.1	7	1.24-5.51	0.07-0.45	6.93	0.002	[156]	373.15	9	2.16-12.07	0.04-0.36	12.7	0.023	[150]
303.15	6	0.84-5.40	0.05-0.42	6.15	0.003	[157]	383	6	11.76-15.56	0.77-0.84	6.58		[164]
303.15	5	3.24-6.41	0.24-0.87	2.41		[158]	393	17	1.00-13.00	0.01-0.31	10.0	0.012	[74]
303.15	5	3.24-6.41	0.24-0.87	2.41		[159]	393	5	11.00-14.71	0.80-0.84	7.42		[164]
303.18	16	0.89-6.32	0.07-0.88	4.29	0.004	[152]	394.2	9	1.03-16.29	0.01-0.55	7.74	0.036	[79]
303.18	16	0.89-6.32	0.07-0.88	4.22	0.003	[153]	423.15	10	3.67-16.08	0.05-0.47	6.53		[71]
308.15	9	1.54-7.43	0.09-0.89	7.54	0.006	[151]	423.15	10	3.67-16.13	0.05-0.52	6.53	0.046	[146]
308.15	16	1.32-7.01	0.09-0.88	3.57	0.002	[152]	473.15	3	7.52-12.80	0.07-0.24	5.55		[71]
308.15	16	1.32-7.01	0.09-0.88	3.57	0.003	[153]	473.15	3	7.52-12.80	0.07-0.24	5.58	0.047	[146]
310.00	19	0.69-7.74	0.03-0.97	3.70	0.002	[146]	477.6	8	5.29-12.51	0.02-0.21	4.63	0.031	[79]
310.15	19	0.48-7.60	0.020-0.97	5.08	0.003	[66]	298-373	70	1.54-15.55	0.10-0.91	6.82		[165]
313.0	11	1.14-7.53	0.07-0.60	2.83		[160]	298-423	46	6.08-16.46	0.49-0.98	2.10		[75]
313.1	5	1.59-6.34	0.09-0.42	3.98	0.004	[156]							

$$MRD(P) = 6.04\% ; \Delta y_{CO_2} = 0.008$$

$$CO_2 + C_2H_5OH ; k_{ij}(T) = 0.0625 + 1.23 \times 10^{-4} T$$

$T/K$	Nº Points	Range $P/$ MPa	Range $x_{CO_2}$	$MRD$ ( $P$ )/%	$\Delta y_{CO_2}$	Ref.	$T/K$	Nº Points	Range $P/$ MPa	Range $x_{CO_2}$	$MRD$ ( $P$ )/%	$\Delta y_{CO_2}$	Ref.
283	5	1.14-4.14	0.10-0.73	3.47	0.010	[166]	313.4	10	0.51-7.91	0.03-0.87	8.23	0.035	[163]
288	5	0.86-4.67	0.07-0.68	2.89	0.014	[166]	313.40	10	0.57-8.11	0.03-0.97	7.84	0.023	[77]
291.15	10	1.16-4.36	0.16-0.73	30.9	0.005	[152]*	313.46	10	1.74-8.02	0.10-0.93	6.59	0.027	[85]
291.15	13	2.45-5.53	0.19-0.98	7.64		[167]	314.2	8	5.54-7.92	0.34-0.87	8.27		[177]
291.15	9	2.09-5.40	0.18-0.99	3.69	0.005	[168]	314.45	6	7.07-8.30	0.55-0.95	7.09		[178]
291.15	3	3.30-4.73	0.24-0.49	12.4		[169]	314.5	6	5.55-7.89	0.34-0.84	9.92	0.021	[179]
291.15	10	1.16-4.36	0.16-0.73	39.5	0.004	[170]*	318.15	3	8.60-8.75	0.90-0.98	6.39		[91]
292	5	1.63-5.08	0.12-0.79	3.69	0.013	[166]	322.5	11	0.57-9.18	0.03-0.92	9.78	0.029	[77]

293.1	8	0.68-5.27	0.05-0.81	4.83	0.017	[67]	323.1	11	2.94-9.17	0.19-0.79	11.1	0.031	[173]
298.17	8	1.16-5.82	0.13-0.81	25.9	0.008	[152]*	323.1	4	5.03-8.20	0.25-0.51	13.0	0.013	[180]
298.17	13	2.79-6.37	0.19-0.98	5.61		[167]	323.15	3	4.93-8.11	0.24-0.49	10.8		[169]
298.17	8	1.16-5.82	0.13-0.81	32.2	0.008	[170]*	323.2	7	5.03-9.24	0.27-0.88	7.76	0.016	[86]
303.1	9	0.91-6.52	0.06-0.91	4.28	0.020	[67]	323.4	5	4.40-7.32	0.21-0.42	7.50	0.035	[172]
303.12	11	1.16-6.48	0.10-0.85	12.2	0.012	[152]	324.17	1	8.22	0.55	4.50		[178]
303.12	13	2.99-7.04	0.19-0.98	5.78		[167]	325.2	9	6.27-9.35	0.33-0.77	9.95	0.026	[179]
303.12	11	1.16-6.48	0.10-0.85	16.4	0.012	[170]	328.2	12	1.65-9.42	0.08-0.63	9.40	0.033	[175]
303.15	3	3.60-5.62	0.24-0.49	5.26		[169]	333.1	9	0.95-10.07	0.05-0.65	9.56	0.047	[67]
304.2	12	3.75-7.22	0.27-0.996	3.12	0.012	[171]	333.2	8	2.15-10.50	0.11-0.69	6.02		[83]
304.2	9	3.31-7.33	0.23-0.997	4.26	0.017	[172]	333.2	7	8.20-10.53	0.41-0.81	7.46	0.023	[86]
304.6	12	2.22-6.98	0.18-0.89	11.3	0.018	[173]	333.2	13	1.35-10.66	0.06-0.73	10.9	0.027	[176]
308.11	16	1.57-7.17	0.11-0.83	6.69	0.016	[152]	333.27	14	0.53-10.63	0.02-0.85	7.46	0.056	[85]
308.11	13	3.27-7.69	0.19-0.98	6.58		[167]	333.4	13	0.54-10.65	0.02-0.82	9.69	0.052	[163]
308.11	16	1.57-7.17	0.12-0.83	14.0	0.014	[170]	333.40	10	0.66-10.61	0.03-0.83	10.00	0.039	[77]
308.15	19	1.55-7.75	0.11-0.99	5.89	0.019	[87]	333.53	5	1.74-10.01	0.08-0.64	3.37	0.044	[88]
308.15	2	7.16-7.44	0.92-0.95	4.79		[90]	333.8	15	0.93-10.84	0.03-0.82	8.46	0.038	[89]
308.2	2	5.83-7.14	0.48-0.82	5.12	0.015	[166]	333.80	13	0.61-11.28	0.03-0.86	15.2	0.030	[77]
308.2	7	7.12-7.67	0.77-0.99	5.73	0.013	[171]	337.2	8	6.22-10.84	0.27-0.70	6.65	0.042	[179]
308.2	6	4.15-7.60	0.28-0.98	4.39	0.009	[174]	343.2	9	1.44-9.35	0.08-0.49	18.8		[83]
308.6	7	3.31-7.27	0.21-0.91	3.99	0.021	[172]	343.2	8	9.00-11.80	0.42-0.76	3.63	0.103	[86]
313.0	14	1.66-7.47	0.10-0.67	4.71	0.037	[89]	344.75	11	0.80-11.93	0.03-0.80	7.93	0.063	[77]
313.1	10	3.02-7.63	0.23-0.82	12.0	0.024	[173]	348.40	7	1.51-12.30	0.06-0.73	4.54	0.063	[89]
313.14	15	0.91-7.92	0.05-0.82	8.76	0.023	[152]	353.15	12	0.52-11.08	0.02-0.49	8.01	0.070	[67]
313.14	16	0.61-7.72	0.05-0.73	12.1	0.030	[139]	353.2	12	3.46-13.90	0.10-0.75	12.0	0.059	[176]
313.14	12	3.51-8.18	0.19-0.95	7.23		[167]	363.2	14	1.12-14.15	0.06-0.77	17.7		[83]
313.14	15	0.91-7.92	0.05-0.82	5.52	0.023	[170]	373.00	7	2.18-14.11	0.06-0.66	1.62	0.085	[89]
313.15	8	0.53-7.18	0.03-0.56	4.27	0.039	[67]	373.15	3	7.10-13.30	0.22-0.54	3.81	0.068	[181]
313.15	3	4.38-6.96	0.24-0.49	10.9		[169]	373.2	5	3.40-12.36	0.13-0.55	12.5		[83]
313.2	10	0.60-8.07	0.03-0.95	6.89	0.031	[76]	391.96	9	1.32-14.62	0.03-0.60	5.79	0.091	[88]
313.2	7	6.35-8.03	0.43-0.95	6.85	0.015	[86]	298-413	26	6.18-15.16	0.65-0.96	5.56		[75]
313.2	10	3.40-7.96	0.19-0.91	5.82	0.027	[172]	323-333	22	0.73-9.46	0.03-0.64	6.19	0.042	[160]
313.2	10	1.60-7.82	0.09-0.84	10.2	0.022	[175]	333-494	75	6.74-14.84	0.20-0.96	4.45		[92]
313.2	8	1.31-7.68	0.10-0.78	16.1	0.008	[176]							

$$MRD(P) = 7.85\% ; \Delta y_{CO_2} = 0.031$$

$$CO_2 + C_3H_7OH ; k_{ij}(T) = 0.118 - 2.15 \times 10^{-5} T$$

<i>T</i> /K	Nº Points	Range <i>P</i> / MPa	Range <i>x</i> <sub>CO<sub>2</sub></sub>	<i>MRD</i> ( <i>P</i> )/%	$\Delta y_{CO_2}$	Ref.	<i>T</i> /K	Nº Points	Range <i>P</i> / MPa	Range <i>x</i> <sub>CO<sub>2</sub></sub>	<i>MRD</i> ( <i>P</i> )/%	$\Delta y_{CO_2}$	Ref.
293.1	8	0.74-5.26	0.05-0.81	4.18	0.005	[68]	333.0	9	2.16-10.46	0.10-0.73	6.59	0.043	[183]
303.1	8	0.64-6.52	0.04-0.79	6.23	0.010	[68]	333.1	10	0.94-9.97	0.04-0.61	7.79	0.030	[68]
305.6	10	2.10-7.20	0.17-0.88	8.87	0.009	[173]	333.15	8	1.83-11.01	0.09-0.78	6.10	0.064	[184]
308.1	9	0.47-6.91	0.02-0.68	9.95	0.020	[182]	333.4	9	0.67-10.82	0.03-0.81	4.13	0.051	[163]
313.0	9	2.15-8.03	0.12-0.83	3.57	0.007	[183]	337.2	10	3.30-8.98	0.14-0.45	9.19	0.021	[185]
313.1	7	2.94-8.04	0.23-0.84	8.62	0.013	[173]	343.15	8	1.39-12.74	0.05-0.77	3.67	0.058	[184]
313.15	8	0.69-7.86	0.03-0.74	5.04	0.016	[68]	344.82	3	11.46-12.32	0.61-0.80	5.92	0.083	[186]
313.15	9	1.41-8.19	0.09-0.92	9.10	0.015	[184]	353.1	12	0.75-12.64	0.03-0.63	8.20	0.046	[68]
313.4	10	0.52-8.18	0.04-0.96	4.56	0.013	[163]	373.16	7	12.06-14.98	0.49-0.77	5.22	0.081	[186]
315.0	8	2.64-7.17	0.14-0.56	6.64	0.014	[185]	397.48	5	12.34-15.77	0.42-0.70	4.76	0.050	[186]
318.15	11	0.54-8.33	0.02-0.70	10.2	0.027	[182]	426.68	6	10.60-15.33	0.18-0.54	20.6	0.120	[186]
323.0	10	2.33-9.57	0.12-0.77	5.42	0.060	[183]	298-423	37	6.27-16.03	0.64-0.94	5.42		[75]
323.15	8	1.53-9.82	0.10-0.76	7.54	0.018	[184]							

$$MRD(P) = 6.89\% ; \Delta y_{CO_2} = 0.033$$

$$CO_2 + C_4H_9OH ; k_{ij}(T) = 0.190 - 1.93 \times 10^{-4} T$$

<i>T</i> /K	Nº Points	Range <i>P</i> / MPa	Range <i>x</i> <sub>CO<sub>2</sub></sub>	<i>MRD</i> ( <i>P</i> )/%	$\Delta y_{CO_2}$	Ref.	<i>T</i> /K	Nº Points	Range <i>P</i> / MPa	Range <i>x</i> <sub>CO<sub>2</sub></sub>	<i>MRD</i> ( <i>P</i> )/%	$\Delta y_{CO_2}$	Ref.
293.1	7	0.63-5.46	0.04-0.74	8.61	0.002	[187]	333.15	3	8.00-10.76	0.44-0.77	9.61		[189]
298.15	1	5.72	0.60	1.10		[189]	333.15	10	1.43-9.82	0.06-0.60	18.9	0.015	[190]
303.1	14	0.52-6.74	0.03-0.84	10.5	0.003	[187]	333.15	11	5.02-11.90	0.26-0.83	9.26	0.052	[195]
313.1	23	0.57-8.11	0.03-0.78	7.65	0.010	[187]	333.58	2	10.76-11.30	0.73-0.86	8.53	0.120	[95]
313.1	8	2.84-8.93	0.22-0.83	6.33	0.009	[188]	337.2	11	6.18-11.78	0.30-0.78	9.36	0.024	[179]
313.15	7	6.70-8.18	0.49-0.95	3.73	0.060	[96]	343.15	10	1.68-10.98	0.05-0.66	33.3	0.021	[190]*
313.15	3	6.39-7.79	0.10-0.65	3.50		[189]	343.15	8	5.02-12.02	0.24-0.64	11.4	0.023	[195]
313.15	8	1.67-7.68	0.09-0.65	11.1	0.009	[190]	353.15	8	5.02-12.02	0.22-0.57	13.8	0.023	[195]
313.15	10	1.69-8.31	0.10-0.95	7.87		[191]	354.06	9	2.07-12.98	0.10-0.68	7.71	0.026	[186]
313.2	8	6.02-7.96	0.41-0.87	5.88		[192]	355.38	2	13.91-14.20	0.75-0.82	4.43	0.082	[95]
313.22	7	2.14-8.06	0.13-0.85	10.3	0.008	[193]	363.17	9	3.09-14.89	0.12-0.76	12.4	0.028	[193]
313.4	9	2.73-8.31	0.16-0.72	11.3		[194]	383.1	11	2.02-16.50	0.08-0.77	7.00	0.024	[188]

314.8	8	4.63-7.98	0.28-0.70	8.14	0.024	[179]	392.72	5	14.57-16.78	0.60-0.81	1.17	0.069	[95]
323.15	3	7.17-9.45	0.44-0.77	9.65		[189]	398.98	10	2.12-15.53	0.08-0.62	7.97	0.000	[186]
323.15	8	2.03-9.27	0.10-0.67	13.8	0.017	[190]	426.95	5	11.89-16.94	0.42-0.70	3.84	0.067	[95]
324.1	15	1.65-10.09	0.09-0.88	7.90	0.094	[187]	430.25	10	2.37-16.13	0.07-0.61	11.0	0.070	[186]
324.16	4	9.63-9.77	0.80-0.90	11.2	0.218	[95]	303-428	28	7.06-17.35	0.71-0.97	4.37		[75]
325.3	9	5.23-9.87	0.29-0.81	10.4	0.051	[179]							
$MRD(P) = 8.76\% ; \Delta y_{CO_2} = 0.034$													

\*Data not included in the means due to their high deviations.



**Table 10.-** Association scheme and PC-SAFT EoS pure-compounds parameters used in the CO<sub>2</sub> + alkan-1-ol modellization.  $m$ ,  $\sigma$ ,  $\varepsilon$ : geometric parameters; for CO<sub>2</sub>, obtained in a previous work [27]; for the alkan-1-ols, rescaled in this work from  $T_c$  and  $P_c$ .  $\kappa^{A_i B_i}$  and  $\varepsilon^{A_i B_i}$ : association parameters extracted from reference [20].

Compound	Association scheme	$m / M$ (mol g <sup>-1</sup> )	$\sigma$ (Å)	$\varepsilon$ (K)	$\kappa^{A_i B_i}$	$\varepsilon^{A_i B_i}$ (K)
CO <sub>2</sub>	+ CH <sub>3</sub> OH: 2C	0.04834	2.8251	163.76		
CH <sub>3</sub> OH	2B	0.05273	3.3264	175.20	0.035176	2899.5
C <sub>2</sub> H <sub>5</sub> OH	Non	0.06554	3.1612	235.72		
C <sub>3</sub> H <sub>7</sub> OH	Non	0.05510	3.2881	236.77		
C <sub>4</sub> H <sub>9</sub> OH	Non	0.04208	3.6000	254.48		

FIGURE 1a

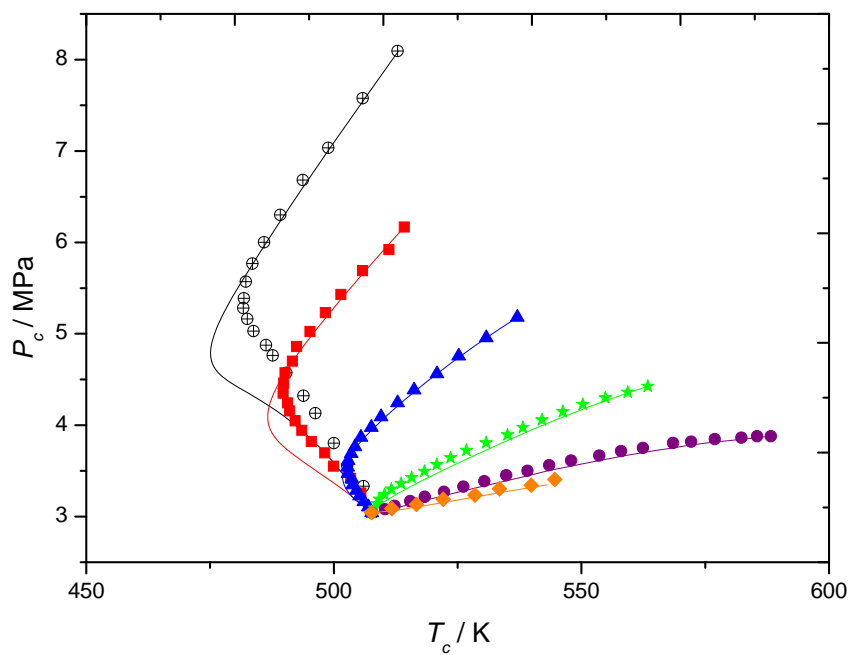


FIGURE 1b

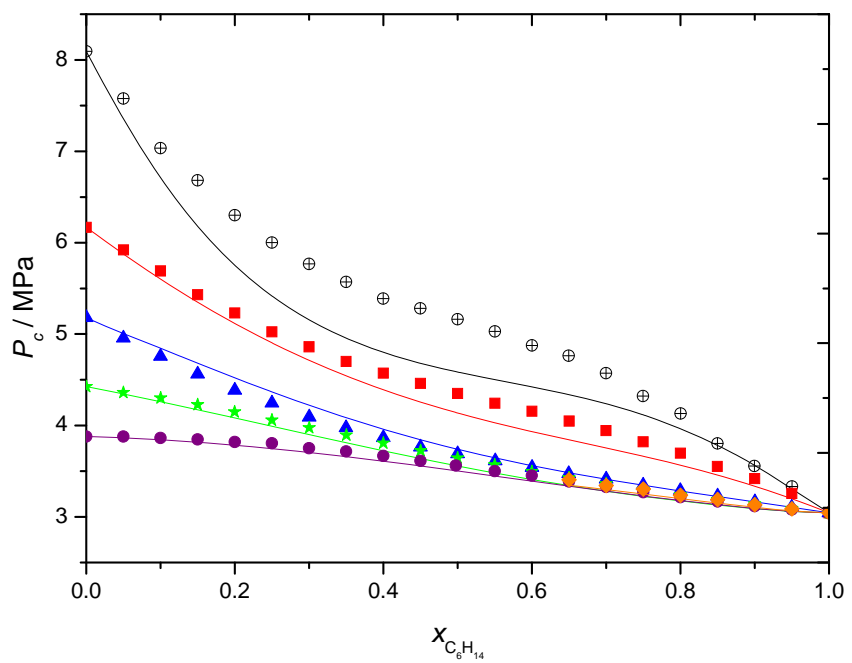


FIGURE 1c

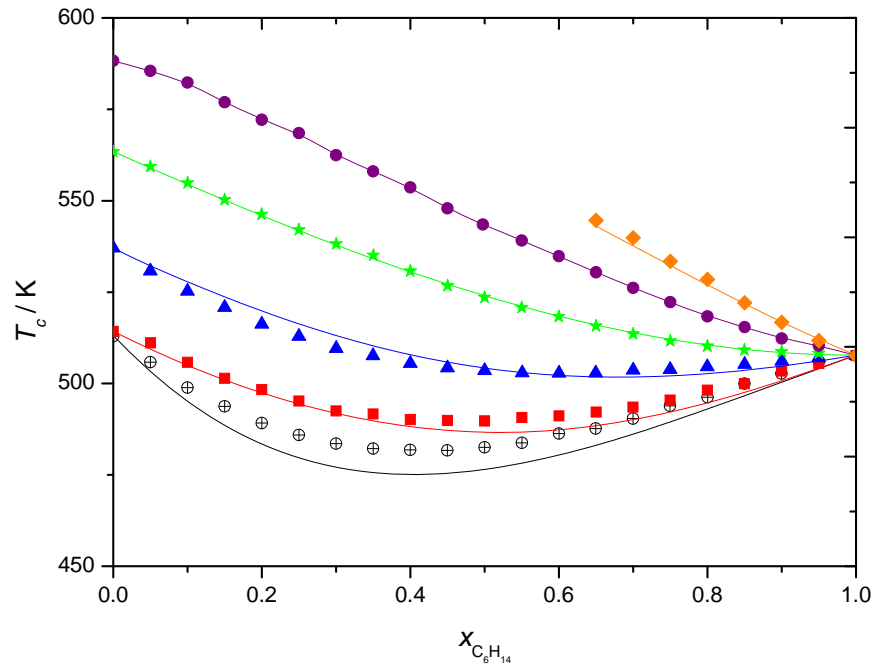


FIGURE 2a

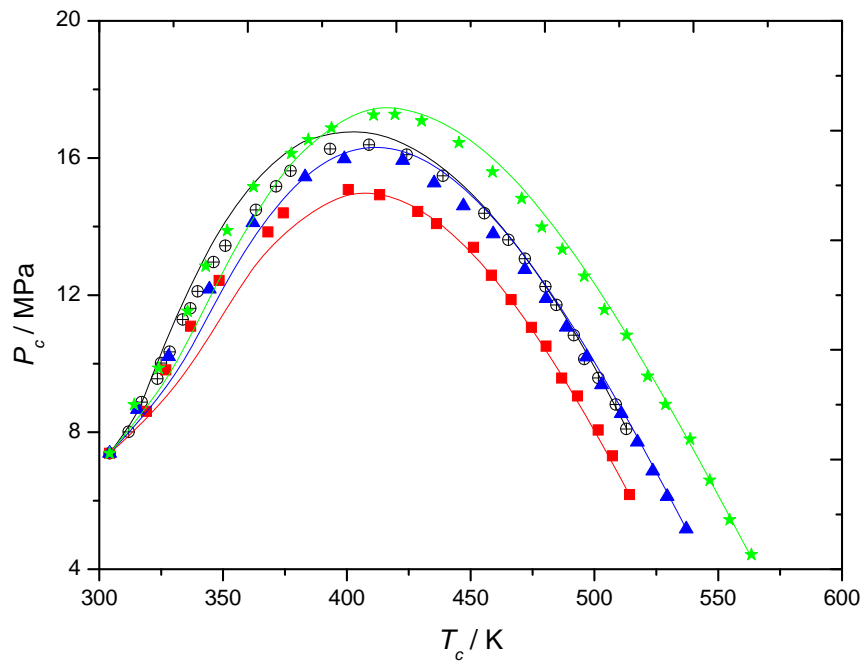


FIGURE 2b

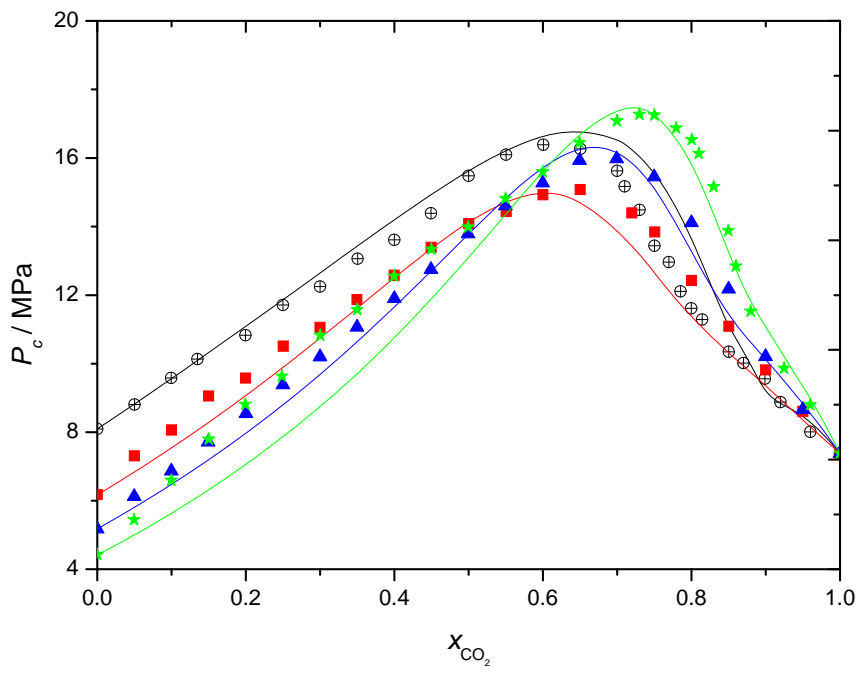


FIGURE 2c

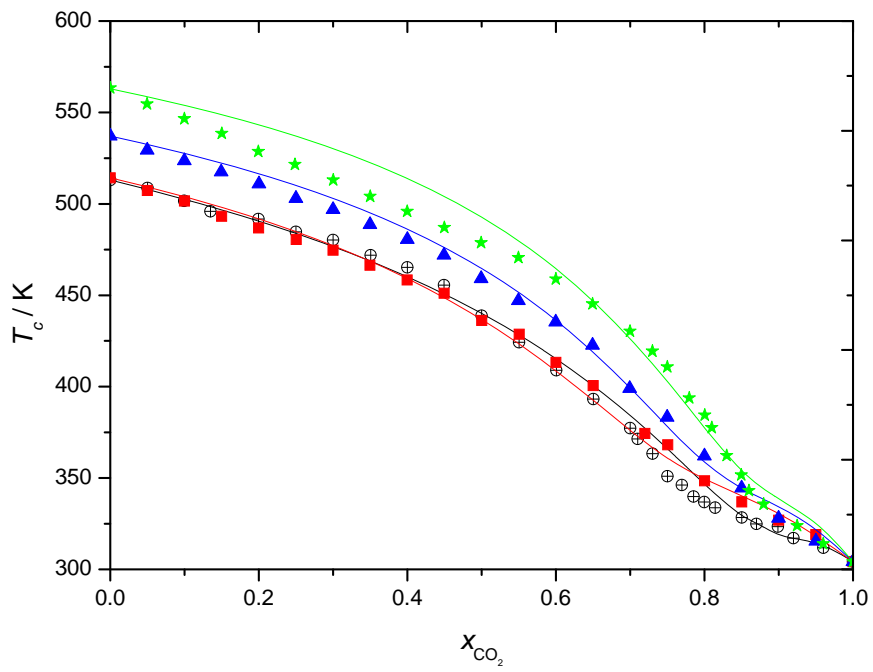


FIGURE 3

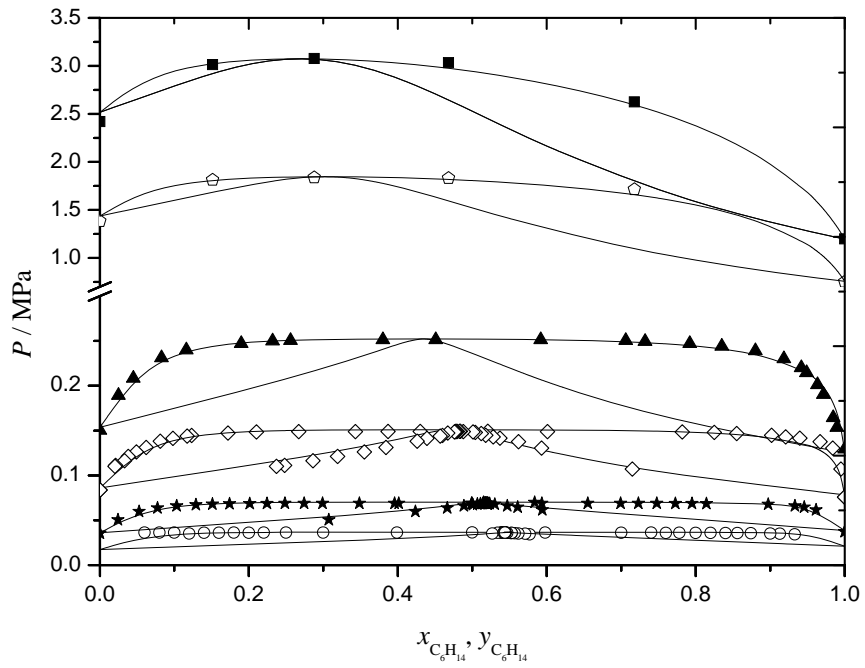


FIGURE 4

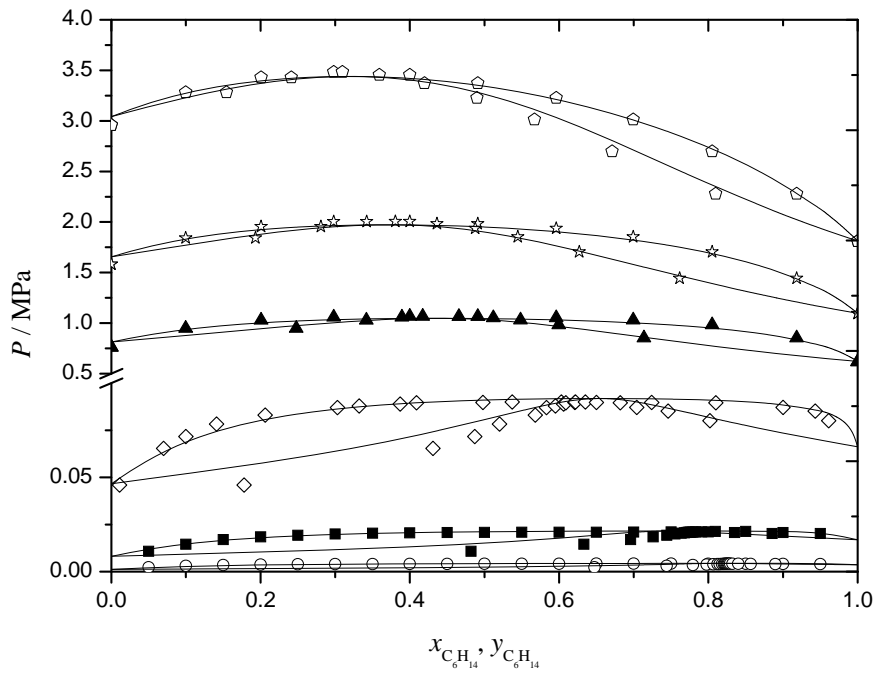


FIGURE 5

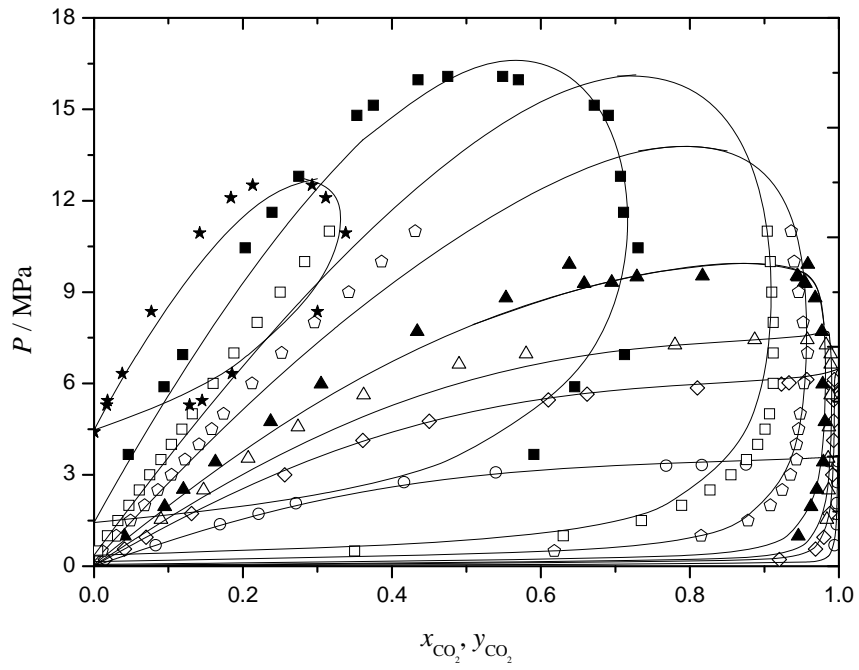
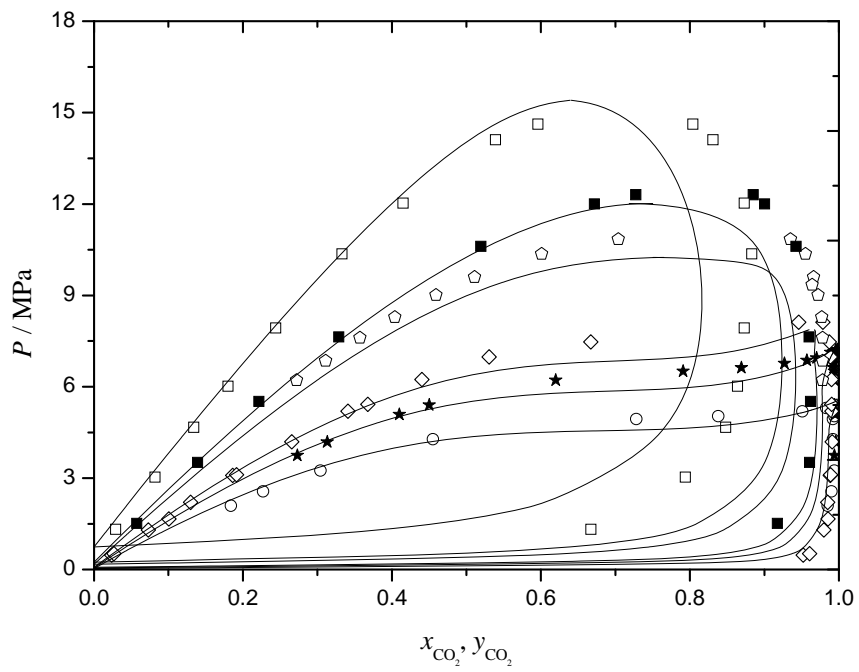


FIGURE 6



## SUPPLEMENTARY DATA

**Experimental determination of the critical loci for  $\{n\text{-C}_6\text{H}_{14}$  or  $\text{CO}_2$  + alkan-1-ol} mixtures. Evaluation of their critical and subcritical behavior using PC-SAFT EoS.**

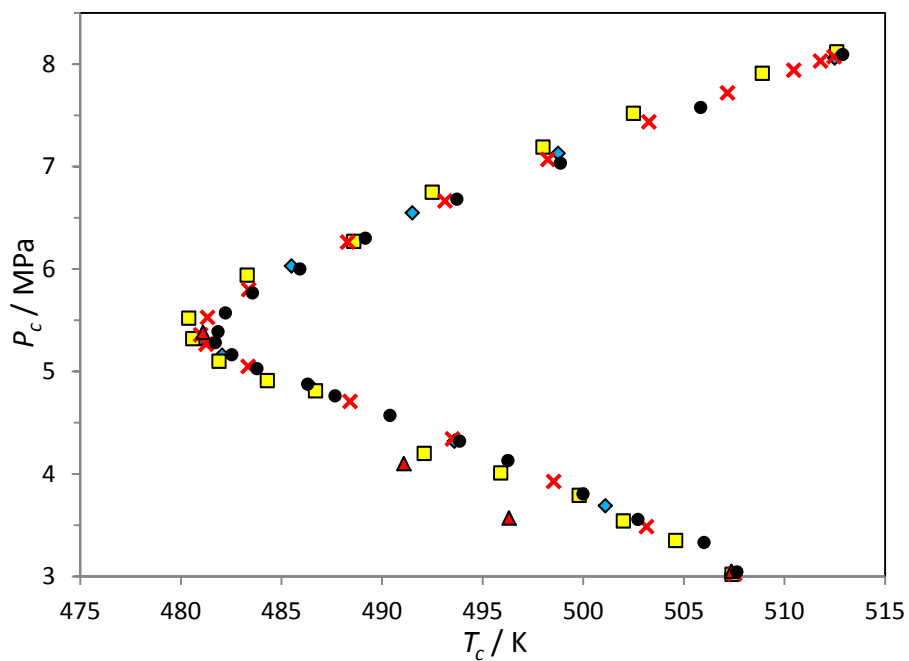
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**Figure SF1.** (a),  $(P_c, T_c)$ ; (b),  $(P_c, x)$  and (c),  $(T_c, x)$  projections for *n*-hexane + methanol critical locus. Experimental results from this work and literature: ●, this work; ◆, ref. [52]; ×, ref. [53]; □, ref. [54]; ▲, ref. [55].

**Figure SF1a**



**Figure SF1b**

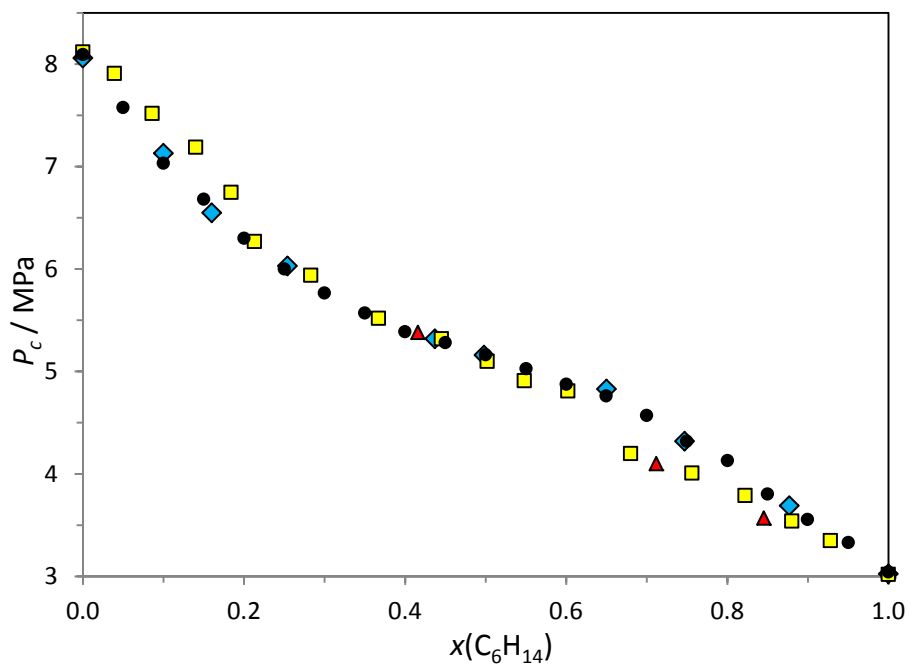




Figure SF1c

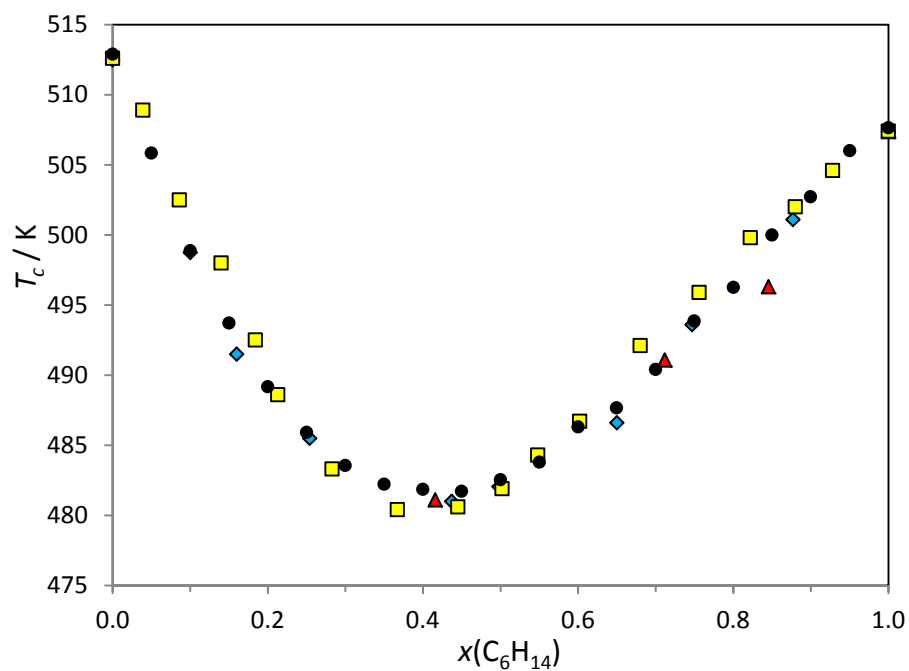


Figure SF2. (a), ( $P_c$ ,  $T_c$ ); (b), ( $P_c$ ,  $x$ ) and (c), ( $T_c$ ,  $x$ ) projections for *n*-hexane + ethanol critical locus. Experimental results from this work and literature: ●, this work; ◆, ref. [38]; □, ref. [56]; ▲, ref. [57]; +, ref. [58]; ×, ref. [59].

Figure SF2a

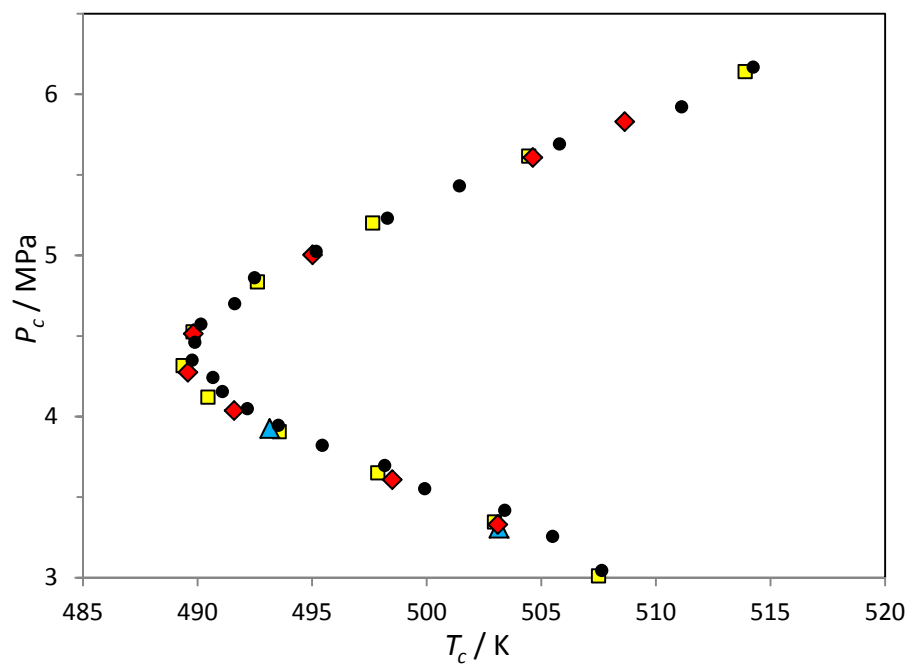


Figure SF2b

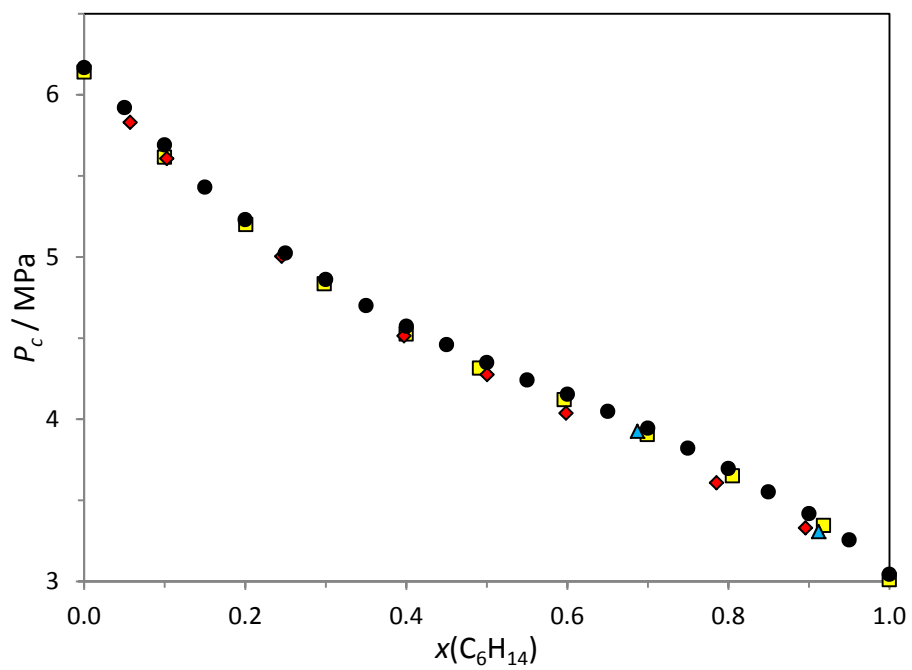
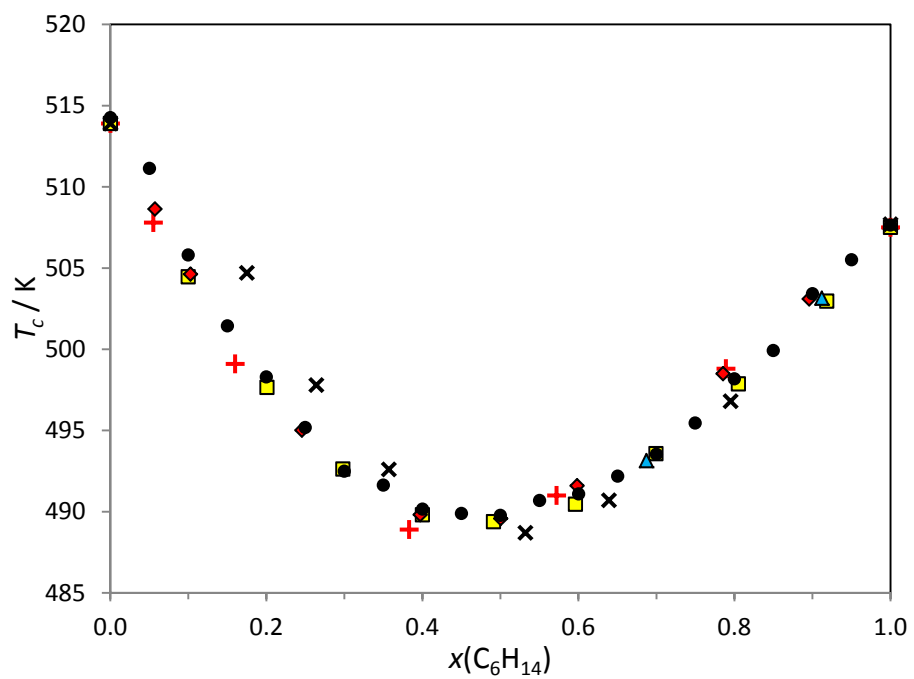
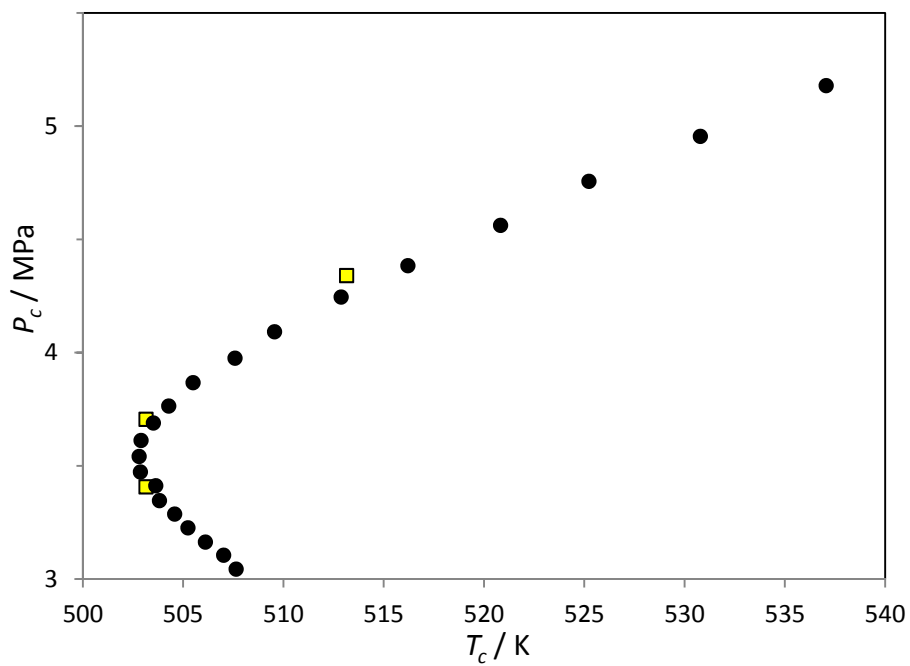


Figure SF2c



**Figure SF3.** (a),  $(P_c, T_c)$ ; (b),  $(P_c, x)$  and (c),  $(T_c, x)$  projections for *n*-hexane + propan-1-ol critical locus. Experimental results from this work and literature: ●, this work; ■, ref. [50]; ◆, ref. [60,61].

**Figure SF3a**



**Figure SF3b**

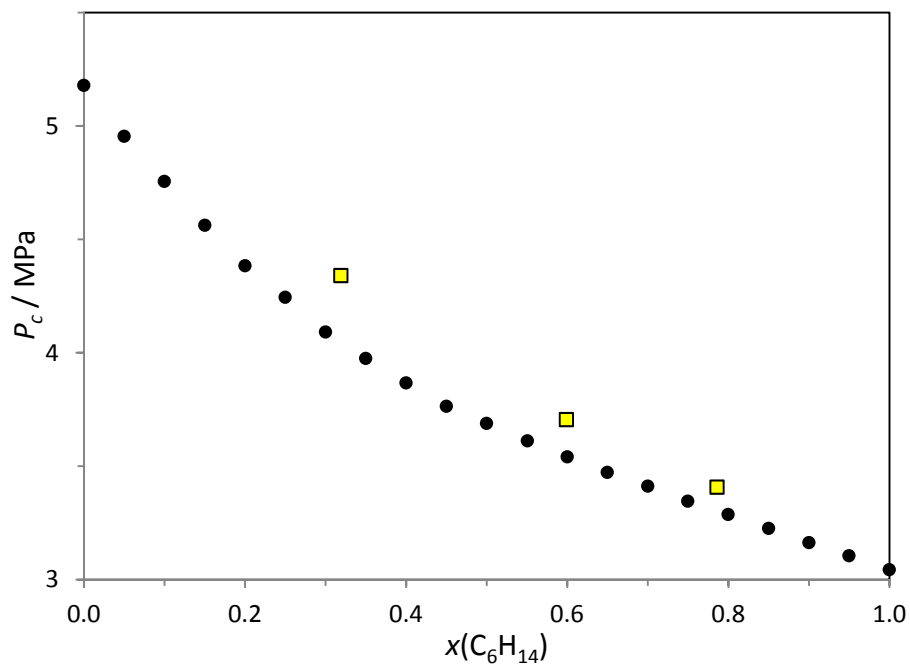


Figure SF3c

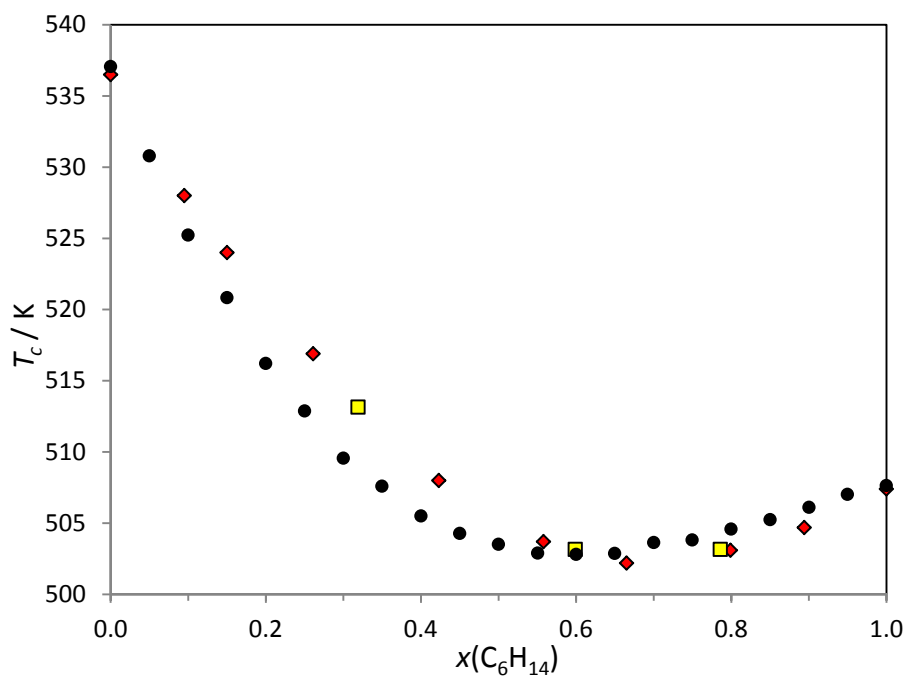


Figure SF4. (a),  $(P_c, T_c)$ ; (b),  $(P_c, x)$  and (c),  $(T_c, x)$  projections for *n*-hexane + butan-1-ol critical locus. Experimental results from this work and literature: ●, this work; ◆, ref. [60,61].

Figure SF4a

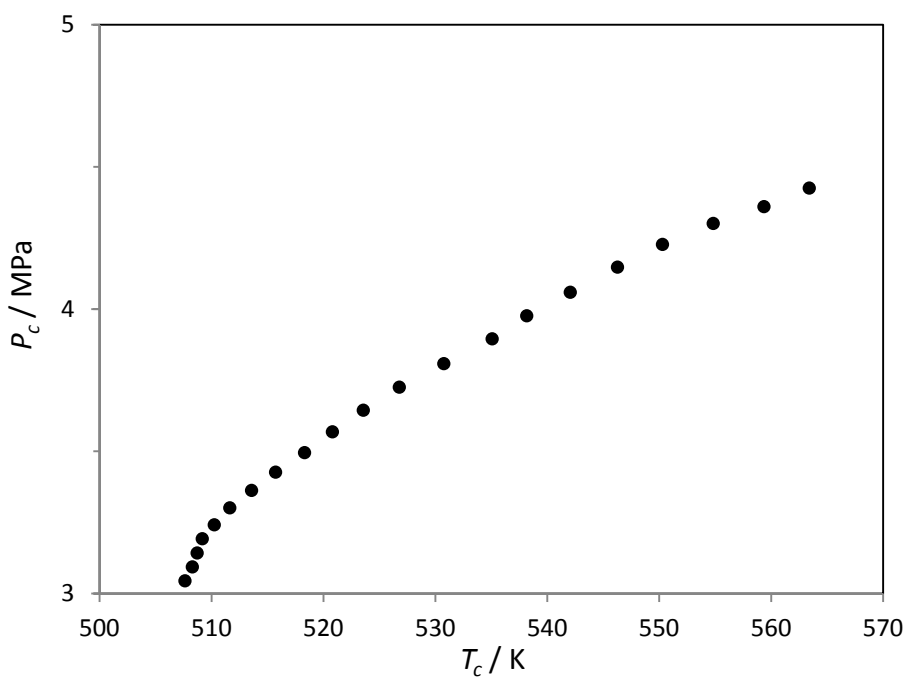


Figure SF4b

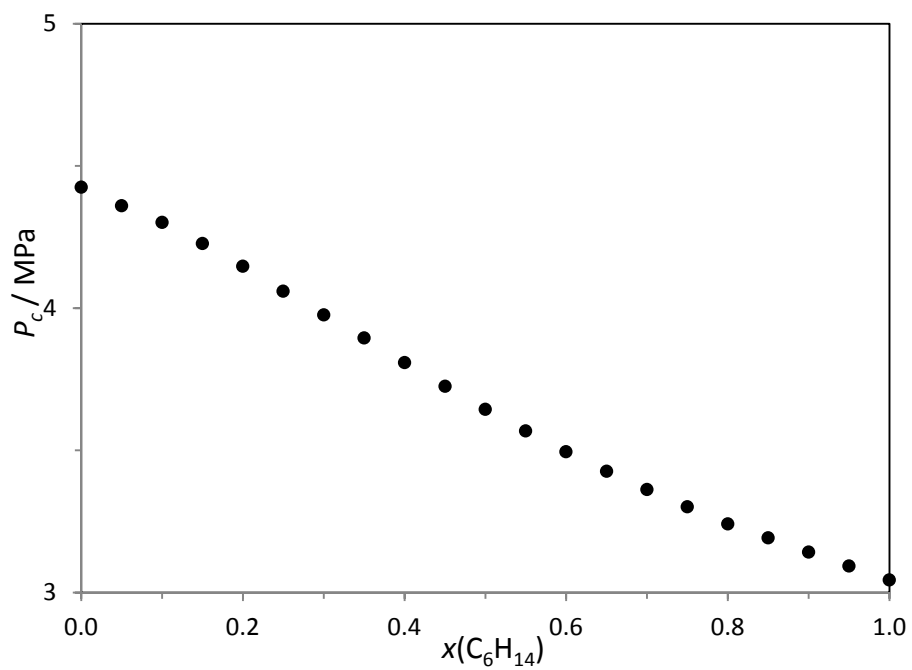
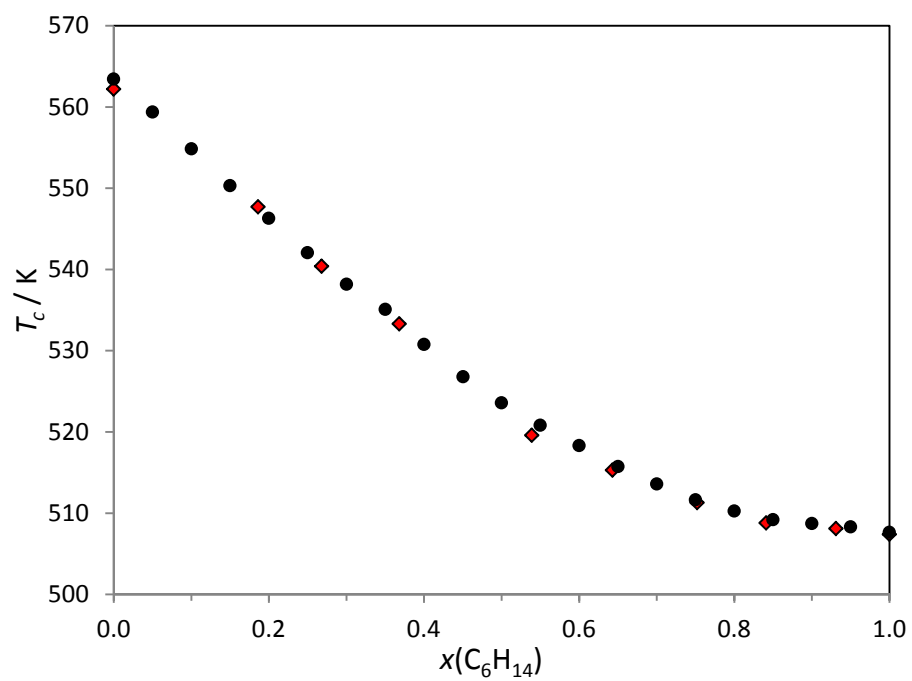
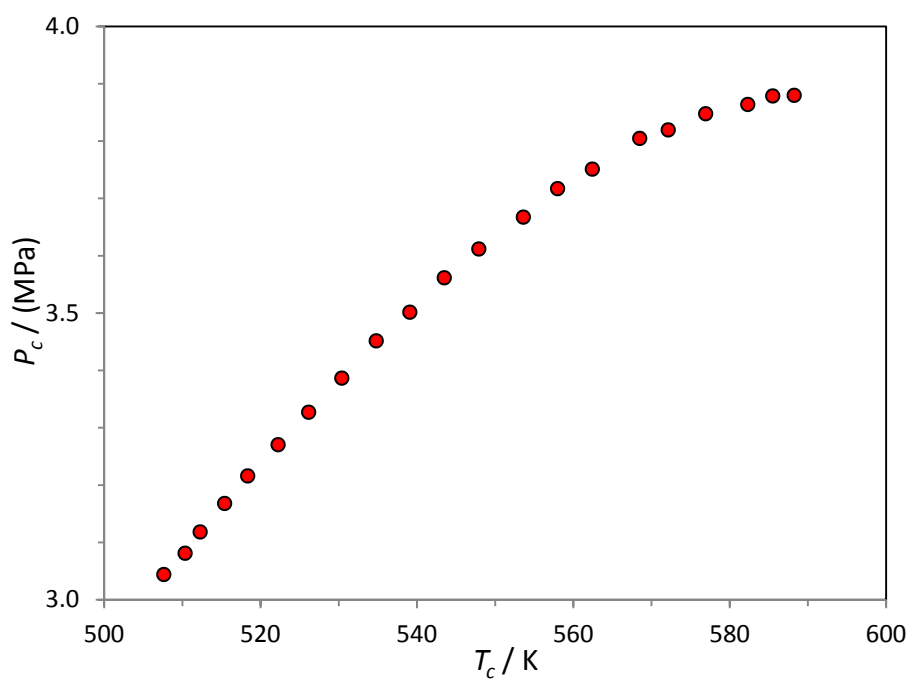


Figure SF4c



**Figure SF5.** (a),  $(P_c, T_c)$ ; (b),  $(P_c, x)$  and (c),  $(T_c, x)$  projections for *n*-hexane + pentan-1-ol critical locus. Experimental results from literature: **x**, ref. [59]; **■**, ref. [62]; **●**, ref. [63] (unpublished data).

**Figure SF5a**



**Figure SF5b**

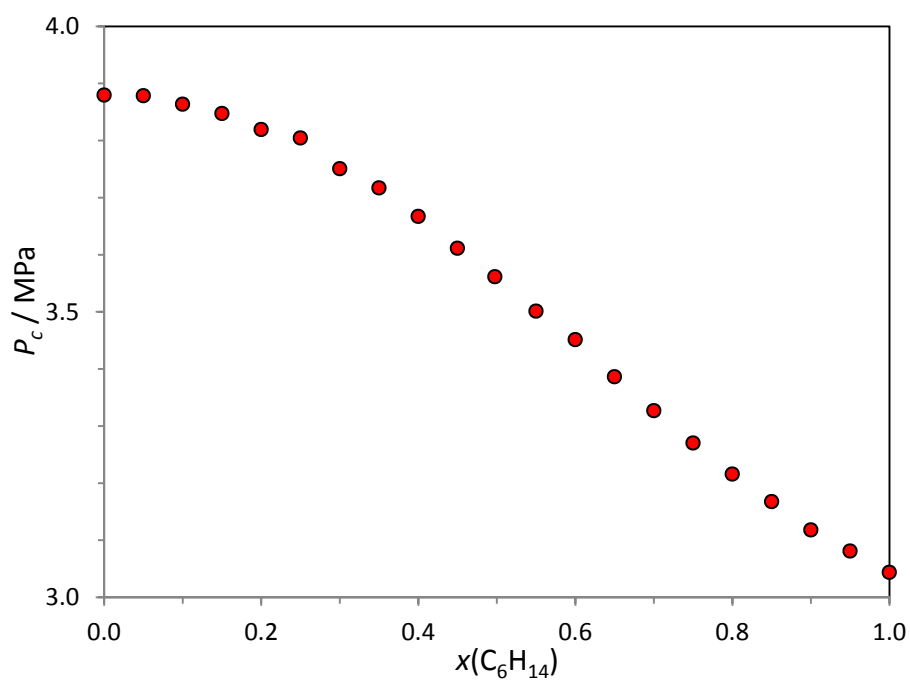


Figure SF5c

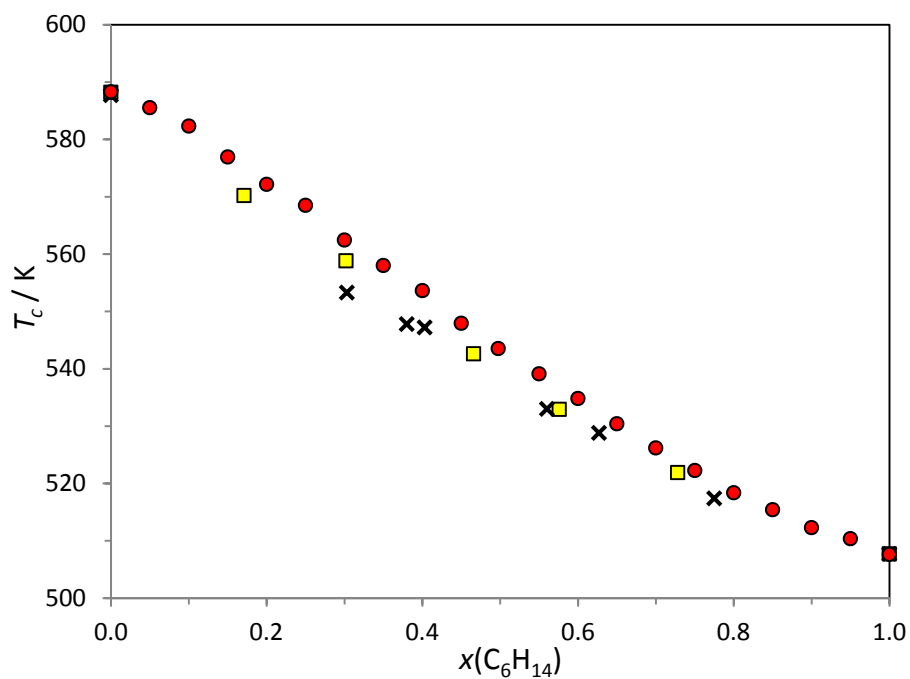


Figure SF6. (a), ( $P_c$ ,  $T_c$ ); (b), ( $P_c$ ,  $x$ ) and (c), ( $T_c$ ,  $x$ ) projections for *n*-hexane + hexan-1-ol critical locus. Experimental results from literature: ●, ref. [63] (unpublished data).

Figure SF6a

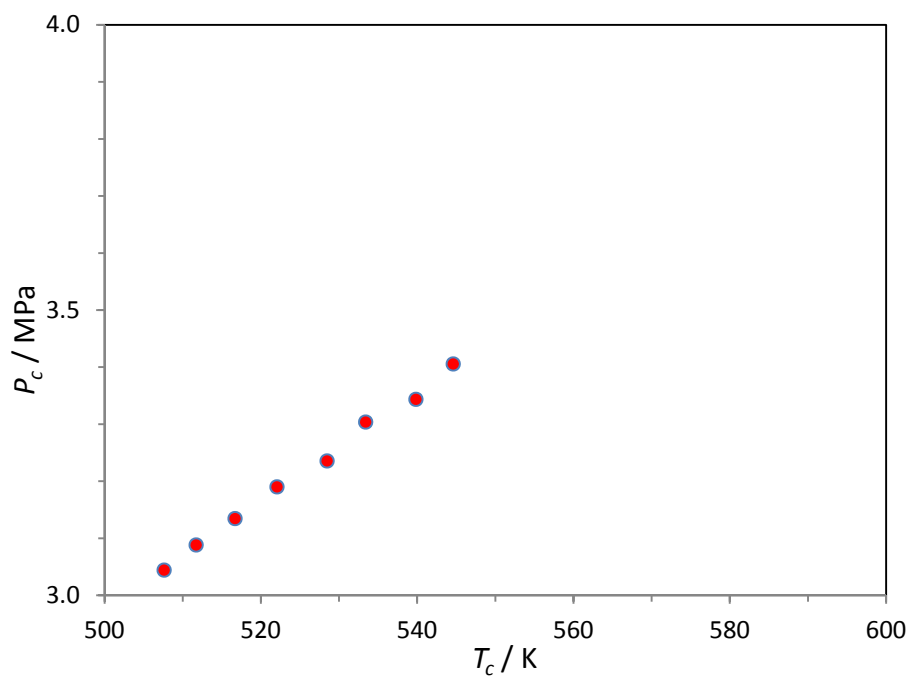


Figure SF6b

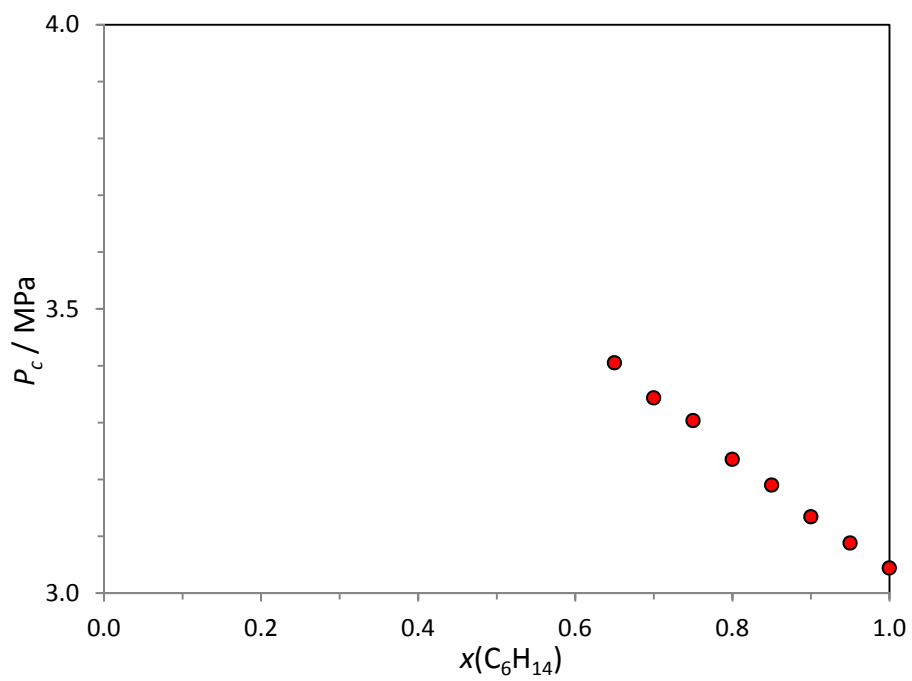
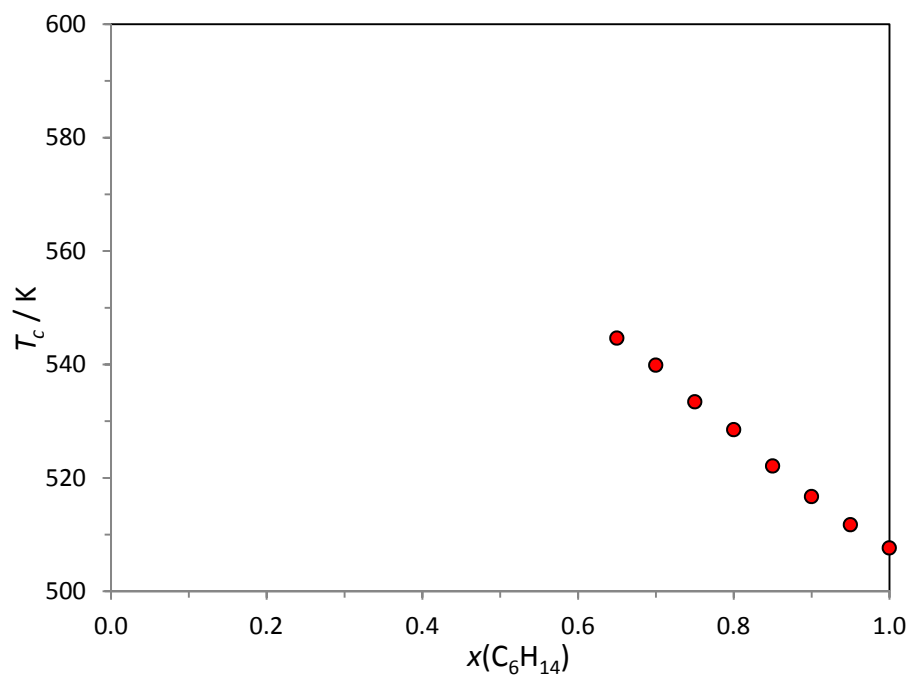


Figure SF6c





## Comparison between this work experimental data and those from literature for the critical loci of *n*-hexane + alkan-1-ol systems.

The results of our current investigation for *n*-hexane + methanol system are in good agreement with those from de Loos et al. [52] ( $x$ ,  $T_c$ ,  $P_c$ ) and Brunner [53] ( $P_c$ ,  $T_c$ ). Liu et al.'s [54] data are also in good agreement with ours in the  $P_c$ - $T_c$  projection; however, in  $T_c$ - $x$  and  $P_c$ - $x$  planes such agreement only holds for the central range of concentrations. Two of the three ( $x$ ,  $T_c$ ,  $P_c$ ) points from Zawisza [55] agree with ours in the  $T_c$ - $x$  projection, but the agreement in  $P_c$ - $T_c$  and  $P_c$ - $x$  is less marked.

For *n*-hexane + ethanol mixtures, Sauermann et al. [56], Seo et al. [57] and Soo et al. [38] provide ( $x$ ,  $T_c$ ,  $P_c$ ) data in very good agreement with our study. The agreement with Young [58] is a little worse and it is even worse compared with Morton et al. [59], whose results differ from those from this study and from other authors', especially in the alcohol-rich region, where the differences reach up to 6 K.

Oh et al.'s [50] is the only investigation in which ( $x$ ,  $T_c$ ,  $P_c$ ) were determined for the *n*-hexane + propan-1-ol system, but only at three compositions.  $P_c$ - $T_c$  projection is in good agreement with our current work, but  $P_c$ - $x$  and  $T_c$ - $x$  plots present some differences with ours, which become greater as the mixture becomes richer in propan-1-ol. Young [60] and Bone and Young [61] provide identical ( $x$ ,  $T_c$ ) data, in good agreement with Oh [50].

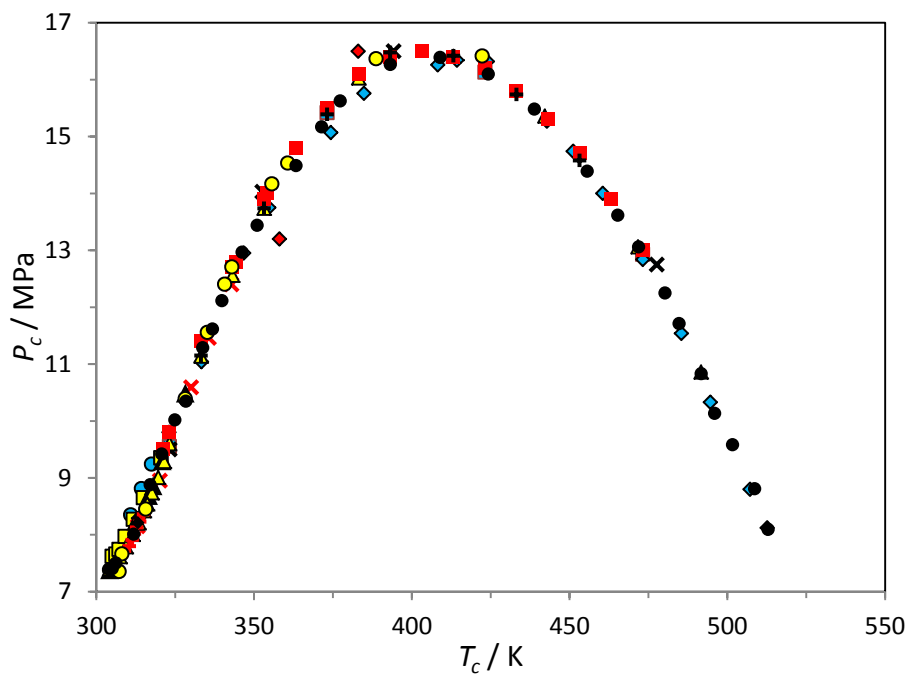
For *n*-hexane + butan-1-ol, we have only found two references, Young [60] and Bone and Young [61] which give identical data ( $x$ ,  $T_c$ ), in very good agreement with this work.

Christou, Sadus and Young [62] and Morton et al. [59] provide whole-composition ( $x$ ,  $T_c$ ) data for *n*-hexane + pentan-1-ol. Laga [63] (unpublished data), with the same apparatus that we used in our investigation, provides whole-composition ( $x$ ,  $T_c$ ,  $P_c$ ) data.  $T_c$  results from Christou et al. are slightly lower than Laga's data and those proposed by Morton are even lower than Christou values.

Unpublished results from Laga [63] were the only data found for *n*-hexane + hexan-1-ol system.

**Figure SF7.** (a),  $(P_c, T_c)$ ; (b),  $(P_c, x)$  and (c),  $(T_c, x)$  projections for CO<sub>2</sub> + methanol critical locus. Experimental results from this work and literature: ●, this work; ◆, ref. [54]; ▲, ref. [70]; ■, ref. [71]; ■, ref. [72,73]; +, ref. [73]; ◆, ref. [74]; ●, ref. [75]; ◆, ref. [76]; ×, ref. [77]; ■, ref. [78]; ×, ref. [79]; ●, ref. [80]; ▲, ref. [81]; +, ref. [93].

**Figure SF7a**



**Figure SF7b**

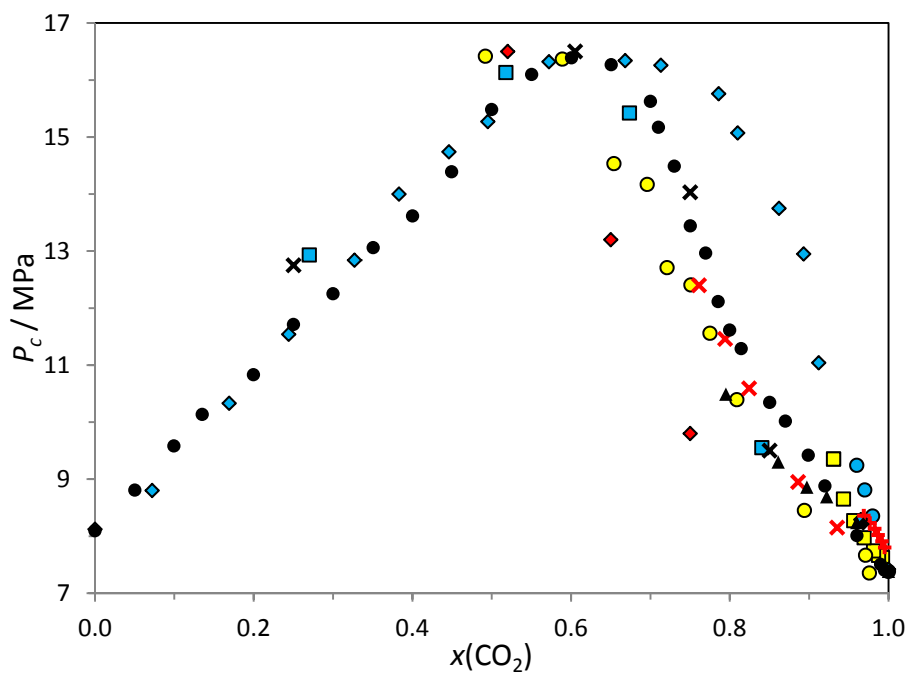
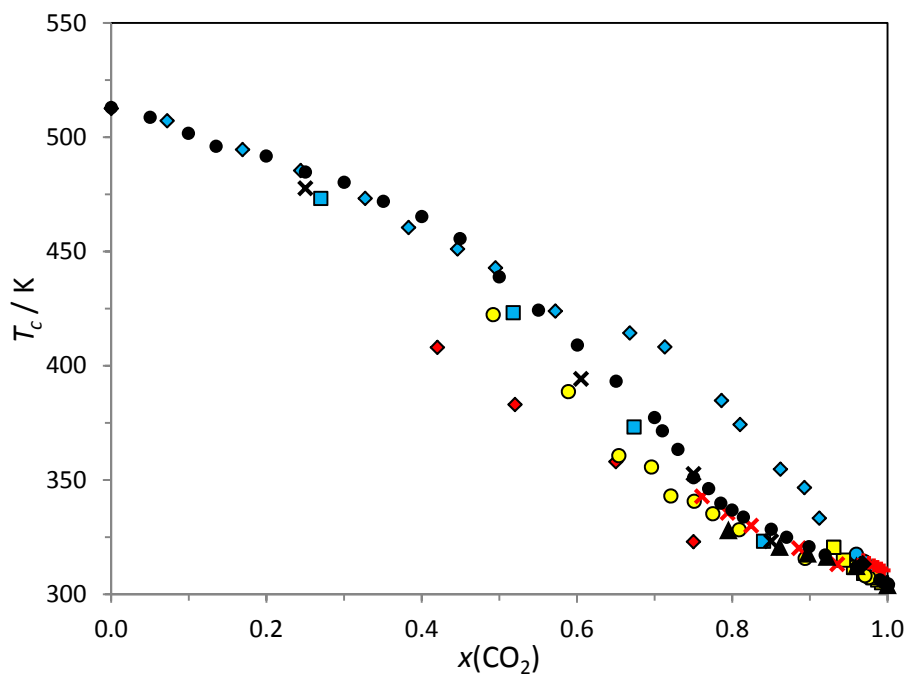


Figure SF7c



**Figure SF8.** (a), ( $P_c$ ,  $T_c$ ); (b), ( $P_c$ ,  $x$ ) and (c), ( $T_c$ ,  $x$ ) projections for CO<sub>2</sub> + ethanol critical locus. Experimental results from this work and literature: ●, this work; ■, ref. [73]; ●, ref. [75]; ◆, ref. [76]; ×, ref. [77]; □, ref. [78]; ◆, ref. [82]; ▲, ref. [83]; ▲, ref. [84]; ●, ref. [85]; +, ref. [86]; ×, ref. [87]; ▲, ref. [88]; ◆, ref. [89]; ◆, ref. [90]; □, ref. [91]; ●, ref. [92]; +, ref. [93].

Figure SF8a

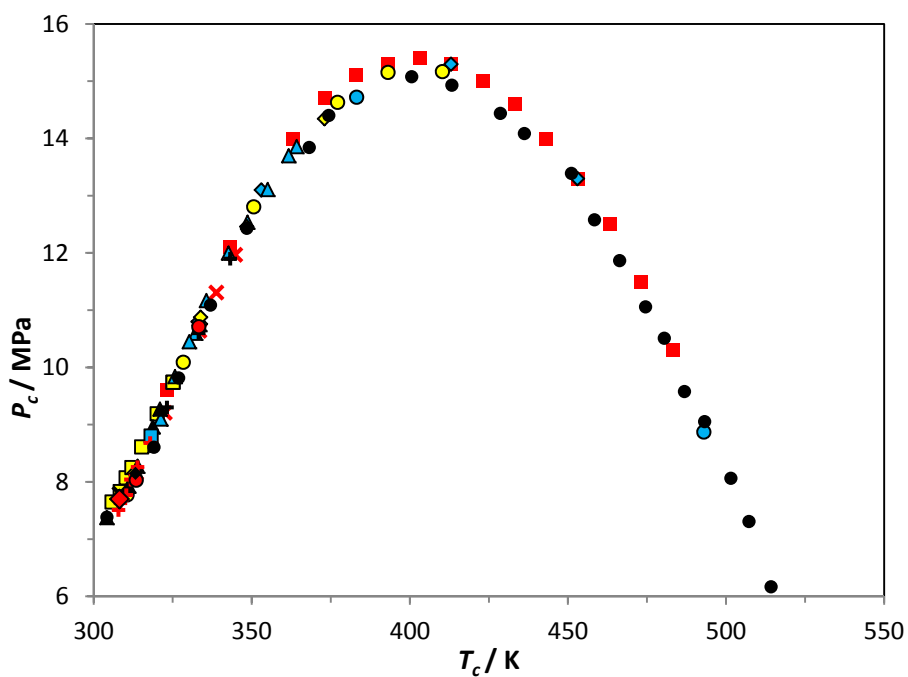


Figure SF8b

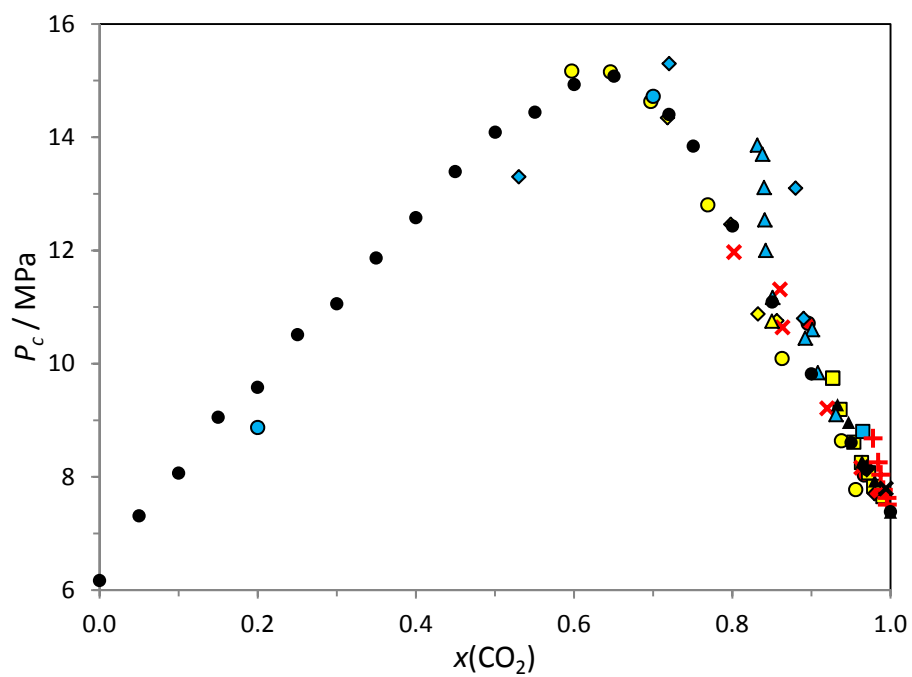
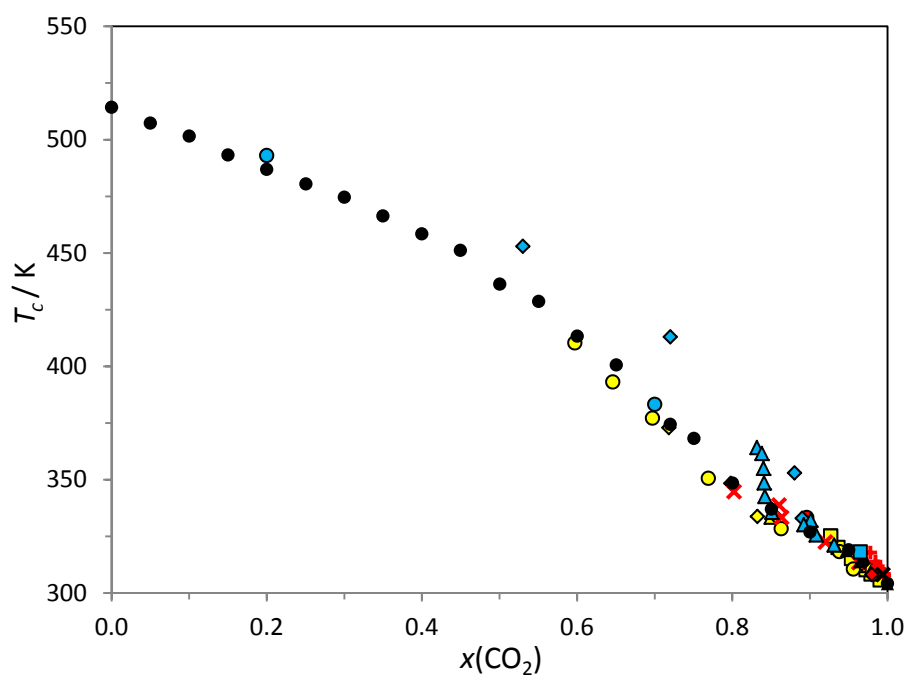
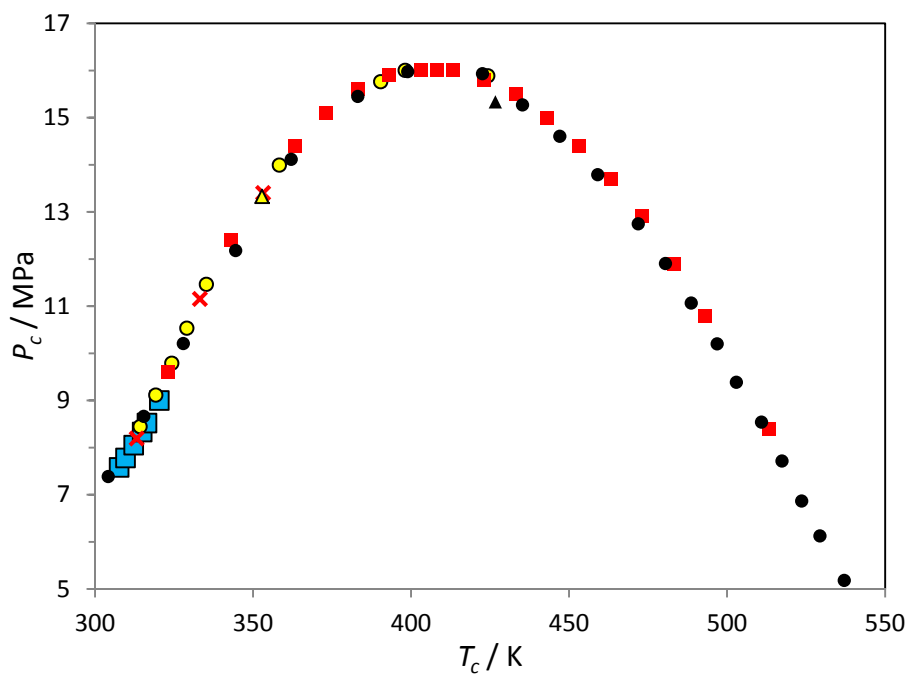


Figure SF8c



**Figure SF9.** (a),  $(P_c, T_c)$ ; (b),  $(P_c, x)$  and (c),  $(T_c, x)$  projections for CO<sub>2</sub> + propan-1-ol critical locus. Experimental results from this work and literature: ●, this work; ×, ref. [68]; ■, ref. [73]; ●, ref. [75]; ■, ref. [78]; ▲, ref. [88]; ▲, ref. [94].

**Figure SF9a**



**Figure SF9b**

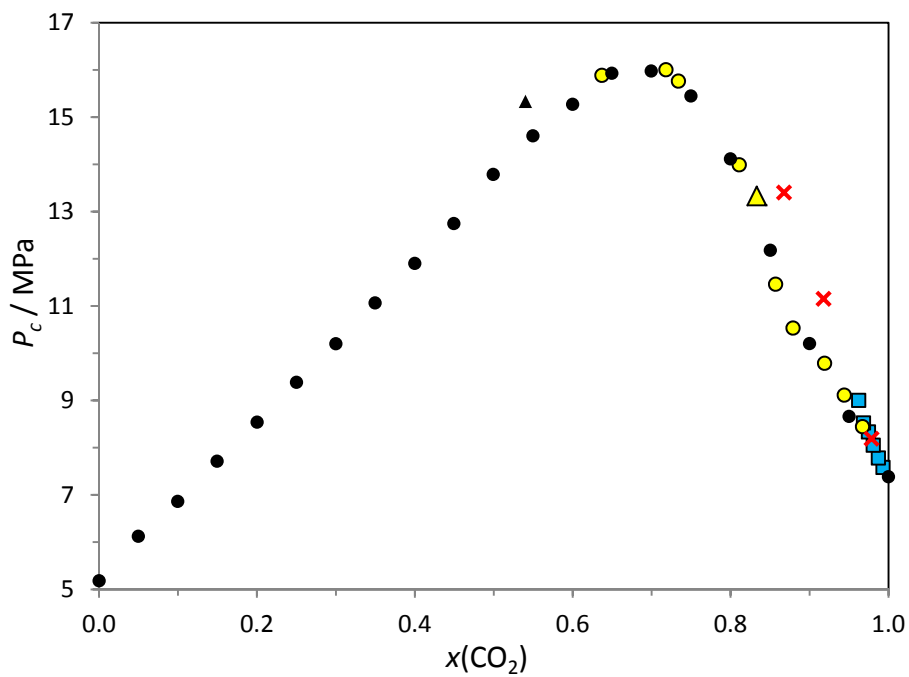


Figure SF9c

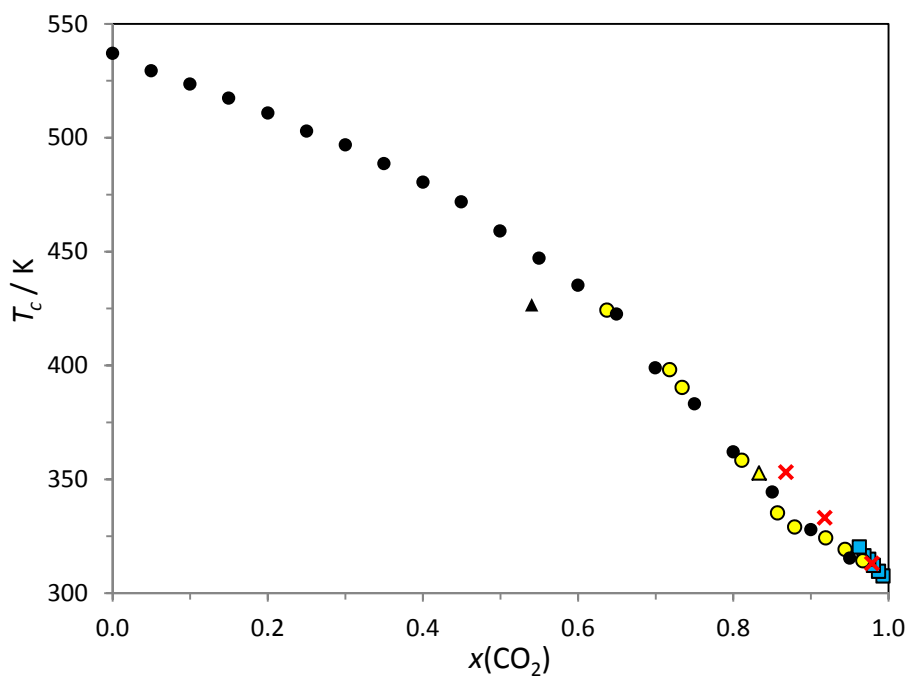


Figure SF10. (a),  $(P_c, T_c)$ ; (b),  $(P_c, x)$  and (c),  $(T_c, x)$  projections for  $\text{CO}_2 + \text{butan-1-ol}$  critical locus. Experimental results from this work and literature: ●, this work; ■, ref. [73]; ○, ref. [75]; □, ref. [78]; +, ref. [95]; ×, ref. [96].

Figure SF10a

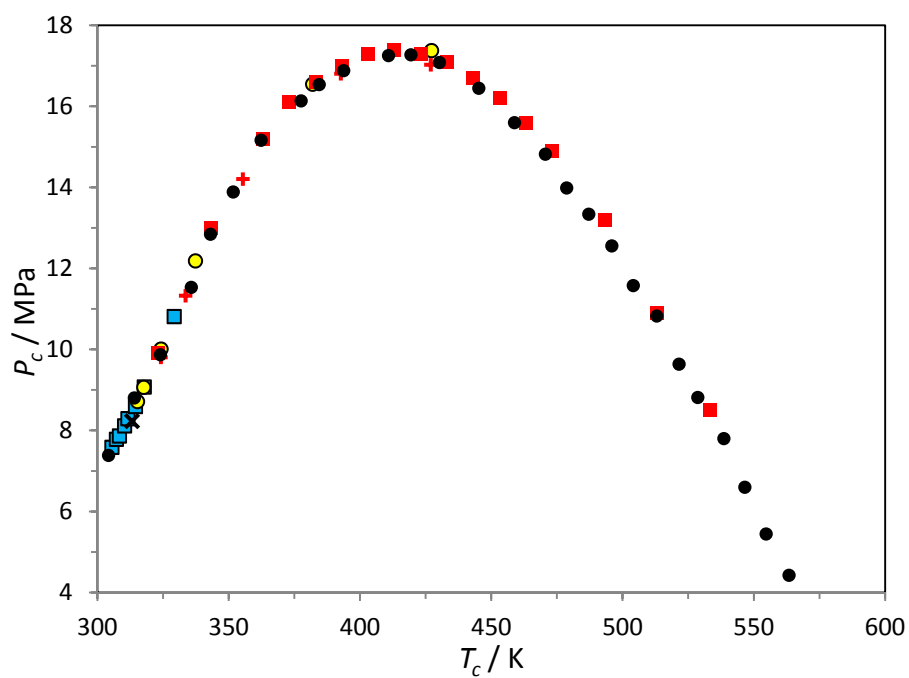


Figure SF10b

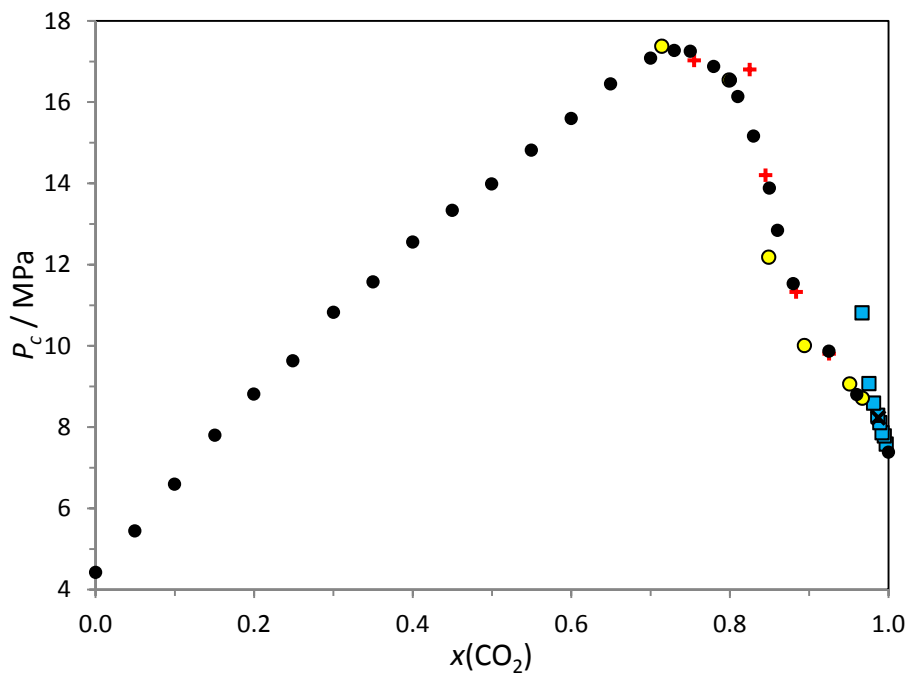
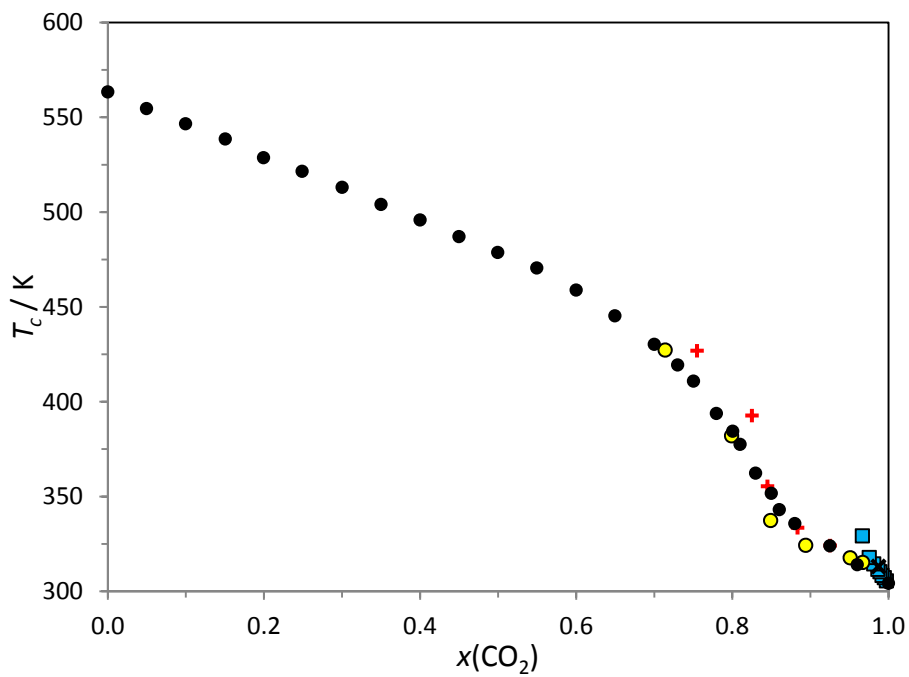


Figure SF10c



## Comparison between this work experimental data and those from literature for the critical loci of CO<sub>2</sub> + alkan-1-ol systems.

For the CO<sub>2</sub> + methanol system, Brunner [70,71], Ziegler et al. [72,73] and Liu et al. [54] give data over the whole range of compositions. The latter author determines ( $x$ ,  $T_c$ ,  $P_c$ ) properties while the others just offer ( $T_c$ ,  $P_c$ ) values. The rest of the references provide data in the rich or very rich zone in CO<sub>2</sub>. The agreement is very good amongst all authors for the  $P_c$ - $T_c$  projection, including our current work (except for Semenova et al. [74], whose data show higher deviations when increasing methanol concentration). Nevertheless,  $T_c$ - $x$  and  $P_c$ - $x$  projections show strong discrepancies: Liu et al. [54] (for  $x_{\text{CO}_2} > 0.6$ ), Semenova et al. [74] and Yeo et al.'s [75] data are the most disperse, showing differences of up to 60 degrees and 6 MPa. Our  $T_c$ - $x$  and  $P_c$ - $x$  results are in good agreement with Yoon et al. [76] and Joung et al. [77], as well as with Liu et al. [54] in the rich-alcohol zone ( $x_{\text{CO}_2} < 0.6$ ) and with Gurdial et al. [78] for its CO<sub>2</sub> richest points; Brunner [71] and Leu et al. [79] report similar data, slightly lower than ours, but in agreement when it comes to the shape of the curve in  $T_c$ - $x$ , while this shape is a little displaced in  $P_c$ - $x$  values.

Only Ziegler et al. [73] provide data along the whole range of compositions for CO<sub>2</sub> + ethanol ( $T_c$ ,  $P_c$ ) measurements. The rest of the authors present data for CO<sub>2</sub>-rich mixtures. Overall agreement is in general good, except with Tian et al. [82] and with Sima et al. [83] for  $x_{\text{CO}_2} < 0.842$ . The agreement is better in the  $P_c$ - $T_c$  projection (where even Tian et al. [82] and Sima et al. [83] are in good agreement with the others) than in  $T_c$ - $x$  or  $P_c$ - $x$  planes, though Ziegler and Dorsey's [72] data present  $P_c$  vs.  $T_c$  values higher than ours.

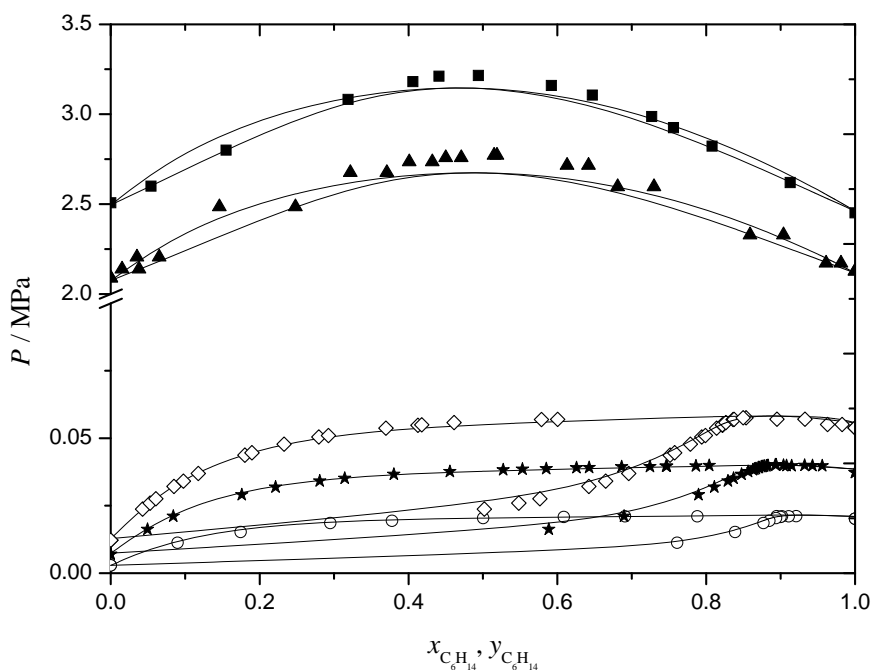
Chang et al. [93] give only graphic data for CO<sub>2</sub> + methanol or + ethanol systems, both in the very rich zone in CO<sub>2</sub>. Their results are slightly higher than ours in the  $P_c$ - $x$  and  $T_c$ - $x$  projections but they are in good agreement in the  $P_c$ - $T_c$  plane.

For CO<sub>2</sub> + propan-1-ol, Ziegler et al. [73] give data along the whole range of compositions providing ( $T_c$ ,  $P_c$ ) measurements. The rest of the references provide ( $x$ ,  $T_c$ ,  $P_c$ ) data for  $0.5 < x_{\text{CO}_2} < 0.85$ . Our results are in very good agreement with Ziegler et al. [73] and Yeo et al. [75]. Secuianu et al. [68] and Gurdial et al.'s [78] data show good agreement with our work in the  $P_c$ - $T_c$  projection, but this agreement is worse in  $T_c$ - $x$  and  $P_c$ - $x$ .

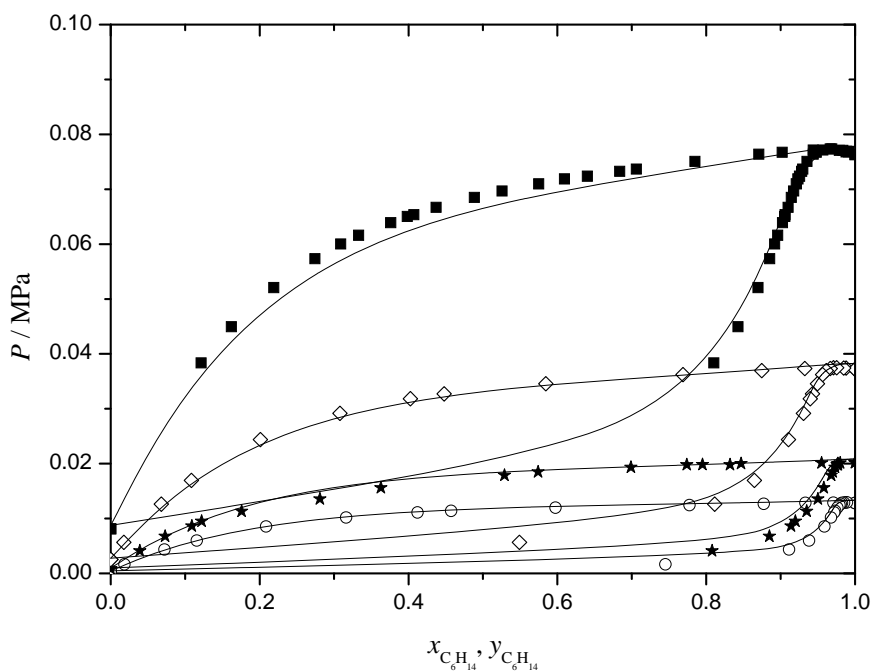


Again, Ziegler et al. [73] are the only authors who give data covering the whole range of compositions for CO<sub>2</sub> + butan-1-ol, while other studies concentrate on CO<sub>2</sub>-rich mixtures. Results from all of the authors, including ours, show very good agreement in the  $P_c$ - $T_c$  projection. In the  $T_c$ - $x$  and  $P_c$ - $x$  planes our results are in very good agreement with several of the points from Yeo et al. [75] and Silva-Oliver and Galicia-Luna [95].

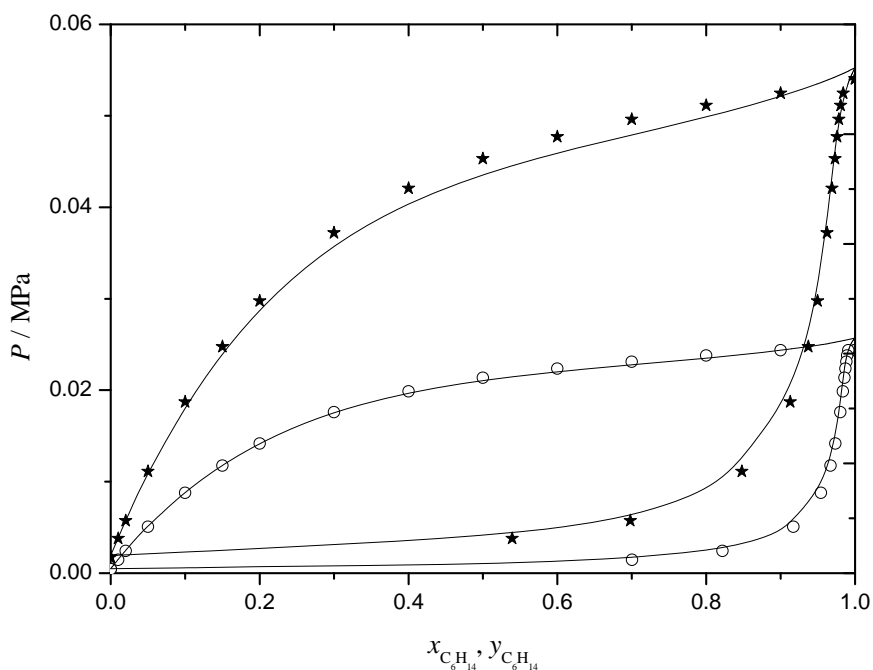
**Figure SF11.** Pressure–mole fraction diagram for *n*-hexane + propan-1-ol VLE. Symbols, experimental data: ○,  $T = 298.15$  K, ref. [119]; ★,  $T = 313.15$  K, ref. [121]; ◇,  $T = 323.15$  K, ref. [123]; ▲,  $T = 483.15$  K, ref. [50]; ■,  $T = 493.15$  K, ref. [50]. Lines, calculated with PC-SAFT EoS using the parameters from Tables 5 and 7.



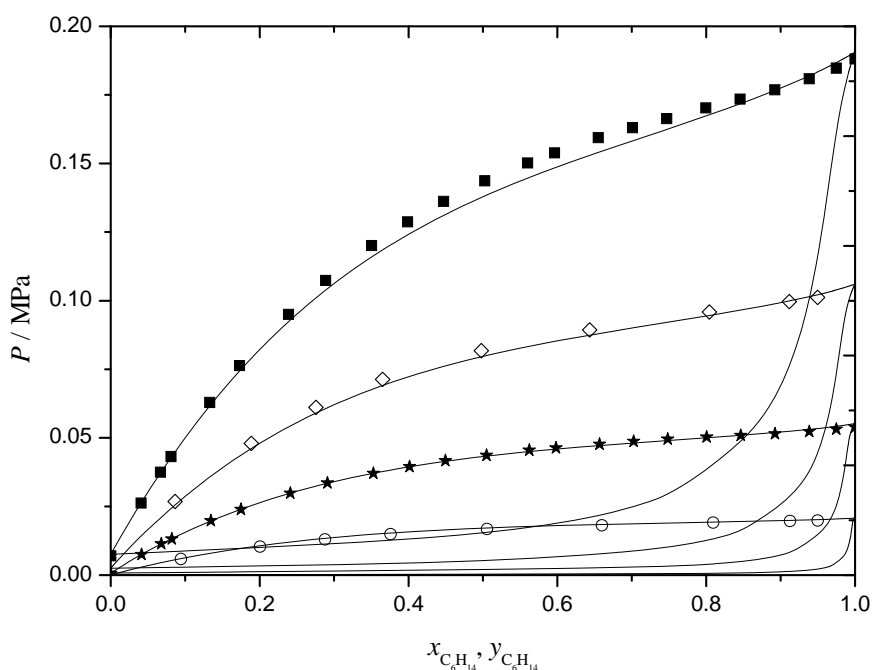
**Figure SF12.** Pressure–mole fraction diagram for *n*-hexane + butan-1-ol VLE. Symbols, experimental data: ○,  $T = 288.15$  K, ref. [124]; ★,  $T = 298.15$  K, ref. [125]; ◇,  $T = 313.15$  K, ref. [124]; ■,  $T = 333.15$  K, ref. [126]. Lines, calculated with PC-SAFT EoS using the parameters from Tables 5 and 7.



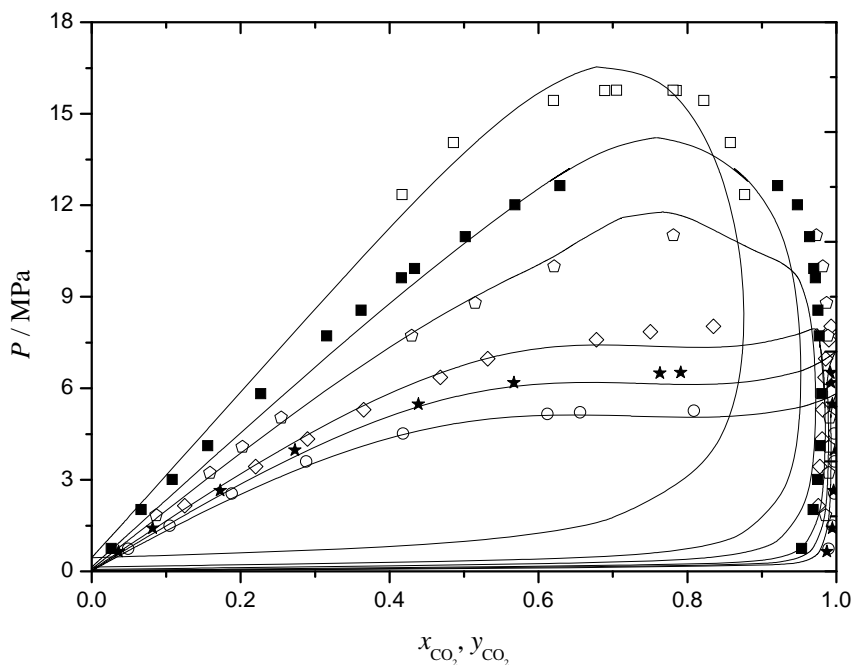
**Figure SF13.** Pressure–mole fraction diagram for *n*-hexane + pentan-1-ol VLE. Symbols, experimental data: ○,  $T = 303.15$  K, ref. [127]; ★,  $T = 323.15$  K, ref. [127]. Lines, calculated with PC-SAFT EoS using the parameters from Tables 5 and 7.



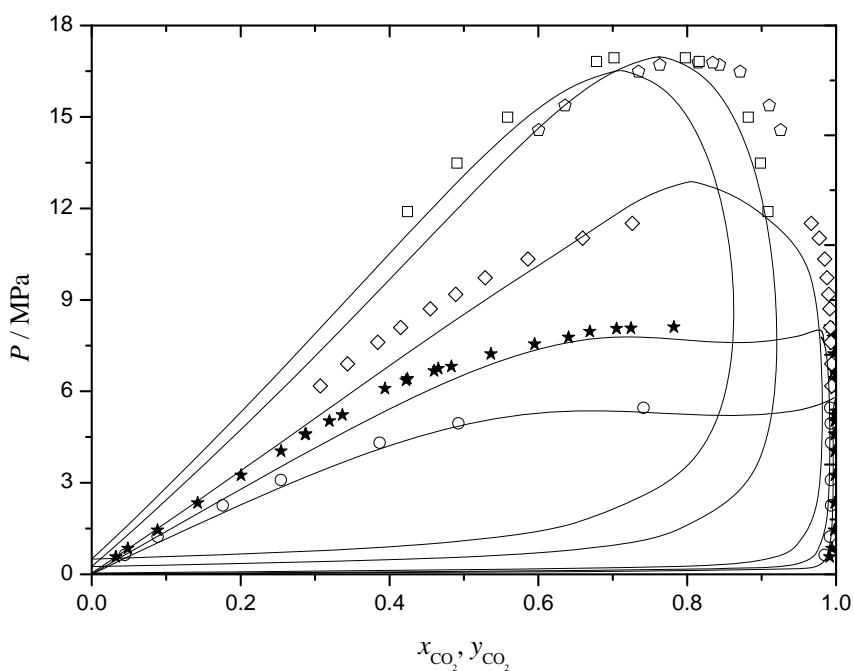
**Figure SF14.** Pressure–mole fraction diagram for *n*-hexane + hexan-1-ol VLE. Symbols, experimental data: ○,  $T = 298.15$  K, ref. [129]; ★,  $T = 323.15$  K, ref. [128]; ◇,  $T = 343.15$  K, ref. [129]; ■,  $T = 363.15$  K, ref. [128]. Lines, calculated with PC-SAFT EoS using the parameters from Tables 5 and 7.



**Figure SF15.** Pressure–mole fraction diagram for CO<sub>2</sub> + propan-1-ol VLE. Symbols, experimental data: ○,  $T = 293.15$  K, ref. [68]; ★,  $T = 303.15$  K, ref. [68]; ◇,  $T = 313$  K, ref. [183]; △,  $T = 333.15$  K, ref. [184]; ■,  $T = 353.15$  K, ref. [68]; □,  $T = 397.48$  K, ref. [186]. Lines, calculated with PC-SAFT EoS using the parameters from Tables 9 and 10.



**Figure SF16.** Pressure–mole fraction diagram for CO<sub>2</sub> + butan-1-ol VLE. Symbols, experimental data: ○,  $T = 293.15$  K, ref. [187]; ★,  $T = 313.15$  K, ref. [187]; ◇,  $T = 337.2$  K, ref. [179]; △,  $T = 392.72$  K, ref. [95]; □,  $T = 426.95$  K, ref. [95]. Lines, calculated with PC-SAFT EoS using the parameters from Tables 9 and 10.



**Table ST1.** Temperature range covered by the data used in the modellization of the studied systems; range of the temperature-dependent binary interaction parameters,  $k_{ij}(T)$ , obtained for these temperatures and temperature-independent binary interaction parameters,  $k_{ij}$ .

System	VLE and critical locus					
	Range $T / K$		Range $k_{ij}(T)$	$k_{ij}$		
$n\text{-C}_6\text{H}_{14}+\text{CH}_3\text{OH}$	293-513		0.0434-0.0742	0.0470		
$n\text{-C}_6\text{H}_{14}+\text{C}_2\text{H}_5\text{OH}$	263-515		0.0116-0.0209	0.0163		
$n\text{-C}_6\text{H}_{14}+\text{C}_3\text{H}_7\text{OH}$	298-537		0.0210-0.0366	0.0289		
$n\text{-C}_6\text{H}_{14}+\text{C}_4\text{H}_9\text{OH}$	288-563		0.00939-0.0169	0.0132		
$n\text{-C}_6\text{H}_{14}+\text{C}_5\text{H}_{11}\text{OH}$	303-588		0.00647-0.0111	0.00900		
$n\text{-C}_6\text{H}_{14}+\text{C}_6\text{H}_{13}\text{OH}$	293-545		0.00774-0.0131	0.0104		
$\text{CO}_2+\text{CH}_3\text{OH}$	213-513		0.0290-0.115	0.0720		
	VLE			Critical locus		
	Range $T / K$	Range $k_{ij}(T)$	$k_{ij}$	Range $T / K$	Range $k_{ij}(T)$	$k_{ij}$
$\text{CO}_2+\text{C}_2\text{H}_5\text{OH}$	283-494	0.0973-0.123	0.104	304-514	0.0790-0.134	0.0910
$\text{CO}_2+\text{C}_3\text{H}_7\text{OH}$	293-427	0.112-0.108	0.109	304-537	0.0806-0.142	0.0949
$\text{CO}_2+\text{C}_4\text{H}_9\text{OH}$	293-430	0.133-0.107	0.120	304-563	0.0882-0.163	0.110

**Table ST2.** Mean relative deviations in critical temperature,  $MRD(T_c)$ , critical pressure,  $MRD(P_c)$ , and bubble pressure,  $MRD(P)$ , and absolute deviations for the solvent mole fraction in the vapor phase,  $\Delta y$ , obtained using the pure-compounds parameters from Tables 5 and 10 and the temperature-dependent or temperature-independent binary interaction parameters for the modelled systems.

System	Binary Interaction Parameters	Critical locus		VLE	
		$MRD(T_c)/\%$	$MRD(P_c)/\%$	$MRD(P)/\%$	$\Delta y_{C_6H_{14}}$
$n-C_6H_{14}+CH_3OH$	$k_{ij}(T)=0.00234+1.40\times 10^{-4}T$ $k_{ij}=0.0470$	0.94	6.26	3.20	0.010
		0.45	6.47	3.86	0.030
$n-C_6H_{14}+C_2H_5OH$	$k_{ij}(T)=0.00187+3.70\times 10^{-5}T$ $k_{ij}=0.0163$	0.50	2.46	3.43	0.026
		0.36	2.28	3.38	0.049
$n-C_6H_{14}+C_3H_7OH$	$k_{ij}(T)=0.00153+6.54\times 10^{-5}T$ $k_{ij}=0.0289$	0.23	1.48	2.01	0.007
		0.26	1.34	4.47	0.014
$n-C_6H_{14}+C_4H_9OH$	$k_{ij}(T)=0.00153+2.73\times 10^{-5}T$ $k_{ij}=0.0132$	0.19	0.97	3.25	0.009
		0.24	0.90	4.29	0.013
$n-C_6H_{14}+C_5H_{11}OH$	$k_{ij}(T)=0.00153+1.63\times 10^{-5}T$ $k_{ij}=0.0090$	0.42	1.07	2.68	0.005
		0.44	1.05	3.83	0.003
$n-C_6H_{14}+C_6H_{13}OH$	$k_{ij}(T)=0.00153+2.12\times 10^{-5}T$ $k_{ij}=0.0104$	0.21	1.12	1.81	0.002
		0.12	0.89	2.56	0.002
System	Binary Interaction Parameters	Critical locus		VLE	
		$MRD(T_c)/\%$	$MRD(P_c)/\%$	$MRD(P)/\%$	$\Delta y_{CO_2}$
$CO_2+CH_3OH$	$k_{ij}(T)=-0.0323+2.88\times 10^{-4}T$ $k_{ij}=0.072$	2.67	7.17	6.04	0.008
		2.92	9.11	11.04	0.010
$CO_2+C_2H_5OH$	$k_{ij}(T)=2.60\times 10^{-4}T$ $k_{ij}=0.091$	1.37	6.17	----	----
		1.32	8.62	----	----
$CO_2+C_3H_7OH$	$k_{ij}(T)=0.0625+1.23\times 10^{-4}T$ $k_{ij}=0.104$	----	----	7.85	0.031
		----	----	9.23	0.034
$CO_2+C_4H_9OH$	$k_{ij}(T)=2.65\times 10^{-4}T$ $k_{ij}=0.095$	1.16	3.53	----	----
		1.20	6.23	----	----
$CO_2+C_5H_{11}OH$	$k_{ij}(T)=0.118-2.15\times 10^{-5}T$ $k_{ij}=0.109$	----	----	6.89	0.033
		----	----	7.87	0.038
$CO_2+C_6H_{13}OH$	$k_{ij}(T)=2.90\times 10^{-4}T$ $k_{ij}=0.110$	1.92	5.17	----	----
		1.56	7.91	----	----
$CO_2+C_7H_{15}OH$	$k_{ij}(T)=0.190-1.93\times 10^{-4}T$ $k_{ij}=0.120$	----	----	8.76	0.034
		----	----	12.2	0.023

**Table ST3.** Comparison between the results from this work modellization and those from literature for *n*-hexane + alkan-1-ol systems.

System	Model	Binary Interaction Parameters	Range T/K	MRD(P)/%	$\Delta y_{C_6H_{14}}$	MRD(T <sub>j</sub> )/%	MRD(P <sub>j</sub> )/%	Ref.
<i>n</i> -C <sub>6</sub> H <sub>14</sub> +CH <sub>3</sub> OH	PC-SAFT	Temperature dependent	293-513	3.20	0.010	0.94	6.26	This work
	tPC-PSAFT	Non temperature dependent	313-348	4.0	----	----	----	[132]
	GC-PC-SAFT	Non temperature dependent	293-448	6-7	----	----	----	[134]
	CPA	Temperature dependent	298-333	2.6	0.018	----	----	[136]
alkane+CH <sub>3</sub> OH	sPC-PSAFT	Fitted	273-423	2.8	0.015	----	----	[137]
	PC-SAFT	Temperature dependent	313-463	3-8	----	----	----	[32]
<i>n</i> -C <sub>6</sub> H <sub>14</sub> + C <sub>2</sub> H <sub>5</sub> OH	PC-SAFT	Temperature dependent	263-515	3.43	0.026	0.50	2.46	This work
	PC-SAFT	Non temperature dependent	488-514	----	----	0.15	----	[133]
	sPC-PSAFT	Non temperature dependent	273.15	3.5	0.009	----	----	[33]
	SAFT-VR	0	263-303	9.7	0.027	----	----	[131]
	CPA	Non temperature dependent	298.15	1.2	0.005	----	----	[136]
<i>n</i> -C <sub>6</sub> H <sub>14</sub> + C <sub>3</sub> H <sub>7</sub> OH	PC-SAFT	Temperature dependent	298-537	2.01	0.007	0.23	1.48	This work
	sPC-PSAFT	0	348.15	5.8	0.024	----	----	[33]
	SAFT-VR	0	318-348	10.3	0.030	----	----	[131]
	CPA	Non temperature dependent	298-323	1.3	0.005	----	----	[136]
<i>n</i> -C <sub>6</sub> H <sub>14</sub> + C <sub>4</sub> H <sub>9</sub> OH	PC-SAFT	Temperature dependent	288-563	3.25	0.009	0.19	0.97	This work
	SAFT-VR	0	323-348	7.67	----	----	----	[131]
	CPA	Non temperature dependent	298-333	3.5	0.005	----	----	[136]
<i>n</i> -C <sub>6</sub> H <sub>14</sub> + C <sub>5</sub> H <sub>11</sub> OH	PC-SAFT	Temperature dependent	303-588	2.68	0.005	0.42	1.07	This work
	PC-SAFT	Non temperature dependent	507-587	----	----	0.10	----	[133]
	SAFT-VR	0	303-545	6.30	----	----	----	[131]
<i>n</i> -C <sub>6</sub> H <sub>14</sub> + C <sub>6</sub> H <sub>13</sub> OH	PC-SAFT	Temperature dependent	293-545	1.81	0.002	0.21	1.12	This work
	sPC-PSAFT	0	323.15	6.3	----	----	----	[33]
	SAFT- $\gamma$	0	323.15	4.08	----	----	----	[135]
	SAFT-VR	0	293-373	5.69	----	----	----	[131]

**Table ST4.** Comparison between the results from this work modellization and those from literature for CO<sub>2</sub> + alkan-1-ol systems.

System	Model	Binary Interaction Parameters	Range T/K	MRD(P)/%	$\Delta y_{CO_2}$	MRD(T <sub>d</sub> )/%	MRD(P <sub>d</sub> )/%	Ref.
CO <sub>2</sub> +CH <sub>3</sub> OH	PC-SAFT	<i>Temperature dependent</i>	213-513	6.04	0.008	2.67	7.17	This work
	PC-SAFT	<i>Non temperature dependent</i>	291-492	----	----	0.08	0.01	[133]
	PC-SAFT	<i>Temperature dependent</i>	230-478	7.9	0.027	----	----	[31]
	PC-SAFT-QD	<i>Temperature dependent</i>	230-478	11.4	0.033	----	----	[31]
	SAFT-VR	<i>Non temperature dependent</i>	313	0.46	0.005	----	----	[139]
	CPA	<i>Non temperature dependent</i>	273-290	1.3	0.001	----	----	[138]
	CPA	<i>Temperature dependent</i>	291-313	----	0.003	----	----	[34]
	PR-WS-VL	<i>Temperature dependent</i>	313-343	2.92	< 0.02	----	----	[140]
CO <sub>2</sub> +C <sub>2</sub> H <sub>5</sub> OH	PC-SAFT	<i>Temperature dependent</i>	283-514	7.85	0.031	1.37	6.17	This work
	PC-SAFT	<i>Non temperature dependent</i>	291-373	----	----	0.12	0.02	[133]
	PC-SAFT	<i>Temperature dependent</i>	291-373	15.9	0.020	----	----	[31]
	PC-SAFT-QD	<i>Temperature dependent</i>	291-373	15.0	0.021	----	----	[31]
	sPC-SAFT	<i>Temperature dependent</i>	291-313	10.2	0.007	----	----	[33]
	SAFT-VR	<i>Non temperature dependent</i>	313	4.03	0.002	----	----	[139]
	CPA	<i>Temperature dependent</i>	291-313	----	0.020	----	----	[34]
	CPA	<i>Non temperature dependent</i>	291	1.0	0.004	----	----	[138]
	PR-WS-VL	<i>Temperature dependent</i>	313-345	1.65	< 0.02	----	----	[140]
	PR-VL	<i>Temperature dependent</i>	283-337	3.08	0.006	----	----	[143]
CO <sub>2</sub> +C <sub>3</sub> H <sub>7</sub> OH	PC-SAFT	<i>Temperature dependent</i>	293-537	6.89	0.033	1.16	3.53	This work
	PC-SAFT	<i>Non temperature dependent</i>	313-333	----	----	0.20	0.01	[133]
	PC-SAFT	<i>Temperature dependent</i>	308-337	12.9	0.003	----	----	[31]



	PC-SAFT-QD	<i>Temperature dependent</i>	308-337	8.2	0.003	----	----	[31]
	CPA	<i>Temperature dependent</i>	315-337	----	0.002	----	----	[34]
	CPA	<i>Non temperature dependent</i>	313-333	7.4	0.002	----	----	[138]
	PR-WS	<i>Temperature dependent</i>	344-427	1.2	0.010	----	----	[94]
	PR-WS-VL	<i>Temperature dependent</i>	313-337	3.5	< 0.02	----	----	[140]
	PR-VL	<i>Temperature dependent</i>	313-337	1.52	0.001	----	----	[143]
CO <sub>2</sub> +C <sub>4</sub> H <sub>9</sub> OH	PC-SAFT	<i>Temperature dependent</i>	293-563	8.76	0.034	1.92	5.17	This work
	PC-SAFT	<i>Non temperature dependent</i>	303-428	----	----	0.18	0.01	[133]
	PC-SAFT	<i>Temperature dependent</i>	293-427	12.1	0.014	----	----	[31]
	PC-SAFT-QD	<i>Temperature dependent</i>	293-427	10.3	0.010	----	----	[31]
	CPA	<i>Temperature dependent</i>	293-324	----	0.005	----	----	[34]
	PT-NRTL	<i>Temperature dependent</i>	324-427	0.9	0.017	----	----	[95]
	PR-WS	<i>Temperature dependent</i>	354-430	1.4	0.008	----	----	[94]
	PR-WS-VL	<i>Temperature dependent</i>	314-337	3.5	< 0.02	----	----	[140]
	PR-VL	<i>Temperature dependent</i>	298-337	1.12	0.012	----	----	[143]