Universidad Zaragoza
1542

# ANEXOS

## Uso de TIC y Flexibilidad de la Estructura Organizativa. Relación con los Resultados de las Agencias de Turismo de Negocios & Eventos de Brasil

## The Use of ICT and Organizational Structure Flexibility. Relationship with Firm Performance in Brazil´s Business Tourism & Events Agencies

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# ANEXO I

# CUESTIONARIO

# CARTA DE PRESENTACIÓN Y CUESTIONARIO

## VERSIÓN EN ESPAÑOL

Departamento de Dirección y Organización de Empresas
Universidad Zaragoza

Zaragoza, 15 de abril de 2016

Estimado (a) Sr. (a),

**El uso de las TIC y la flexibilidad organizativa** son dos de las variables competitivas que en los últimos años están recibiendo mayor atención tanto por empresas, como por entes públicos, pero de las que se dispone de una menor contrastación empírica, sobre todo en el ámbito de las empresas turísticas en el segmento de viajes corporativos, de incentivos y eventos.

Para conocer qué relación existe entre el uso de las TIC y la flexibilidad organizativa, estamos realizando un estudio en la Universidad Zaragoza (España), subvencionado por CAPES – MEC (Coordenação de Aperfeiçoamento de Pessoal de Nível Superior - Ministério da Educação - Brasil) sobre las empresas turísticas de Brasil. El objetivo es determinar cómo las TIC y distintas formas de flexibilidad en la organización incrementan las probabilidades de obtener un mejor resultado, ayudando de esta forma a las empresas en la toma de decisiones.

Somos conscientes del coste de su tiempo, pero en esta fase del trabajo necesitamos que nos ayude a conocer la realidad de las empresas. Por ello, pedimos su colaboración cumplimentando el cuestionario adjunto, el cual le ocupará **aproximadamente 10 minutos**.

Toda la información que usted nos proporcione, será tratada con absoluta discreción y utilizada de forma agregada y exclusivamente para esta investigación.

Por favor, responda a todas las preguntas. Si no sabe la respuesta exacta, responda lo más aproximado posible o póngase en contacto con **María José Vela Jiménez** (mjvela@unizar.es), **Silvia Abella Garcés** (sabella@unizar.es) o con **Eliane Hala Santos** (604609@unizar.es) a través del teléfono +34-876554936, +34-974239373 o +34-697222176. Por nuestra parte, existe el compromiso de enviarle los principales resultados de la investigación al término de la misma, si así lo desea.

Agradeciéndole de antemano su colaboración, le saludan atentamente,

Fdo. Profª Dra. María José Vela Jiménez
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La información suministrada tiene como objetivo estudiar la influencia del uso de las TIC sobre la flexibilidad organizativa y su relación con los resultados de las empresas turísticas del segmento de viajes corporativos, de incentivos y eventos de Brasil. La divulgación y publicación de los resultados del estudio serán de forma agregada y **confidencial**, sin identificar ninguna información específica de las empresas encuestadas.
Por favor, responda a las preguntas teniendo en cuenta la situación de todas las agencias/sucursal/oficinas que pertenecen a su empresa. **Muchas gracias por su colaboración.**

**CUESTIONES:**

**1º)** Indique, por favor, si en el año 2015, en la empresa se utilizaron las siguientes aplicaciones y recursos tecnológicos. Marque 0 si no se utilizó el recurso, y si se utilizó, aplique la escala de 1 " muy poco" a 7 "mucho":

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 1. Sistema de gestión de la solicitud y aprobación de viajes corporativos | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 2. Informes gerenciales online y personalizados al cliente | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 3. Perfiles electrónicos de los viajeros | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 4. Aplicaciones móviles de gestión de viajes | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 5. Sistema de self-booking (búsqueda y reserva de viajes) | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 6. Sistema de self-ticketing (búsqueda, reserva y emisión de viajes) | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 7. Portales en la web personalizados a los clientes | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 8. Sistema de rastreo y localización de los pasajeros en situaciones de emergencias y crisis | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 9. Sistema de Gestión de Eventos | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 10. Sistemas GDS – Global Distribution System | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 11. Sistemas CRS – Central Reservation System | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 12. Sistemas de BI – Business Intelligence | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 13. Aplicación web para formación corporativa | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 14. Big Data | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 15. Infraestructura tecnológica móvil y/o fija corporativa | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 16. Aplicaciones de front office y back office para las agencias de viajes | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 17. Aplicación de Booking online | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |

**2º)** Indique, por favor, el porcentaje de empleados que, en el año 2015, disfrutaron de las siguientes prácticas en la empresa:

| | 0 | 0.1-15% | 16-30% | 31-45% | 46-55% | 56-70% | 71-85% | 86-100% |
|---|---|---|---|---|---|---|---|---|
| 1. Teletrabajo | | | | | | | | |
| 2. Rotación horizontal de tareas | | | | | | | | |
| 3. Rotación vertical ascendente de tareas | | | | | | | | |
| 4. Equipos de trabajo polivalentes | | | | | | | | |
| 5. Semana laboral compartida | | | | | | | | |
| 6. Equipos de mejora y solución de problemas | | | | | | | | |
| 7. Contrato fijo a tiempo parcial | | | | | | | | |
| 8. Horario laboral flexible | | | | | | | | |
| 9. Reducción de jornada laboral | | | | | | | | |
| 10. Horas extraordinarias | | | | | | | | |
| 11. Contratación temporal | | | | | | | | |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 12. Trabajo por turnos | | | | | | | | |
| 13. Cómputo anual de horas | | | | | | | | |
| 14. Jubilación anticipada | | | | | | | | |
| 15. Semana laboral reducida | | | | | | | | |

**3º)** Indique, por favor, en qué medida, en el año 2015, la empresa utilizó los siguientes trabajadores. Marque el 0 si no lo utilizó, y si lo utilizó use una escala de 1 “muy poco” a 7 “mucho”:

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 1. Autónomos que trabajan para la empresa | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 2. Empleados de empresas de trabajo temporal | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 3. Subcontratación | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |

**4º)** Indique, por favor, en qué medida, en el año 2015, la empresa utilizó las siguientes líneas de actuación organizativa. Marque el 0 si no se utilizó, y si se utilizó, use una escala de 1 “muy poco” a 7 “mucho”:

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 1. Agrupación de empleados por proyectos de trabajo | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 2. Autogestión de los equipos respecto al método de trabajo | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 3. Autogestión de los equipos respecto a la programación del trabajo | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 4. Autogestión de los equipos respecto al control de los objetivos | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 5. Autogestión de los equipos para elegir su propio líder o responsable | | | | | | | | |
| 6. Participación en la definición del contenido de sus puestos y forma de realizar el trabajo | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 7. Autonomía en la toma de decisiones en el trabajo | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 8. Autonomía en la ejecución del trabajo | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 9. Delegación de decisiones operativas | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 10. Delegación de decisiones estratégicas | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 11. Remuneración de los equipos en función de los resultados | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |

**5º)** Indique, por favor, el porcentaje de cada una de las siguientes actividades que se subcontrataron en el año 2015 a otras empresas.

| | % Subcontratado | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| | 0 | 0.1-10 | 11-20 | 21-30 | 31-50 | 51-75 | 76-99 | 100 |
| 1. Compras | | | | | | | | |
| 2. Producción y prestación de servicios | | | | | | | | |
| 3. Logística | | | | | | | | |
| 4. Actividades comerciales | | | | | | | | |
| 5. Actividades administrativas | | | | | | | | |
| 6. Gestión de personal | | | | | | | | |
| 7. Investigación y desarrollo | | | | | | | | |
| 8. Publicidad | | | | | | | | |
| 9. Servicio al cliente | | | | | | | | |
| 10. Tecnología de la información y comunicación | | | | | | | | |
| 11. Formación | | | | | | | | |

**6º)** Indique, por favor, el grado de cooperación externa con clientes y/o proveedores que tuvo su empresa en el año 2015 en las siguientes actividades. Utilice una escala de 1 "muy bajo" a 7 "muy alto"; marque el 0 si no existió:

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 1. Formación/Conferencias/Seminarios | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 2. Desarrollo de productos o servicios | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 3. Desarrollo de procesos | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 4. Benchmarking e intercambio de experiencias | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 5. Transferencia de tecnología de la información y comunicación | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 6. Acciones de marketing conjuntas | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 7. Producción y prestación de servicios | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 8. Logística | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 9. Actividades comerciales | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 10. Servicio al cliente | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |

**7º)** Indique, por favor, su grado de acuerdo con las siguientes afirmaciones respecto al sector en el que se encuentra su empresa (considere la situación en los últimos 3 años):

| | EN DESACUERDO | | | INSEGURO | DE ACUERDO | | |
|---|---|---|---|---|---|---|---|
| | Muy | En general | Un poco | | Un poco | En general | Muy |
| 1. Los cambios en el entorno de su mercado local han sido intensos | | | | | | | |
| 2. Sus clientes han solicitado regularmente nuevos productos y servicios | | | | | | | |
| 3. Se han presentado cambios en su mercado local continuamente | | | | | | | |
| 4. Los productos/servicios de este sector se quedan obsoletos con mucha rapidez | | | | | | | |
| 5. Las prácticas de marketing cambian con mucha frecuencia en este sector | | | | | | | |
| 6. La tecnología utilizada cambia muy rápidamente en este sector | | | | | | | |

**8º)** Indique, por favor, su grado de acuerdo con las siguientes afirmaciones sobre la estrategia utilizada por su empresa. Marque 0 si no se utiliza la estrategia, y si se utiliza use una escala de 1 "muy en desacuerdo" a 7 " totalmente de acuerdo" (considere la situación en los últimos 3 años):

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 1. Realizamos con frecuencia innovaciones importantes de producto o servicio | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 2. Bajamos los precios con frecuencia | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 3. Incrementamos los productos y servicios incluidos en los paquetes de viaje para reducir costes | | | | | | | | |
| 4. Diferenciamos nuestros productos y servicios por la disposición y la rapidez de respuesta por el uso de tecnología de información y comunicación | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 5. Nuestra máxima preocupación es minimizar los costes | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 6. Diferenciamos nuestros productos o servicios por calidad | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |

**9º)** Indique, por favor, su percepción sobre los resultados de su empresa en el año 2015 en relación a empresas similares del sector. Marque 0 "si no se ha producido el resultado" y si se ha producido, utilice una escala de 1 "muy por debajo de empresas similares del sector" a 7 "muy por encima de empresas similares del sector":

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 1. Ofrece productos de calidad | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 2. Dispone de procesos internos eficientes | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 3. Cuenta con clientes satisfechos | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 4. Se adapta a los cambios en el mercado | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 5. Está creciendo | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 6. Es rentable | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 7. Tiene empleados satisfechos/motivados | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 8. Absentismo laboral | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 9. Innovaciones de proceso | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 10. Innovaciones de producto y/o servicio | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 11. Rentabilidad sobre activos | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 12. Rentabilidad sobre ventas | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 13. Resultado financiero global | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 14. Relaciones con clientes | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 15. Relaciones con proveedores | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 16. Mejora de la calidad de los productos y servicios | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 17. Mejora en el nivel de la calidad de los procesos | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |

**10º)** Por favor, indique aproximadamente, para el año 2015, el número de personas que se encuentran en los siguientes grupos:

| | |
|---|---|
| 1. Plantilla total | |
| 2. Plantilla total de hombres | |
| 3. Plantilla total de mujeres | |
| 4. Plantilla total a tiempo completo | |
| 5. Plantilla total a tiempo parcial | |

| | |
|---|---|
| 6. Autónomos que trabajan para la empresa | |
| 7. Empleados de la empresa con contrato fijo | |
| 8. Empleados de la empresa con contrato temporal | |
| 9. Trabajadores de empresas de trabajo temporal | |
| 10. Nº de despidos | |
| 11. Nº de abandonos voluntarios | |

**11º)** Indique, por favor, los siguientes datos de su empresa:

| | |
|---|---|
| Año de constitución de la empresa | |
| Nº de niveles jerárquicos entre el gerente y los empleados (ambos incluidos) | |
| Nº de niveles jerárquicos totales en la empresa (desde el nivel más bajo hasta el nivel más alto) | |
| Facturación aproximada (en reales) en el año de 2015 | |

**12º)** La empresa trabaja en el ámbito de:

| | **SI** | **NO** |
|---|---|---|
| Viajes corporativos | | |
| Viajes de incentivos | | |
| Eventos | | |
| Otros | | |

**Nombre de la empresa**………………………………………………………………

**MUCHAS GRACIAS POR SU COLABORACIÓN**

# CUESTIONARIO

# VERSION EN PORTUGUÉS

# Pesquisa a Empresas Brasileiras do segmento de Viagens Corporativas, de Incentivos e Eventos

Estimado (a) Sr. (a),

O uso da Tecnologia da Informação e Comunicação (TIC) e da Flexibilidade Organizacional são duas das variáveis competitivas que nos últimos anos estão recebendo maior atenção tanto pelas empresas, como pelas entidades públicas, mas que ainda disponibiliza de pouca comprovação empírica, sobretudo no âmbito das empresas turísticas do segmento de viagens corporativas, de incentivos e eventos.

Para conhecer que relação existe entre o uso das TIC e a flexibilidade organizacional, estamos realizando um estudo na Universidad Zaragoza (Espanha), apoiados por CAPES – MEC (Coordenação de Aperfeiçoamento de Pessoal de Nível Superior - Ministério da Educação - Brasil) sobre empresas turísticas brasileiras. O objetivo é determinar como as TIC e as diferentes formas de flexibilidade na organização, incrementam as probabilidades de obter um melhor resultado, ajudando dessa forma as empresas na tomada de decisões.

Somos conscientes do custo de seu tempo, mas nesta fase do trabalho precisamos que nos ajude a conhecer a realidade das empresas. Por isso, pedimos sua colaboração preenchendo o questionário em anexo, o qual lhe ocupará aproximadamente 10 minutos.
Toda a informação que o (a) senhor (a) nos proporcione, será tratada com absoluta discrição e utilizada de forma agregada e exclusivamente para essa pesquisa.

Por favor responda a todas as perguntas, considerando a situação de todas as filiais que pertencem à sua empresa. Se não souber a resposta exata, responda o mais aproximado possível ou entre em contato com a Profª Dra. María José Vela Jiménez (mjvela@unizar.es), Profª Dra. Silvia Abella Garcés (sabella@unizar.es) ou com Eliane Hala Santos (604609@unizar.es) através dos telefones +34-876554936, +34-974239373 ou +34-697222176.

De nossa parte, existe o compromisso de lhe enviar os principais resultados da pesquisa ao final da mesma, se assim desejar.

Agradecendo antecipadamente sua colaboração, cumprimentamos-lhe atentamente.

*Obrigatório

1. **1- Indique, por favor se no ano de 2015, a empresa utilizou as seguintes aplicações e recursos tecnológicos:** *
   Marque 0 se não se utilizou o recurso e se utilizou, aplique a escala de 1 “muito pouco” a 7 “muito”
   *Marcar apenas uma oval por linha.*

| | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
|---|---|---|---|---|---|---|---|---|
| Sistema de Gestão de Solicitação e Aprovação de Viagens Corporativas | | | | | | | | |
| Relatórios Gerenciais online e customizados aos clientes | | | | | | | | |
| Perfis eletrônicos de viajantes | | | | | | | | |
| Aplicações móveis (Apps) de gestão de viagens | | | | | | | | |
| Sistema de self-booking (busca e reserva de viagens) | | | | | | | | |
| Sistema de self-ticketing (busca, reserva e emissão de viagens) | | | | | | | | |
| Portais na web customizados aos clientes | | | | | | | | |
| Sistema de rastreamento e localização de passageiros em situações de emergências e crises | | | | | | | | |
| Sistema de Gestão de Eventos | | | | | | | | |
| Sistema GDS - Sistema Global de Distribuição | | | | | | | | |
| Sistema CRS - Sistema Central de Reservas | | | | | | | | |
| Sistemas BI - Business Intelligence | | | | | | | | |
| Aplicacão web para formação corporativa | | | | | | | | |
| Big Data | | | | | | | | |
| Infraestrutura tecnológica móvel e/ou fixa corporativa | | | | | | | | |
| Aplicações de front office e back office para agências de viagens | | | | | | | | |
| Ferramentas de Booking online | | | | | | | | |

# Práticas Flexíveis de Trabalho

Perguntas referentes a utilização e ao percentual de empregados em práticas flexíveis na sua empresa

2. **2- Indique, por favor, a porcentagem de empregados que no ano de 2015, desfrutaram das seguintes práticas na empresa:** *

% Empregados

*Marcar apenas uma oval por linha.*

| | 0 | 0.1-15 | 16-30 | 31-45 | 46-55 | 56-70 | 71-85 | 86-100 |
|---|---|---|---|---|---|---|---|---|
| Teletrabalho (trabalho remoto) | | | | | | | | |
| Rodízio horizontal de tarefas | | | | | | | | |
| Rodízio vertical ascendente de tarefas | | | | | | | | |
| Equipes de trabalho polivalentes | | | | | | | | |
| Semana de trabalho compartilhada | | | | | | | | |
| Equipes de melhoria e solução de problemas | | | | | | | | |
| Contrato fixo em tempo parcial | | | | | | | | |
| Horário de trabalho flexível | | | | | | | | |
| Redução de horas de trabalho | | | | | | | | |
| Horas extras | | | | | | | | |
| Contratação temporária | | | | | | | | |
| Trabalho por turnos | | | | | | | | |
| Cálculo anual de horas | | | | | | | | |
| Aposentadoria antecipada | | | | | | | | |
| Semana de trabalho reduzida | | | | | | | | |

3. **3- Indique, por favor, em que medida no ano de 2015, a empresa utilizou os seguintes trabalhadores:** *

Marque o 0 se não utilizou, e se utilizou, use uma escala de 1 “muito pouco” a 7 “muito”

*Marcar apenas uma oval por linha.*

| | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
|---|---|---|---|---|---|---|---|---|
| Autônomos que trabalham para a empresa | | | | | | | | |
| Empregados de empresas de trabalho temporário | | | | | | | | |
| Terceirizados | | | | | | | | |

# Estrutura Organizacional

Perguntas referentes as linhas de atuação na estrutura organizacional de sua empresa

4. **4- Indique, por favor, em que medida no ano de 2015, a empresa utilizou as seguintes linhas de atuação organizacional:** *

Marque o 0 se não utilizou, e se utilizou, use uma escala de 1 "muito pouco" a 7 "muito"
*Marcar apenas uma oval por linha.*

| | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
|---|---|---|---|---|---|---|---|---|
| Agrupamento de empregados por projetos de trabalho | | | | | | | | |
| Autogestão de equipes com respeito ao método de trabalho | | | | | | | | |
| Autogestão de equipes com respeito a programação do trabalho | | | | | | | | |
| Autogestão de equipes com respeito ao controle dos objetivos | | | | | | | | |
| Autogestão de equipes para eleger seu próprio líder ou responsável | | | | | | | | |
| Participação na definição do conteúdo de seus postos e na forma de realizar o trabalho | | | | | | | | |
| Autonomia na tomada de decisões no trabalho | | | | | | | | |
| Autonomia na execução do trabalho | | | | | | | | |
| Delegação de decisões operacionais | | | | | | | | |
| Delegação de decisões estratégicas | | | | | | | | |
| Remuneração de equipes em função dos resultados | | | | | | | | |

5. **5- Indique, por favor, a porcentagem de cada uma das seguintes atividades que foram subcontratadas no ano 2015 em outras empresas:** *

% Subcontratado
*Marcar apenas uma oval por linha.*

| | 0 | 0.1-10 | 11-20 | 21-30 | 31-50 | 51-75 | 76-99 | 100 |
|---|---|---|---|---|---|---|---|---|
| Compras | | | | | | | | |
| Produção e prestação de serviços | | | | | | | | |
| Logística | | | | | | | | |
| Atividades comerciais | | | | | | | | |
| Atividades administrativas | | | | | | | | |
| Gestão de pessoal | | | | | | | | |
| Pesquisa e desenvolvimento | | | | | | | | |
| Publicidade | | | | | | | | |
| Serviço ao cliente | | | | | | | | |
| Tecnologia da informação e comunicação | | | | | | | | |
| Formação | | | | | | | | |

6. **6- Indique, por favor, o grau de cooperação externa com clientes e/ou fornecedores que sua empresa teve no ano de 2015 nas seguintes atividades:** *

Marque o 0 se não existiu cooperação, e se existiu, utilize uma escala de 1 “muito baixo” a 7 “muito alto”

*Marcar apenas uma oval por linha.*

| | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
|---|---|---|---|---|---|---|---|---|
| Formação/Conferências/Seminários | | | | | | | | |
| Desenvolvimento de produtos ou serviços | | | | | | | | |
| Desenvolvimento de processos | | | | | | | | |
| Benchmarking e intercâmbio de experiências | | | | | | | | |
| Transferência de tecnologia de informação e comunicação | | | | | | | | |
| Ações de marketing conjuntas | | | | | | | | |
| Produção e prestação de serviços | | | | | | | | |
| Logística | | | | | | | | |
| Atividades comerciais | | | | | | | | |
| Serviço ao cliente | | | | | | | | |

# Setor e Estratégia da empresa

Perguntas referentes ao Setor e a Estratégia de sua Empresa

7. **7- Indique, por favor, seu grau de acordo nas seguintes afirmações com respeito ao setor de sua empresa em 2015:** *

Considere a situação nos últimos 3 anos

*Marcar apenas uma oval por linha.*

| | Muito em desacordo | Em geral desacordo | Um pouco em desacordo | Inseguro | Um pouco de acordo | Em geral de acordo | Muito de acordo |
|---|---|---|---|---|---|---|---|
| As mudanças no ambiente de seu mercado local tem sido intensos | | | | | | | |
| Seus clientes tem solicitado regularmente novos produtos e serviços | | | | | | | |
| Houveram mudanças em seu mercado local de forma contínua | | | | | | | |
| As práticas de marketing mudam com muita frequência neste setor | | | | | | | |
| A tecnologia utilizada está mudando muito rapidamente neste setor | | | | | | | |
| Os produtos e serviços deste setor tornam-se obsoletos muito rapidamente | | | | | | | |

8. **8- Indique, por favor, seu grau de acordo nas seguintes afirmações sobre a estratégia utilizada por sua empresa :** *

Marque 0 se não se utiliza a estratégia, e se utiliza, use uma escala de 1 “muito em desacordo” a 7 “totalmente de acordo” (considere a situação nos últimos 3 anos)

*Marcar apenas uma oval por linha.*

| | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
|---|---|---|---|---|---|---|---|---|
| Realizamos com frequência inovações importantes de produtos ou serviços | | | | | | | | |
| Baixamos os preços com frequência | | | | | | | | |
| Incluímos produtos e serviços em pacotes de viagens para reduzir custos | | | | | | | | |
| Diferenciamos nossos produtos e serviços pela disposição e rapidez de resposta no uso de tecnologia da informação e comunicação | | | | | | | | |
| Nossa máxima preocupação é minimizar os custos | | | | | | | | |
| Diferenciamos nossos produtos ou serviços por qualidade | | | | | | | | |

# Resultados da Empresa

Perguntas referentes aos Resultados de sua Empresa

9. **9- Indique, por favor, sua percepção sobre os resultados da sua empresa no ano de 2015 em relação a empresas similares do setor:** *

Marque 0 “se não foi produzido o resultado” e se foi produzido, utilize uma escala de 1 “muito abaixo de empresas similares do setor” a 7 “muito acima de empresas similares do setor”:

*Marcar apenas uma oval por linha.*

| | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
|---|---|---|---|---|---|---|---|---|
| Oferece produtos de qualidade | | | | | | | | |
| Dispõe de processos internos eficientes | | | | | | | | |
| Possui clientes satisfeitos | | | | | | | | |
| Se adapta as mudanças do mercado | | | | | | | | |
| Está crescendo | | | | | | | | |
| É rentável | | | | | | | | |
| Tem empregados satisfeitos/motivados | | | | | | | | |
| Absentismo laboral | | | | | | | | |
| Inovações de processo | | | | | | | | |
| Inovações de produto ou serviço | | | | | | | | |
| Rentabilidade sobre ativos | | | | | | | | |
| Rentabilidade sobre vendas | | | | | | | | |
| Resultado financeiro global | | | | | | | | |
| Relações com clientes | | | | | | | | |
| Relações com fornecedores | | | | | | | | |
| Melhora da qualidade de produtos e serviços | | | | | | | | |
| Melhora no nível de qualidade dos processos | | | | | | | | |

# Dados da Empresa

Perguntas referente aos dados gerais e de identificação de sua Empresa

## 10- Indique, por favor, aproximadamente para o ano de 2015, o número de pessoas que se encontra nos seguintes grupos:

10. **Total de empregados** *

11. **Total de empregados Homens** *

12. **Total de empregados Mulheres** *

13. **Total de empregados a Tempo completo** *

14. **Total de empregados a Tempo parcial** *

15. **Autônomos que trabalham na empresa** *

16. **Empregados com Contrato fixo** *

17. **Empregados com Contrato temporário** *

18. **Trabalhadores de empresas de trabalho temporário** *

19. **Nº de demissões** *

20. **Nº demissões voluntárias** *

## 11- Indique, por favor, os seguintes dados da sua empresa:

21. **Ano de constituição da empresa** *

22. **Nº de níveis hierárquicos entre o gerente e os empregados (ambos incluídos)** *

23. **Nº de níveis hierárquicos total na empresa (desde o nível mais baixo ao nível mais alto)** *

24. **Faturamento bruto (em Reais) no ano de 2015** *
Por favor, marcar somente uma resposta (segundo classificação do porte de empresas SEBRAE)
*Marcar apenas uma oval.*

- Até R$ 60.000,00
- De R$ 60.000,01 a R$ 360.000,00
- De R$ 360.000,01 a R$ 3.600.000,00
- Acima de R$ 3.600.000,01

25. **Indique, por favor, as atividades em que sua empresa atua:** *
Por favor, marque pelo menos uma resposta
*Marcar tudo o que for aplicável.*

- [ ] Viagens Corporativas
- [ ] Incentivos
- [ ] Eventos
- [ ] Outros

26. **Nome da empresa**

Com tecnologia Google Forms

# ANEXO II

## MODELOS DE ECUACIONES ESTRUCTURALES

## 1. MODELOS DE ECUACIONES ESTRUCTURALES

Los modelos de ecuaciones estructurales (Estructural Equation Moleling, SEM) son también conocidos como análisis estructural de covarianza o como modelos causales (Lavee, 1988; Arbuckle, 2007; Byrne, 2010), y constituyen un instrumento básico de análisis en la presente Tesis Doctoral. Las razones que justifican la utilización de esta aproximación metodológica, también denominada de covarianzas, han sido las siguientes:

- Estos modelos permiten abordar los fenómenos objeto de estudio en toda su globalidad, teniendo en cuenta su gran complejidad. Es decir, permiten considerar las múltiples causas y relaciones.

- Es un instrumento que simplifica las grandes matrices multivariantes, ya que al agrupar las relaciones entre un gran número de variables en unos pocos factores, pone de relieve lo esencial.

- Son modelos que permiten al investigador introducir información y posteriormente reformular los modelos según su ajuste a los datos, en base a la información que proporcionan los estadísticos e índices de bondad de ajuste de los modelos.

- Se trata de una metodología que permite aceptar el error de medida como inherente al estudio, de forma que se introduce como parte de la especificación del modelo, y de esta manera es posible cuantificar la calidad de la medición de los datos.

Así, la metodología de ecuaciones estructurales nos va a permitir estimar varias ecuaciones a la vez; ecuaciones que pueden estar interrelacionadas, lo que significa que la variable dependiente en una ecuación puede ser una variable independiente en otra. Esto nos permite modelizar relaciones complejas que no serían posibles con ninguna otra de las técnicas multivariantes.

Para ello, esta metodología requiere la especificación de dimensiones o variables latentes, es decir variables teóricas que no son susceptibles de observación directa, y que se infieren a partir de un conjunto de variables observadas o indicadores, dando lugar a los modelos de medida que comprenden los análisis factoriales confirmatorios. Por otro lado, esta metodología permite analizar la posible influencia de dichas variables sobre otras variables, tanto observadas como latentes. De la relación de los modelos de medida con otras variables surgen los modelos de ecuaciones estructurales.

## 2. ETAPAS EN LA CONSTRUCCIÓN DE MODELOS DE ECUACIONES ESTRUCTURALES

Esta metodología estadística, como toda metodología científica, es la consecuencia de un proceso interactivo entre teoría y práctica, en el que subyacen una serie de etapas que se resumen a continuación, y que son las seguidas para la aplicación de esta herramienta en la presente Tesis Doctoral.

1- Etapa de especificación. La especificación consiste en establecer formalmente un modelo, que en esencia es una explicación teórica de por qué las variables están o no relacionadas. Esta etapa, por tanto, se centra más en el conocimiento teórico que sobre el fenómeno se tenga, que en el instrumento estadístico. Así, en esta fase, se traduce en un conjunto de ecuaciones las teorías que se han formulado previamente, y que hacen referencia a: a) las variables latentes o dimensiones que deben considerarse; b) los efectos entre las variables latentes (directo, indirecto, conjunto); c) los indicadores que asignamos a cada dimensión; d) las covarianzas entre variables exógenas.

2- Etapa de identificación. Una vez establecido el apoyo teórico del modelo de ecuaciones estructurales, se debe validar el sustento de cada una de las variables que van a formar parte del mismo, de forma que con dichas variables se pueda estimar de una forma inequívoca los parámetros del modelo. En esta etapa, por tanto, se determina si las covarianzas entre las variables observables facilitan información suficiente para estimar los parámetros del modelo.

3. Etapa de estimación. Cuando se dispone de la información muestral y de las relaciones establecidas entre covarianzas y parámetros, puede procederse a la estimación. La etapa de estimación requiere decidir sobre el criterio que se elegirá para

determinar los mejores estimadores, así como sobre las propiedades estadísticas deseables de los mismos. En concreto, consiste en la utilización de algún algoritmo de optimización para la función criterio elegida, y en este sentido son muchos los métodos disponibles, considerándose como estándares los siguientes: LS (least squares), GLS (generalizad least sequares), ML (maximun likelihood), ADF (asymptotic distribution-free). En la presente Tesis Doctoral, siguiendo a Rivera y Satorra (2002), el método seleccionado para todos los modelos a efectos de estimación de parámetros es el método de Máxima Verosimilitud (ML), aunque a efectos de inferencia se procederá a analizar los errores estándares robustos de los parámetros estimados.

4. Etapa de evaluación. Una vez estimado el modelo habrá que evaluar el ajuste entre nuestros datos al modelo propuesto. La valoración de las estructuras planteadas o de las hipótesis inherentes a los modelos teóricos propuestos debe realizarse en dos etapas. Una primera en la que se procede a analizar el ajuste del modelo de medida y del modelo estructural y una segunda en la que se procede a juzgar la idoneidad del modelo (la adecuada o razonable representación de la realidad) mediante una serie de índices y estadísticos que figuran en el epígrafe siguiente.

## 3. BONDAD DE AJUSTE DE LOS MODELOS SEM

Como ya se ha indicado, una vez el modelo ha sido identificado y estimado, habrá que evaluar el ajuste de nuestros datos al modelo propuesto, y para ello habrá que proceder a: (1) evaluar el ajuste del modelo de medida, (2) evaluar el ajuste del modelo estructural y (3) evaluar el ajuste global del modelo

### 3.1. Ajuste de los componentes del modelo

Las medidas de ajuste de los componentes del modelo se obtienen a partir de las estimaciones de los parámetros y de las estimaciones de sus varianzas. En primer lugar, se evalúa su significación y, posteriormente, se comprueba la coherencia existente con las hipótesis. En segundo lugar, se calculan para cada una de las ecuaciones del modelo los coeficientes de determinación, para poder determinar el poder predictivo de las variables explicativas.

### 3.1.1. Ajuste del modelo de medida

En cuanto al modelo de medida, el paso inicial consiste en obtener una visión preliminar sobre la adecuación de los instrumentos de medida utilizados para valorar el efecto de unas variables sobre otras. La metodología del análisis exploratorio establece una serie de requisitos que deben cumplir los indicadores de las escalas y, de esta forma, establece también un procedimiento para eliminar aquellos indicadores que impiden que las escalas alcancen valores aceptables en sus propiedades de medida. Para detectar qué indicadores son susceptibles de ser eliminados habrá que analizar la fiabilidad y dimensionalidad de la escala.

El análisis de fiabilidad permite comprobar la consistencia interna de la escala, es decir, si la escala se encuentra libre de error aleatorio y es capaz de ofrecer unos resultados estables. Así, una escala va a ser fiable si los individuos han contestado de forma coherente y consistente a todos los indicadores que la componen y, de esta manera, los indicadores se encuentran altamente correlacionados (Churchill, 1979). Para analizar la consistencia interna de la escala disponemos de dos instrumentos bastante utilizados en áreas de la Ciencia de la Administración (Chandler y Lyon, 2001): el estadístico Alpha de Cronbach y la correlación ítem-total.

El estadístico Alpha de Cronbach es un parámetro frecuentemente utilizado para analizar la consistencia interna de la escala y su fiabilidad (Nunnaly, 1978). En general, se puede garantizar la fiabilidad de la escala si el valor de este indicador es superior a 0,8 (Grande y Abascal, 2003); aunque en estudios de carácter exploratorio, un valor superior a 0,6 se considera ya aceptable (Miquel *et al*., 1996).

Si la escala inicialmente no supera estos límites, su fiabilidad puede mejorar eliminando aquellos indicadores que tienen una baja correlación con el resto de indicadores (Bagozzi, 1981). De esta forma, cuando un indicador no alcanza el nivel óptimo de 0,3 en la correlación ítem-total, se considera que no está suficientemente correlacionado con el resto de indicadores y, por tanto, no es significativa su permanencia en dicha escala (Nurosis, 1993).

Analizada la fiabilidad de la escala, con el fin de llegar a una estructura subyacente de las variables/indicadores objeto de estudio, habrá que analizar el conjunto de relaciones entre dichas variables mediante el Análisis de Componentes Principales.

El Análisis de Componentes Principales es una técnica de reducción de dimensiones que nos permite conseguir variables latentes, que son transformaciones matemáticas exactas de las variables observadas (componentes principales) (Luque, 2000). El número de componentes a retener se define a partir de las comunalidades de las variables originales y los porcentajes de varianza explicada de las primeras componentes principales. Se considera que un indicador debería tener al menos un 50% de su varianza en común con la variable latente, estableciendo así como límite de aceptación para la fiabilidad el valor 0,50 (Sharma, 1996).

Por otro lado, los indicadores han de tener una alta consistencia interna, es decir, han de ser una medida válida del concepto a estudiar. Dicha consistencia interna va a ser medida a través de la fiabilidad compuesta, en un análisis posterior. Así, otra medida a considerar según McDonald (1997) es el coeficiente de fiabilidad Omega (IFC). Es una medida que en parte coincide con el coeficiente Alpha de Cronbach, pero permite tener en cuenta todos los constructos implicados en la escala. Si el valor obtenido es superior a 0,70 significa que los indicadores miden adecuadamente dicha variable latente.

Por último, otra medida muy utilizada como medida complementaria a la fiabilidad es el índice planteado por Fornell y Larcker (1981), el cual pretende recoger la parte de varianza explicada de un conjunto de medidas por la variable latente (AVE).

La obtención de valores altos refleja que los indicadores son verdaderamente representativos del constructo latente. Así, valores de este índice superiores a 0,5 se consideran adecuados y, superiores a 0,6 deseables (Fornell y Larcker, 1981; Bagozzi y Yi, 1988). En cuanto a la utilización de estos índices, Baumgartner y Homburg (1996) son partidarios del empleo, como mínimo, de una medida de fiabilidad que se base en las cargas factoriales.

### 3.1.2. Ajuste del modelo estructural

En cuanto al ajuste del modelo estructural, lo primero a analizar es la significación alcanzada por los coeficientes estimados. Un parámetro no significativo indicará que la relación propuesta no tiene ningún efecto sustancial y es susceptible de eliminación del modelo, sobre todo si su interpretación teórica es débil. Otra medida para evaluar el modelo estructural es el $R^2$ (coeficiente de fiabilidad) y la matriz de correlaciones estandarizadas entre las variables latentes (para el caso de utilizar como matriz inicial la matriz de varianzas-covarianzas). Si su valor es bajo indica, si se trata de una variable observable, una pobre validez, y si se trata de una variable latente sugiere que no todas las variables relevantes para su predicción han sido incorporadas en el modelo. Cuanto más se acerque a la unidad, mejor representada estará la relación estructural propuesta.

## 3.2. Ajuste global del modelo

Existirá un ajuste perfecto del modelo cuando haya una correspondencia perfecta entre la matriz reproducida por el modelo y la matriz de observaciones. Las medidas de calidad de ajuste son de tres tipos: (1) Medidas de ajuste absoluto[1], (2) Medidas de ajuste incremental[2] y (3) Medidas de ajuste de Parsimonia[3].

### 3.2.1. Medidas de ajuste absoluto

Las medidas de ajuste absoluto determinan el grado en que el modelo conjunto (modelos estructural y de medida) predice la matriz de correlación o covarianza observada.

---

[1] Dicen en qué medida el modelo de forma conjunta predice la matriz de correlación observada (o de varianza según proceda), sin distinguir si el modelo de ajuste es mejor o peor en el modelo de medida o estructural.

[2] Comparan el modelo propuesto con otros especificados por el investigador.

[3] Ofrecen comparación entre modelos, siendo su principal objetivo determinar la cantidad de ajuste logrado por cada coeficiente estimado.

La primera medida aplicada en la presente Tesis Doctoral es el estadístico Chi-cuadrado ($\chi^2$). Valores bajos de $\chi^2$ nos llevarán a no rechazar la hipótesis nula. Con este test se persigue que no existan diferencias significativas entre la matriz observada y la estimada, por lo que para no rechazar la hipótesis nula el nivel de significación debe ser superior a 0,05 o 0,01 (dependiendo del grado de exigencia).

Sin embargo, este test es muy sensible a los diferentes tamaños de muestra, así como al número de categorías de la variable respuesta, por lo que se recomienda complementar este indicador con otras medidas de calidad de ajuste. Entre las medidas de bondad de ajuste desarrolladas para completar la visión aportada por el anterior estadístico, se encuentra el Chi-cuadrado de Satorra-Bentler (Satorra y Bentler, 1994), utilizado en esta Tesis Doctoral. Este estadístico suele presentar un valor inferior al anterior, ya que se calcula bajo condiciones de no normalidad con la matriz de covarianzas asintóticas.

En cuanto a la raíz cuadrada de la media de los residuos al cuadrado (SRMR-Root Mean Square Residual), también aplicada en esta Tesis, se basa en un promedio de los residuos entre la matriz de observaciones inicial y la matriz estimada por el modelo. En la medida en que el SRMR se acerque a cero, los errores entre ambas matrices serán muy pequeños, lo que significará que el ajuste es bueno.

Por último, en relación al RMSEA (Root Mean Square Error of Approximation) que es una medida introducida por Steiger (1990) para intentar eliminar el inconveniente que presenta la Chi-cuadrado cuando la muestra es lo suficientemente grande, describe la diferencia de las matrices por grado de libertad, es decir, la bondad de ajuste que debería ser esperada si el modelo fuera estimado, pero a diferencia del SRMR, en términos de población y no en términos de muestra.

### 3.2.2. Medidas de ajuste incremental

Estas medidas permiten comparar el modelo propuesto con el modelo de independencia en el cual se asume que no hay asociaciones entre las variables.

Dentro de estas medidas incrementales podemos destacar el Normed Fit Index (NFI), Non Norme Fit Index (NNFI), Incremetal Fit Index (IFI) y el Comparative Fit Index (CFI).

El NFI, índice de ajuste normado (Bentler y Bonett, 1980), es una de las medidas más populares que va de 0 (ningún ajuste) a 1 (ajuste perfecto), y evalúa la disminución del estadístico Chi-cuadrado de nuestro modelo con respecto al modelo base. En este caso tampoco existe un valor absoluto que indique un nivel de ajuste aceptable, pero un valor recomendable es 0,90 (Hair *et al.*, 2004) o cercano a 0,90 (Shumacker y Lomax, 1996).

El NNFI, índice de ajusto no normado o índice Tucker-Lewis (TLI), definido por Tucker y Lewis (1973), realiza una comparación por grados de libertad del modelo propuesto y del nulo. Valores por encima de 0,9 indican un buen ajuste del modelo (Schumacker y Lomax, 1996).

El IFI o índice de ajuste incremental, definido por Bollen (1989), relaciona la chi-cuadrado de los modelos propuesto y nulo. Valores superiores a 0,9 se consideran aceptables.

Por último, el CFI introducido por Bentler (1990), también representa una comparación entre el modelo estimado y el modelo nulo o independiente. Los valores se encuentran entre cero y uno, indicando los valores elevados altos niveles de calidad del ajuste. El CFI resulta apropiado cuando el tamaño de la muestra es reducido.

En esta Tesis Doctoral se ha optado por dicho conjunto de estadísticos e índices porque en muchas ocasiones el estadístico Chi-cuadrado nos lleva al rechazo del modelo por cuestiones directamente relacionadas con el tamaño de la muestra o con el número de parámetros a estimar. Destacar que el estadístico RMSEA proporciona una medida de ajuste aproximado del modelo, es decir, relaja la hipótesis de ajuste perfecto, hipótesis subyacente al estadístico Chi-cuadrado.

### 3.2.3. Medidas de ajuste de parsimonia

Siguiendo a Hair (2004), las medidas de ajuste de parsimonia relacionan la calidad del modelo al número de coeficientes estimados exigidos para conseguir este nivel de ajuste. Sus objetivos básicos son diagnosticar si el ajuste del modelo se ha conseguido debido a un sobreajuste de los datos por tener demasiados coeficientes. Este procedimiento es similar al ajuste del $R^2$ en una regresión múltiple. Sin embargo, dado que no existe ningún test de significación estadístico, su uso en un sentido absoluto, está limitado en muchos casos a comparaciones entre modelos alternativos.

Entre los índices más utilizados destaca la Chi-cuadrado normada, que es el ratio de la chi-cuadrado dividida por los grados de libertad. Valores menores que 1 o superiores a 2 ó 3 indican modelos inapropiados. Esta medida, sin embargo, es poco fiable (Hair, 2004), de forma que los investigadores suelen combinarla con otras medidas de bondad de ajuste como el índice de ajuste normado de parsimonia (PNFI), siendo el valor mínimo recomendado 0,7.

# ANEXO III

# ANALISIS FIABILIDAD INICIAL – USO TIC

**Escala: ALL VARIABLES**

**Resumen de procesamiento de casos**

| | | N | % |
|---|---|---|---|
| Casos | Válido | 170 | 100,0 |
| | Excluido[a] | 0 | ,0 |
| | Total | 170 | 100,0 |

a. La eliminación por lista se basa en todas las variables del procedimiento.

**Estadísticas de fiabilidad**

| Alfa de Cronbach | Alfa de Cronbach basada en elementos estandarizados | N de elementos |
|---|---|---|
| ,896 | ,896 | 12 |

**Estadísticas de elemento**

| | Media | Desviación estándar | N |
|---|---|---|---|
| p.1.1 - [Sistema de gestión de la solicitud y aprobación de viajes corporativos] | 3,6941 | 2,96936 | 170 |
| p.1.2 - [Informes gerenciales online y personalizados al cliente] | 4,0059 | 2,78733 | 170 |
| p.1.3 - [Perfiles electrónicos de los viajeros ] | 3,4235 | 2,71257 | 170 |
| p.1.5 - [Sistema de self-booking (búsqueda y reserva de viajes)] | 4,8765 | 2,65402 | 170 |
| p.1.6 - [Sistema de self-ticketing (búsqueda, reserva y emisión de viajes)] | 4,4000 | 2,79136 | 170 |

| | | | |
|---|---|---|---|
| p.1.8 - [Sistema de rastreo y localización de los pasajeros en situaciones de emergencias y crisis] | 2,1353 | 2,59709 | 170 |
| p.1.9 - [Sistema de Gestión de Eventos] | 2,3647 | 2,61469 | 170 |
| p.1.10 - [Sistemas GDS – Sistema Global de Distribuición] | 4,7059 | 2,89388 | 170 |
| p.1.11 - [Sistema CRS - Sistema Central de Reservas] | 3,5059 | 2,90530 | 170 |
| p.1.12 - [Sistemas BI - Business Intelligence] | 2,3706 | 2,83851 | 170 |
| p.1.16 - [Aplicaciones de front office y back office para las agencias de viajes] | 4,6235 | 2,72171 | 170 |
| p.1.17 - [Aplicación de Booking online] | 4,6176 | 2,61102 | 170 |

**Correlación entre elementos entre elementos**

| | p.1.1 - [Sistema de gestión de la solicitud y aprobación de viajes corporativos] | p.1.2 - [Informes gerenciales online y personalizados al cliente] | p.1.3 - [Perfiles electrónicos de los viajeros ] | p.1.5 - [Sistema de self-booking (búsqueda y reserva de viajes)] |
|---|---|---|---|---|
| p.1.1 - [Sistema de gestión de la solicitud y aprobación de viajes corporativos] | 1,000 | ,679 | ,594 | ,544 |
| p.1.2 - [Informes gerenciales online y personalizados al cliente] | ,679 | 1,000 | ,653 | ,514 |
| p.1.3 - [Perfiles electrónicos de los viajeros ] | ,594 | ,653 | 1,000 | ,529 |
| p.1.5 - [Sistema de self-booking (búsqueda y reserva de viajes)] | ,544 | ,514 | ,529 | 1,000 |
| p.1.6 - [Sistema de self-ticketing (búsqueda, reserva y emisión de viajes)] | ,380 | ,431 | ,393 | ,731 |

| | | | | |
|---|---|---|---|---|
| p.1.8 - [Sistema de rastreo y localización de los pasajeros en situaciones de emergencias y crisis] | ,508 | ,550 | ,623 | ,325 |
| p.1.9 - [Sistema de Gestión de Eventos] | ,226 | ,389 | ,267 | ,138 |
| p.1.10 - [Sistemas GDS – Sistema Global de Distribuición] | ,394 | ,428 | ,477 | ,423 |
| p.1.11 - [Sistema CRS - Sistema Central de Reservas] | ,386 | ,420 | ,437 | ,426 |
| p.1.12 - [Sistemas BI - Business Intelligence] | ,422 | ,485 | ,469 | ,380 |
| p.1.16 - [Aplicaciones de front office y back office para las agencias de viajes] | ,404 | ,471 | ,495 | ,458 |
| p.1.17 - [Aplicación de Booking online] | ,364 | ,421 | ,467 | ,523 |

**Correlación entre elementos entre elementos**

| | p.1.6 - [Sistema de self-ticketing (búsqueda, reserva y emisión de viajes)] | p.1.8 - [Sistema de rastreo y localización de los pasajeros en situaciones de emergencias y crisis] | p.1.9 - [Sistema de Gestión de Eventos] | p.1.10 - [Sistemas GDS – Sistema Global de Distribuición] |
|---|---|---|---|---|
| p.1.1 - [Sistema de gestión de la solicitud y aprobación de viajes corporativos] | ,380 | ,508 | ,226 | ,394 |
| p.1.2 - [Informes gerenciales online y personalizados al cliente] | ,431 | ,550 | ,389 | ,428 |
| p.1.3 - [Perfiles electrónicos de los viajeros ] | ,393 | ,623 | ,267 | ,477 |
| p.1.5 - [Sistema de self-booking (búsqueda y reserva de viajes)] | ,731 | ,325 | ,138 | ,423 |
| p.1.6 - [Sistema de self-ticketing (búsqueda, reserva y emisión de viajes)] | 1,000 | ,322 | ,235 | ,248 |

| | | | | |
|---|---|---|---|---|
| p.1.8 - [Sistema de rastreo y localización de los pasajeros en situaciones de emergencias y crisis] | ,322 | 1,000 | ,314 | ,268 |
| p.1.9 - [Sistema de Gestión de Eventos] | ,235 | ,314 | 1,000 | ,156 |
| p.1.10 - [Sistemas GDS – Sistema Global de Distribuición] | ,248 | ,268 | ,156 | 1,000 |
| p.1.11 - [Sistema CRS - Sistema Central de Reservas] | ,370 | ,439 | ,282 | ,443 |
| p.1.12 - [Sistemas BI - Business Intelligence] | ,384 | ,512 | ,499 | ,360 |
| p.1.16 - [Aplicaciones de front office y back office para las agencias de viajes] | ,342 | ,408 | ,240 | ,448 |
| p.1.17 - [Aplicación de Booking online] | ,387 | ,314 | ,279 | ,411 |

**Correlación entre elementos entre elementos**

| | p.1.11 - [Sistema CRS - Sistema Central de Reservas] | p.1.12 - [Sistemas BI - Business Intelligence] | p.1.16 - [Aplicaciones de front office y back office para las agencias de viajes] | p.1.17 - [Aplicación de Booking online] |
|---|---|---|---|---|
| p.1.1 - [Sistema de gestión de la solicitud y aprobación de viajes corporativos] | ,386 | ,422 | ,404 | ,364 |
| p.1.2 - [Informes gerenciales online y personalizados al cliente] | ,420 | ,485 | ,471 | ,421 |
| p.1.3 - [Perfiles electrónicos de los viajeros ] | ,437 | ,469 | ,495 | ,467 |
| p.1.5 - [Sistema de self-booking (búsqueda y reserva de viajes)] | ,426 | ,380 | ,458 | ,523 |
| p.1.6 - [Sistema de self-ticketing (búsqueda, reserva y emisión de viajes)] | ,370 | ,384 | ,342 | ,387 |
| p.1.8 - [Sistema de rastreo y localización de los pasajeros en situaciones de emergencias y crisis] | ,439 | ,512 | ,408 | ,314 |
| p.1.9 - [Sistema de Gestión de Eventos] | ,282 | ,499 | ,240 | ,279 |

| | | | | |
|---|---|---|---|---|
| p.1.10 - [Sistemas GDS – Sistema Global de Distribuición] | ,443 | ,360 | ,448 | ,411 |
| p.1.11 - [Sistema CRS - Sistema Central de Reservas] | 1,000 | ,457 | ,480 | ,415 |
| p.1.12 - [Sistemas BI - Business Intelligence] | ,457 | 1,000 | ,462 | ,411 |
| p.1.16 - [Aplicaciones de front office y back office para las agencias de viajes] | ,480 | ,462 | 1,000 | ,539 |
| p.1.17 - [Aplicación de Booking online] | ,415 | ,411 | ,539 | 1,000 |

**Estadísticas de elemento de resumen**

| | Media | Mínimo | Máximo | Rango | Máximo / Mínimo | Varianza |
|---|---|---|---|---|---|---|
| Medias de elemento | 3,727 | 2,135 | 4,876 | 2,741 | 2,284 | ,980 |
| Varianzas de elemento | 7,622 | 6,745 | 8,817 | 2,072 | 1,307 | ,490 |
| Covariables entre elementos | 3,193 | ,957 | 5,617 | 4,661 | 5,872 | ,807 |
| Correlaciones entre elementos | ,419 | ,138 | ,731 | ,593 | 5,304 | ,013 |

**Estadísticas de elemento de resumen**

| | N de elementos |
|---|---|
| Medias de elemento | 12 |
| Varianzas de elemento | 12 |
| Covariables entre elementos | 12 |
| Correlaciones entre elementos | 12 |

**Estadísticas de total de elemento**

| | Media de escala si el elemento se ha suprimido | Varianza de escala si el elemento se ha suprimido | Correlación total de elementos corregida | Correlación múltiple al cuadrado |
|---|---|---|---|---|
| p.1.1 - [Sistema de gestión de la solicitud y aprobación de viajes corporativos] | 41,0294 | 424,396 | ,652 | ,552 |

| | | | | |
|---|---|---|---|---|
| p.1.2 - [Informes gerenciales online y personalizados al cliente] | 40,7176 | 421,482 | ,731 | ,617 |
| p.1.3 - [Perfiles electrónicos de los viajeros ] | 41,3000 | 424,507 | ,725 | ,608 |
| p.1.5 - [Sistema de self-booking (búsqueda y reserva de viajes)] | 39,8471 | 432,249 | ,668 | ,694 |
| p.1.6 - [Sistema de self-ticketing (búsqueda, reserva y emisión de viajes)] | 40,3235 | 440,338 | ,553 | ,576 |
| p.1.8 - [Sistema de rastreo y localización de los pasajeros en situaciones de emergencias y crisis] | 42,5882 | 439,971 | ,608 | ,513 |
| p.1.9 - [Sistema de Gestión de Eventos] | 42,3588 | 462,267 | ,390 | ,327 |
| p.1.10 - [Sistemas GDS – Sistema Global de Distribuición] | 40,0176 | 439,899 | ,533 | ,374 |
| p.1.11 - [Sistema CRS - Sistema Central de Reservas] | 41,2176 | 431,828 | ,602 | ,395 |
| p.1.12 - [Sistemas BI - Business Intelligence] | 42,3529 | 429,449 | ,641 | ,484 |
| p.1.16 - [Aplicaciones de front office y back office para las agencias de viajes] | 40,1000 | 434,114 | ,630 | ,448 |
| p.1.17 - [Aplicación de Booking online] | 40,1059 | 440,545 | ,598 | ,430 |

**Estadísticas de total de elemento**

| | Alfa de Cronbach si el elemento se ha suprimido |
|---|---|
| p.1.1 - [Sistema de gestión de la solicitud y aprobación de viajes corporativos] | ,886 |
| p.1.2 - [Informes gerenciales online y personalizados al cliente] | ,882 |
| p.1.3 - [Perfiles electrónicos de los viajeros ] | ,882 |
| p.1.5 - [Sistema de self-booking (búsqueda y reserva de viajes)] | ,885 |
| p.1.6 - [Sistema de self-ticketing (búsqueda, reserva y emisión de viajes)] | ,891 |
| p.1.8 - [Sistema de rastreo y localización de los pasajeros en situaciones de emergencias y crisis] | ,888 |
| p.1.9 - [Sistema de Gestión de Eventos] | ,899 |
| p.1.10 - [Sistemas GDS – Sistema Global de Distribuición] | ,892 |
| p.1.11 - [Sistema CRS - Sistema Central de Reservas] | ,889 |

| | |
|---|---|
| p.1.12 - [Sistemas BI - Business Intelligence] | ,886 |
| p.1.16 - [Aplicaciones de front office y back office para las agencias de viajes] | ,887 |
| p.1.17 - [Aplicación de Booking online] | ,889 |

# ANEXO IV

# ANÁLISIS FACTORIAL EXPLORATORIO – USO TIC

**Matriz de correlaciones**

| | | p.1.1 - [Sistema de gestión de la solicitud y aprobación de viajes corporativos] | p.1.2 - [Informes gerenciales online y personalizados al cliente] | p.1.3 - [Perfiles electrónicos de los viajeros] | p.1.5 - [Sistema de self-booking (búsqueda y reserva de viajes)] | p.1.6 - [Sistema de self-ticketing (búsqueda, reserva y emisión de viajes)] | p.1.8 - [Sistema de rastreo y localización de los pasajeros en situaciones de emergencias y crisis] | p.1.9 - [Sistema de Gestión de Eventos] | p.1.10 - [Sistemas GDS – Sistema Global de Distribución] |
|---|---|---|---|---|---|---|---|---|---|
| Correlación | p.1.1 - [Sistema de gestión de la solicitud y aprobación de viajes corporativos] | 1,000 | ,679 | ,594 | ,544 | ,380 | ,508 | ,226 | ,394 |
| | p.1.2 - [Informes gerenciales online y personalizados al cliente] | ,679 | 1,000 | ,653 | ,514 | ,431 | ,550 | ,389 | ,428 |
| | p.1.3 - [Perfiles electrónicos de los viajeros] | ,594 | ,653 | 1,000 | ,529 | ,393 | ,623 | ,267 | ,477 |
| | p.1.5 - [Sistema de self-booking (búsqueda y reserva de viajes)] | ,544 | ,514 | ,529 | 1,000 | ,731 | ,325 | ,138 | ,423 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| p.1.6 - [Sistema de self-ticketing (búsqueda, reserva y emisión de viajes)] | ,380 | ,431 | ,393 | ,731 | 1,000 | ,322 | ,235 | ,248 |
| p.1.8 - [Sistema de rastreo y localización de los pasajeros en situaciones de emergencias y crisis] | ,508 | ,550 | ,623 | ,325 | ,322 | 1,000 | ,314 | ,268 |
| p.1.9 - [Sistema de Gestión de Eventos] | ,226 | ,389 | ,267 | ,138 | ,235 | ,314 | 1,000 | ,156 |
| p.1.10 - [Sistemas GDS – Sistema Global de Distribuición] | ,394 | ,428 | ,477 | ,423 | ,248 | ,268 | ,156 | 1,000 |
| p.1.11 - [Sistema CRS - Sistema Central de Reservas] | ,386 | ,420 | ,437 | ,426 | ,370 | ,439 | ,282 | ,443 |
| p.1.12 - [Sistemas BI - Business Intelligence] | ,422 | ,485 | ,469 | ,380 | ,384 | ,512 | ,499 | ,360 |
| p.1.16 - [Aplicaciones de front office y back office para las agencias de viajes] | ,404 | ,471 | ,495 | ,458 | ,342 | ,408 | ,240 | ,448 |
| p.1.17 - [Aplicación de Booking online] | ,364 | ,421 | ,467 | ,523 | ,387 | ,314 | ,279 | ,411 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| Sig. (unilateral) | p.1.1 - [Sistema de gestión de la solicitud y aprobación de viajes corporativos] | | ,000 | ,000 | ,000 | ,000 | ,000 | ,001 | ,000 |
| | p.1.2 - [Informes gerenciales online y personalizados al cliente] | ,000 | | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 |
| | p.1.3 - [Perfiles electrónicos de los viajeros] | ,000 | ,000 | | ,000 | ,000 | ,000 | ,000 | ,000 |
| | p.1.5 - [Sistema de self-booking (búsqueda y reserva de viajes)] | ,000 | ,000 | ,000 | | ,000 | ,000 | ,037 | ,000 |
| | p.1.6 - [Sistema de self-ticketing (búsqueda, reserva y emisión de viajes)] | ,000 | ,000 | ,000 | ,000 | | ,000 | ,001 | ,001 |
| | p.1.8 - [Sistema de rastreo y localización de los pasajeros en situaciones de emergencias y crisis] | ,000 | ,000 | ,000 | ,000 | ,000 | | ,000 | ,000 |
| | p.1.9 - [Sistema de Gestión de Eventos] | ,001 | ,000 | ,000 | ,037 | ,001 | ,000 | | ,021 |
| | p.1.10 - [Sistemas GDS – Sistema Global de Distribuición] | ,000 | ,000 | ,000 | ,000 | ,001 | ,000 | ,021 | |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| p.1.11 - [Sistema CRS - Sistema Central de Reservas] | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 |
| p.1.12 - [Sistemas BI - Business Intelligence] | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 |
| p.1.16 - [Aplicaciones de front office y back office para las agencias de viajes] | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 | ,001 | ,000 |
| p.1.17 - [Aplicación de Booking online] | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 |

**Matriz de correlaciones**

| | | p.1.11 - [Sistema CRS - Sistema Central de Reservas] | p.1.12 - [Sistemas BI - Business Intelligence] | p.1.16 - [Aplicaciones de front office y back office para las agencias de viajes] | p.1.17 - [Aplicación de Booking online] |
|---|---|---|---|---|---|
| Correlación | p.1.1 - [Sistema de gestión de la solicitud y aprobación de viajes corporativos] | ,386 | ,422 | ,404 | ,364 |
| | p.1.2 - [Informes gerenciales online y personalizados al cliente] | ,420 | ,485 | ,471 | ,421 |
| | p.1.3 - [Perfiles electrónicos de los viajeros] | ,437 | ,469 | ,495 | ,467 |
| | p.1.5 - [Sistema de self-booking (búsqueda y reserva de viajes)] | ,426 | ,380 | ,458 | ,523 |

| | | | | | |
|---|---|---|---|---|---|
| | p.1.6 - [Sistema de self-ticketing (búsqueda, reserva y emisión de viajes)] | ,370 | ,384 | ,342 | ,387 |
| | p.1.8 - [Sistema de rastreo y localización de los pasajeros en situaciones de emergencias y crisis] | ,439 | ,512 | ,408 | ,314 |
| | p.1.9 - [Sistema de Gestión de Eventos] | ,282 | ,499 | ,240 | ,279 |
| | p.1.10 - [Sistemas GDS – Sistema Global de Distribuición] | ,443 | ,360 | ,448 | ,411 |
| | p.1.11 - [Sistema CRS - Sistema Central de Reservas] | 1,000 | ,457 | ,480 | ,415 |
| | p.1.12 - [Sistemas BI - Business Intelligence] | ,457 | 1,000 | ,462 | ,411 |
| | p.1.16 - [Aplicaciones de front office y back office para las agencias de viajes] | ,480 | ,462 | 1,000 | ,539 |
| | p.1.17 - [Aplicación de Booking online] | ,415 | ,411 | ,539 | 1,000 |
| Sig. (unilateral) | p.1.1 - [Sistema de gestión de la solicitud y aprobación de viajes corporativos] | ,000 | ,000 | ,000 | ,000 |
| | p.1.2 - [Informes gerenciales online y personalizados al cliente] | ,000 | ,000 | ,000 | ,000 |
| | p.1.3 - [Perfiles electrónicos de los viajeros] | ,000 | ,000 | ,000 | ,000 |
| | p.1.5 - [Sistema de self-booking (búsqueda y reserva de viajes)] | ,000 | ,000 | ,000 | ,000 |
| | p.1.6 - [Sistema de self-ticketing (búsqueda, reserva y emisión de viajes)] | ,000 | ,000 | ,000 | ,000 |

| | | | | | |
|---|---|---|---|---|---|
| | p.1.8 - [Sistema de rastreo y localización de los pasajeros en situaciones de emergencias y crisis] | ,000 | ,000 | ,000 | ,000 |
| | p.1.9 - [Sistema de Gestión de Eventos] | ,000 | ,000 | ,001 | ,000 |
| | p.1.10 - [Sistemas GDS – Sistema Global de Distribuición] | ,000 | ,000 | ,000 | ,000 |
| | p.1.11 - [Sistema CRS - Sistema Central de Reservas] | | ,000 | ,000 | ,000 |
| | p.1.12 - [Sistemas BI - Business Intelligence] | ,000 | | ,000 | ,000 |
| | p.1.16 - [Aplicaciones de front office y back office para las agencias de viajes] | ,000 | ,000 | | ,000 |
| | p.1.17 - [Aplicación de Booking online] | ,000 | ,000 | ,000 | |

**Prueba de KMO y Bartlett**

| | | |
|---|---|---|
| Medida Kaiser-Meyer-Olkin de adecuación de muestreo | | ,883 |
| Prueba de esfericidad de Bartlett | Aprox. Chi-cuadrado | 956,863 |
| | gl | 66 |
| | Sig. | ,000 |

**Matriz de componente**[a]

| | Componente | | | |
|---|---|---|---|---|
| | 1 | 2 | 3 | 4 |
| p.1.2 - [Informes gerenciales online y personalizados al cliente] | ,794 | ,110 | -,300 | ,024 |
| p.1.3 - [Perfiles electrónicos de los viajeros] | ,793 | ,022 | -,291 | -,149 |
| p.1.5 - [Sistema de self-booking (búsqueda y reserva de viajes)] | ,738 | -,502 | | ,283 |
| p.1.1 - [Sistema de gestión de la solicitud y aprobación de viajes corporativos] | ,732 | -,037 | -,444 | -,019 |

| | | | | |
|---|---|---|---|---|
| p.1.12 - [Sistemas BI - Business Intelligence] | ,703 | ,373 | ,196 | ,110 |
| p.1.16 - [Aplicaciones de front office y back office para las agencias de viajes] | ,702 | -,068 | ,261 | -,273 |
| p.1.8 - [Sistema de rastreo y localización de los pasajeros en situaciones de emergencias y crisis] | ,685 | ,335 | -,338 | -,041 |
| p.1.11 - [Sistema CRS - Sistema Central de Reservas] | ,672 | ,026 | ,251 | -,173 |
| p.1.17 - [Aplicación de Booking online] | ,671 | -,177 | ,384 | -,075 |
| p.1.6 - [Sistema de self-ticketing (búsqueda, reserva y emisión de viajes)] | ,634 | -,364 | ,071 | ,581 |
| p.1.10 - [Sistemas GDS – Sistema Global de Distribuición] | ,613 | -,188 | ,153 | -,493 |
| p.1.9 - [Sistema de Gestión de Eventos] | ,458 | ,646 | ,306 | ,320 |

Método de extracción: análisis de componentes principales.[a]

a. 4 componentes extraídos.

**Comunalidades**

| | Extracción |
|---|---|
| p.1.1 - [Sistema de gestión de la solicitud y aprobación de viajes corporativos] | ,735 |
| p.1.2 - [Informes gerenciales online y personalizados al cliente] | ,733 |
| p.1.3 - [Perfiles electrónicos de los viajeros] | ,737 |
| p.1.5 - [Sistema de self-booking (búsqueda y reserva de viajes)] | ,878 |
| p.1.6 - [Sistema de self-ticketing (búsqueda, reserva y emisión de viajes)] | ,877 |

| | |
|---|---|
| p.1.8 - [Sistema de rastreo y localización de los pasajeros en situaciones de emergencias y crisis] | ,697 |
| p.1.9 - [Sistema de Gestión de Eventos] | ,822 |
| p.1.10 - [Sistemas GDS – Sistema Global de Distribuición] | ,677 |
| p.1.11 - [Sistema CRS - Sistema Central de Reservas] | ,545 |
| p.1.12 - [Sistemas BI - Business Intelligence] | ,684 |
| p.1.16 - [Aplicaciones de front office y back office para las agencias de viajes] | ,640 |
| p.1.17 - [Aplicación de Booking online] | ,634 |

Método de extracción: análisis de componentes principales.

**Varianza total explicada**

| Componente | Sumas de extracción de cargas al cuadrado | | | Sumas de rotación de cargas al cuadrado | |
|---|---|---|---|---|---|
| | Total | % de varianza | % acumulado | Total | % de varianza |
| 1 | 5,686 | 47,384 | 47,384 | 2,746 | 22,885 |
| 2 | 1,139 | 9,492 | 56,876 | 2,478 | 20,650 |
| 3 | ,925 | 7,710 | 64,586 | 1,848 | 15,401 |
| 4 | ,909 | 7,579 | 72,165 | 1,587 | 13,229 |

**Varianza total explicada**

| Componente | Sumas de rotación de cargas al cuadrado |
|---|---|
| | % acumulado |
| 1 | 22,885 |
| 2 | 43,535 |
| 3 | 58,936 |
| 4 | 72,165 |

Método de extracción: análisis de componentes principales.

**Matriz de componente rotado**[a]

| | Componente | | | |
|---|---|---|---|---|
| | 1 | 2 | 3 | 4 |
| p.1.1 - [Sistema de gestión de la solicitud y aprobación de viajes corporativos] | ,781 | ,211 | ,282 | ,030 |
| p.1.8 - [Sistema de rastreo y localización de los pasajeros en situaciones de emergencias y crisis] | ,747 | ,169 | ,037 | ,330 |
| p.1.2 - [Informes gerenciales online y personalizados al cliente] | ,735 | ,261 | ,263 | ,238 |
| p.1.3 - [Perfiles electrónicos de los viajeros] | ,731 | ,389 | ,197 | ,108 |
| p.1.10 - [Sistemas GDS – Sistema Global de Distribuición] | ,287 | ,767 | ,046 | -,062 |
| p.1.16 - [Aplicaciones de front office y back office para las agencias de viajes] | ,257 | ,714 | ,173 | ,188 |
| p.1.17 - [Aplicación de Booking online] | ,100 | ,662 | ,370 | ,221 |
| p.1.11 - [Sistema CRS - Sistema Central de Reservas] | ,252 | ,610 | ,172 | ,283 |
| p.1.6 - [Sistema de self-ticketing (búsqueda, reserva y emisión de viajes)] | ,196 | ,127 | ,886 | ,192 |
| p.1.5 - [Sistema de self-booking (búsqueda y reserva de viajes)] | ,323 | ,361 | ,802 | -,021 |
| p.1.9 - [Sistema de Gestión de Eventos] | ,138 | ,079 | ,062 | ,890 |
| p.1.12 - [Sistemas BI - Business Intelligence] | ,346 | ,352 | ,172 | ,641 |

Método de extracción: análisis de componentes principales.

Método de rotación: Varimax con normalización Kaiser.[a]

a. La rotación ha convergido en 6 iteraciones.

**Matriz de transformación de componente**

| Componente | 1 | 2 | 3 | 4 |
|---|---|---|---|---|
| 1 | ,617 | ,570 | ,424 | ,338 |
| 2 | ,194 | -,222 | -,585 | ,755 |
| 3 | -,753 | ,509 | ,085 | ,409 |
| 4 | -,123 | -,606 | ,686 | ,385 |

Método de extracción: análisis de componentes principales.

Método de rotación: Varimax con normalización Kaiser.

# ANEXO V

# ANÁLISIS FACTORIAL CONFIRMATORIO

# USO TIC – PRIMER ORDEN

```
1
  EQS, A STRUCTURAL EQUATION PROGRAM          MULTIVARIATE SOFTWARE, INC.
  COPYRIGHT BY P.M. BENTLER                   VERSION 6.1 (C) 1985 - 2005
(B85).


    PROGRAM CONTROL INFORMATION

    /TITLE
      master confirmatorio tic
    /SPECIFICATIONS
    VARIABLES= 17 ; CASES= 170 ;
    DATAFILE='C:\tesis1\base brasiltic.ESS';
      MATRIX=RAW;METHOD=ML,robust;
    /LABELS
    V1=P.1.1; V2=P.1.2; V3=P.1.3; V4=P.1.4; V5=P.1.5; V6=P.1.6; V7=P.1.7;
    V8=P.1.8; V9=P.1.9; V10=P.1.10; V11=P.1.11; V12=P.1.12;
    V13=P.1.13; V14=P.1.14; V15=P.1.15; V16=P.1.16;
    V17=P.1.17;
    /EQUATIONS
    V1=F1+ E1;
    V8=*F1+E8;
    V2=*F1+E2;
    V3=*F1+E3;
    V10=F2+E10;
    V16=*F2+E16;
    V17=*F2+E17;
    V11=*F2+E11;
    V6=F3+E6;
    V5=*F3+E5;
    V9=F4+E9;
    V12=*F4+E12;
    /VARIANCES
    E1 TO E3=*; E5 TO E6=*;
    E8 TO E12=*;
    E16 TO E17=*;
    F1 TO F4=*;
    /COVARIANCES
    F1 TO F4=*;
    /TECHNICAL
    ITR=100
    /PRINT
    FIT=ALL;
    EFFECT=YES;
    /WTEST
    /LMTEST
    /END


       39 RECORDS OF INPUT MODEL FILE WERE READ


    DATA IS READ FROM C:\tesis1\base brasiltic.ESS
```

THERE ARE 17 VARIABLES AND 170 CASES
IT IS A RAW DATA ESS FILE

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SAMPLE STATISTICS BASED ON COMPLETE CASES

UNIVARIATE STATISTICS
---------------------

| VARIABLE | P.1.1 V1 | P.1.2 V2 | P.1.3 V3 | P.1.5 V5 | P.1.6 V6 |
|---|---|---|---|---|---|
| MEAN | 3.6941 | 4.0059 | 3.4235 | 4.8765 | 4.4000 |
| SKEWNESS (G1) | -.1427 | -.3284 | -.0187 | -.8703 | -.5597 |
| KURTOSIS (G2) | -1.6839 | -1.4951 | -1.5302 | -.8141 | -1.3132 |
| STANDARD DEV. | 2.9694 | 2.7873 | 2.7126 | 2.6540 | 2.7914 |

| VARIABLE | P.1.8 V8 | P.1.9 V9 | P.1.10 V10 | P.1.11 V11 | P.1.12 V12 |
|---|---|---|---|---|---|
| MEAN | 2.1353 | 2.3647 | 4.7059 | 3.5059 | 2.3706 |
| SKEWNESS (G1) | .8348 | .6639 | -.7765 | -.0322 | .6738 |
| KURTOSIS (G2) | -.8715 | -1.0669 | -1.1465 | -1.6572 | -1.2320 |
| STANDARD DEV. | 2.5971 | 2.6147 | 2.8939 | 2.9053 | 2.8385 |

| VARIABLE | P.1.16 V16 | P.1.17 V17 |
|---|---|---|
| MEAN | 4.6235 | 4.6176 |
| SKEWNESS (G1) | -.7038 | -.6901 |
| KURTOSIS (G2) | -1.0836 | -1.0056 |
| STANDARD DEV. | 2.7217 | 2.6110 |

MULTIVARIATE KURTOSIS
---------------------

MARDIA'S COEFFICIENT (G2,P) = 35.1918
NORMALIZED ESTIMATE = 12.5160

ELLIPTICAL THEORY KURTOSIS ESTIMATES

```
                      -----------------------------------

   MARDIA-BASED KAPPA =         .2095 MEAN SCALED UNIVARIATE KURTOSIS =
-.4139

   MARDIA-BASED KAPPA IS USED IN COMPUTATION. KAPPA=           .2095


   CASE NUMBERS WITH LARGEST CONTRIBUTION TO NORMALIZED MULTIVARIATE
KURTOSIS:
   -------------------------------------------------------------------
-----

   CASE NUMBER           31           32           81          156
158

   ESTIMATE        292.5144     551.1414     374.9072     505.7532
470.6613


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  COVARIANCE  MATRIX TO BE ANALYZED:  12 VARIABLES (SELECTED FROM  17
VARIABLES)
  BASED ON   170 CASES.
```

| | | P.1.1 V1 | P.1.2 V2 | P.1.3 V3 | P.1.5 V5 | P.1.6 V6 |
|---|---|---|---|---|---|---|
| P.1.1 | V1 | 8.817 | | | | |
| P.1.2 | V2 | 5.617 | 7.769 | | | |
| P.1.3 | V3 | 4.781 | 4.938 | 7.358 | | |
| P.1.5 | V5 | 4.287 | 3.800 | 3.810 | 7.044 | |
| P.1.6 | V6 | 3.147 | 3.353 | 2.978 | 5.417 | 7.792 |
| P.1.8 | V8 | 3.917 | 3.981 | 4.392 | 2.242 | 2.336 |
| P.1.9 | V9 | 1.757 | 2.838 | 1.892 | .957 | 1.717 |
| P.1.10 | V10 | 3.389 | 3.451 | 3.741 | 3.247 | 2.006 |
| P.1.11 | V11 | 3.327 | 3.399 | 3.441 | 3.282 | 3.004 |
| P.1.12 | V12 | 3.558 | 3.838 | 3.611 | 2.863 | 3.040 |
| P.1.16 | V16 | 3.269 | 3.576 | 3.657 | 3.308 | 2.595 |
| P.1.17 | V17 | 2.823 | 3.061 | 3.305 | 3.621 | 2.822 |

| | | P.1.8 V8 | P.1.9 V9 | P.1.10 V10 | P.1.11 V11 | P.1.12 V12 |
|---|---|---|---|---|---|---|
| P.1.8 | V8 | 6.745 | | | | |
| P.1.9 | V9 | 2.134 | 6.837 | | | |
| P.1.10 | V10 | 2.016 | 1.179 | 8.375 | | |
| P.1.11 | V11 | 3.316 | 2.140 | 3.724 | 8.441 | |

```
    P.1.12    V12           3.772        3.704        2.956        3.770
8.057
    P.1.16    V16           2.886        1.706        3.528        3.795
3.566
    P.1.17    V17           2.129        1.904        3.106        3.147
3.048


                        P.1.16     P.1.17
                           V16        V17
    P.1.16   V16         7.408
    P.1.17   V17         3.832      6.817


  BENTLER-WEEKS STRUCTURAL REPRESENTATION:

        NUMBER OF DEPENDENT VARIABLES = 12
            DEPENDENT V'S :     1    2    3    5    6    8    9   10   11
12
            DEPENDENT V'S :    16   17

        NUMBER OF INDEPENDENT VARIABLES = 16
            INDEPENDENT F'S :     1    2    3    4
            INDEPENDENT E'S :     1    2    3    5    6    8    9   10
11   12
            INDEPENDENT E'S :    16   17

        NUMBER OF FREE PARAMETERS =  30
        NUMBER OF FIXED NONZERO PARAMETERS =  16

 *** WARNING MESSAGES ABOVE, IF ANY, REFER TO THE MODEL PROVIDED.
     CALCULATIONS FOR INDEPENDENCE MODEL NOW BEGIN.

 *** WARNING MESSAGES ABOVE, IF ANY, REFER TO INDEPENDENCE MODEL.
     CALCULATIONS FOR USER'S MODEL NOW BEGIN.


  3RD STAGE OF COMPUTATION REQUIRED     84184 WORDS OF MEMORY.
  PROGRAM ALLOCATED 200000000 WORDS

  DETERMINANT OF INPUT MATRIX IS    .10795D+09

  PARAMETER ESTIMATES APPEAR IN ORDER,
  NO SPECIAL PROBLEMS WERE ENCOUNTERED DURING OPTIMIZATION.


  RESIDUAL COVARIANCE MATRIX  (S-SIGMA) :


                        P.1.1      P.1.2      P.1.3      P.1.5      P.1.6
                           V1         V2         V3         V5         V6
    P.1.1    V1          .000
    P.1.2    V2          .386       .000
    P.1.3    V3         -.248      -.147       .000
    P.1.5    V5          .494      -.037       .121       .000
    P.1.6     V6             .135         .307         .049         .000
.000
```

```
    P.1.8     V8           -.193       -.175        .396       -.773        -
.057
    P.1.9      V9             -.455          .601         -.259          -.636
.453
    P.1.10    V10           .164        .190        .605         .030        -
.548
    P.1.11     V11            -.127         -.094          .083          -.165
.268
    P.1.12     V12            -.315         -.078        -.154           .075
.827
    P.1.16    V16          -.290       -.023        .197       -.242        -
.223
    P.1.17     V17            -.412         -.211          .159           .393
.260


                       P.1.8      P.1.9      P.1.10     P.1.11     P.1.12
                          V8         V9         V10        V11        V12
    P.1.8     V8          .000
    P.1.9     V9          .376       .000
    P.1.10    V10        -.546      -.632       .000
    P.1.11    V11         .571       .200       .257       .000
    P.1.12     V12            .695          .000         -.214           .375
.000
    P.1.16     V16            .058         -.292         -.043          -.030
.069
    P.1.17    V17          -.442        .087       -.141       -.331        -
.132


                       P.1.16     P.1.17
                          V16        V17
    P.1.16    V16         .000
    P.1.17    V17         .249       .000


                     AVERAGE  ABSOLUTE   COVARIANCE   RESIDUALS          =
.2281
       AVERAGE  OFF-DIAGONAL  ABSOLUTE   COVARIANCE   RESIDUALS          =
.2696


  STANDARDIZED RESIDUAL MATRIX:


                       P.1.1      P.1.2      P.1.3      P.1.5      P.1.6
                          V1         V2         V3         V5         V6
    P.1.1     V1          .000
    P.1.2     V2          .047       .000
    P.1.3     V3         -.031      -.019       .000
    P.1.5     V5          .063      -.005       .017       .000
    P.1.6      V6             .016          .039          .007           .000
.000
    P.1.8     V8           -.025       -.024        .056       -.112        -
.008
    P.1.9      V9             -.059          .082         -.036          -.092
.062
```

| | | | | | | |
|---|---|---|---|---|---|---|
| P.1.10 | V10 | .019 | .024 | .077 | .004 | -.068 |
| P.1.11 | V11 | -.015 | -.012 | .010 | -.021 | .033 |
| P.1.12 | V12 | -.037 | -.010 | -.020 | .010 | .104 |
| P.1.16 | V16 | -.036 | -.003 | .027 | -.034 | -.029 |
| P.1.17 | V17 | -.053 | -.029 | .022 | .057 | .036 |

| | | P.1.8 V8 | P.1.9 V9 | P.1.10 V10 | P.1.11 V11 | P.1.12 V12 |
|---|---|---|---|---|---|---|
| P.1.8 | V8 | .000 | | | | |
| P.1.9 | V9 | .055 | .000 | | | |
| P.1.10 | V10 | -.073 | -.083 | .000 | | |
| P.1.11 | V11 | .076 | .026 | .031 | .000 | |
| P.1.12 | V12 | .094 | .000 | -.026 | .045 | .000 |
| P.1.16 | V16 | .008 | -.041 | -.005 | -.004 | .009 |
| P.1.17 | V17 | -.065 | .013 | -.019 | -.044 | -.018 |

| | | P.1.16 V16 | P.1.17 V17 |
|---|---|---|---|
| P.1.16 | V16 | .000 | |
| P.1.17 | V17 | .035 | .000 |

AVERAGE ABSOLUTE STANDARDIZED RESIDUALS = .0303

AVERAGE OFF-DIAGONAL ABSOLUTE STANDARDIZED RESIDUALS = .0358



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MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

LARGEST STANDARDIZED RESIDUALS:

| NO. | PARAMETER | ESTIMATE | NO. | PARAMETER | ESTIMATE |
|---|---|---|---|---|---|
| 1 | V8, V5 | -.112 | 11 | V17, V8 | -.065 |
| 2 | V12, V6 | .104 | 12 | V5, V1 | .063 |
| 3 | V12, V8 | .094 | 13 | V9, V6 | .062 |
| 4 | V9, V5 | -.092 | 14 | V9, V1 | -.059 |
| 5 | V10, V9 | -.083 | 15 | V17, V5 | .057 |
| 6 | V9, V2 | .082 | 16 | V8, V3 | .056 |
| 7 | V10, V3 | .077 | 17 | V9, V8 | .055 |
| 8 | V11, V8 | .076 | 18 | V17, V1 | -.053 |
| 9 | V10, V8 | -.073 | 19 | V2, V1 | .047 |
| 10 | V10, V6 | -.068 | 20 | V12, V11 | .045 |

```
  DISTRIBUTION OF STANDARDIZED RESIDUALS


     ----------------------------------------
     !                                      !
   60-                                      -
     !                                      !
     !                                      !
     !                                      !
     !                                       !             RANGE      FREQ
PERCENT
   45-                    *                 -
     !                     *                 !    1   -0.5  -  --         0
.00%
     !                     *                 !    2   -0.4  -  -0.5       0
.00%
     !                     *                 !    3   -0.3  -  -0.4       0
.00%
     !                  *  *                 !    4   -0.2  -  -0.3       0
.00%
   30-                  *  *                 -    5   -0.1  -  -0.2       1
1.28%
     !                  *  *                 !    6    0.0  -  -0.1      32
41.03%
     !                  *  *                 !    7    0.1  -   0.0      44
56.41%
     !                  *  *                 !    8    0.2  -   0.1       1
1.28%
     !                  *  *                 !    9    0.3  -   0.2       0
.00%
   15-                  *  *                 -    A    0.4  -   0.3       0
.00%
     !                  *  *                 !    B    0.5  -   0.4       0
.00%
     !                  *  *                 !    C     ++  -   0.5       0
.00%
     !                  *  *                !   -----------------------
-------
     !                  *  *                 !             TOTAL        78
100.00%
     ----------------------------------------
        1  2  3  4  5  6  7  8  9  A  B  C       EACH "*" REPRESENTS  3
RESIDUALS


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)



  GOODNESS OF FIT SUMMARY FOR METHOD = ML
```

```
  INDEPENDENCE MODEL CHI-SQUARE        =     985.035 ON    66 DEGREES OF
FREEDOM

  INDEPENDENCE AIC =   853.03460   INDEPENDENCE CAIC =   580.07190
         MODEL AIC =   -18.05481          MODEL CAIC =  -216.57314

  CHI-SQUARE =       77.945 BASED ON      48 DEGREES OF FREEDOM
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00404

  THE   NORMAL   THEORY   RLS   CHI-SQUARE   FOR   THIS   ML   SOLUTION   IS
78.245.

  FIT INDICES
  -----------
  BENTLER-BONETT     NORMED FIT INDEX =      .921
  BENTLER-BONETT NON-NORMED FIT INDEX =      .955
  COMPARATIVE FIT INDEX (CFI)         =      .967
  BOLLEN   (IFI) FIT INDEX            =      .968
  MCDONALD (MFI) FIT INDEX            =      .916
  LISREL    GFI  FIT INDEX            =      .928
  LISREL   AGFI  FIT INDEX            =      .884
  ROOT MEAN-SQUARE RESIDUAL (RMR)     =      .310
  STANDARDIZED RMR                    =      .041
  ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .061
  90% CONFIDENCE INTERVAL OF RMSEA  (        .034,        .084)

  RELIABILITY COEFFICIENTS
  ------------------------
  CRONBACH'S ALPHA                    =      .896
  COEFFICIENT ALPHA FOR AN OPTIMAL SHORT SCALE               =      .899
  BASED ON 11 VARIABLES, ALL EXCEPT:
  P.1.9
  RELIABILITY COEFFICIENT RHO         =      .924
  GREATEST LOWER BOUND RELIABILITY                           =      .945
  GLB RELIABILITY FOR AN OPTIMAL SHORT SCALE                 =      .945
  BASED ON ALL VARIABLES
  BENTLER'S DIMENSION-FREE LOWER BOUND RELIABILITY           =      .945
  SHAPIRO'S LOWER BOUND RELIABILITY FOR A WEIGHTED COMPOSITE  =      .951
  WEIGHTS THAT ACHIEVE SHAPIRO'S LOWER BOUND:
  P.1.1     P.1.2     P.1.3     P.1.5     P.1.6     P.1.8
      .345      .343      .335      .381      .330      .277
  P.1.9     P.1.10    P.1.11    P.1.12    P.1.16    P.1.17
      .150      .223      .242      .264      .249      .240



  GOODNESS OF FIT SUMMARY FOR METHOD = ROBUST

  ROBUST INDEPENDENCE MODEL CHI-SQUARE =    1047.906 ON    66 DEGREES OF
FREEDOM

  INDEPENDENCE AIC =   915.90633   INDEPENDENCE CAIC =   642.94363
         MODEL AIC =   -36.99059          MODEL CAIC =  -235.50892

  SATORRA-BENTLER SCALED CHI-SQUARE =      59.0094 ON       48 DEGREES OF
FREEDOM
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .13252

  RESIDUAL-BASED TEST STATISTIC                        =   118.620
```

```
PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00000

YUAN-BENTLER RESIDUAL-BASED TEST STATISTIC         =    69.868
PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .02130

YUAN-BENTLER RESIDUAL-BASED F-STATISTIC     =      1.784
DEGREES OF FREEDOM  =                         48,   122
PROBABILITY VALUE FOR THE F-STATISTIC IS          .00589

FIT INDICES
-----------
BENTLER-BONETT     NORMED FIT INDEX =      .944
BENTLER-BONETT NON-NORMED FIT INDEX =      .985
COMPARATIVE FIT INDEX (CFI)         =      .989
BOLLEN   (IFI) FIT INDEX            =      .989
MCDONALD (MFI) FIT INDEX            =      .968
ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .037
90% CONFIDENCE INTERVAL OF RMSEA  (        .000,        .065)


                       ITERATIVE SUMMARY

                   PARAMETER
ITERATION          ABS CHANGE         ALPHA                FUNCTION
    1               2.595504         1.00000                .92257
    2                .891852          .50000                .64181
    3                .385339         1.00000                .55425
    4                .119479         1.00000                .46422
    5                .058323         1.00000                .46146
    6                .008304         1.00000                .46125
    7                .007802         1.00000                .46122
    8                .001209         1.00000                .46121
    9                .001145         1.00000                .46121
   10                .000171         1.00000                .46121

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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
  (ROBUST STATISTICS IN PARENTHESES)


 P.1.1   =V1  =   1.000 F1    + 1.000 E1



 P.1.2   =V2  =   1.011*F1    + 1.000 E2
                   .093
                 10.875@
```

```
              (    .068)
              ( 14.890@

P.1.3   =V3  =     .972*F1    + 1.000 E3
                   .091
                 10.739@
              (    .070)
              ( 13.981@

P.1.5   =V5  =    1.260*F3    + 1.000 E5
                   .135
                  9.349@
              (    .123)
              ( 10.238@

P.1.6   =V6  =    1.000 F3    + 1.000 E6



P.1.8   =V8  =     .795*F1    + 1.000 E8
                   .088
                  9.023@
              (    .075)
              ( 10.560@

P.1.9   =V9  =    1.000 F4    + 1.000 E9



P.1.10  =V10 =    1.000 F2    + 1.000 E10



P.1.11  =V11 =    1.071*F2    + 1.000 E11
                   .155
                  6.915@
              (    .121)
              (   8.823@

P.1.12  =V12 =    1.751*F4    + 1.000 E12
                   .311
                  5.621@
              (    .277)
              (   6.329@

P.1.16  =V16 =    1.103*F2    + 1.000 E16
                   .149
                  7.398@
              (    .115)
              (   9.576@

P.1.17  =V17 =    1.003*F2    + 1.000 E17
                   .141
```

```
                  7.127@
               (   .127)
               (  7.877@


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES
  ----------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                 V                                F
                ---                              ---
                              I F1  -   F1             5.173*I
                              I                         .916 I
                              I                        5.645@I
                              I                     (   .635)I
                              I                     (  8.146@I
                              I                              I
                              I F2  -   F2             3.236*I
                              I                         .777 I
                              I                        4.166@I
                              I                     (   .693)I
                              I                     (  4.669@I
                              I                              I
                              I F3  -   F3             4.300*I
                              I                         .834 I
                              I                        5.153@I
                              I                     (   .737)I
                              I                     (  5.835@I
                              I                              I
                              I F4  -   F4             2.116*I
                              I                         .616 I
                              I                        3.433@I
                              I                     (   .562)I
                              I                     (  3.763@I
                              I                              I


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES
  ----------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                 E                                D
                ---                              ---
 E1  -P.1.1              3.645*I                                I
                          .484 I                                I
                         7.533@I                                I
                       (   .579)I                               I
```

```
                            (  6.291@I                                I
                                     I                                I
E2  -P.1.2                     2.479*I                                I
                                .371 I                                I
                               6.678@I                                I
                            (   .420)I                                I
                            (  5.899@I                                I
                                     I                                I
E3  -P.1.3                     2.468*I                                I
                                .360 I                                I
                               6.859@I                                I
                            (   .436)I                                I
                            (  5.668@I                                I
                                     I                                I
E5  -P.1.5                      .220*I                                I
                                .555 I                                I
                                .397 I                                I
                            (   .563)I                                I
                            (   .391)I                                I
                                     I                                I
E6  -P.1.6                     3.492*I                                I
                                .516 I                                I
                               6.767@I                                I
                            (   .651)I                                I
                            (  5.360@I                                I
                                     I                                I
E8  -P.1.8                     3.479*I                                I
                                .429 I                                I
                               8.105@I                                I
                            (   .452)I                                I
                            (  7.703@I                                I
                                     I                                I
E9  -P.1.9                     4.721*I                                I
                                .595 I                                I
                               7.932@I                                I
                            (   .554)I                                I
                            (  8.517@I                                I
                                     I                                I
E10 -P.1.10                    5.138*I                                I
                                .631 I                                I
                               8.140@I                                I
                            (   .647)I                                I
                            (  7.937@I                                I
                                     I                                I
E11 -P.1.11                    4.728*I                                I
                                .601 I                                I
                               7.871@I                                I
                            (   .566)I                                I
                            (  8.359@I                                I
                                     I                                I
E12 -P.1.12                    1.572*I                                I
                                .938 I                                I
                               1.677 I                                I
                            (   .939)I                                I
                            (  1.675)I                                I
                                     I                                I
E16 -P.1.16                    3.467*I                                I
                                .479 I                                I
                               7.246@I                                I
```

```
                       (    .505)I                                I
                       (   6.870@I                                I
                                 I                                I
 E17 -P.1.17               3.560*I                                I
                            .466 I                                I
                           7.643@I                                I
                       (    .612)I                                I
                       (   5.814@I                                I
                                 I                                I


28-Apr-17      PAGE :  9  EQS     Licensee:
  TITLE:    master confirmatorio tic

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  COVARIANCES AMONG INDEPENDENT VARIABLES
  ---------------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                V                                F
               ---                              ---
                                 I F2  -   F2            3.225*I
                                 I F1  -   F1             .590 I
                                 I                       5.465@I
                                 I                   (    .508)I
                                 I                   (   6.352@I
                                 I                             I
                                 I F3  -   F3            3.012*I
                                 I F1  -   F1             .585 I
                                 I                       5.152@I
                                 I                   (    .515)I
                                 I                   (   5.845@I
                                 I                             I
                                 I F4  -   F4            2.212*I
                                 I F1  -   F1             .515 I
                                 I                       4.296@I
                                 I                   (    .451)I
                                 I                   (   4.899@I
                                 I                             I
                                 I F3  -   F3            2.554*I
                                 I F2  -   F2             .528 I
                                 I                       4.836@I
                                 I                   (    .499)I
                                 I                   (   5.118@I
                                 I                             I
                                 I F4  -   F4            1.811*I
                                 I F2  -   F2             .446 I
                                 I                       4.063@I
                                 I                   (    .383)I
                                 I                   (   4.722@I
                                 I                             I
                                 I F4  -   F4            1.264*I
                                 I F3  -   F3             .368 I
                                 I                       3.438@I
                                 I                   (    .349)I
                                 I                   (   3.620@I
                                 I                             I
```

MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

DECOMPOSITION OF EFFECTS WITH NONSTANDARDIZED VALUES
STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

PARAMETER TOTAL EFFECTS
-----------------------

```
P.1.1   =V1  =   1.000 F1    + 1.000 E1

P.1.2   =V2  =   1.011*F1    + 1.000 E2

P.1.3   =V3  =    .972*F1    + 1.000 E3

P.1.5   =V5  =   1.260*F3    + 1.000 E5

P.1.6   =V6  =   1.000 F3    + 1.000 E6

P.1.8   =V8  =    .795*F1    + 1.000 E8

P.1.9   =V9  =   1.000 F4    + 1.000 E9

P.1.10  =V10 =   1.000 F2    + 1.000 E10
```

```
 P.1.11  =V11 =   1.071*F2    + 1.000 E11


 P.1.12  =V12 =   1.751*F4    + 1.000 E12


 P.1.16  =V16 =   1.103*F2    + 1.000 E16


 P.1.17  =V17 =   1.003*F2    + 1.000 E17



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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  DECOMPOSITION OF EFFECTS WITH STANDARDIZED VALUES

  PARAMETER TOTAL EFFECTS
  -----------------------

 P.1.1   =V1  =    .766 F1    +  .643 E1

 P.1.2   =V2  =    .825*F1    +  .565 E2

 P.1.3   =V3  =    .815*F1    +  .579 E3

 P.1.5   =V5  =    .984*F3    +  .177 E5

 P.1.6   =V6  =    .743 F3    +  .669 E6

 P.1.8   =V8  =    .696*F1    +  .718 E8

 P.1.9   =V9  =    .556 F4    +  .831 E9

 P.1.10  =V10 =    .622 F2    +  .783 E10

 P.1.11  =V11 =    .663*F2    +  .748 E11

 P.1.12  =V12 =    .897*F4    +  .442 E12
```

```
 P.1.16  =V16 =    .729*F2    +  .684 E16

 P.1.17  =V17 =    .691*F2    +  .723 E17
```

```
28-Apr-17      PAGE : 12  EQS     Licensee:
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  STANDARDIZED SOLUTION:                                            R-
SQUARED



 P.1.1         =V1      =         .766   F1            +   .643   E1
.587
 P.1.2         =V2      =         .825*F1              +   .565   E2
.681
 P.1.3         =V3      =         .815*F1              +   .579   E3
.665
 P.1.5         =V5      =         .984*F3              +   .177   E5
.969
 P.1.6         =V6      =         .743   F3            +   .669   E6
.552
 P.1.8         =V8      =         .696*F1              +   .718   E8
.484
 P.1.9         =V9      =         .556   F4            +   .831   E9
.310
 P.1.10      =V10    =         .622    F2            +   .783    E10
.386
 P.1.11      =V11    =         .663*F2               +   .748    E11
.440
 P.1.12      =V12    =         .897*F4               +   .442    E12
.805
 P.1.16      =V16    =         .729*F2               +   .684    E16
.532
 P.1.17      =V17    =         .691*F2               +   .723    E17
.478
```

```
28-Apr-17      PAGE : 13  EQS     Licensee:
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  CORRELATIONS AMONG INDEPENDENT VARIABLES
  ---------------------------------------

                 V                                F
                ---                              ---
                             I F2  -   F2               .788*I
                             I F1  -   F1                    I
                             I                               I
                             I F3  -   F3               .639*I
                             I F1  -   F1                    I
                             I                               I
```

```
I F4  -   F4              .669*I
I F1  -   F1                   I
I                              I
I F3  -   F3              .685*I
I F2  -   F2                   I
I                              I
I F4  -   F4              .692*I
I F2  -   F2                   I
I                              I
I F4  -   F4              .419*I
I F3  -   F3                   I
I                              I
```

```
 ------------------------------------------------------------------------
-------
                           E N D    O F    M E T H O D
 ------------------------------------------------------------------------
-------


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  WALD TEST (FOR DROPPING PARAMETERS)
  ROBUST INFORMATION MATRIX USED IN THIS WALD TEST
  MULTIVARIATE WALD TEST BY SIMULTANEOUS PROCESS


         CUMULATIVE  MULTIVARIATE  STATISTICS                  UNIVARIATE
INCREMENT
         ----------------------------------            ----------------
----

  STEP   PARAMETER    CHI-SQUARE   D.F.   PROBABILITY          CHI-SQUARE
PROBABILITY
  ---- -----------  ----------  ----  -----------       ----------  -----
------

    1      E5,E5           .153       1         .696                 .153
.696
    2     E12,E12         2.805       2         .246                2.652
.103
```

TITLE: master confirmatorio tic

MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

LAGRANGE MULTIPLIER TEST (FOR ADDING PARAMETERS)

ORDERED UNIVARIATE TEST STATISTICS:

| NO | CODE | PARAMETER | CHI-SQUARE | PROB. | HANCOCK 48 DF PROB. | PARAMETER CHANGE | STANDARDIZED CHANGE |
|---|---|---|---|---|---|---|---|
| -- | ------ | --------- | ------ | ----- | -------- | --------- | -------- |
| 1 | 2 12 | V8,F3 | 8.421 | .004 | 1.000 | -.308 | -.057 |
| 2 | 2 12 | V5,F4 | 6.482 | .011 | 1.000 | -.495 | -.128 |
| 3 | 2 12 | V6,F4 | 6.482 | .011 | 1.000 | .393 | .097 |
| 4 | 2 12 | V8,F4 | 6.030 | .014 | 1.000 | .440 | .116 |
| 5 | 2 12 | V1,F3 | 3.648 | .056 | 1.000 | .219 | .036 |
| 6 | 2 12 | V17,F3 | 3.235 | .072 | 1.000 | .235 | .043 |
| 7 | 2 12 | V9,F3 | 3.106 | .078 | 1.000 | -.195 | -.036 |
| 8 | 2 12 | V12,F3 | 3.106 | .078 | 1.000 | .341 | .058 |
| 9 | 2 12 | V9,F2 | 2.956 | .086 | 1.000 | -.646 | -.137 |
| 10 | 2 12 | V12,F2 | 2.956 | .086 | 1.000 | 1.132 | .222 |
| 11 | 2 12 | V3,F2 | 2.396 | .122 | 1.000 | .312 | .064 |
| 12 | 2 12 | V1,F4 | 2.188 | .139 | 1.000 | -.287 | -.066 |
| 13 | 2 12 | V5,F1 | 2.170 | .141 | 1.000 | -.380 | -.063 |
| 14 | 2 12 | V6,F1 | 2.170 | .141 | 1.000 | .302 | .048 |
| 15 | 2 12 | V11,F4 | 1.682 | .195 | 1.000 | .306 | .073 |
| 16 | 2 12 | V5,F2 | 1.546 | .214 | 1.000 | -.583 | -.122 |
| 17 | 2 12 | V6,F2 | 1.546 | .214 | 1.000 | .463 | .092 |
| 18 | 2 12 | V16,F3 | 1.459 | .227 | 1.000 | -.164 | -.029 |
| 19 | 2 12 | V17,F1 | .957 | .328 | 1.000 | -.176 | -.030 |
| 20 | 2 12 | V10,F4 | .725 | .394 | 1.000 | -.203 | -.048 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 21 | 2 | 12 | V1,F2 | .606 | .436 | 1.000 | -.174 | -.033 |
| 22 | 2 | 12 | V10,F1 | .557 | .456 | 1.000 | .148 | .023 |
| 23 | 2 | 12 | V3,F4 | .493 | .483 | 1.000 | -.120 | -.031 |
| 24 | 2 | 12 | V3,F3 | .429 | .513 | 1.000 | .067 | .012 |
| 25 | 2 | 12 | V17,F4 | .368 | .544 | 1.000 | -.128 | -.034 |
| 26 | 2 | 12 | V8,F2 | .367 | .545 | 1.000 | -.123 | -.026 |
| 27 | 2 | 12 | V11,F3 | .328 | .567 | 1.000 | -.083 | -.014 |
| 28 | 2 | 12 | V11,F1 | .184 | .668 | 1.000 | .086 | .013 |
| 29 | 2 | 12 | V2,F2 | .109 | .741 | 1.000 | -.068 | -.014 |
| 30 | 2 | 12 | V2,F4 | .015 | .902 | 1.000 | .022 | .005 |
| 31 | 2 | 12 | V2,F3 | .014 | .906 | 1.000 | -.012 | -.002 |
| 32 | 2 | 12 | V16,F4 | .013 | .908 | 1.000 | .025 | .006 |
| 33 | 2 | 12 | V16,F1 | .011 | .918 | 1.000 | -.019 | -.003 |
| 34 | 2 | 12 | V10,F3 | .001 | .979 | 1.000 | .004 | .001 |
| 35 | 2 | 12 | V9,F1 | .000 | .995 | 1.000 | -.002 | .000 |
| 36 | 2 | 12 | V12,F1 | .000 | .995 | 1.000 | .003 | .000 |
| 37 | 2 | 0 | V6,F3 | .000 | 1.000 | 1.000 | .000 | .000 |
| 38 | 2 | 0 | V9,F4 | .000 | 1.000 | 1.000 | .000 | .000 |
| 39 | 2 | 0 | V10,F2 | .000 | 1.000 | 1.000 | .000 | .000 |
| 40 | 2 | 0 | V1,F1 | .000 | 1.000 | 1.000 | .000 | .000 |

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MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

MULTIVARIATE LAGRANGE MULTIPLIER TEST BY SIMULTANEOUS PROCESS IN STAGE 1

PARAMETER SETS (SUBMATRICES) ACTIVE AT THIS STAGE ARE:

PVV PFV PFF PDD GVV GVF GFV GFF BVF BFF

CUMULATIVE MULTIVARIATE STATISTICS UNIVARIATE INCREMENT

```
        ---------------------------------      ------------------------
-----

HANCOCK'S

SEQUENTIAL
 STEP   PARAMETER   CHI-SQUARE  D.F.   PROB.   CHI-SQUARE   PROB.  D.F.
PROB.
 ----  -----------  ----------  ----   -----   ----------   -----  ----
-----
    1       V8,F3        8.421     1    .004        8.421    .004    48
1.000
    2       V5,F4       14.903     2    .001        6.482    .011    47
1.000
    3       V8,F4       19.136     3    .000        4.232    .040    46
1.000


  LAGRANGIAN MULTIPLIER TEST REQUIRED    19635 WORDS OF MEMORY.
  PROGRAM ALLOCATES ******** WORDS.
1
  Execution begins at 14:13:24
  Execution ends   at 14:13:24
  Elapsed time =        .00 seconds
```

# ANEXO VI

# ANÁLISIS FACTORIAL CONFIRMATORIO

# USO TIC – SEGUNDO ORDEN

```
     1
       EQS,  A  STRUCTURAL  EQUATION  PROGRAM                MULTIVARIATE
SOFTWARE, INC.
       COPYRIGHT BY P.M. BENTLER                          VERSION 6.1 (C) 1985
- 2005 (B85).

         PROGRAM CONTROL INFORMATION

/TITLE
 master confirmatorio tic segundo orden dos factores
/SPECIFICATIONS
VARIABLES= 17 ; CASES= 170 ;
DATAFILE='C:\tesis1\base brasiltic.ESS';
 MATRIX=RAW;METHOD=ML,robust;
/LABELS
V1=P.1.1; V2=P.1.2; V3=P.1.3; V4=P.1.4; V5=P.1.5; V6=P.1.6; V7=P.1.7;
V8=P.1.8; V9=P.1.9; V10=P.1.10; V11=P.1.11; V12=P.1.12;
V13=P.1.13; V14=P.1.14; V15=P.1.15; V16=P.1.16;
V17=P.1.17;
/EQUATIONS
V1=F1+ E1;
V8=*F1+E8;
V2=*F1+E2;
V3=*F1+E3;
V10=F2+E10;
V16=*F2+E16;
V17=*F2+E17;
V11=*F2+E11;
V6=F3+E6;
V5=*F3+E5;
V9=F4+E9;
V12=*F4+E12;
F1=*F5+D1;
F2=*F5+D2;
F3=*F5+D3;
/VARIANCES
E1 TO E3=*; E5 TO E6=*;
E8 TO E12=*;
E16 TO E17=*;
D1 TO D3=*;
F5=1;
F4=*;
/COVARIANCES
F4 TO F5=*;
/TECHNICAL
ITR=100
/PRINT
FIT=ALL;
EFFECT=YES;
/WTEST
/LMTEST
/END
```

```
            44 RECORDS OF INPUT MODEL FILE WERE READ

         DATA IS READ FROM C:\tesis1\base brasiltic.ESS
         THERE ARE  17 VARIABLES AND   170 CASES
         IT IS A RAW DATA ESS FILE

     28-Apr-17      PAGE :  2  EQS     Licensee:
       TITLE:   master confirmatorio tic segundo orden dos factores

       SAMPLE STATISTICS BASED ON COMPLETE CASES

                                   UNIVARIATE STATISTICS
                                   ---------------------

        VARIABLE            P.1.1        P.1.2        P.1.3        P.1.5
P.1.6
                            V1            V2            V3            V5
V6

        MEAN                  3.6941       4.0059       3.4235       4.8765
4.4000

        SKEWNESS (G1)       -.1427      -.3284      -.0187      -.8703     -
.5597

        KURTOSIS (G2)      -1.6839    -1.4951    -1.5302      -.8141    -
1.3132

        STANDARD DEV.        2.9694       2.7873       2.7126       2.6540
2.7914

        VARIABLE            P.1.8        P.1.9        P.1.10       P.1.11
P.1.12
                            V8            V9            V10           V11
V12

        MEAN                  2.1353       2.3647       4.7059       3.5059
2.3706

        SKEWNESS  (G1)          .8348          .6639        -.7765         -
.0322      .6738

        KURTOSIS (G2)       -.8715     -1.0669     -1.1465     -1.6572     -
1.2320

        STANDARD DEV.        2.5971       2.6147       2.8939       2.9053
2.8385

        VARIABLE          P.1.16     P.1.17
                             V16        V17
```

```
MEAN                 4.6235     4.6176

SKEWNESS (G1)        -.7038     -.6901

KURTOSIS (G2)       -1.0836    -1.0056

STANDARD DEV.        2.7217     2.6110
```

MULTIVARIATE KURTOSIS
---------------------

MARDIA'S COEFFICIENT (G2,P) = 35.1918
NORMALIZED ESTIMATE = 12.5160

ELLIPTICAL THEORY KURTOSIS ESTIMATES
------------------------------------

MARDIA-BASED KAPPA = .2095 MEAN SCALED UNIVARIATE KURTOSIS = -.4139

MARDIA-BASED KAPPA IS USED IN COMPUTATION. KAPPA= .2095

CASE NUMBERS WITH LARGEST CONTRIBUTION TO NORMALIZED MULTIVARIATE KURTOSIS:
---------------------------------------------------------------------------

| | | | | | |
|---|---|---|---|---|---|
| CASE NUMBER | 31 | 32 | 81 | 156 | 158 |
| ESTIMATE | 292.5144 | 551.1414 | 374.9072 | 505.7532 | 470.6613 |

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COVARIANCE MATRIX TO BE ANALYZED: 12 VARIABLES (SELECTED FROM 17 VARIABLES)
BASED ON 170 CASES.

| | | P.1.1 | P.1.2 | P.1.3 | P.1.5 | P.1.6 |
|---|---|---|---|---|---|---|
| | | V1 | V2 | V3 | V5 | V6 |
| P.1.1 | V1 | 8.817 | | | | |
| P.1.2 | V2 | 5.617 | 7.769 | | | |
| P.1.3 | V3 | 4.781 | 4.938 | 7.358 | | |
| P.1.5 | V5 | 4.287 | 3.800 | 3.810 | 7.044 | |
| P.1.6 | V6 | 3.147 | 3.353 | 2.978 | 5.417 | 7.792 |

```
          P.1.8     V8           3.917       3.981       4.392       2.242
2.336
          P.1.9     V9           1.757       2.838       1.892        .957
1.717
          P.1.10    V10          3.389       3.451       3.741       3.247
2.006
          P.1.11    V11          3.327       3.399       3.441       3.282
3.004
          P.1.12    V12          3.558       3.838       3.611       2.863
3.040
          P.1.16    V16          3.269       3.576       3.657       3.308
2.595
          P.1.17    V17          2.823       3.061       3.305       3.621
2.822


                            P.1.8        P.1.9        P.1.10       P.1.11
P.1.12
                              V8           V9           V10          V11
V12
          P.1.8    V8          6.745
          P.1.9    V9          2.134      6.837
          P.1.10   V10         2.016      1.179      8.375
          P.1.11   V11         3.316      2.140      3.724      8.441
          P.1.12    V12          3.772       3.704       2.956       3.770
8.057
          P.1.16    V16          2.886       1.706       3.528       3.795
3.566
          P.1.17    V17          2.129       1.904       3.106       3.147
3.048


                            P.1.16     P.1.17
                              V16        V17
          P.1.16   V16         7.408
          P.1.17   V17         3.832      6.817


       BENTLER-WEEKS STRUCTURAL REPRESENTATION:

             NUMBER OF DEPENDENT VARIABLES = 15
                 DEPENDENT V'S :      1     2     3     5     6     8     9
10   11   12
                 DEPENDENT V'S :    16   17
                 DEPENDENT F'S :     1    2    3

             NUMBER OF INDEPENDENT VARIABLES = 17
                 INDEPENDENT F'S :     4    5
                 INDEPENDENT E'S :     1     2     3     5     6     8     9
10   11   12
                 INDEPENDENT E'S :    16   17
                 INDEPENDENT D'S :     1    2    3

             NUMBER OF FREE PARAMETERS =  28
             NUMBER OF FIXED NONZERO PARAMETERS =  20

      *** WARNING MESSAGES ABOVE, IF ANY, REFER TO THE MODEL PROVIDED.
          CALCULATIONS FOR INDEPENDENCE MODEL NOW BEGIN.
```

```
*** WARNING MESSAGES ABOVE, IF ANY, REFER TO INDEPENDENCE MODEL.
    CALCULATIONS FOR USER'S MODEL NOW BEGIN.


 3RD STAGE OF COMPUTATION REQUIRED     84108 WORDS OF MEMORY.
 PROGRAM ALLOCATED 200000000 WORDS

 DETERMINANT OF INPUT MATRIX IS    .10795D+09

IN ITERATION #  2, MATRIX W_CFUNCT MAY NOT BE POSITIVE DEFINITE.

 PARAMETER ESTIMATES APPEAR IN ORDER,
 NO SPECIAL PROBLEMS WERE ENCOUNTERED DURING OPTIMIZATION.



 RESIDUAL COVARIANCE MATRIX  (S-SIGMA) :


                             P.1.1        P.1.2        P.1.3        P.1.5
P.1.6
                                V1           V2           V3           V5
V6
           P.1.1    V1          .000
           P.1.2    V2          .414        .000
           P.1.3    V3         -.253       -.159        .000
           P.1.5    V5          .608        .074        .206        .000
           P.1.6      V6                   .047            .214            -
.059        .000        .000
           P.1.8     V8          -.180       -.168         .378        -.692
-.136
           P.1.9      V9            -.197         .859        -.023          -
.858        .188
           P.1.10    V10          .058         .078         .477         .154
-.600
           P.1.11     V11          -.227        -.200        -.041           -
.018        .223
           P.1.12     V12          -.149         .085        -.020           -
.579        .141
           P.1.16    V16         -.402       -.141         .061        -.100
-.276
           P.1.17         V17                        -.469                 -
.272        .080        .564        .247


                             P.1.8        P.1.9        P.1.10       P.1.11
P.1.12
                                V8           V9           V10          V11
V12
           P.1.8    V8          .000
           P.1.9    V9          .575        .000
           P.1.10   V10        -.640       -.464        .000
           P.1.11   V11         .482        .387        .234        .000
           P.1.12     V12                  .816            .000            -
.160        .445        .000
           P.1.16     V16          -.042        -.104        -.077           -
.051        .133
```

| | | | | | | |
|---|---|---|---|---|---|---|
| P.1.17 | V17 | -.496 | .280 | -.127 | -.302 | -.032 |

| | | P.1.16 V16 | P.1.17 V17 |
|---|---|---|---|
| P.1.16 | V16 | .000 | |
| P.1.17 | V17 | .269 | .000 |

AVERAGE ABSOLUTE COVARIANCE RESIDUALS = .2242
AVERAGE OFF-DIAGONAL ABSOLUTE COVARIANCE RESIDUALS = .2650

STANDARDIZED RESIDUAL MATRIX:

| | | P.1.1 V1 | P.1.2 V2 | P.1.3 V3 | P.1.5 V5 | P.1.6 V6 |
|---|---|---|---|---|---|---|
| P.1.1 | V1 | .000 | | | | |
| P.1.2 | V2 | .050 | .000 | | | |
| P.1.3 | V3 | -.031 | -.021 | .000 | | |
| P.1.5 | V5 | .077 | .010 | .029 | .000 | |
| P.1.6 | V6 | .006 | .028 | -.008 | .000 | .000 |
| P.1.8 | V8 | -.023 | -.023 | .054 | -.100 | -.019 |
| P.1.9 | V9 | -.025 | .118 | -.003 | -.124 | .026 |
| P.1.10 | V10 | .007 | .010 | .061 | .020 | -.074 |
| P.1.11 | V11 | -.026 | -.025 | -.005 | -.002 | .028 |
| P.1.12 | V12 | -.018 | .011 | -.003 | -.077 | .018 |
| P.1.16 | V16 | -.050 | -.019 | .008 | -.014 | -.036 |
| P.1.17 | V17 | -.060 | -.037 | .011 | .081 | .034 |

| | | P.1.8 V8 | P.1.9 V9 | P.1.10 V10 | P.1.11 V11 | P.1.12 V12 |
|---|---|---|---|---|---|---|
| P.1.8 | V8 | .000 | | | | |
| P.1.9 | V9 | .085 | .000 | | | |
| P.1.10 | V10 | -.085 | -.061 | .000 | | |
| P.1.11 | V11 | .064 | .051 | .028 | .000 | |
| P.1.12 | V12 | .111 | .000 | -.020 | .054 | .000 |
| P.1.16 | V16 | -.006 | -.015 | -.010 | -.006 | .017 |

```
          P.1.17    V17          -.073        .041       -.017       -.040
-.004


                                  P.1.16     P.1.17
                                     V16        V17
          P.1.16   V16              .000
          P.1.17   V17              .038       .000


                                AVERAGE    ABSOLUTE    STANDARDIZED    RESIDUALS
=         .0299
                   AVERAGE   OFF-DIAGONAL   ABSOLUTE   STANDARDIZED   RESIDUALS
=         .0354


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       MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


       LARGEST STANDARDIZED RESIDUALS:

           NO.     PARAMETER   ESTIMATE       NO.     PARAMETER   ESTIMATE
           ---     ---------   --------       ---     ---------   --------
            1      V9,   V5       -.124       11      V17,  V8       -.073
            2      V9,   V2        .118       12      V11,  V8        .064
            3      V12,  V8        .111       13      V10,  V9       -.061
            4      V8,   V5       -.100       14      V10,  V3        .061
            5      V10,  V8       -.085       15      V17,  V1       -.060
            6      V9,   V8        .085       16      V12,  V11       .054
            7      V17,  V5        .081       17      V8,   V3        .054
            8      V5,   V1        .077       18      V11,  V9        .051
            9      V12,  V5       -.077       19      V2,   V1        .050
           10      V10,  V6       -.074       20      V16,  V1       -.050


       DISTRIBUTION OF STANDARDIZED RESIDUALS


          ----------------------------------------
          !                                      !
        60-                                      -
          !                                      !
          !                                      !
          !                                      !
          !                                          !             RANGE
FREQ PERCENT
        45-                                      -
          !                  *                     !    1    -0.5   -   --
0    .00%
          !                 *                    !    2    -0.4   -   -0.5
0    .00%
          !                 *                    !    3    -0.3   -   -0.4
0    .00%
```

```
          !                   *  *                 !    4   -0.2  -  -0.3
0    .00%
        30-                   *  *                 -    5   -0.1  -  -0.2
2   2.56%
          !                   *  *                 !    6    0.0  -  -0.1
42  53.85%
          !                   *  *                 !    7    0.1  -   0.0
32  41.03%
          !                   *  *                 !    8    0.2  -   0.1
2   2.56%
          !                   *  *                 !    9    0.3  -   0.2
0    .00%
        15-                   *  *                 -    A    0.4  -   0.3
0    .00%
          !                   *  *                 !    B    0.5  -   0.4
0    .00%
          !                   *  *                 !    C     ++  -   0.5
0    .00%
          !                  *  *                 !    ------------------
-------------
          !                *  *  *  *                 !            TOTAL
78 100.00%
          ----------------------------------------
             1  2  3  4  5  6  7  8  9  A  B  C     EACH "*" REPRESENTS
3 RESIDUALS


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       MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)



       GOODNESS OF FIT SUMMARY FOR METHOD = ML

       INDEPENDENCE MODEL CHI-SQUARE          =      985.035 ON     66
DEGREES OF FREEDOM

       INDEPENDENCE AIC =   853.03460   INDEPENDENCE CAIC =   580.07190
              MODEL AIC =   -15.98415          MODEL CAIC =  -222.77407

       CHI-SQUARE =        84.016 BASED ON      50 DEGREES OF FREEDOM
       PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00184

       THE  NORMAL  THEORY  RLS  CHI-SQUARE  FOR  THIS  ML  SOLUTION  IS
84.203.

       FIT INDICES
       -----------
       BENTLER-BONETT     NORMED FIT INDEX =      .915
       BENTLER-BONETT NON-NORMED FIT INDEX =      .951
       COMPARATIVE FIT INDEX (CFI)         =      .963
       BOLLEN   (IFI) FIT INDEX            =      .964
       MCDONALD (MFI) FIT INDEX            =      .905
       LISREL    GFI  FIT INDEX            =      .923
       LISREL   AGFI  FIT INDEX            =      .880
       ROOT MEAN-SQUARE RESIDUAL (RMR)     =      .318
```

```
       STANDARDIZED RMR                        =      .043
       ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .063
       90% CONFIDENCE INTERVAL OF RMSEA  (        .038,         .086)

       RELIABILITY COEFFICIENTS
       ------------------------
       CRONBACH'S ALPHA                        =      .896
       COEFFICIENT    ALPHA    FOR    AN    OPTIMAL    SHORT    SCALE
=      .899
       BASED ON 11 VARIABLES, ALL EXCEPT:
       P.1.9
       RELIABILITY COEFFICIENT RHO             =      .924
       GREATEST            LOWER            BOUND            RELIABILITY
=      .945
       GLB    RELIABILITY    FOR    AN    OPTIMAL    SHORT    SCALE
=      .945
       BASED ON ALL VARIABLES
       BENTLER'S     DIMENSION-FREE     LOWER     BOUND     RELIABILITY
=      .945
       SHAPIRO'S  LOWER  BOUND  RELIABILITY  FOR  A  WEIGHTED  COMPOSITE
=      .951
       WEIGHTS THAT ACHIEVE SHAPIRO'S LOWER BOUND:
       P.1.1     P.1.2     P.1.3     P.1.5     P.1.6     P.1.8
           .345      .343      .335      .381      .330      .277
       P.1.9     P.1.10    P.1.11    P.1.12    P.1.16    P.1.17
           .150      .223      .242      .264      .249      .240



       GOODNESS OF FIT SUMMARY FOR METHOD = ROBUST

       ROBUST  INDEPENDENCE  MODEL  CHI-SQUARE  =      1047.906  ON      66
DEGREES OF FREEDOM

       INDEPENDENCE AIC =   915.90633   INDEPENDENCE CAIC =   642.94363
              MODEL AIC =   -36.34854          MODEL CAIC =  -243.13847

       SATORRA-BENTLER  SCALED  CHI-SQUARE  =       63.6515  ON        50
DEGREES OF FREEDOM
       PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .09293

       RESIDUAL-BASED TEST STATISTIC                      =   143.182
       PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00000

       YUAN-BENTLER RESIDUAL-BASED TEST STATISTIC         =    77.722
       PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00725

       YUAN-BENTLER RESIDUAL-BASED F-STATISTIC     =      2.033
       DEGREES OF FREEDOM  =                         50,   120
       PROBABILITY VALUE FOR THE F-STATISTIC IS         .00089

       FIT INDICES
       -----------
       BENTLER-BONETT     NORMED FIT INDEX =      .939
       BENTLER-BONETT NON-NORMED FIT INDEX =      .982
       COMPARATIVE FIT INDEX (CFI)         =      .986
       BOLLEN   (IFI) FIT INDEX            =      .986
       MCDONALD (MFI) FIT INDEX            =      .961
```

```
 ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .040
 90% CONFIDENCE INTERVAL OF RMSEA  (        .000,        .067)


                        ITERATIVE SUMMARY

                    PARAMETER
 ITERATION                     ABS  CHANGE                  ALPHA
FUNCTION
     1                           2.173264                  .50000
1.94785
     2                           1.533585                  .50000
1.03516
     3                                                    .666608
1.00000         .87169
     4                                                    .118574
1.00000         .50530
     5                                                    .056969
1.00000         .49755
     6                                                    .017512
1.00000         .49717
     7                                                    .004688
1.00000         .49714
     8                                                    .001535
1.00000         .49714
     9                                                    .000427
1.00000         .49714

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 MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


 MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
 STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
 (ROBUST STATISTICS IN PARENTHESES)


P.1.1   =V1  =   1.000 F1    + 1.000 E1




P.1.2   =V2  =   1.013*F1    + 1.000 E2
                  .094
                10.795@
              (   .070)
              ( 14.479@

P.1.3   =V3  =    .980*F1    + 1.000 E3
                  .091
                10.730@
              (   .070)
              ( 13.924@
```

```
P.1.5   =V5  =   1.187*F3    + 1.000 E5
                  .123
                 9.612@
             (    .108)
             ( 11.041@

P.1.6   =V6  =   1.000 F3    + 1.000 E6



P.1.8   =V8  =    .797*F1    + 1.000 E8
                  .089
                 8.992@
             (    .076)
             ( 10.520@

P.1.9   =V9  =   1.000 F4    + 1.000 E9



P.1.10  =V10 =   1.000 F2    + 1.000 E10



P.1.11  =V11 =   1.067*F2    + 1.000 E11
                  .154
                 6.937@
             (    .122)
             (  8.769@

P.1.12  =V12 =   1.896*F4    + 1.000 E12
                  .370
                 5.120@
             (    .331)
             (  5.727@

P.1.16  =V16 =   1.102*F2    + 1.000 E16
                  .148
                 7.436@
             (    .114)
             (  9.679@

P.1.17  =V17 =    .988*F2    + 1.000 E17
                  .139
                 7.093@
             (    .124)
             (  7.954@
```

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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  CONSTRUCT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
  (ROBUST STATISTICS IN PARENTHESES)



    F1   =F1  =   1.991*F5    + 1.000 D1
                   .209
                  9.502@
              (   .160)
              ( 12.476@

    F2   =F2  =   1.673*F5    + 1.000 D2
                   .215
                  7.789@
              (   .193)
              (  8.680@

    F3   =F3  =   1.557*F5    + 1.000 D3
                   .215
                  7.250@
              (   .191)
              (  8.132@


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES
  ----------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                V                                F
               ---                              ---
                              I F4  -   F4              1.953*I
                              I                          .604 I
                              I                         3.233@I
                              I                      (   .549)I
                              I                      (  3.555@I
                              I                               I
                              I F5  -   F5              1.000 I
                              I                               I
                              I                               I
                              I                               I
                              I                               I
                              I                               I


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 MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

 VARIANCES OF INDEPENDENT VARIABLES
 ----------------------------------
 STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                 E                                 D
                ---                               ---
E1  -P.1.1              3.679*I D1  -   F1              1.176*I
                         .487 I                          .380 I
                        7.548@I                         3.093@I
                     (   .585)I                      (   .460)I
                     (  6.285@I                      (  2.555@I
                              I                               I
E2  -P.1.2              2.500*I D2  -   F2               .470*I
                         .374 I                          .269 I
                        6.690@I                         1.747 I
                     (   .432)I                      (   .305)I
                     (  5.789@I                      (  1.544)I
                              I                               I
E3  -P.1.3              2.426*I D3  -   F3              2.139*I
                         .358 I                          .431 I
                        6.779@I                         4.966@I
                     (   .433)I                      (   .432)I
                     (  5.599@I                      (  4.951@I
                              I                               I
E5  -P.1.5               .615*I                               I
                         .521 I                               I
                        1.179 I                               I
                     (   .552)I                               I
                     (  1.113)I                               I
                              I                               I
E6  -P.1.6              3.228*I                               I
                         .508 I                               I
                        6.354@I                               I
                     (   .627)I                               I
                     (  5.152@I                               I
                              I                               I
E8  -P.1.8              3.477*I                               I
                         .430 I                               I
                        8.096@I                               I
                     (   .451)I                               I
                     (  7.712@I                               I
                              I                               I
E9  -P.1.9              4.883*I                               I
                         .613 I                               I
                        7.961@I                               I
                     (   .554)I                               I
                     (  8.808@I                               I
                              I                               I
E10 -P.1.10             5.104*I                               I
                         .630 I                               I
                        8.102@I                               I
                     (   .647)I                               I
                     (  7.890@I                               I
                              I                               I
E11 -P.1.11             4.717*I                               I
```

```
                          .602 I                             I
                         7.840@I                             I
                      (   .561)I                             I
                      (  8.415@I                             I
                               I                             I
 E12 -P.1.12             1.032*I                             I
                         1.109 I                             I
                          .931 I                             I
                      (  1.100)I                             I
                      (   .938)I                             I
                               I                             I
 E16 -P.1.16             3.435*I                             I
                          .479 I                             I
                         7.178@I                             I
                      (   .498)I                             I
                      (  6.904@I                             I
                               I                             I
 E17 -P.1.17             3.623*I                             I
                          .472 I                             I
                         7.676@I                             I
                      (   .610)I                             I
                      (  5.943@I                             I
                               I                             I
```

```
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  COVARIANCES AMONG INDEPENDENT VARIABLES
  ---------------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                 V                                F
                ---                              ---
                               I F5  -   F5               .982*I
                               I F4  -   F4               .212 I
                               I                         4.638@I
                               I                      (   .195)I
                               I                      (  5.037@I
                               I                               I
```

```
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  DECOMPOSITION OF EFFECTS WITH NONSTANDARDIZED VALUES
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

  PARAMETER TOTAL EFFECTS
  -----------------------

 P.1.1   =V1  =   1.000 F1    + 1.991 F5    + 1.000 E1    + 1.000
D1
                                 .209
                                9.502@
```

```
                                       (    .160)
                                       ( 12.476@


      P.1.2    =V2  =    1.013*F1    + 2.016 F5    + 1.000 E2    + 1.013
D1
                          .094          .196                        .094
                        10.795@       10.289@                     10.795@
                      (   .070)     (   .262)                   (   .070)
                      ( 14.479@     (  7.699@                   ( 14.479@


      P.1.3    =V3  =     .980*F1    + 1.950 F5    + 1.000 E3    +  .980
D1
                          .091          .191                        .091
                        10.730@       10.224@                     10.730@
                      (   .070)     (   .253)                   (   .070)
                      ( 13.924@     (  7.722@                   ( 13.924@


      P.1.5    =V5  =    1.187*F3    + 1.848 F5    + 1.000 E5    + 1.187
D3
                          .123          .192                        .123
                         9.612@        9.631@                      9.612@
                      (   .108)     (   .367)                   (   .108)
                      ( 11.041@     (  5.039@                   ( 11.041@


      P.1.6    =V6  =    1.000 F3    + 1.557 F5    + 1.000 E6    + 1.000
D3
                                        .215
                                       7.250@
                                    (   .191)
                                    (  8.132@


      P.1.8    =V8  =     .797*F1    + 1.587 F5    + 1.000 E8    +  .797
D1
                          .089          .184                        .089
                         8.992@        8.639@                      8.992@
                      (   .076)     (   .226)                   (   .076)
                      ( 10.520@     (  7.013@                   ( 10.520@


      P.1.9   =V9  =   1.000 F4    + 1.000 E9




      P.1.10  =V10 =   1.000 F2    + 1.673 F5    + 1.000 E10   + 1.000
D2
                                        .215
                                       7.789@
                                    (   .193)
                                    (  8.680@
```

```
 P.1.11  =V11 =   1.067*F2    + 1.785 F5    + 1.000 E11   + 1.067
D2
                   .154          .214                         .154
                  6.937@        8.329@                       6.937@
               (   .122)     (   .369)                    (   .122)
               (  8.769@     (  4.843@                    (  8.769@


 P.1.12  =V12 =   1.896*F4    + 1.000 E12




 P.1.16  =V16 =   1.102*F2    + 1.844 F5    + 1.000 E16   + 1.102
D2
                   .148          .198                         .148
                  7.436@        9.312@                       7.436@
               (   .114)     (   .368)                    (   .114)
               (  9.679@     (  5.005@                    (  9.679@


 P.1.17  =V17 =    .988*F2    + 1.654 F5    + 1.000 E17   +  .988
D2
                   .139          .192                         .139
                  7.093@        8.616@                       7.093@
               (   .124)     (   .358)                    (   .124)
               (  7.954@     (  4.621@                    (  7.954@


    F1   =F1  =   1.991*F5    + 1.000 D1




    F2   =F2  =   1.673*F5    + 1.000 D2




    F3   =F3  =   1.557*F5    + 1.000 D3
```



```
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  DECOMPOSITION OF EFFECTS WITH NONSTANDARDIZED VALUES
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

  PARAMETER INDIRECT EFFECTS
```

```
 --------------------------

P.1.1   =V1  =   1.991 F5    + 1.000 D1
                  .209
                 9.502@
              (   .160)
              ( 12.476@

P.1.2   =V2  =   2.016 F5    + 1.013 D1
                  .196          .094
                10.289@       10.795@
              (   .262)     (   .070)
              (  7.699@     ( 14.479@

P.1.3   =V3  =   1.950 F5    +  .980 D1
                  .191          .091
                10.224@       10.730@
              (   .253)     (   .070)
              (  7.722@     ( 13.924@

P.1.5   =V5  =   1.848 F5    + 1.187 D3
                  .192          .123
                 9.631@        9.612@
              (   .367)     (   .108)
              (  5.039@     ( 11.041@

P.1.6   =V6  =   1.557 F5    + 1.000 D3
                  .215
                 7.250@
              (   .191)
              (  8.132@

P.1.8   =V8  =   1.587 F5    +  .797 D1
                  .184          .089
                 8.639@        8.992@
              (   .226)     (   .076)
              (  7.013@     ( 10.520@

P.1.10  =V10 =   1.673 F5    + 1.000 D2
                  .215
                 7.789@
              (   .193)
              (  8.680@

P.1.11  =V11 =   1.785 F5    + 1.067 D2
                  .214          .154
                 8.329@        6.937@
              (   .369)     (   .122)
              (  4.843@     (  8.769@

P.1.16  =V16 =   1.844 F5    + 1.102 D2
                  .198          .148
                 9.312@        7.436@
              (   .368)     (   .114)
              (  5.005@     (  9.679@

P.1.17  =V17 =   1.654 F5    +  .988 D2
                  .192          .139
```

```
                 8.616@        7.093@
              (   .358)     (   .124)
              (  4.621@     (  7.954@
```

```
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  DECOMPOSITION OF EFFECTS WITH STANDARDIZED VALUES

  PARAMETER TOTAL EFFECTS
  -----------------------

 P.1.1   =V1  =    .763 F1    +  .670 F5    +  .646 E1    +  .365
D1

 P.1.2   =V2  =    .824*F1    +  .723 F5    +  .567 E2    +  .394
D1

 P.1.3   =V3  =    .819*F1    +  .719 F5    +  .574 E3    +  .392
D1

 P.1.5   =V5  =    .955*F3    +  .696 F5    +  .295 E5    +  .654
D3

 P.1.6   =V6  =    .765 F3    +  .558 F5    +  .644 E6    +  .524
D3

 P.1.8   =V8  =    .696*F1    +  .611 F5    +  .718 E8    +  .333
D1

 P.1.9   =V9  =    .535 F4    +  .845 E9

 P.1.10  =V10 =    .625 F2    +  .578 F5    +  .781 E10   +  .237
D2

 P.1.11  =V11 =    .664*F2    +  .615 F5    +  .748 E11   +  .252
D2

 P.1.12  =V12 =    .934*F4    +  .358 E12

 P.1.16  =V16 =    .732*F2    +  .678 F5    +  .681 E16   +  .278
D2

 P.1.17  =V17 =    .685*F2    +  .633 F5    +  .729 E17   +  .260
D2

    F1   =F1  =    .878*F5    +  .478 D1

    F2   =F2  =    .925*F5    +  .379 D2

    F3   =F3  =    .729*F5    +  .685 D3
```

```
28-Apr-17       PAGE : 14   EQS      Licensee:
 TITLE:   master confirmatorio tic segundo orden dos factores

 MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

 DECOMPOSITION OF EFFECTS WITH STANDARDIZED VALUES

 PARAMETER INDIRECT EFFECTS
 --------------------------

P.1.1   =V1  =    .670 F5    +  .365 D1

P.1.2   =V2  =    .723 F5    +  .394 D1

P.1.3   =V3  =    .719 F5    +  .392 D1

P.1.5   =V5  =    .696 F5    +  .654 D3

P.1.6   =V6  =    .558 F5    +  .524 D3

P.1.8   =V8  =    .611 F5    +  .333 D1

P.1.10  =V10 =    .578 F5    +  .237 D2

P.1.11  =V11 =    .615 F5    +  .252 D2

P.1.16  =V16 =    .678 F5    +  .278 D2

P.1.17  =V17 =    .633 F5    +  .260 D2


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 MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


 STANDARDIZED                                      SOLUTION:
R-SQUARED


       P.1.1          =V1       =          .763   F1            +   .646
E1                                      .583
       P.1.2           =V2       =          .824*F1            +   .567
E2                                      .678
       P.1.3           =V3       =          .819*F1            +   .574
E3                                      .670
       P.1.5           =V5       =          .955*F3            +   .295
E5                                      .913
       P.1.6          =V6       =          .765   F3            +   .644
E6                                      .586
       P.1.8           =V8       =          .696*F1            +   .718
E8                                      .484
       P.1.9          =V9       =          .535   F4            +   .845
E9                                      .286
```

```
      P.1.10        =V10    =          .625    F2              +    .781
E10                                   .391
      P.1.11        =V11    =            .664*F2              +    .748
E11                                   .441
      P.1.12        =V12    =            .934*F4              +    .358
E12                                   .872
      P.1.16        =V16    =            .732*F2              +    .681
E16                                   .536
      P.1.17        =V17    =            .685*F2              +    .729
E17                                   .469
         F1            =F1       =          .878*F5              +    .478
D1                                    .771
         F2            =F2       =          .925*F5              +    .379
D2                                    .856
         F3            =F3       =          .729*F5              +    .685
D3                                    .531
```

```
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       MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

       CORRELATIONS AMONG INDEPENDENT VARIABLES
       ---------------------------------------

                       V                                 F
                      ---                               ---
                                I F5  -   F5                 .703*I
                                I F4  -   F4                      I
                                I                                 I
```

```
      ------------------------------------------------------------------
-------------
                                E N D    O F    M E T H O D
      ------------------------------------------------------------------
-------------
```

```
     28-Apr-17      PAGE : 17  EQS     Licensee:
       TITLE:   master confirmatorio tic segundo orden dos factores

       MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


       WALD TEST (FOR DROPPING PARAMETERS)
       ROBUST INFORMATION MATRIX USED IN THIS WALD TEST
       MULTIVARIATE WALD TEST BY SIMULTANEOUS PROCESS
```

```
              CUMULATIVE MULTIVARIATE STATISTICS              UNIVARIATE
INCREMENT
              ---------------------------------              ----------
----------

       STEP  PARAMETER   CHI-SQUARE  D.F.  PROBABILITY       CHI-SQUARE
PROBABILITY
       ---- -----------  ----------  ----  -----------       ----------
-----------

         1               E12,E12                                    .881
1       .348            .881        .348
         2                  E5,E5                                  1.748
2       .417            .867        .352
         3         D2,D2              4.275          3              .233
2.527        .112


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       TITLE:   master confirmatorio tic segundo orden dos factores

       MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


       LAGRANGE MULTIPLIER TEST (FOR ADDING PARAMETERS)


       ORDERED UNIVARIATE TEST STATISTICS:
                                                            HANCOCK
STANDAR-
                                            CHI-                          50  DF
PARAMETER   DIZED
        NO      CODE       PARAMETER        SQUARE        PROB.       PROB.
CHANGE    CHANGE
        --    ------    ---------      ------     -----   -------- -------
--  --------
         1    2  12         V5,F4      10.689      .001      1.000      -
.523     -.141
         2    2  20         V8,F3       6.276      .012      1.000      -
.267     -.048
         3       2   12             V8,F4           5.900            .015
1.000      .395      .109
         4    2  22         F2,F1       4.928      .026      1.000      -
.717     -.175
         5    2  22         F1,F2       4.928      .026      1.000      -
1.793     -.437
         6    2  10         D2,D1       4.928      .026      1.000      -
.844    -1.134
         7    2  16         F3,F4       4.928      .026      1.000      -
.391     -.131
         8       2   12             V6,F4           4.456            .035
1.000      .382      .098
         9       2   20            V17,F3           4.306            .038
1.000      .260      .047
        10       2   20             V5,F2           3.719            .054
1.000      .897      .187
        11       2   20             V1,F3           3.344            .067
1.000      .210      .033
```

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 12 | 2 | 20 | V9,F3 | 3.240 | .072 | 1.000 | -.259 | -.046 |
| 13 | 2 | 20 | V9,F1 | 2.150 | .143 | 1.000 | .396 | .067 |
| 14 | 2 | 20 | V6,F2 | 1.889 | .169 | 1.000 | -.666 | -.132 |
| 15 | 2 | 12 | V11,F4 | 1.861 | .173 | 1.000 | .288 | .071 |
| 16 | 2 | 20 | V3,F2 | 1.846 | .174 | 1.000 | .298 | .061 |
| 17 | 2 | 22 | F2,F3 | 1.469 | .225 | 1.000 | .155 | .040 |
| 18 | 2 | 10 | D3,D2 | 1.469 | .225 | 1.000 | .331 | .330 |
| 19 | 2 | 16 | F1,F4 | 1.469 | .225 | 1.000 | .251 | .079 |
| 20 | 2 | 22 | F3,F2 | 1.469 | .225 | 1.000 | .704 | .182 |
| 21 | 2 | 20 | V17,F1 | 1.454 | .228 | 1.000 | -.238 | -.040 |
| 22 | 2 | 20 | V12,F3 | 1.191 | .275 | 1.000 | -.153 | -.025 |
| 23 | 2 | 12 | V3,F5 | 1.162 | .281 | 1.000 | .608 | .224 |
| 24 | 2 | 20 | V1,F2 | 1.017 | .313 | 1.000 | -.246 | -.046 |
| 25 | 2 | 12 | V1,F4 | .789 | .375 | 1.000 | -.155 | -.037 |
| 26 | 2 | 22 | F1,F3 | .684 | .408 | 1.000 | .126 | .026 |
| 27 | 2 | 16 | F2,F4 | .684 | .408 | 1.000 | .144 | .057 |
| 28 | 2 | 10 | D3,D1 | .684 | .408 | 1.000 | .269 | .169 |
| 29 | 2 | 22 | F3,F1 | .684 | .408 | 1.000 | .228 | .047 |
| 30 | 2 | 12 | V16,F5 | .640 | .424 | 1.000 | -.987 | -.363 |
| 31 | 2 | 20 | V16,F3 | .608 | .435 | 1.000 | -.100 | -.017 |
| 32 | 2 | 20 | V12,F2 | .537 | .463 | 1.000 | .446 | .087 |
| 33 | 2 | 20 | V5,F1 | .520 | .471 | 1.000 | .159 | .026 |
| 34 | 2 | 12 | V10,F4 | .462 | .497 | 1.000 | -.146 | -.036 |
| 35 | 2 | 12 | V11,F5 | .437 | .508 | 1.000 | .823 | .283 |
| 36 | 2 | 20 | V3,F3 | .424 | .515 | 1.000 | .065 | .011 |
| 37 | 2 | 20 | V8,F2 | .418 | .518 | 1.000 | -.143 | -.030 |
| 38 | 2 | 20 | V16,F1 | .394 | .530 | 1.000 | -.131 | -.021 |
| 39 | 2 | 12 | V8,F5 | .327 | .568 | 1.000 | -.319 | -.123 |
| 40 | 2 | 20 | V2,F2 | .270 | .603 | 1.000 | -.117 | -.023 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 41 | 2 | 20 | V10,F1 | .219 | .640 | 1.000 | .102 | .016 |
| 42 | 2 | 12 | V3,F4 | .205 | .650 | 1.000 | -.069 | -.018 |
| 43 | 2 | 12 | V1,F5 | .166 | .684 | 1.000 | -.252 | -.085 |
| 44 | 2 | 12 | V2,F4 | .088 | .766 | 1.000 | .046 | .012 |
| 45 | 2 | 12 | V16,F4 | .080 | .777 | 1.000 | .054 | .014 |
| 46 | 2 | 20 | V12,F1 | .054 | .816 | 1.000 | .067 | .010 |
| 47 | 2 | 12 | V2,F5 | .052 | .820 | 1.000 | -.132 | -.047 |
| 48 | 2 | 20 | V6,F1 | .041 | .840 | 1.000 | -.047 | -.007 |
| 49 | 2 | 20 | V2,F3 | .039 | .843 | 1.000 | .020 | .003 |
| 50 | 2 | 12 | V17,F4 | .013 | .911 | 1.000 | -.021 | -.006 |
| 51 | 2 | 12 | V17,F5 | .010 | .920 | 1.000 | .114 | .044 |
| 52 | 2 | 20 | V11,F1 | .005 | .942 | 1.000 | .016 | .002 |
| 53 | 2 | 12 | V10,F5 | .005 | .942 | 1.000 | .088 | .031 |
| 54 | 2 | 20 | V11,F3 | .005 | .945 | 1.000 | -.010 | -.002 |
| 55 | 2 | 20 | V10,F3 | .003 | .960 | 1.000 | .007 | .001 |
| 56 | 2 | 20 | V9,F2 | .000 | .988 | 1.000 | -.009 | -.002 |
| 57 | 2 | 12 | V12,F5 | .000 | 1.000 | 1.000 | .000 | .000 |
| 58 | 2 | 12 | V9,F5 | .000 | 1.000 | 1.000 | .000 | .000 |
| 59 | 2 | 0 | V1,F1 | .000 | 1.000 | 1.000 | .000 | .000 |
| 60 | 2 | 0 | V9,F4 | .000 | 1.000 | 1.000 | .000 | .000 |
| 61 | 2 | 12 | V6,F5 | .000 | 1.000 | 1.000 | .000 | .000 |
| 62 | 2 | 12 | V5,F5 | .000 | 1.000 | 1.000 | .000 | .000 |
| 63 | 2 | 0 | V6,F3 | .000 | 1.000 | 1.000 | .000 | .000 |
| 64 | 2 | 0 | V10,F2 | .000 | 1.000 | 1.000 | .000 | .000 |
| 65 | 2 | 0 | F5,F5 | .000 | 1.000 | 1.000 | .000 | .000 |

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TITLE: master confirmatorio tic segundo orden dos factores

MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

```
        MULTIVARIATE LAGRANGE MULTIPLIER TEST BY SIMULTANEOUS PROCESS IN
STAGE  1

        PARAMETER SETS (SUBMATRICES) ACTIVE AT THIS STAGE ARE:

           PVV PFV PFF PDD GVV GVF GFV GFF BVF BFF


              CUMULATIVE  MULTIVARIATE  STATISTICS          UNIVARIATE
INCREMENT
              ----------------------------------      -------------------
-----------

HANCOCK'S

SEQUENTIAL
       STEP   PARAMETER   CHI-SQUARE  D.F.    PROB.   CHI-SQUARE   PROB.
D.F.   PROB.
       ----  -----------  ----------  ----    -----   ----------   -----
----   -----
          1       V5,F4       10.689     1     .001       10.689    .001
50   1.000
          2       V8,F3       17.638     2     .000        6.950    .008
49   1.000
          3       V8,F4       24.460     3     .000        6.822    .009
48   1.000


        LAGRANGIAN MULTIPLIER TEST REQUIRED    25443 WORDS OF MEMORY.
        PROGRAM ALLOCATES ******** WORDS.
      1
        Execution begins at 14:16:59
        Execution ends   at 14:17:00
        Elapsed time =       1.00 seconds
```

# ANEXO VII

# ANALISIS FIABILIDAD INICIAL – FLEX

**Escala: ALL VARIABLES**

**Resumen de procesamiento de casos**

| | | N | % |
|---|---|---|---|
| Casos | Válido | 170 | 100,0 |
| | Excluido[a] | 0 | ,0 |
| | Total | 170 | 100,0 |

a. La eliminación por lista se basa en todas las variables del procedimiento.

**Estadísticas de fiabilidad**

| Alfa de Cronbach | N de elementos |
|---|---|
| ,907 | 19 |

**Estadísticas de elemento**

| | Media | Desviación estándar | N |
|---|---|---|---|
| p.2.2 - [Rotación horizontal de tareas] | 1,8765 | 2,12954 | 170 |
| p.2.3 - [Rodízio vertical ascendente de tarefas] | 1,4588 | 1,89082 | 170 |
| p.2.4 - [Equipos de trabajo polivalentes] | 2,9471 | 2,53090 | 170 |
| p.2.6 - [Equipos de mejora y solución de problemas] | 2,0882 | 2,31496 | 170 |
| p.3.1 - [Autónomos que trabajan para la empresa] | 2,2059 | 2,38560 | 170 |
| p.3.3 - [Subcontratación] | 1,9000 | 2,36255 | 170 |
| p.4.1- [Agrupación de empleados por proyectos de trabajo] | 2,7294 | 2,44411 | 170 |

| | | | |
|---|---|---|---|
| p.4.2 - [Autogestión de los equipos respecto al método de trabajo] | 2,8235 | 2,38177 | 170 |
| p.4.3 - [Autogestión de los equipos respecto a la programación del trabajo] | 2,6882 | 2,41847 | 170 |
| p.4.4 - [Autogestión de los equipos respecto al control de los objetivos] | 2,6647 | 2,43725 | 170 |
| p.4.7 - [Autonomía en la toma de decisiones en el trabajo] | 3,4059 | 2,26237 | 170 |
| p.4.8 - [Autonomía en la ejecución del trabajo] | 4,0471 | 2,27102 | 170 |
| p.4.9 - [Delegación de decisiones operativas] | 3,5353 | 2,36629 | 170 |
| p.4.10 - [Delegación de decisiones estratégicas] | 2,7706 | 2,31799 | 170 |
| p.6.1 - [Formación/Conferencias/Seminarios] | 2,8294 | 2,32818 | 170 |
| p.6.2 - [Desarrollo de productos o servicios] | 2,9235 | 2,22414 | 170 |
| p.6.3 - [Desarrollo de procesos] | 2,5529 | 2,30772 | 170 |
| p.6.4 - [Benchmarking e intercambio de experiencias] | 2,3765 | 2,18102 | 170 |
| p.6.5 - [Transferencia de tecnología de la información y comunicación] | 2,1118 | 2,25435 | 170 |

**Estadísticas de total de elemento**

| | Media de escala si el elemento se ha suprimido | Varianza de escala si el elemento se ha suprimido | Correlación total de elementos corregida | Alfa de Cronbach si el elemento se ha suprimido |
|---|---|---|---|---|
| p.2.2 - [Rotación horizontal de tareas] | 48,0588 | 670,636 | ,413 | ,906 |
| p.2.3 - [Rodízio vertical ascendente de tarefas] | 48,4765 | 672,204 | ,458 | ,905 |
| p.2.4 - [Equipos de trabajo polivalentes] | 46,9882 | 649,834 | ,500 | ,904 |
| p.2.6 - [Equipos de mejora y solución de problemas] | 47,8471 | 656,012 | ,501 | ,904 |
| p.3.1 - [Autónomos que trabajan para la empresa] | 47,7294 | 681,062 | ,273 | ,910 |
| p.3.3 - [Subcontratación] | 48,0353 | 674,614 | ,330 | ,908 |
| p.4.1- [Agrupación de empleados por proyectos de trabajo] | 47,2059 | 636,366 | ,636 | ,900 |
| p.4.2 - [Autogestión de los equipos respecto al método de trabajo] | 47,1118 | 628,987 | ,720 | ,898 |
| p.4.3 - [Autogestión de los equipos respecto a la programación del trabajo] | 47,2471 | 626,081 | ,734 | ,897 |
| p.4.4 - [Autogestión de los equipos respecto al control de los objetivos] | 47,2706 | 624,790 | ,739 | ,897 |
| p.4.7 - [Autonomía en la toma de decisiones en el trabajo] | 46,5294 | 650,901 | ,561 | ,902 |
| p.4.8 - [Autonomía en la ejecución del trabajo] | 45,8882 | 643,082 | ,629 | ,900 |
| p.4.9 - [Delegación de decisiones operativas] | 46,4000 | 636,786 | ,656 | ,900 |
| p.4.10 - [Delegación de decisiones estratégicas] | 47,1647 | 645,464 | ,593 | ,901 |
| p.6.1 - [Formación/Conferencias/Seminarios] | 47,1059 | 653,231 | ,522 | ,903 |

| | | | | |
|---|---|---|---|---|
| p.6.2 - [Desarrollo de productos o servicios] | 47,0118 | 652,509 | ,557 | ,902 |
| p.6.3 - [Desarrollo de procesos] | 47,3824 | 648,344 | ,571 | ,902 |
| p.6.4 - [Benchmarking e intercambio de experiencias] | 47,5588 | 651,680 | ,577 | ,902 |
| p.6.5 - [Transferencia de tecnología de la información y comunicación] | 47,8235 | 651,081 | ,561 | ,902 |

# ANEXO VIII

# ANÁLISIS FACTORIAL EXPLORATORIO – FLEX

**Matriz de correlaciones**

| | | p.2.2 - [Rotación horizontal de tareas] | p.2.3 - [Rodízio vertical ascendente de tarefas] | p.2.4 - [Equipos de trabajo polivalentes] | p.2.6 - [Equipos de mejora y solución de problemas] | p.3.1 - [Autónomos que trabajan para la empresa] | p.3.3 - [Subcontratación] | p.4.1- [Agrupación de empleados por proyectos de trabajo] | p.4.2 - [Autogestión de los equipos respecto al método de trabajo] | p.4.3 - [Autogestión de los equipos respecto a la programación del trabajo] | p.4.4 - [Autogestión de los equipos respecto al control de los objetivos] | p.4.7 - [Autonomía en la toma de decisiones en el trabajo] |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Correlación | p.2.2 - [Rotación horizontal de tareas] | 1,000 | ,758 | ,520 | ,520 | ,074 | ,018 | ,225 | ,255 | ,205 | ,235 | ,251 |
| | p.2.3 - [Rodízio vertical ascendente de tarefas] | ,758 | 1,000 | ,492 | ,563 | ,102 | ,088 | ,241 | ,249 | ,262 | ,279 | ,182 |
| | p.2.4 - [Equipos de trabajo polivalentes] | ,520 | ,492 | 1,000 | ,626 | ,095 | ,047 | ,353 | ,328 | ,330 | ,371 | ,278 |
| | p.2.6 - [Equipos de mejora y solución de problemas] | ,520 | ,563 | ,626 | 1,000 | -,018 | ,089 | ,302 | ,316 | ,312 | ,334 | ,289 |
| | p.3.1 - [Autónomos que trabajan para la empresa] | ,074 | ,102 | ,095 | -,018 | 1,000 | ,485 | ,309 | ,163 | ,197 | ,214 | ,151 |

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| p.3.3 - [Subcontratación] | ,018 | ,088 | ,047 | ,089 | ,485 | 1,000 | ,346 | ,248 | ,328 | ,227 | ,163 |
| p.4.1- [Agrupación de empleados por proyectos de trabajo] | ,225 | ,241 | ,353 | ,302 | ,309 | ,346 | 1,000 | ,679 | ,682 | ,617 | ,338 |
| p.4.2 - [Autogestión de los equipos respecto al método de trabajo] | ,255 | ,249 | ,328 | ,316 | ,163 | ,248 | ,679 | 1,000 | ,915 | ,859 | ,399 |
| p.4.3 - [Autogestión de los equipos respecto a la programación del trabajo] | ,205 | ,262 | ,330 | ,312 | ,197 | ,328 | ,682 | ,915 | 1,000 | ,887 | ,383 |
| p.4.4 - [Autogestión de los equipos respecto al control de los objetivos] | ,235 | ,279 | ,371 | ,334 | ,214 | ,227 | ,617 | ,859 | ,887 | 1,000 | ,413 |
| p.4.7 - [Autonomía en la toma de decisiones en el trabajo] | ,251 | ,182 | ,278 | ,289 | ,151 | ,163 | ,338 | ,399 | ,383 | ,413 | 1,000 |
| p.4.8 - [Autonomía en la ejecución del trabajo] | ,346 | ,304 | ,386 | ,367 | ,169 | ,169 | ,421 | ,491 | ,479 | ,505 | ,797 |

| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | p.4.9 - [Delegación de decisiones operativas] | ,280 | ,238 | ,430 | ,352 | ,205 | ,184 | ,380 | ,457 | ,475 | ,515 | ,662 |
| | p.4.10 - [Delegación de decisiones estratégicas] | ,240 | ,235 | ,239 | ,315 | ,161 | ,223 | ,399 | ,483 | ,477 | ,475 | ,564 |
| | p.6.1 - [Formación/Conferencias/Seminarios] | ,042 | ,124 | ,188 | ,131 | ,254 | ,252 | ,310 | ,350 | ,361 | ,399 | ,244 |
| | p.6.2 - [Desarrollo de productos o servicios] | ,179 | ,224 | ,259 | ,317 | ,111 | ,214 | ,349 | ,382 | ,376 | ,370 | ,251 |
| | p.6.3 - [Desarrollo de procesos] | ,193 | ,266 | ,162 | ,271 | ,111 | ,247 | ,303 | ,380 | ,437 | ,419 | ,212 |
| | p.6.4 - [Benchmarking e intercambio de experiencias] | ,197 | ,266 | ,338 | ,320 | ,119 | ,134 | ,329 | ,454 | ,451 | ,472 | ,263 |
| | p.6.5 - [Transferencia de tecnología de la información y comunicación] | ,157 | ,260 | ,163 | ,200 | ,155 | ,214 | ,320 | ,356 | ,337 | ,365 | ,322 |
| Sig. (unilateral) | p.2.2 - [Rotación horizontal de tareas] | | ,000 | ,000 | ,000 | ,170 | ,410 | ,002 | ,000 | ,004 | ,001 | ,000 |

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | p.2.3 - [Rodízio vertical ascendente de tarefas] | ,000 | | ,000 | ,000 | ,092 | ,126 | ,001 | ,001 | ,000 | ,000 | ,009 |
| | p.2.4 - [Equipos de trabajo polivalentes] | ,000 | ,000 | | ,000 | ,109 | ,273 | ,000 | ,000 | ,000 | ,000 | ,000 |
| | p.2.6 - [Equipos de mejora y solución de problemas] | ,000 | ,000 | ,000 | | ,406 | ,124 | ,000 | ,000 | ,000 | ,000 | ,000 |
| | p.3.1 - [Autónomos que trabajan para la empresa] | ,170 | ,092 | ,109 | ,406 | | ,000 | ,000 | ,017 | ,005 | ,002 | ,025 |
| | p.3.3 - [Subcontratación] | ,410 | ,126 | ,273 | ,124 | ,000 | | ,000 | ,001 | ,000 | ,001 | ,017 |
| | p.4.1- [Agrupación de empleados por proyectos de trabajo] | ,002 | ,001 | ,000 | ,000 | ,000 | ,000 | | ,000 | ,000 | ,000 | ,000 |
| | p.4.2 - [Autogestión de los equipos respecto al método de trabajo] | ,000 | ,001 | ,000 | ,000 | ,017 | ,001 | ,000 | | ,000 | ,000 | ,000 |

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| p.4.3 - [Autogestión de los equipos respecto a la programación del trabajo] | ,004 | ,000 | ,000 | ,000 | ,005 | ,000 | ,000 | ,000 | | ,000 | ,000 |
| p.4.4 - [Autogestión de los equipos respecto al control de los objetivos] | ,001 | ,000 | ,000 | ,000 | ,002 | ,001 | ,000 | ,000 | ,000 | | ,000 |
| p.4.7 - [Autonomía en la toma de decisiones en el trabajo] | ,000 | ,009 | ,000 | ,000 | ,025 | ,017 | ,000 | ,000 | ,000 | ,000 | |
| p.4.8 - [Autonomía en la ejecución del trabajo] | ,000 | ,000 | ,000 | ,000 | ,014 | ,014 | ,000 | ,000 | ,000 | ,000 | ,000 |
| p.4.9 - [Delegación de decisiones operativas] | ,000 | ,001 | ,000 | ,000 | ,004 | ,008 | ,000 | ,000 | ,000 | ,000 | ,000 |
| p.4.10 - [Delegación de decisiones estratégicas] | ,001 | ,001 | ,001 | ,000 | ,018 | ,002 | ,000 | ,000 | ,000 | ,000 | ,000 |
| p.6.1 - [Formación/Conferencias/Seminarios] | ,292 | ,053 | ,007 | ,044 | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 | ,001 |
| p.6.2 - [Desarrollo de productos o servicios] | ,010 | ,002 | ,000 | ,000 | ,074 | ,003 | ,000 | ,000 | ,000 | ,000 | ,000 |

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| p.6.3 - [Desarrollo de procesos] | ,006 | ,000 | ,017 | ,000 | ,074 | ,001 | ,000 | ,000 | ,000 | ,000 | ,003 |
| p.6.4 - [Benchmarking e intercambio de experiencias] | ,005 | ,000 | ,000 | ,000 | ,061 | ,041 | ,000 | ,000 | ,000 | ,000 | ,000 |
| p.6.5 - [Transferencia de tecnología de la información y comunicación] | ,020 | ,000 | ,017 | ,004 | ,022 | ,003 | ,000 | ,000 | ,000 | ,000 | ,000 |

**Matriz de correlaciones**

| | | p.4.8 - [Autonomía en la ejecución del trabajo] | p.4.9 - [Delegación de decisiones operativas] | p.4.10 - [Delegación de decisiones estratégicas] | p.6.1 - [Formación/Conferencias/Seminarios] | p.6.2 - [Desarrollo de productos o servicios] | p.6.3 - [Desarrollo de procesos] | p.6.4 - [Benchmarking e intercambio de experiencias] | p.6.5 - [Transferencia de tecnología de la información y comunicación] |
|---|---|---|---|---|---|---|---|---|---|
| Correlación | p.2.2 - [Rotación horizontal de tareas] | ,346 | ,280 | ,240 | ,042 | ,179 | ,193 | ,197 | ,157 |
| | p.2.3 - [Rodízio vertical ascendente de tarefas] | ,304 | ,238 | ,235 | ,124 | ,224 | ,266 | ,266 | ,260 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| | p.2.4 - [Equipos de trabajo polivalentes] | ,386 | ,430 | ,239 | ,188 | ,259 | ,162 | ,338 | ,163 |
| | p.2.6 - [Equipos de mejora y solución de problemas] | ,367 | ,352 | ,315 | ,131 | ,317 | ,271 | ,320 | ,200 |
| | p.3.1 - [Autónomos que trabajan para la empresa] | ,169 | ,205 | ,161 | ,254 | ,111 | ,111 | ,119 | ,155 |
| | p.3.3 - [Subcontratación] | ,169 | ,184 | ,223 | ,252 | ,214 | ,247 | ,134 | ,214 |
| | p.4.1- [Agrupación de empleados por proyectos de trabajo] | ,421 | ,380 | ,399 | ,310 | ,349 | ,303 | ,329 | ,320 |
| | p.4.2 - [Autogestión de los equipos respecto al método de trabajo] | ,491 | ,457 | ,483 | ,350 | ,382 | ,380 | ,454 | ,356 |
| | p.4.3 - [Autogestión de los equipos respecto a la programación del trabajo] | ,479 | ,475 | ,477 | ,361 | ,376 | ,437 | ,451 | ,337 |
| | p.4.4 - [Autogestión de los equipos respecto al control de los objetivos] | ,505 | ,515 | ,475 | ,399 | ,370 | ,419 | ,472 | ,365 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| | p.4.7 - [Autonomía en la toma de decisiones en el trabajo] | ,797 | ,662 | ,564 | ,244 | ,251 | ,212 | ,263 | ,322 |
| | p.4.8 - [Autonomía en la ejecución del trabajo] | 1,000 | ,701 | ,591 | ,229 | ,202 | ,219 | ,228 | ,273 |
| | p.4.9 - [Delegación de decisiones operativas] | ,701 | 1,000 | ,772 | ,303 | ,263 | ,320 | ,297 | ,312 |
| | p.4.10 - [Delegación de decisiones estratégicas] | ,591 | ,772 | 1,000 | ,225 | ,230 | ,307 | ,220 | ,341 |
| | p.6.1 - [Formación/Conferencias/Seminarios] | ,229 | ,303 | ,225 | 1,000 | ,621 | ,582 | ,586 | ,566 |
| | p.6.2 - [Desarrollo de productos o servicios] | ,202 | ,263 | ,230 | ,621 | 1,000 | ,668 | ,538 | ,597 |
| | p.6.3 - [Desarrollo de procesos] | ,219 | ,320 | ,307 | ,582 | ,668 | 1,000 | ,543 | ,682 |
| | p.6.4 - [Benchmarking e intercambio de experiencias] | ,228 | ,297 | ,220 | ,586 | ,538 | ,543 | 1,000 | ,600 |
| | p.6.5 - [Transferencia de tecnología de la información y comunicación] | ,273 | ,312 | ,341 | ,566 | ,597 | ,682 | ,600 | 1,000 |
| Sig. (unilateral) | p.2.2 - [Rotación horizontal de tareas] | ,000 | ,000 | ,001 | ,292 | ,010 | ,006 | ,005 | ,020 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| | p.2.3 - [Rodízio vertical ascendente de tarefas] | ,000 | ,001 | ,001 | ,053 | ,002 | ,000 | ,000 | ,000 |
| | p.2.4 - [Equipos de trabajo polivalentes] | ,000 | ,000 | ,001 | ,007 | ,000 | ,017 | ,000 | ,017 |
| | p.2.6 - [Equipos de mejora y solución de problemas] | ,000 | ,000 | ,000 | ,044 | ,000 | ,000 | ,000 | ,004 |
| | p.3.1 - [Autónomos que trabajan para la empresa] | ,014 | ,004 | ,018 | ,000 | ,074 | ,074 | ,061 | ,022 |
| | p.3.3 - [Subcontratación] | ,014 | ,008 | ,002 | ,000 | ,003 | ,001 | ,041 | ,003 |
| | p.4.1- [Agrupación de empleados por proyectos de trabajo] | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 |
| | p.4.2 - [Autogestión de los equipos respecto al método de trabajo] | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 |
| | p.4.3 - [Autogestión de los equipos respecto a la programación del trabajo] | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 |
| | p.4.4 - [Autogestión de los equipos respecto al control de los objetivos] | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| p.4.7 - [Autonomía en la toma de decisiones en el trabajo] | ,000 | ,000 | ,000 | ,001 | ,000 | ,003 | ,000 | ,000 |
| p.4.8 - [Autonomía en la ejecución del trabajo] | | ,000 | ,000 | ,001 | ,004 | ,002 | ,001 | ,000 |
| p.4.9 - [Delegación de decisiones operativas] | ,000 | | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 |
| p.4.10 - [Delegación de decisiones estratégicas] | ,000 | ,000 | | ,002 | ,001 | ,000 | ,002 | ,000 |
| p.6.1 - [Formación/Conferencias/Seminarios] | ,001 | ,000 | ,002 | | ,000 | ,000 | ,000 | ,000 |
| p.6.2 - [Desarrollo de productos o servicios] | ,004 | ,000 | ,001 | ,000 | | ,000 | ,000 | ,000 |
| p.6.3 - [Desarrollo de procesos] | ,002 | ,000 | ,000 | ,000 | ,000 | | ,000 | ,000 |
| p.6.4 - [Benchmarking e intercambio de experiencias] | ,001 | ,000 | ,002 | ,000 | ,000 | ,000 | | ,000 |
| p.6.5 - [Transferencia de tecnología de la información y comunicación] | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 | ,000 | |

**Prueba de KMO y Bartlett**

| | | |
|---|---|---|
| Medida Kaiser-Meyer-Olkin de adecuación de muestreo | | ,852 |
| Prueba de esfericidad de Bartlett | Aprox. Chi-cuadrado | 2207,949 |
| | gl | 171 |
| | Sig. | ,000 |

**Matriz de componente[a]**

| | Componente | | | | |
|---|---|---|---|---|---|
| | 1 | 2 | 3 | 4 | 5 |
| p.4.4 - [Autogestión de los equipos respecto al control de los objetivos] | ,805 | | -,224 | ,262 | -,309 |
| p.4.3 - [Autogestión de los equipos respecto a la programación del trabajo] | ,800 | | -,267 | ,342 | -,305 |
| p.4.2 - [Autogestión de los equipos respecto al método de trabajo] | ,791 | | -,248 | ,311 | -,352 |
| p.4.9 - [Delegación de decisiones operativas] | ,714 | ,254 | -,288 | -,376 | |
| p.4.1- [Agrupación de empleados por proyectos de trabajo] | ,691 | | -,225 | ,379 | |
| p.4.8 - [Autonomía en la ejecución del trabajo] | ,691 | ,361 | -,304 | -,311 | |
| p.4.10 - [Delegación de decisiones estratégicas] | ,660 | ,199 | -,335 | -,319 | |
| p.6.4 - [Benchmarking e intercambio de experiencias] | ,636 | -,344 | ,324 | | -,134 |
| p.6.3 - [Desarrollo de procesos] | ,628 | -,456 | ,313 | -,157 | |
| p.4.7 - [Autonomía en la toma de decisiones en el trabajo] | ,627 | ,246 | -,315 | -,462 | |
| p.6.5 - [Transferencia de tecnología de la información y comunicación] | ,616 | -,441 | ,263 | -,273 | |
| p.6.2 - [Desarrollo de productos o servicios] | ,610 | -,435 | ,354 | -,127 | |
| p.6.1 - [Formación/Conferencias/Seminarios] | ,575 | -,544 | ,172 | -,152 | |

| | | | | | |
|---|---|---|---|---|---|
| p.2.4 - [Equipos de trabajo polivalentes] | ,554 | ,437 | ,322 | ,132 | |
| p.2.6 - [Equipos de mejora y solución de problemas] | ,553 | ,427 | ,406 | | |
| p.2.2 - [Rotación horizontal de tareas] | ,458 | ,547 | ,454 | ,125 | ,167 |
| p.2.3 - [Rodízio vertical ascendente de tarefas] | ,493 | ,431 | ,518 | ,184 | ,191 |
| p.3.1 - [Autónomos que trabajan para la empresa] | ,297 | -,170 | -,258 | ,297 | ,700 |
| p.3.3 - [Subcontratación] | ,360 | -,258 | -,252 | ,310 | ,590 |

Método de extracción: análisis de componentes principales.[a]

a. 5 componentes extraídos.

**Comunalidades**

| | Extracción |
|---|---|
| p.2.2 - [Rotación horizontal de tareas] | ,759 |
| p.2.3 - [Rodízio vertical ascendente de tarefas] | ,767 |
| p.2.4 - [Equipos de trabajo polivalentes] | ,619 |
| p.2.6 - [Equipos de mejora y solución de problemas] | ,658 |
| p.3.1 - [Autónomos que trabajan para la empresa] | ,762 |
| p.3.3 - [Subcontratación] | ,704 |
| p.4.1- [Agrupación de empleados por proyectos de trabajo] | ,676 |
| p.4.2 - [Autogestión de los equipos respecto al método de trabajo] | ,909 |
| p.4.3 - [Autogestión de los equipos respecto a la programación del trabajo] | ,927 |
| p.4.4 - [Autogestión de los equipos respecto al control de los objetivos] | ,864 |

| | |
|---|---|
| p.4.7 - [Autonomía en la toma de decisiones en el trabajo] | ,775 |
| p.4.8 - [Autonomía en la ejecución del trabajo] | ,800 |
| p.4.9 - [Delegación de decisiones operativas] | ,805 |
| p.4.10 - [Delegación de decisiones estratégicas] | ,693 |
| p.6.1 - [Formación/Conferencias/Seminarios] | ,688 |
| p.6.2 - [Desarrollo de productos o servicios] | ,702 |
| p.6.3 - [Desarrollo de procesos] | ,725 |
| p.6.4 - [Benchmarking e intercambio de experiencias] | ,648 |
| p.6.5 - [Transferencia de tecnología de la información y comunicación] | ,724 |

Método de extracción: análisis de componentes principales.

**Varianza total explicada**

| Componente | Sumas de extracción de cargas al cuadrado | | | Sumas de rotación de cargas al cuadrado | |
|---|---|---|---|---|---|
| | Total | % de varianza | % acumulado | Total | % de varianza |
| 1 | 7,373 | 38,804 | 38,804 | 3,480 | 18,318 |
| 2 | 2,266 | 11,925 | 50,729 | 3,207 | 16,878 |
| 3 | 1,919 | 10,103 | 60,831 | 3,095 | 16,288 |
| 4 | 1,376 | 7,240 | 68,072 | 2,846 | 14,977 |
| 5 | 1,270 | 6,686 | 74,758 | 1,576 | 8,296 |

**Varianza total explicada**

| Componente | Sumas de rotación de cargas al cuadrado |
|---|---|
| | % acumulado |
| 1 | 18,318 |
| 2 | 35,197 |
| 3 | 51,485 |
| 4 | 66,462 |
| 5 | 74,758 |

Método de extracción: análisis de componentes principales.

**Matriz de componente rotado[a]**

| | Componente | | | | |
|---|---|---|---|---|---|
| | 1 | 2 | 3 | 4 | 5 |
| p.6.3 - [Desarrollo de procesos] | ,815 | ,170 | ,110 | ,121 | |
| p.6.5 - [Transferencia de tecnología de la información y comunicación] | ,811 | | ,214 | | |
| p.6.2 - [Desarrollo de productos o servicios] | ,801 | ,165 | | ,158 | |
| p.6.1 - [Formación/Conferencias/Seminarios] | ,783 | ,156 | ,125 | | ,187 |
| p.6.4 - [Benchmarking e intercambio de experiencias] | ,719 | ,292 | | ,202 | |
| p.4.3 - [Autogestión de los equipos respecto a la programación del trabajo] | ,246 | ,883 | ,245 | ,125 | ,109 |
| p.4.2 - [Autogestión de los equipos respecto al método de trabajo] | ,235 | ,875 | ,258 | ,141 | |
| p.4.4 - [Autogestión de los equipos respecto al control de los objetivos] | ,267 | ,825 | ,290 | ,157 | |
| p.4.1- [Agrupación de empleados por proyectos de trabajo] | ,170 | ,697 | ,192 | ,187 | ,299 |
| p.4.7 - [Autonomía en la toma de decisiones en el trabajo] | ,151 | ,131 | ,848 | ,115 | |
| p.4.9 - [Delegación de decisiones operativas] | ,178 | ,221 | ,826 | ,189 | |
| p.4.8 - [Autonomía en la ejecución del trabajo] | | ,256 | ,815 | ,247 | |
| p.4.10 - [Delegación de decisiones estratégicas] | ,150 | ,257 | ,763 | ,113 | |
| p.2.2 - [Rotación horizontal de tareas] | | | ,146 | ,856 | |
| p.2.3 - [Rodízio vertical ascendente de tarefas] | ,147 | | | ,854 | |

| | | | | | |
|---|---|---|---|---|---|
| p.2.6 - [Equipos de mejora y solución de problemas] | ,164 | ,172 | ,192 | ,747 | |
| p.2.4 - [Equipos de trabajo polivalentes] | | ,227 | ,196 | ,720 | |
| p.3.1 - [Autónomos que trabajan para la empresa] | | | ,101 | | ,860 |
| p.3.3 - [Subcontratación] | ,158 | ,180 | | | ,800 |

Método de extracción: análisis de componentes principales.
Método de rotación: Varimax con normalización Kaiser.[a]
a. La rotación ha convergido en 6 iteraciones.

**Matriz de transformación de componente**

| Componente | 1 | 2 | 3 | 4 | 5 |
|---|---|---|---|---|---|
| 1 | ,516 | ,546 | ,499 | ,392 | ,182 |
| 2 | -,669 | -,064 | ,346 | ,622 | -,202 |
| 3 | ,450 | -,353 | -,465 | ,619 | -,271 |
| 4 | -,289 | ,565 | -,633 | ,224 | ,382 |
| 5 | ,004 | -,504 | ,113 | ,163 | ,840 |

Método de extracción: análisis de componentes principales.
Método de rotación: Varimax con normalización Kaiser.

**<u>CORRELACIÓN ÍTEM-TOTAL DIMENSIÓN F7 QUE DE REFIERE A LA FLEXIBILIDAD EXTERNA DE PUESTOS</u>**

**Estadísticas de total de elemento**

| | Media de escala si el elemento se ha suprimido | Varianza de escala si el elemento se ha suprimido | Correlación total de elementos corregida | Correlación múltiple al cuadrado |
|---|---|---|---|---|
| p.3.1 - [Autónomos que trabajan para la empresa] | 1,9000 | 5,582 | ,485 | ,235 |
| p.3.3 - [Subcontratación] | 2,2059 | 5,691 | ,485 | ,235 |

# ANEXO IX

# ANÁLISIS FACTORIAL CONFIRMATORIO

# FLEX – PRIMER ORDEN

```
1
  EQS, A STRUCTURAL EQUATION PROGRAM          MULTIVARIATE SOFTWARE, INC.
  COPYRIGHT BY P.M. BENTLER                   VERSION 6.1 (C) 1985 - 2005
(B85).


    PROGRAM CONTROL INFORMATION

    /TITLE
     master confirmatorio flex
    /SPECIFICATIONS
    VARIABLES= 58 ; CASES= 170 ;
    DATAFILE='C:\tesis1\base brasilticflex.ESS';
     MATRIX=RAW;METHOD=ML,robust;
    /LABELS
    V1=P.1.1; V2=P.1.2; V3=P.1.3; V4=P.1.4; V5=P.1.5; V6=P.1.6;
    V7=P.1.7;
    V8=P.1.8; V9=P.1.9; V10=P.1.10; V11=P.1.11; V12=P.1.12;
    V13=P.1.13; V14=P.1.14; V15=P.1.15; V16=P.1.16;
       V17=P.1.17;   V18=P.2.1;   V19=P.2.2;   V20=P.2.3;   V21=P.2.4;
V22=P.2.5;
    V23=P.2.6; V24=P.2.7; V25=P.2.8; V26=P.2.9; V27=P.2.10;
    V28=P.2.11; V29=P.2.12;
    V30=P.2.13; V31=P.2.14; V32=P.2.15; V33=P.3.1; V34=P.3.2;
    V35=P.3.3; V36=P.4.1;
    V37=P.4.2; V38=P.4.3; V39=P.4.4; V40=P.4.5; V41=P.4.6; V42=P.4.7;
    V43=P.4.8;
    V44=P.4.9; V45=P.4.10; V46=P.4.11;
    V47=P.6.1; V48=P.6.2; V49=P.6.3; V50=P.6.4; V51=P.6.5; V52=P.6.6;
    V53=P.6.7;
    V54=P.6.8; V55=P.6.9; V56=P.6.10; V57=P.11.2LI; V58=P.11.3LI;
    /EQUATIONS
    V19=F6+E19;
    V20=*F6+E20;
    V21=*F6+E21;
    V23=*F6+E23;
    V33=F7+E33;
    V35=*F7+E35;
    V36=F8+E36;
    V37=*F8+E37;
    V38=*F8+E38;
    V39=*F8+E39;
    V42=F9+E42;
    V43=*F9+E43;
    V44=*F9+E44;
    V45=*F9+E45;
    V47=F10+E47;
    V48=*F10+E48;
    V49=*F10+E49;
    V50=*F10+E50;
    V51=*F10+E51;
    /VARIANCES
    E19 TO E21=*;
    E23=*;
```

```
F6 TO F9=*;
F10=*;
E35 TO E39=*;
E33=*;
E42 TO E45=*;
E47 TO E51=*;
/COVARIANCES
F6,F7=*;
F6,F8=*;
F6,F9=*;
F6,F10=*;
F7,F8=*;
```

```
12-May-17      PAGE :  2  EQS     Licensee:
  TITLE:    master confirmatorio flex
```

```
F7,F9=*;
F7,F10=*;
F8,F9=*;
F8,F10=*;
F9,F10=*;
/TECHNICAL
ITR=100
/PRINT
FIT=ALL;
EFFECT=YES;
/WTEST
/LMTEST
/END
```

```
   65 RECORDS OF INPUT MODEL FILE WERE READ

DATA IS READ FROM C:\tesis1\base brasilticflex.ESS
THERE ARE  58 VARIABLES AND   170 CASES
IT IS A RAW DATA ESS FILE
```

```
12-May-17      PAGE :  3  EQS     Licensee:
  TITLE:    master confirmatorio flex
```

SAMPLE STATISTICS BASED ON COMPLETE CASES

UNIVARIATE STATISTICS
---------------------

| VARIABLE | P.2.2 V19 | P.2.3 V20 | P.2.4 V21 | P.2.6 V23 | P.3.1 V33 |
|---|---|---|---|---|---|
| MEAN | 1.8765 | 1.4588 | 2.9471 | 2.0882 | 2.2059 |
| SKEWNESS (G1) | 1.2422 | 1.5942 | .4243 | 1.0549 | .8539 |
| KURTOSIS (G2) | .3913 | 1.6513 | -1.3650 | -.2638 | -.6331 |

| | | | | | |
|---|---|---|---|---|---|
| STANDARD DEV. | 2.1295 | 1.8908 | 2.5309 | 2.3150 | 2.3856 |

| VARIABLE | P.3.3 V35 | P.4.1 V36 | P.4.2 V37 | P.4.3 V38 | P.4.4 V39 |
|---|---|---|---|---|---|
| MEAN | 1.9000 | 2.7294 | 2.8235 | 2.6882 | 2.6647 |
| SKEWNESS (G1) | 1.1054 | .4621 | .2998 | .4307 | .4202 |
| KURTOSIS (G2) | -.1092 | -1.1132 | -1.2121 | -1.1559 | -1.1980 |
| STANDARD DEV. | 2.3626 | 2.4441 | 2.3818 | 2.4185 | 2.4372 |

| VARIABLE | P.4.7 V42 | P.4.8 V43 | P.4.9 V44 | P.4.10 V45 | P.6.1 V47 |
|---|---|---|---|---|---|
| MEAN | 3.4059 | 4.0471 | 3.5353 | 2.7706 | 2.8294 |
| SKEWNESS (G1) | .1232 | -.2498 | -.0173 | .4803 | .3455 |
| KURTOSIS (G2) | -1.1944 | -1.1031 | -1.3026 | -1.0218 | -1.0645 |
| STANDARD DEV. | 2.2624 | 2.2710 | 2.3663 | 2.3180 | 2.3282 |

| VARIABLE | P.6.2 V48 | P.6.3 V49 | P.6.4 V50 | P.6.5 V51 |
|---|---|---|---|---|
| MEAN | 2.9235 | 2.5529 | 2.3765 | 2.1118 |
| SKEWNESS (G1) | .2227 | .5477 | .4525 | .8085 |
| KURTOSIS (G2) | -1.0536 | -.9088 | -.9277 | -.5685 |
| STANDARD DEV. | 2.2241 | 2.3077 | 2.1810 | 2.2544 |

MULTIVARIATE KURTOSIS
---------------------

MARDIA'S COEFFICIENT (G2,P) = 136.2259
NORMALIZED ESTIMATE = 31.4378

ELLIPTICAL THEORY KURTOSIS ESTIMATES
------------------------------------

MARDIA-BASED KAPPA = .3414 MEAN SCALED UNIVARIATE KURTOSIS = -.2483

MARDIA-BASED KAPPA IS USED IN COMPUTATION. KAPPA= .3414

CASE NUMBERS WITH LARGEST CONTRIBUTION TO NORMALIZED MULTIVARIATE KURTOSIS:

---------------------------------------------------------------------
-----

| CASE NUMBER | 21 | 58 | 85 | 139 | 150 |
|---|---|---|---|---|---|
| ESTIMATE | 1031.3328 | 511.3388 | 1673.7663 | 435.7062 | 769.0909 |

12-May-17 PAGE : 4 EQS Licensee:
TITLE: master confirmatorio flex

COVARIANCE MATRIX TO BE ANALYZED: 19 VARIABLES (SELECTED FROM 58 VARIABLES)
BASED ON 170 CASES.

| | | P.2.2<br>V19 | P.2.3<br>V20 | P.2.4<br>V21 | P.2.6<br>V23 | P.3.1<br>V33 |
|---|---|---|---|---|---|---|
| P.2.2 | V19 | 4.535 | | | | |
| P.2.3 | V20 | 3.051 | 3.575 | | | |
| P.2.4 | V21 | 2.804 | 2.356 | 6.405 | | |
| P.2.6 | V23 | 2.561 | 2.462 | 3.667 | 5.359 | |
| P.3.1 | V33 | .375 | .461 | .573 | -.101 | 5.691 |
| P.3.3 | V35 | .088 | .395 | .279 | .488 | 2.731 |
| P.4.1 | V36 | 1.173 | 1.113 | 2.181 | 1.710 | 1.802 |
| P.4.2 | V37 | 1.292 | 1.123 | 1.979 | 1.743 | .924 |
| P.4.3 | V38 | 1.056 | 1.197 | 2.019 | 1.750 | 1.136 |
| P.4.4 | V39 | 1.219 | 1.285 | 2.290 | 1.882 | 1.247 |
| P.4.7 | V42 | 1.210 | .777 | 1.590 | 1.514 | .815 |
| P.4.8 | V43 | 1.674 | 1.304 | 2.221 | 1.931 | .913 |
| P.4.9 | V44 | 1.410 | 1.067 | 2.573 | 1.929 | 1.155 |
| P.4.10 | V45 | 1.185 | 1.029 | 1.402 | 1.689 | .888 |
| P.6.1 | V47 | .210 | .546 | 1.109 | .707 | 1.408 |
| P.6.2 | V48 | .848 | .941 | 1.457 | 1.634 | .590 |
| P.6.3 | V49 | .950 | 1.159 | .947 | 1.448 | .613 |
| P.6.4 | V50 | .917 | 1.098 | 1.866 | 1.617 | .620 |
| P.6.5 | V51 | .754 | 1.108 | .929 | 1.043 | .835 |

| | | P.3.3<br>V35 | P.4.1<br>V36 | P.4.2<br>V37 | P.4.3<br>V38 | P.4.4<br>V39 |
|---|---|---|---|---|---|---|
| P.3.3 | V35 | 5.582 | | | | |

```
     P.4.1    V36        1.996      5.974
     P.4.2    V37        1.396      3.952      5.673
     P.4.3    V38        1.874      4.033      5.270      5.849
     P.4.4     V39           1.309        3.678        4.988        5.226
5.940
     P.4.7     V42            .869        1.868        2.149        2.098
2.279
     P.4.8     V43            .904        2.338        2.653        2.630
2.797
     P.4.9     V44           1.030        2.199        2.574        2.718
2.968
     P.4.10    V45           1.220        2.263        2.669        2.674
2.686
     P.6.1     V47           1.385        1.764        1.940        2.035
2.262
     P.6.2     V48           1.122        1.896        2.022        2.023
2.004
     P.6.3     V49           1.346        1.707        2.086        2.440
2.358
     P.6.4     V50            .689        1.753        2.357        2.378
2.512
     P.6.5     V51           1.141        1.764        1.913        1.840
2.008


                       P.4.7      P.4.8      P.4.9      P.4.10     P.6.1
                          V42        V43        V44        V45        V47
     P.4.7    V42        5.118
     P.4.8    V43        4.093      5.158
     P.4.9    V44        3.545      3.768      5.599
     P.4.10   V45        2.958      3.111      4.236      5.373
     P.6.1     V47           1.283        1.209        1.672        1.215
5.420
     P.6.2     V48           1.262        1.021        1.384        1.184
3.218
     P.6.3     V49           1.106        1.145        1.750        1.642
3.124
     P.6.4     V50           1.296        1.130        1.531        1.111
2.976
     P.6.5     V51           1.641        1.397        1.662        1.783
2.972


                       P.6.2      P.6.3      P.6.4      P.6.5
                          V48        V49        V50        V51
     P.6.2    V48        4.947
     P.6.3    V49        3.427      5.326
     P.6.4    V50        2.609      2.731      4.757
     P.6.5    V51        2.991      3.547      2.952      5.082


  BENTLER-WEEKS STRUCTURAL REPRESENTATION:

        NUMBER OF DEPENDENT VARIABLES = 19
            DEPENDENT V'S :    19    20    21    23    33    35    36    37    38
39
            DEPENDENT V'S :    42    43    44    45    47    48    49    50    51
```

NUMBER OF INDEPENDENT VARIABLES = 24
INDEPENDENT F'S : 6 7 8 9 10
INDEPENDENT E'S : 19 20 21 23 33 35 36 37
38 39
INDEPENDENT E'S : 42 43 44 45 47 48 49 50
51

NUMBER OF FREE PARAMETERS = 48
NUMBER OF FIXED NONZERO PARAMETERS = 24

*** WARNING MESSAGES ABOVE, IF ANY, REFER TO THE MODEL PROVIDED.
CALCULATIONS FOR INDEPENDENCE MODEL NOW BEGIN.

*** WARNING MESSAGES ABOVE, IF ANY, REFER TO INDEPENDENCE MODEL.
CALCULATIONS FOR USER'S MODEL NOW BEGIN.

3RD STAGE OF COMPUTATION REQUIRED 444121 WORDS OF MEMORY.
PROGRAM ALLOCATED 2000000 WORDS

DETERMINANT OF INPUT MATRIX IS .67791D+08

IN ITERATION # 1, MATRIX W_CFUNCT MAY NOT BE POSITIVE DEFINITE.
YOU HAVE BAD START VALUES TO BEGIN WITH.
IF ABOVE MESSAGE APPEARS ON EVERY ITERATION, PLEASE PROVIDE BETTER START VALUES AND RE-RUN THE JOB.

*** NOTE *** RESIDUAL-BASED STATISTICS CANNOT BE
CALCULATED BECAUSE OF PIVOTING PROBLEMS.

PARAMETER ESTIMATES APPEAR IN ORDER,
NO SPECIAL PROBLEMS WERE ENCOUNTERED DURING OPTIMIZATION.

RESIDUAL COVARIANCE MATRIX (S-SIGMA) :

| | | P.2.2 V19 | P.2.3 V20 | P.2.4 V21 | P.2.6 V23 | P.3.1 V33 |
|---|---|---|---|---|---|---|
| P.2.2 | V19 | .000 | | | | |
| P.2.3 | V20 | .228 | .000 | | | |
| P.2.4 | V21 | -.190 | -.330 | .000 | | |
| P.2.6 | V23 | -.318 | -.121 | .929 | .000 | |
| P.3.1 | V33 | .125 | .237 | .336 | -.329 | .000 |
| P.3.3 | V35 | -.267 | .077 | -.059 | .164 | .000 |
| P.4.1 | V36 | .060 | .114 | 1.122 | .692 | .923 |
| P.4.2 | V37 | -.156 | -.176 | .602 | .419 | -.218 |
| P.4.3 | V38 | -.453 | -.157 | .583 | .369 | -.055 |
| P.4.4 | V39 | -.216 | -.002 | .925 | .569 | .115 |
| P.4.7 | V42 | -.225 | -.510 | .225 | .202 | .103 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.4.8 | V43 | .158 | -.057 | .779 | .543 | .160 |
| P.4.9 | V44 | -.178 | -.358 | 1.063 | .476 | .367 |
| P.4.10 | V45 | -.214 | -.226 | .072 | .410 | .193 |
| P.6.1 | V47 | -.830 | -.386 | .121 | -.243 | .611 |
| P.6.2 | V48 | -.197 | .002 | .463 | .677 | -.213 |
| P.6.3 | V49 | -.179 | .146 | -.127 | .415 | -.253 |
| P.6.4 | V50 | -.028 | .251 | .967 | .753 | -.105 |
| P.6.5 | V51 | -.315 | .150 | -.087 | .066 | .015 |

| | | P.3.3<br>V35 | P.4.1<br>V36 | P.4.2<br>V37 | P.4.3<br>V38 | P.4.4<br>V39 |
|---|---|---|---|---|---|---|
| P.3.3 | V35 | .000 | | | | |
| P.4.1 | V36 | .748 | .000 | | | |
| P.4.2 | V37 | -.227 | .068 | .000 | | |
| P.4.3 | V38 | .182 | -.016 | .006 | .000 | |
| P.4.4 | V39 | -.299 | -.171 | -.016 | .010 | .000 |
| P.4.7 | V42 | -.144 | .007 | -.270 | -.424 | -.118 |
| P.4.8 | V43 | -.166 | .372 | .097 | -.035 | .263 |
| P.4.9 | V44 | -.090 | .140 | -.102 | -.072 | .315 |
| P.4.10 | V45 | .232 | .450 | .312 | .216 | .350 |
| P.6.1 | V47 | .252 | .175 | -.126 | -.119 | .214 |
| P.6.2 | V48 | -.018 | .296 | -.058 | -.145 | -.058 |
| P.6.3 | V49 | .114 | -.020 | -.159 | .099 | .133 |
| P.6.4 | V50 | -.342 | .308 | .477 | .419 | .649 |
| P.6.5 | V51 | -.024 | .130 | -.211 | -.375 | -.097 |

| | | P.4.7<br>V42 | P.4.8<br>V43 | P.4.9<br>V44 | P.4.10<br>V45 | P.6.1<br>V47 |
|---|---|---|---|---|---|---|
| P.4.7 | V42 | .000 | | | | |
| P.4.8 | V43 | .511 | .000 | | | |
| P.4.9 | V44 | -.205 | -.196 | .000 | | |
| P.4.10 | V45 | -.346 | -.380 | .581 | .000 | |
| P.6.1 | V47 | -.020 | -.168 | .230 | -.055 | .000 |
| P.6.2 | V48 | -.049 | -.365 | -.067 | -.095 | .178 |
| P.6.3 | V49 | -.310 | -.350 | .184 | .263 | -.156 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.6.4 | V50 | .111 | -.122 | .220 | -.044 | .229 |
| P.6.5 | V51 | .301 | -.018 | .180 | .478 | -.133 |

| | | P.6.2 V48 | P.6.3 V49 | P.6.4 V50 | P.6.5 V51 |
|---|---|---|---|---|---|
| P.6.2 | V48 | .000 | | | |
| P.6.3 | V49 | .125 | .000 | | |
| P.6.4 | V50 | -.156 | -.252 | .000 | |
| P.6.5 | V51 | -.134 | .174 | .128 | .000 |

AVERAGE ABSOLUTE COVARIANCE RESIDUALS = .2327

AVERAGE OFF-DIAGONAL ABSOLUTE COVARIANCE RESIDUALS = .2585

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MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

STANDARDIZED RESIDUAL MATRIX:

| | | P.2.2 V19 | P.2.3 V20 | P.2.4 V21 | P.2.6 V23 | P.3.1 V33 |
|---|---|---|---|---|---|---|
| P.2.2 | V19 | .000 | | | | |
| P.2.3 | V20 | .057 | .000 | | | |
| P.2.4 | V21 | -.035 | -.069 | .000 | | |
| P.2.6 | V23 | -.065 | -.028 | .159 | .000 | |
| P.3.1 | V33 | .025 | .053 | .056 | -.060 | .000 |
| P.3.3 | V35 | -.053 | .017 | -.010 | .030 | .000 |
| P.4.1 | V36 | .011 | .025 | .181 | .122 | .158 |
| P.4.2 | V37 | -.031 | -.039 | .100 | .076 | -.038 |
| P.4.3 | V38 | -.088 | -.034 | .095 | .066 | -.010 |
| P.4.4 | V39 | -.042 | .000 | .150 | .101 | .020 |
| P.4.7 | V42 | -.047 | -.119 | .039 | .039 | .019 |
| P.4.8 | V43 | .033 | -.013 | .136 | .103 | .030 |
| P.4.9 | V44 | -.035 | -.080 | .177 | .087 | .065 |
| P.4.10 | V45 | -.043 | -.051 | .012 | .076 | .035 |
| P.6.1 | V47 | -.167 | -.088 | .021 | -.045 | .110 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.6.2 | V48 | -.042 | .001 | .082 | .132 | -.040 |
| P.6.3 | V49 | -.036 | .034 | -.022 | .078 | -.046 |
| P.6.4 | V50 | -.006 | .061 | .175 | .149 | -.020 |
| P.6.5 | V51 | -.066 | .035 | -.015 | .013 | .003 |

| | | P.3.3 V35 | P.4.1 V36 | P.4.2 V37 | P.4.3 V38 | P.4.4 V39 |
|---|---|---|---|---|---|---|
| P.3.3 | V35 | .000 | | | | |
| P.4.1 | V36 | .129 | .000 | | | |
| P.4.2 | V37 | -.040 | .012 | .000 | | |
| P.4.3 | V38 | .032 | -.003 | .001 | .000 | |
| P.4.4 | V39 | -.052 | -.029 | -.003 | .002 | .000 |
| P.4.7 | V42 | -.027 | .001 | -.050 | -.078 | -.021 |
| P.4.8 | V43 | -.031 | .067 | .018 | -.006 | .048 |
| P.4.9 | V44 | -.016 | .024 | -.018 | -.013 | .055 |
| P.4.10 | V45 | .042 | .079 | .056 | .038 | .062 |
| P.6.1 | V47 | .046 | .031 | -.023 | -.021 | .038 |
| P.6.2 | V48 | -.003 | .055 | -.011 | -.027 | -.011 |
| P.6.3 | V49 | .021 | -.004 | -.029 | .018 | .024 |
| P.6.4 | V50 | -.066 | .058 | .092 | .079 | .122 |
| P.6.5 | V51 | -.004 | .024 | -.039 | -.069 | -.018 |

| | | P.4.7 V42 | P.4.8 V43 | P.4.9 V44 | P.4.10 V45 | P.6.1 V47 |
|---|---|---|---|---|---|---|
| P.4.7 | V42 | .000 | | | | |
| P.4.8 | V43 | .100 | .000 | | | |
| P.4.9 | V44 | -.038 | -.036 | .000 | | |
| P.4.10 | V45 | -.066 | -.072 | .106 | .000 | |
| P.6.1 | V47 | -.004 | -.032 | .042 | -.010 | .000 |
| P.6.2 | V48 | -.010 | -.072 | -.013 | -.018 | .034 |
| P.6.3 | V49 | -.059 | -.067 | .034 | .049 | -.029 |
| P.6.4 | V50 | .023 | -.025 | .043 | -.009 | .045 |
| P.6.5 | V51 | .059 | -.004 | .034 | .091 | -.025 |

| | | P.6.2 V48 | P.6.3 V49 | P.6.4 V50 | P.6.5 V51 |
|---|---|---|---|---|---|

| | | | | | |
|---|---|---|---|---|---|
| P.6.2 | V48 | .000 | | | |
| P.6.3 | V49 | .024 | .000 | | |
| P.6.4 | V50 | -.032 | -.050 | .000 | |
| P.6.5 | V51 | -.027 | .033 | .026 | .000 |

AVERAGE ABSOLUTE STANDARDIZED RESIDUALS =
.0434
AVERAGE OFF-DIAGONAL ABSOLUTE STANDARDIZED RESIDUALS =
.0483

LARGEST STANDARDIZED RESIDUALS:

| NO. | PARAMETER | ESTIMATE | NO. | PARAMETER | ESTIMATE |
|---|---|---|---|---|---|
| 1 | V36, V21 | .181 | 11 | V36, V35 | .129 |
| 2 | V44, V21 | .177 | 12 | V36, V23 | .122 |
| 3 | V50, V21 | .175 | 13 | V50, V39 | .122 |
| 4 | V47, V19 | -.167 | 14 | V42, V20 | -.119 |
| 5 | V23, V21 | .159 | 15 | V47, V33 | .110 |
| 6 | V36, V33 | .158 | 16 | V45, V44 | .106 |
| 7 | V39, V21 | .150 | 17 | V43, V23 | .103 |
| 8 | V50, V23 | .149 | 18 | V39, V23 | .101 |
| 9 | V43, V21 | .136 | 19 | V37, V21 | .100 |
| 10 | V48, V23 | .132 | 20 | V43, V42 | .100 |

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MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

DISTRIBUTION OF STANDARDIZED RESIDUALS

```
    ----------------------------------------
    !                                      !
 100-                                      -
    !                                      !
    !                    *                 !
    !                    *                 !
    !                 *  *                 !          RANGE         FREQ
PERCENT
  75-                 *  *                 -
    !                 *  *                 !    1   -0.5  -  --         0
.00%
    !                 *  *                 !    2   -0.4  -  -0.5       0
.00%
    !                 *  *                 !    3   -0.3  -  -0.4       0
.00%
    !                 *  *                 !    4   -0.2  -  -0.3       0
.00%
  50-                 *  *                 -    5   -0.1  -  -0.2       2
1.05%
```

```
     !                 *  *                 !    6    0.0   -   -0.1    82
43.16%
     !                 *  *                 !    7    0.1   -    0.0    90
47.37%
     !                 *  *                 !    8    0.2   -    0.1    16
8.42%
     !                 *  *                 !    9    0.3   -    0.2     0
.00%
   25-                 *  *                 -    A    0.4   -    0.3     0
.00%
     !                 *  *                 !    B    0.5   -    0.4     0
.00%
     !                 *  *  *              !    C     ++   -    0.5     0
.00%
     !                 *  *  *             !    -----------------------
-------
     !                 *  *  *              !           TOTAL       190
100.00%
     ----------------------------------------
        1  2  3  4  5  6  7  8  9  A  B  C       EACH "*" REPRESENTS  5
RESIDUALS


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)



  GOODNESS OF FIT SUMMARY FOR METHOD = ML

  INDEPENDENCE MODEL CHI-SQUARE         =    2305.727 ON   171 DEGREES OF
FREEDOM

  INDEPENDENCE AIC =  1963.72674   INDEPENDENCE CAIC =  1256.50520
         MODEL AIC =    25.57291          MODEL CAIC =  -561.71047

  CHI-SQUARE =      309.573 BASED ON     142 DEGREES OF FREEDOM
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00000

  THE   NORMAL   THEORY   RLS   CHI-SQUARE   FOR   THIS   ML   SOLUTION   IS
295.231.

  FIT INDICES
  -----------
  BENTLER-BONETT     NORMED FIT INDEX =      .866
  BENTLER-BONETT NON-NORMED FIT INDEX =      .905
  COMPARATIVE FIT INDEX (CFI)         =      .922
  BOLLEN   (IFI) FIT INDEX            =      .923
  MCDONALD (MFI) FIT INDEX            =      .611
  LISREL    GFI  FIT INDEX            =      .845
  LISREL   AGFI  FIT INDEX            =      .792
  ROOT MEAN-SQUARE RESIDUAL (RMR)     =      .324
  STANDARDIZED RMR                    =      .059
  ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .084
  90% CONFIDENCE INTERVAL OF RMSEA  (        .071,        .096)
```

```
RELIABILITY COEFFICIENTS
------------------------
CRONBACH'S ALPHA                    =      .907
COEFFICIENT ALPHA FOR AN OPTIMAL SHORT SCALE                =      .959
BASED ON THE FOLLOWING  3 VARIABLES
P.4.2     P.4.3     P.4.4
RELIABILITY COEFFICIENT RHO         =      .948
GREATEST LOWER BOUND RELIABILITY                            =      .973
GLB RELIABILITY FOR AN OPTIMAL SHORT SCALE                  =      .976
BASED ON 16 VARIABLES, ALL EXCEPT:
P.3.1     P.3.3     P.4.1
BENTLER'S DIMENSION-FREE LOWER BOUND RELIABILITY            =      .973
SHAPIRO'S LOWER BOUND RELIABILITY FOR A WEIGHTED COMPOSITE  =      .982
WEIGHTS THAT ACHIEVE SHAPIRO'S LOWER BOUND:
P.2.2     P.2.3     P.2.4     P.2.6     P.3.1     P.3.3
    .154      .153      .171      .168      .079      .123
P.4.1     P.4.2     P.4.3     P.4.4     P.4.7     P.4.8
    .247      .384      .419      .360      .196      .232
P.4.9     P.4.10    P.6.1     P.6.2     P.6.3     P.6.4
    .236      .226      .154      .165      .215      .179
P.6.5
    .181


GOODNESS OF FIT SUMMARY FOR METHOD = ROBUST

ROBUST INDEPENDENCE MODEL CHI-SQUARE =    2087.596 ON   171 DEGREES OF
FREEDOM

INDEPENDENCE AIC =  1745.59648   INDEPENDENCE CAIC =  1038.37494
       MODEL AIC =   -50.95386          MODEL CAIC =  -638.23724

SATORRA-BENTLER SCALED CHI-SQUARE =     233.0461 ON      142 DEGREES OF
FREEDOM
PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00000

FIT INDICES
-----------
BENTLER-BONETT     NORMED FIT INDEX =      .888
BENTLER-BONETT NON-NORMED FIT INDEX =      .943
COMPARATIVE FIT INDEX (CFI)         =      .952
BOLLEN   (IFI) FIT INDEX            =      .953
MCDONALD (MFI) FIT INDEX            =      .765
ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .062
90% CONFIDENCE INTERVAL OF RMSEA  (        .047,        .075)


                       ITERATIVE SUMMARY

                   PARAMETER
ITERATION          ABS CHANGE          ALPHA                FUNCTION
    1               1.965706           .50000               5.94672
    2                .917549          1.00000               1.90780
    3                .067172          1.00000               1.83497
    4                .020312          1.00000               1.83260
    5                .007811          1.00000               1.83205
```

```
     6               .003130        1.00000               1.83188
     7               .001601        1.00000               1.83182
     8               .001014        1.00000               1.83180
     9               .000543        1.00000               1.83179

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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
  (ROBUST STATISTICS IN PARENTHESES)


 P.2.2   =V19 =   1.000 F6    + 1.000 E19




 P.2.3   =V20 =    .897*F6    + 1.000 E20
                   .078
                 11.542@
              (   .076)
              ( 11.773@

 P.2.4   =V21 =    .951*F6    + 1.000 E21
                   .106
                  8.940@
              (   .088)
              ( 10.823@

 P.2.6   =V23 =    .915*F6    + 1.000 E23
                   .096
                  9.496@
              (   .088)
              ( 10.367@

 P.3.1   =V33 =   1.000 F7    + 1.000 E33




 P.3.3   =V35 =   1.422*F7    + 1.000 E35
                   .420
                  3.383@
              (   .413)
              (  3.442@

 P.4.1   =V36 =   1.000 F8    + 1.000 E36
```

```
 P.4.2   =V37 =   1.300*F8    + 1.000 E37
                   .108
                 12.032@
               (   .119)
               ( 10.955@

 P.4.3   =V38 =   1.355*F8    + 1.000 E38
                   .110
                 12.315@
               (   .126)
               ( 10.763@

 P.4.4   =V39 =   1.288*F8    + 1.000 E39
                   .110
                 11.661@
               (   .122)
               ( 10.529@

 P.4.7   =V42 =   1.000 F9    + 1.000 E42




 P.4.8   =V43 =   1.057*F9    + 1.000 E43
                   .083
                 12.716@
               (   .074)
               ( 14.266@


  MEASUREMENT   EQUATIONS   WITH   STANDARD   ERRORS   AND   TEST   STATISTICS
(CONTINUED)


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  TITLE:    master confirmatorio flex

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)
  (ROBUST STATISTICS IN PARENTHESES)

 P.4.9   =V44 =   1.106*F9    + 1.000 E44
                   .087
                 12.792@
               (   .078)
               ( 14.169@

 P.4.10  =V45 =    .975*F9    + 1.000 E45
                   .088
                 11.122@
               (   .083)
               ( 11.799@

 P.6.1   =V47 =   1.000 F10   + 1.000 E47
```

```
 P.6.2   =V48 =   1.007*F10   + 1.000 E48
                   .100
                 10.037@
               (   .089)
               ( 11.284@

 P.6.3   =V49 =   1.086*F10   + 1.000 E49
                   .104
                 10.448@
               (   .093)
               ( 11.660@

 P.6.4   =V50 =    .909*F10   + 1.000 E50
                   .099
                  9.211@
               (   .092)
               (  9.925@

 P.6.5   =V51 =   1.028*F10   + 1.000 E51
                   .102
                 10.117@
               (   .102)
               ( 10.032@


12-May-17      PAGE : 10  EQS     Licensee:
  TITLE:    master confirmatorio flex

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES
  ----------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                 V                                F
                ---                              ---
                              I F6  -   F6              3.148*I
                              I                          .504 I
                              I                         6.240@I
                              I                      (   .545)I
                              I                      (  5.779@I
                              I                               I
                              I F7  -   F7              1.921*I
                              I                          .710 I
                              I                         2.706@I
                              I                      (   .737)I
                              I                      (  2.606@I
                              I                               I
                              I F8  -   F8              2.987*I
                              I                          .569 I
                              I                         5.246@I
                              I                      (   .552)I
                              I                      (  5.410@I
                              I                               I
```

```
                                          I F9  -   F9             3.389*I
                                          I                          .544 I
                                          I                         6.231@I
                                          I                      (   .429)I
                                          I                      (  7.894@I
                                          I                               I
                                          I F10 -   F10            3.020*I
                                          I                          .554 I
                                          I                         5.447@I
                                          I                      (   .467)I
                                          I                      (  6.469@I
                                          I                               I
```

```
12-May-17      PAGE : 11  EQS     Licensee:
  TITLE:    master confirmatorio flex

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES
  ----------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                   E                                D
                  ---                              ---
 E19 -P.2.2              1.387*I                                 I
                          .238 I                                 I
                         5.828@I                                 I
                      (   .422)I                                 I
                      (  3.291@I                                 I
                               I                                 I
 E20 -P.2.3              1.042*I                                 I
                          .186 I                                 I
                         5.611@I                                 I
                      (   .262)I                                 I
                      (  3.976@I                                 I
                               I                                 I
 E21 -P.2.4              3.558*I                                 I
                          .441 I                                 I
                         8.068@I                                 I
                      (   .500)I                                 I
                      (  7.112@I                                 I
                               I                                 I
 E23 -P.2.6              2.725*I                                 I
                          .348 I                                 I
                         7.825@I                                 I
                      (   .493)I                                 I
                      (  5.533@I                                 I
                               I                                 I
 E33 -P.3.1              3.770*I                                 I
                          .676 I                                 I
                         5.577@I                                 I
                      (   .771)I                                 I
                      (  4.893@I                                 I
                               I                                 I
 E35 -P.3.3              1.700*I                                 I
                         1.101 I                                 I
                         1.543 I                                 I
```

```
                     (  1.146)I                                I
                     (  1.483)I                                I
                              I                                I
 E36 -P.4.1             2.986*I                                I
                         .336 I                                I
                        8.882@I                                I
                     (   .471)I                                I
                     (  6.346@I                                I
                              I                                I
 E37 -P.4.2              .623*I                                I
                         .100 I                                I
                        6.227@I                                I
                     (   .191)I                                I
                     (  3.253@I                                I
                              I                                I
 E38 -P.4.3              .361*I                                I
                         .087 I                                I
                        4.143@I                                I
                     (   .274)I                                I
                     (  1.317)I                                I
                              I                                I
 E39 -P.4.4              .981*I                                I
                         .131 I                                I
                        7.487@I                                I
                     (   .346)I                                I
                     (  2.840@I                                I
                              I                                I
 E42 -P.4.7             1.729*I                                I
                         .238 I                                I
                        7.269@I                                I
                     (   .273)I                                I
                     (  6.328@I                                I
                              I                                I
 E43 -P.4.8             1.372*I                                I
                         .212 I                                I
                        6.459@I                                I
                     (   .362)I                                I
                     (  3.794@I                                I
                              I                                I


12-May-17      PAGE : 12  EQS     Licensee:
  TITLE:    master confirmatorio flex

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES (CONTINUED)
  ----------------------------------------------

 E44 -P.4.9             1.450*I                                I
                         .228 I                                I
                        6.359@I                                I
                     (   .357)I                                I
                     (  4.066@I                                I
                              I                                I
 E45 -P.4.10            2.154*I                                I
                         .278 I                                I
                        7.739@I                                I
```

```
                      (   .294)I                               I
                      (  7.335@I                               I
                               I                               I
 E47 -P.6.1              2.400*I                               I
                           .310 I                              I
                         7.746@I                               I
                      (   .427)I                               I
                      (  5.620@I                               I
                               I                               I
 E48 -P.6.2              1.887*I                               I
                           .258 I                              I
                         7.319@I                               I
                      (   .434)I                               I
                      (  4.349@I                               I
                               I                               I
 E49 -P.6.3              1.761*I                               I
                           .257 I                              I
                         6.850@I                               I
                      (   .359)I                               I
                      (  4.910@I                               I
                               I                               I
 E50 -P.6.4              2.259*I                               I
                           .285 I                              I
                         7.924@I                               I
                      (   .325)I                               I
                      (  6.960@I                               I
                               I                               I
 E51 -P.6.5              1.890*I                               I
                           .261 I                              I
                         7.240@I                               I
                      (   .329)I                               I
                      (  5.742@I                               I
                               I                               I


12-May-17      PAGE : 13  EQS     Licensee:
  TITLE:    master confirmatorio flex

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  COVARIANCES AMONG INDEPENDENT VARIABLES
  ---------------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                V                                F
               ---                              ---
                               I F7  -   F7                .250*I
                               I F6  -   F6                .245 I
                               I                          1.017 I
                               I                      (   .280)I
                               I                      (   .891)I
                               I                                I
                               I F8  -   F8               1.114*I
                               I F6  -   F6                .290 I
                               I                          3.839@I
                               I                      (   .317)I
                               I                      (  3.513@I
                               I                                I
                               I F9  -   F9               1.435*I
```

```
I F6  -   F6               .322 I
I                         4.453@I
I                      (   .287)I
I                      (  5.007@I
I                               I
I F10 -   F10             1.039*I
I F6  -   F6               .296 I
I                         3.515@I
I                      (   .288)I
I                      (  3.613@I
I                               I
I F8  -   F8               .878*I
I F7  -   F7               .319 I
I                         2.752@I
I                      (   .350)I
I                      (  2.509@I
I                               I
I F9  -   F9               .712*I
I F7  -   F7               .304 I
I                         2.347@I
I                      (   .307)I
I                      (  2.319@I
I                               I
I F10 -   F10              .797*I
I F7  -   F7               .311 I
I                         2.566@I
I                      (   .351)I
I                      (  2.268@I
I                               I
I F9  -   F9              1.861*I
I F8  -   F8               .346 I
I                         5.383@I
I                      (   .329)I
I                      (  5.652@I
I                               I
I F10 -   F10             1.589*I
I F8  -   F8               .323 I
I                         4.927@I
I                      (   .299)I
I                      (  5.324@I
I                               I
I F10 -   F10             1.303*I
I F9  -   F9               .314 I
I                         4.148@I
I                      (   .305)I
I                      (  4.273@I
I                               I
```

```
12-May-17      PAGE : 14  EQS     Licensee:
  TITLE:    master confirmatorio flex

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  DECOMPOSITION OF EFFECTS WITH NONSTANDARDIZED VALUES
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

  PARAMETER TOTAL EFFECTS
```

```
 -----------------------
P.2.2   =V19 =   1.000 F6    + 1.000 E19

P.2.3   =V20 =    .897*F6    + 1.000 E20

P.2.4   =V21 =    .951*F6    + 1.000 E21

P.2.6   =V23 =    .915*F6    + 1.000 E23

P.3.1   =V33 =   1.000 F7    + 1.000 E33

P.3.3   =V35 =   1.422*F7    + 1.000 E35

P.4.1   =V36 =   1.000 F8    + 1.000 E36

P.4.2   =V37 =   1.300*F8    + 1.000 E37

P.4.3   =V38 =   1.355*F8    + 1.000 E38

P.4.4   =V39 =   1.288*F8    + 1.000 E39
```

```
 P.4.7   =V42 =   1.000 F9    + 1.000 E42

 P.4.8   =V43 =   1.057*F9    + 1.000 E43

 P.4.9   =V44 =   1.106*F9    + 1.000 E44

 P.4.10  =V45 =    .975*F9    + 1.000 E45

 P.6.1   =V47 =   1.000 F10   + 1.000 E47

 P.6.2   =V48 =   1.007*F10   + 1.000 E48

 P.6.3   =V49 =   1.086*F10   + 1.000 E49

 P.6.4   =V50 =    .909*F10   + 1.000 E50

 P.6.5   =V51 =   1.028*F10   + 1.000 E51
12-May-17      PAGE : 15  EQS     Licensee:
  TITLE:    master confirmatorio flex

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)
```

DECOMPOSITION OF EFFECTS WITH STANDARDIZED VALUES

PARAMETER TOTAL EFFECTS
-----------------------

```
P.2.2   =V19 =    .833 F6    +  .553 E19

P.2.3   =V20 =    .842*F6    +  .540 E20

P.2.4   =V21 =    .667*F6    +  .745 E21

P.2.6   =V23 =    .701*F6    +  .713 E23

P.3.1   =V33 =    .581 F7    +  .814 E33

P.3.3   =V35 =    .834*F7    +  .552 E35

P.4.1   =V36 =    .707 F8    +  .707 E36

P.4.2   =V37 =    .944*F8    +  .331 E37

P.4.3   =V38 =    .969*F8    +  .249 E38

P.4.4   =V39 =    .914*F8    +  .406 E39

P.4.7   =V42 =    .814 F9    +  .581 E42

P.4.8   =V43 =    .857*F9    +  .516 E43

P.4.9   =V44 =    .861*F9    +  .509 E44

P.4.10  =V45 =    .774*F9    +  .633 E45

P.6.1   =V47 =    .746 F10   +  .665 E47

P.6.2   =V48 =    .786*F10   +  .618 E48

P.6.3   =V49 =    .818*F10   +  .575 E49

P.6.4   =V50 =    .725*F10   +  .689 E50

P.6.5   =V51 =    .793*F10   +  .610 E51
```

12-May-17      PAGE : 16  EQS     Licensee:
TITLE:    master confirmatorio flex

MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

STANDARDIZED SOLUTION:                                    R-
SQUARED

P.2.2           =V19    =           .833    F6               +    .553    E19
.694

```
 P.2.3          =V20   =          .842*F6           +   .540   E20
.708
 P.2.4          =V21   =          .667*F6           +   .745   E21
.445
 P.2.6          =V23   =          .701*F6           +   .713   E23
.491
 P.3.1          =V33   =         .581   F7          +   .814   E33
.338
 P.3.3          =V35   =          .834*F7           +   .552   E35
.695
 P.4.1          =V36   =         .707   F8          +   .707   E36
.500
 P.4.2          =V37   =          .944*F8           +   .331   E37
.890
 P.4.3          =V38   =          .969*F8           +   .249   E38
.938
 P.4.4          =V39   =          .914*F8           +   .406   E39
.835
 P.4.7          =V42   =         .814   F9          +   .581   E42
.662
 P.4.8          =V43   =          .857*F9           +   .516   E43
.734
 P.4.9          =V44   =          .861*F9           +   .509   E44
.741
 P.4.10        =V45   =         .774*F9             +   .633   E45
.599
 P.6.1          =V47   =          .746   F10        +   .665   E47
.557
 P.6.2          =V48   =          .786*F10          +   .618   E48
.619
 P.6.3          =V49   =          .818*F10          +   .575   E49
.669
 P.6.4          =V50   =          .725*F10          +   .689   E50
.525
 P.6.5          =V51   =          .793*F10          +   .610   E51
.628


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  TITLE:    master confirmatorio flex

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  CORRELATIONS AMONG INDEPENDENT VARIABLES
  ---------------------------------------

                  V                                F
                 ---                              ---
                               I F7  -   F7              .102*I
                               I F6  -   F6                   I
                               I                              I
                               I F8  -   F8              .363*I
                               I F6  -   F6                   I
                               I                              I
                               I F9  -   F9              .439*I
                               I F6  -   F6                   I
                               I                              I
                               I F10 -   F10             .337*I
```

```
I F6  -   F6                     I
I                                I
I F8  -   F8                .367*I
I F7  -   F7                     I
I                                I
I F9  -   F9                .279*I
I F7  -   F7                     I
I                                I
I F10 -   F10               .331*I
I F7  -   F7                     I
I                                I
I F9  -   F9                .585*I
I F8  -   F8                     I
I                                I
I F10 -   F10               .529*I
I F8  -   F8                     I
I                                I
I F10 -   F10               .407*I
I F9  -   F9                     I
I                                I
```

```
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                          E N D   O F   M E T H O D
 -------------------------------------------------------------------------
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  TITLE:    master confirmatorio flex

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  WALD TEST (FOR DROPPING PARAMETERS)
  ROBUST INFORMATION MATRIX USED IN THIS WALD TEST
  MULTIVARIATE WALD TEST BY SIMULTANEOUS PROCESS



         CUMULATIVE  MULTIVARIATE  STATISTICS                  UNIVARIATE
INCREMENT
         ----------------------------------             ----------------
----

  STEP   PARAMETER    CHI-SQUARE   D.F.   PROBABILITY          CHI-SQUARE
PROBABILITY
  ---- -----------  ----------  ----  -----------       ----------  -----
------

    1      F7,F6           .793       1         .373                 .793
.373
```

```
    2     E35,E35         2.611        2         .271                1.817
.178
    3     E38,E38         3.959        3         .266                1.348
.246
    4     F10,F7          7.068        4         .132                3.109
.078
    5      F8,F7          8.411        5         .135                1.343
.246
    6      F9,F7          9.006        6         .173                 .594
.441
    7      F7,F7         10.424        7         .166                1.418
.234
```

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12-May-17      PAGE : 19  EQS     Licensee:
  TITLE:    master confirmatorio flex

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  LAGRANGE MULTIPLIER TEST (FOR ADDING PARAMETERS)


  ORDERED UNIVARIATE TEST STATISTICS:
                                                                HANCOCK
STANDAR-
                                            CHI-                 142  DF    PARAMETER
DIZED
   NO     CODE       PARAMETER        SQUARE      PROB.      PROB.     CHANGE
CHANGE
   --   ------    ---------      ------     -----  -------- ---------  --
------
    1     2   12        V36,F7        8.961       .003      1.000       .373
.110
    2     2   12        V21,F9        6.753       .009      1.000       .265
.057
    3     2   12        V20,F9        6.286       .012      1.000      -.169
-.049
    4     2   12        V19,F10       5.844       .016      1.000      -.182
-.049
    5     2   12        V47,F6        5.818       .016      1.000      -.206
-.050
    6     2   12        V21,F8        5.589       .018      1.000       .236
.054
    7     2   12        V50,F8        5.216       .022      1.000       .206
.055
    8     2   12        V37,F7        4.751       .029      1.000      -.144
-.044
    9     2   12        V23,F9        4.352       .037      1.000       .190
.044
   10     2   12        V19,F8        4.145       .042      1.000      -.150
-.041
   11     2   12        V42,F8        3.647       .056      1.000      -.167
-.043
   12     2   12        V38,F7        3.472       .062      1.000       .115
.034
   13     2   12        V50,F6        3.358       .067      1.000       .150
.039
```

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 14 | 2 | 12 | V39,F9 | 3.356 | .067 | 1.000 | .113 | .025 |
| 15 | 2 | 12 | V23,F8 | 3.194 | .074 | 1.000 | .159 | .040 |
| 16 | 2 | 12 | V38,F9 | 3.067 | .080 | 1.000 | -.087 | -.020 |
| 17 | 2 | 12 | V23,F10 | 3.032 | .082 | 1.000 | .159 | .039 |
| 18 | 2 | 12 | V43,F6 | 2.885 | .089 | 1.000 | .129 | .032 |
| 19 | 2 | 12 | V38,F6 | 2.689 | .101 | 1.000 | -.072 | -.017 |
| 20 | 2 | 12 | V43,F10 | 2.501 | .114 | 1.000 | -.118 | -.030 |
| 21 | 2 | 12 | V47,F7 | 2.413 | .120 | 1.000 | .184 | .057 |
| 22 | 2 | 12 | V42,F6 | 2.320 | .128 | 1.000 | -.122 | -.030 |
| 23 | 2 | 12 | V45,F8 | 2.220 | .136 | 1.000 | .140 | .035 |
| 24 | 2 | 12 | V51,F8 | 2.003 | .157 | 1.000 | -.123 | -.032 |
| 25 | 2 | 12 | V36,F6 | 1.999 | .157 | 1.000 | .126 | .029 |
| 26 | 2 | 12 | V19,F7 | 1.887 | .170 | 1.000 | -.130 | -.044 |
| 27 | 2 | 12 | V39,F7 | 1.741 | .187 | 1.000 | -.102 | -.030 |
| 28 | 2 | 12 | V39,F10 | 1.576 | .209 | 1.000 | .078 | .019 |
| 29 | 2 | 12 | V39,F6 | 1.501 | .221 | 1.000 | .068 | .016 |
| 30 | 2 | 12 | V45,F7 | 1.391 | .238 | 1.000 | .129 | .040 |
| 31 | 2 | 12 | V36,F9 | 1.361 | .243 | 1.000 | .115 | .026 |
| 32 | 2 | 12 | V50,F7 | 1.346 | .246 | 1.000 | -.132 | -.044 |
| 33 | 2 | 12 | V21,F10 | 1.190 | .275 | 1.000 | .112 | .025 |
| 34 | 2 | 12 | V44,F10 | 1.161 | .281 | 1.000 | .084 | .020 |
| 35 | 2 | 12 | V35,F9 | 1.100 | .294 | 1.000 | -.197 | -.045 |
| 36 | 2 | 12 | V33,F9 | 1.100 | .294 | 1.000 | .139 | .032 |
| 37 | 2 | 12 | V51,F9 | 1.029 | .310 | 1.000 | .078 | .019 |
| 38 | 2 | 12 | V20,F8 | .937 | .333 | 1.000 | -.063 | -.019 |
| 39 | 2 | 12 | V36,F10 | .811 | .368 | 1.000 | .090 | .021 |
| 40 | 2 | 12 | V19,F9 | .805 | .369 | 1.000 | -.068 | -.017 |
| 41 | 2 | 12 | V48,F9 | .782 | .377 | 1.000 | -.068 | -.017 |
| 42 | 2 | 12 | V45,F10 | .681 | .409 | 1.000 | .070 | .017 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 43 | 2 | 12 | V38,F10 | .640 | .424 | 1.000 | -.040 | -.010 |
| 44 | 2 | 12 | V20,F7 | .499 | .480 | 1.000 | .059 | .023 |
| 45 | 2 | 12 | V43,F7 | .435 | .509 | 1.000 | -.063 | -.020 |
| 46 | 2 | 12 | V35,F6 | .314 | .575 | 1.000 | -.083 | -.020 |
| 47 | 2 | 12 | V33,F6 | .314 | .575 | 1.000 | .059 | .014 |
| 48 | 2 | 12 | V37,F10 | .305 | .581 | 1.000 | -.030 | -.007 |
| 49 | 2 | 12 | V48,F6 | .300 | .584 | 1.000 | .043 | .011 |
| 50 | 2 | 12 | V42,F7 | .289 | .591 | 1.000 | -.055 | -.017 |
| 51 | 2 | 12 | V43,F8 | .253 | .615 | 1.000 | .042 | .011 |
| 52 | 2 | 12 | V48,F8 | .248 | .619 | 1.000 | -.043 | -.011 |
| 53 | 2 | 12 | V45,F6 | .236 | .627 | 1.000 | -.042 | -.010 |
| 54 | 2 | 12 | V23,F7 | .222 | .637 | 1.000 | .055 | .017 |
| 55 | 2 | 12 | V21,F7 | .193 | .660 | 1.000 | .057 | .016 |
| 56 | 2 | 12 | V50,F9 | .187 | .666 | 1.000 | .035 | .009 |
| 57 | 2 | 12 | V48,F7 | .174 | .677 | 1.000 | -.045 | -.015 |
| 58 | 2 | 12 | V49,F9 | .173 | .677 | 1.000 | -.032 | -.008 |
| 59 | 2 | 12 | V20,F10 | .110 | .740 | 1.000 | .022 | .007 |
| 60 | 2 | 12 | V49,F6 | .086 | .770 | 1.000 | .023 | .006 |
| 61 | 2 | 12 | V51,F6 | .061 | .804 | 1.000 | -.019 | -.005 |
| 62 | 2 | 12 | V47,F8 | .055 | .814 | 1.000 | -.022 | -.006 |
| 63 | 2 | 12 | V37,F6 | .045 | .833 | 1.000 | .010 | .002 |
| 64 | 2 | 12 | V42,F10 | .039 | .844 | 1.000 | -.015 | -.004 |
| 65 | 2 | 12 | V44,F7 | .034 | .853 | 1.000 | .018 | .006 |
| 66 | 2 | 12 | V49,F8 | .025 | .874 | 1.000 | .014 | .003 |
| 67 | 2 | 12 | V33,F8 | .023 | .879 | 1.000 | -.035 | -.008 |
| 68 | 2 | 12 | V35,F8 | .023 | .879 | 1.000 | .049 | .012 |
| 69 | 2 | 12 | V51,F7 | .018 | .893 | 1.000 | -.015 | -.005 |
| 70 | 2 | 12 | V49,F7 | .018 | .895 | 1.000 | .014 | .004 |
| 71 | 2 | 12 | V37,F9 | .012 | .913 | 1.000 | -.006 | -.001 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 72 | 2 | 12 | V35,F10 | .008 | .927 | 1.000 | .022 | .005 |
| 73 | 2 | 12 | V33,F10 | .008 | .927 | 1.000 | -.016 | -.004 |
| 74 | 2 | 12 | V47,F9 | .006 | .939 | 1.000 | -.006 | -.001 |
| 75 | 2 | 12 | V44,F6 | .004 | .948 | 1.000 | .005 | .001 |
| 76 | 2 | 12 | V44,F8 | .000 | .998 | 1.000 | .000 | .000 |
| 77 | 2 | 0 | V36,F8 | .000 | 1.000 | 1.000 | .000 | .000 |
| 78 | 2 | 0 | V47,F10 | .000 | 1.000 | 1.000 | .000 | .000 |
| 79 | 2 | 0 | V33,F7 | .000 | 1.000 | 1.000 | .000 | .000 |
| 80 | 2 | 0 | V42,F9 | .000 | 1.000 | 1.000 | .000 | .000 |
| 81 | 2 | 0 | V19,F6 | .000 | 1.000 | 1.000 | .000 | .000 |

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TITLE: master confirmatorio flex

MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

MULTIVARIATE LAGRANGE MULTIPLIER TEST BY SIMULTANEOUS PROCESS IN STAGE 1

PARAMETER SETS (SUBMATRICES) ACTIVE AT THIS STAGE ARE:

PVV PFV PFF PDD GVV GVF GFV GFF BVF BFF

| | CUMULATIVE MULTIVARIATE STATISTICS | | | | UNIVARIATE INCREMENT | | HANCOCK'S SEQUENTIAL | |
|---|---|---|---|---|---|---|---|---|
| STEP | PARAMETER | CHI-SQUARE | D.F. | PROB. | CHI-SQUARE | PROB. | D.F. | PROB. |
| 1 | V36,F7 | 8.961 | 1 | .003 | 8.961 | .003 | 142 | 1.000 |
| 2 | V21,F9 | 15.714 | 2 | .000 | 6.753 | .009 | 141 | 1.000 |
| 3 | V23,F9 | 22.189 | 3 | .000 | 6.475 | .011 | 140 | 1.000 |
| 4 | V47,F6 | 28.007 | 4 | .000 | 5.818 | .016 | 139 | 1.000 |
| 5 | V50,F8 | 32.774 | 5 | .000 | 4.767 | .029 | 138 | 1.000 |

```
LAGRANGIAN MULTIPLIER TEST REQUIRED    72100 WORDS OF MEMORY.
PROGRAM ALLOCATES  2000000 WORDS.
Execution begins at 13:43:59
Execution ends   at 13:44:00
Elapsed time =       1.00 seconds
```

# ANEXO X

# ANÁLISIS FACTORIAL CONFIRMATORIO

# FLEX – SEGUNDO ORDEN

```
1
  EQS, A STRUCTURAL EQUATION PROGRAM          MULTIVARIATE SOFTWARE, INC.
  COPYRIGHT BY P.M. BENTLER                   VERSION 6.1 (C) 1985 - 2005
(B85).


    PROGRAM CONTROL INFORMATION

      /TITLE
        master confirmatorio flex
      /SPECIFICATIONS
      VARIABLES= 58 ; CASES= 170 ;
      DATAFILE='C:\tesis1\base brasilticflex.ESS';
        MATRIX=RAW;METHOD=ML,robust;
      /LABELS
      V1=P.1.1; V2=P.1.2; V3=P.1.3; V4=P.1.4; V5=P.1.5; V6=P.1.6; V7=P.1.7;
      V8=P.1.8; V9=P.1.9; V10=P.1.10; V11=P.1.11; V12=P.1.12;
      V13=P.1.13; V14=P.1.14; V15=P.1.15; V16=P.1.16;
         V17=P.1.17;   V18=P.2.1;   V19=P.2.2;   V20=P.2.3;   V21=P.2.4; V22=P.2.5;
      V23=P.2.6; V24=P.2.7; V25=P.2.8; V26=P.2.9; V27=P.2.10; V28=P.2.11; V29=P.2.12;
      V30=P.2.13; V31=P.2.14; V32=P.2.15; V33=P.3.1; V34=P.3.2; V35=P.3.3; V36=P.4.1;
      V37=P.4.2; V38=P.4.3; V39=P.4.4; V40=P.4.5; V41=P.4.6; V42=P.4.7; V43=P.4.8;
      V44=P.4.9; V45=P.4.10; V46=P.4.11;
      V47=P.6.1; V48=P.6.2; V49=P.6.3; V50=P.6.4; V51=P.6.5; V52=P.6.6; V53=P.6.7;
      V54=P.6.8; V55=P.6.9; V56=P.6.10; V57=P.11.2LI; V58=P.11.3LI;
      /EQUATIONS
      V19=F6+E19;
      V20=*F6+E20;
      V21=*F6+E21;
      V23=*F6+E23;
      V33=F7+E33;
      V35=*F7+E35;
      V36=F8+E36;
      V37=*F8+E37;
      V38=*F8+E38;
      V39=*F8+E39;
      V42=F9+E42;
      V43=*F9+E43;
      V44=*F9+E44;
      V45=*F9+E45;
      V47=F10+E47;
      V48=*F10+E48;
      V49=*F10+E49;
      V50=*F10+E50;
      V51=*F10+E51;
      F8=*F11+D8;
      F9=*F11+D9;
      /VARIANCES
```

```
E19 TO E21=*;
E23=*;
F6 TO F7=*;
F10=*;
E35 TO E39=*;
E33=*;
E42 TO E45=*;
E47 TO E51=*;
D8 TO D9=*;
F11=1;
/COVARIANCES
F6,F7=*;


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F6,F10=*;
F6,F11=*;
F7,F10=*;
F7,F11=*;
F10,F11=*;
/TECHNICAL
ITR=100
/PRINT
FIT=ALL;
EFFECT=YES;
/WTEST
/LMTEST
/END


       65 RECORDS OF INPUT MODEL FILE WERE READ


    DATA IS READ FROM C:\tesis1\base brasilticflex.ESS
    THERE ARE  58 VARIABLES AND   170 CASES
    IT IS A RAW DATA ESS FILE


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  TITLE:    master confirmatorio flex


  SAMPLE STATISTICS BASED ON COMPLETE CASES


                          UNIVARIATE STATISTICS
                          ---------------------
```

| VARIABLE | P.2.2 V19 | P.2.3 V20 | P.2.4 V21 | P.2.6 V23 | P.3.1 V33 |
|---|---|---|---|---|---|
| MEAN | 1.8765 | 1.4588 | 2.9471 | 2.0882 | 2.2059 |
| SKEWNESS (G1) | 1.2422 | 1.5942 | .4243 | 1.0549 | .8539 |
| KURTOSIS (G2) | .3913 | 1.6513 | -1.3650 | -.2638 | -.6331 |

| | | | | | |
|---|---|---|---|---|---|
| STANDARD DEV. | 2.1295 | 1.8908 | 2.5309 | 2.3150 | 2.3856 |

| VARIABLE | P.3.3 V35 | P.4.1 V36 | P.4.2 V37 | P.4.3 V38 | P.4.4 V39 |
|---|---|---|---|---|---|
| MEAN | 1.9000 | 2.7294 | 2.8235 | 2.6882 | 2.6647 |
| SKEWNESS (G1) | 1.1054 | .4621 | .2998 | .4307 | .4202 |
| KURTOSIS (G2) | -.1092 | -1.1132 | -1.2121 | -1.1559 | -1.1980 |
| STANDARD DEV. | 2.3626 | 2.4441 | 2.3818 | 2.4185 | 2.4372 |

| VARIABLE | P.4.7 V42 | P.4.8 V43 | P.4.9 V44 | P.4.10 V45 | P.6.1 V47 |
|---|---|---|---|---|---|
| MEAN | 3.4059 | 4.0471 | 3.5353 | 2.7706 | 2.8294 |
| SKEWNESS (G1) | .1232 | -.2498 | -.0173 | .4803 | .3455 |
| KURTOSIS (G2) | -1.1944 | -1.1031 | -1.3026 | -1.0218 | -1.0645 |
| STANDARD DEV. | 2.2624 | 2.2710 | 2.3663 | 2.3180 | 2.3282 |

| VARIABLE | P.6.2 V48 | P.6.3 V49 | P.6.4 V50 | P.6.5 V51 |
|---|---|---|---|---|
| MEAN | 2.9235 | 2.5529 | 2.3765 | 2.1118 |
| SKEWNESS (G1) | .2227 | .5477 | .4525 | .8085 |
| KURTOSIS (G2) | -1.0536 | -.9088 | -.9277 | -.5685 |
| STANDARD DEV. | 2.2241 | 2.3077 | 2.1810 | 2.2544 |

MULTIVARIATE KURTOSIS
---------------------

MARDIA'S COEFFICIENT (G2,P) = 136.2259
NORMALIZED ESTIMATE = 31.4378

ELLIPTICAL THEORY KURTOSIS ESTIMATES
------------------------------------

MARDIA-BASED KAPPA = .3414 MEAN SCALED UNIVARIATE KURTOSIS = -.2483

MARDIA-BASED KAPPA IS USED IN COMPUTATION. KAPPA= .3414

CASE NUMBERS WITH LARGEST CONTRIBUTION TO NORMALIZED MULTIVARIATE KURTOSIS:

```
   -------------------------------------------------------------------------
-----

   CASE NUMBER          21              58              85              139
150

   ESTIMATE        1031.3328       511.3388      1673.7663       435.7062
769.0909


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  COVARIANCE   MATRIX  TO  BE  ANALYZED:   19  VARIABLES  (SELECTED  FROM   58
VARIABLES)
  BASED ON   170 CASES.


                       P.2.2       P.2.3       P.2.4       P.2.6       P.3.1
                          V19         V20         V21         V23         V33
     P.2.2    V19       4.535
     P.2.3    V20       3.051       3.575
     P.2.4    V21       2.804       2.356       6.405
     P.2.6    V23       2.561       2.462       3.667       5.359
     P.3.1     V33           .375         .461         .573         -.101
5.691
     P.3.3     V35           .088         .395         .279          .488
2.731
     P.4.1     V36          1.173        1.113        2.181        1.710
1.802
     P.4.2     V37          1.292        1.123        1.979        1.743
.924
     P.4.3     V38          1.056        1.197        2.019        1.750
1.136
     P.4.4     V39          1.219        1.285        2.290        1.882
1.247
     P.4.7     V42          1.210         .777        1.590        1.514
.815
     P.4.8     V43          1.674        1.304        2.221        1.931
.913
     P.4.9     V44          1.410        1.067        2.573        1.929
1.155
     P.4.10    V45          1.185        1.029        1.402        1.689
.888
     P.6.1     V47           .210         .546        1.109         .707
1.408
     P.6.2     V48           .848         .941        1.457        1.634
.590
     P.6.3     V49           .950        1.159         .947        1.448
.613
     P.6.4     V50           .917        1.098        1.866        1.617
.620
     P.6.5     V51           .754        1.108         .929        1.043
.835


                       P.3.3       P.4.1       P.4.2       P.4.3       P.4.4
                          V35         V36         V37         V38         V39
     P.3.3    V35       5.582
```

```
     P.4.1    V36         1.996      5.974
     P.4.2    V37         1.396      3.952      5.673
     P.4.3    V38         1.874      4.033      5.270      5.849
     P.4.4     V39            1.309         3.678         4.988         5.226
5.940
     P.4.7     V42             .869         1.868         2.149         2.098
2.279
     P.4.8     V43             .904         2.338         2.653         2.630
2.797
     P.4.9     V44            1.030         2.199         2.574         2.718
2.968
     P.4.10    V45            1.220         2.263         2.669         2.674
2.686
     P.6.1     V47            1.385         1.764         1.940         2.035
2.262
     P.6.2     V48            1.122         1.896         2.022         2.023
2.004
     P.6.3     V49            1.346         1.707         2.086         2.440
2.358
     P.6.4     V50             .689         1.753         2.357         2.378
2.512
     P.6.5     V51            1.141         1.764         1.913         1.840
2.008


                       P.4.7      P.4.8      P.4.9      P.4.10     P.6.1
                          V42        V43        V44        V45        V47
     P.4.7    V42         5.118
     P.4.8    V43         4.093      5.158
     P.4.9    V44         3.545      3.768      5.599
     P.4.10   V45         2.958      3.111      4.236      5.373
     P.6.1     V47            1.283         1.209         1.672         1.215
5.420
     P.6.2     V48            1.262         1.021         1.384         1.184
3.218
     P.6.3     V49            1.106         1.145         1.750         1.642
3.124
     P.6.4     V50            1.296         1.130         1.531         1.111
2.976
     P.6.5     V51            1.641         1.397         1.662         1.783
2.972


                       P.6.2      P.6.3      P.6.4      P.6.5
                          V48        V49        V50        V51
     P.6.2    V48         4.947
     P.6.3    V49         3.427      5.326
     P.6.4    V50         2.609      2.731      4.757
     P.6.5    V51         2.991      3.547      2.952      5.082


  BENTLER-WEEKS STRUCTURAL REPRESENTATION:

        NUMBER OF DEPENDENT VARIABLES = 21
            DEPENDENT V'S :    19   20   21   23   33   35   36   37   38
39
            DEPENDENT V'S :    42   43   44   45   47   48   49   50   51
```

```
            DEPENDENT F'S :     8    9

        NUMBER OF INDEPENDENT VARIABLES = 25
            INDEPENDENT F'S :     6    7   10   11
            INDEPENDENT E'S :    19   20   21   23   33   35   36   37
38   39
            INDEPENDENT E'S :    42   43   44   45   47   48   49   50
51
            INDEPENDENT D'S :     8    9

        NUMBER OF FREE PARAMETERS =  46
        NUMBER OF FIXED NONZERO PARAMETERS =  27

 *** WARNING MESSAGES ABOVE, IF ANY, REFER TO THE MODEL PROVIDED.
     CALCULATIONS FOR INDEPENDENCE MODEL NOW BEGIN.

 *** WARNING MESSAGES ABOVE, IF ANY, REFER TO INDEPENDENCE MODEL.
     CALCULATIONS FOR USER'S MODEL NOW BEGIN.


  3RD STAGE OF COMPUTATION REQUIRED    442597 WORDS OF MEMORY.
  PROGRAM ALLOCATED   2000000 WORDS

  DETERMINANT OF INPUT MATRIX IS    .67791D+08

 IN ITERATION #  1, MATRIX W_CFUNCT MAY NOT BE POSITIVE DEFINITE.
  YOU HAVE BAD START VALUES TO BEGIN WITH.
  IF ABOVE MESSAGE APPEARS ON EVERY ITERATION, PLEASE PROVIDE BETTER
START VALUES AND RE-RUN THE JOB.

 *** NOTE *** RESIDUAL-BASED STATISTICS CANNOT BE
              CALCULATED BECAUSE OF PIVOTING PROBLEMS.

  PARAMETER ESTIMATES APPEAR IN ORDER,
  NO SPECIAL PROBLEMS WERE ENCOUNTERED DURING OPTIMIZATION.



  RESIDUAL COVARIANCE MATRIX  (S-SIGMA) :


                      P.2.2      P.2.3      P.2.4      P.2.6      P.3.1
                         V19        V20        V21        V23        V33
     P.2.2    V19        .000
     P.2.3    V20        .216       .000
     P.2.4    V21       -.175      -.331       .000
     P.2.6    V23       -.307      -.124       .949       .000
     P.3.1     V33          .118         .230         .330        -.335
.000
     P.3.3     V35         -.269         .073        -.060         .162
.000
     P.4.1     V36         -.070        -.008       1.002         .576
.951
     P.4.2    V37        -.325      -.335       .446       .268      -
.182
     P.4.3    V38        -.628      -.322       .423       .213      -
.017
     P.4.4     V39         -.383        -.160         .772         .420
.151
```

| | | | | | | |
|---|---|---|---|---|---|---|
| P.4.7 | V42 | .034 | -.284 | .475 | .441 | .010 |
| P.4.8 | V43 | .437 | .188 | 1.049 | .802 | .067 |
| P.4.9 | V44 | .098 | -.116 | 1.330 | .732 | .258 |
| P.4.10 | V45 | .028 | -.014 | .306 | .634 | .096 |
| P.6.1 | V47 | -.828 | -.390 | .126 | -.239 | .597 |
| P.6.2 | V48 | -.194 | .000 | .469 | .683 | -.225 |
| P.6.3 | V49 | -.176 | .143 | -.121 | .421 | -.267 |
| P.6.4 | V50 | -.025 | .250 | .974 | .759 | -.115 |
| P.6.5 | V51 | -.316 | .144 | -.084 | .068 | -.001 |

| | | P.3.3 V35 | P.4.1 V36 | P.4.2 V37 | P.4.3 V38 | P.4.4 V39 |
|---|---|---|---|---|---|---|
| P.3.3 | V35 | .000 | | | | |
| P.4.1 | V36 | .812 | .000 | | | |
| P.4.2 | V37 | -.144 | .066 | .000 | | |
| P.4.3 | V38 | .269 | -.015 | .006 | .000 | |
| P.4.4 | V39 | -.217 | -.172 | -.019 | .011 | .000 |
| P.4.7 | V42 | -.252 | .010 | -.267 | -.419 | -.115 |
| P.4.8 | V43 | -.275 | .385 | .113 | -.016 | .280 |
| P.4.9 | V44 | -.219 | .128 | -.119 | -.087 | .299 |
| P.4.10 | V45 | .117 | .436 | .294 | .199 | .332 |
| P.6.1 | V47 | .256 | .245 | -.035 | -.022 | .305 |
| P.6.2 | V48 | -.012 | .370 | .037 | -.045 | .037 |
| P.6.3 | V49 | .120 | .058 | -.057 | .207 | .234 |
| P.6.4 | V50 | -.335 | .375 | .565 | .512 | .736 |
| P.6.5 | V51 | -.022 | .199 | -.122 | -.281 | -.009 |

| | | P.4.7 V42 | P.4.8 V43 | P.4.9 V44 | P.4.10 V45 | P.6.1 V47 |
|---|---|---|---|---|---|---|
| P.4.7 | V42 | .000 | | | | |
| P.4.8 | V43 | .547 | .000 | | | |
| P.4.9 | V44 | -.214 | -.185 | .000 | | |
| P.4.10 | V45 | -.358 | -.376 | .539 | .000 | |
| P.6.1 | V47 | -.154 | -.302 | .070 | -.198 | .000 |
| P.6.2 | V48 | -.182 | -.498 | -.226 | -.237 | .180 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.6.3 | V49 | -.454 | -.495 | .011 | .109 | -.156 |
| P.6.4 | V50 | -.008 | -.241 | .078 | -.171 | .234 |
| P.6.5 | V51 | .160 | -.160 | .011 | .327 | -.143 |

| | | P.6.2 V48 | P.6.3 V49 | P.6.4 V50 | P.6.5 V51 |
|---|---|---|---|---|---|
| P.6.2 | V48 | .000 | | | |
| P.6.3 | V49 | .130 | .000 | | |
| P.6.4 | V50 | -.147 | -.244 | .000 | |
| P.6.5 | V51 | -.140 | .166 | .126 | .000 |

AVERAGE ABSOLUTE COVARIANCE RESIDUALS = .2401

AVERAGE OFF-DIAGONAL ABSOLUTE COVARIANCE RESIDUALS = .2667

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MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

STANDARDIZED RESIDUAL MATRIX:

| | | P.2.2 V19 | P.2.3 V20 | P.2.4 V21 | P.2.6 V23 | P.3.1 V33 |
|---|---|---|---|---|---|---|
| P.2.2 | V19 | .000 | | | | |
| P.2.3 | V20 | .054 | .000 | | | |
| P.2.4 | V21 | -.033 | -.069 | .000 | | |
| P.2.6 | V23 | -.062 | -.028 | .162 | .000 | |
| P.3.1 | V33 | .023 | .051 | .055 | -.061 | .000 |
| P.3.3 | V35 | -.053 | .016 | -.010 | .030 | .000 |
| P.4.1 | V36 | -.013 | -.002 | .162 | .102 | .163 |
| P.4.2 | V37 | -.064 | -.074 | .074 | .049 | -.032 |
| P.4.3 | V38 | -.122 | -.070 | .069 | .038 | -.003 |
| P.4.4 | V39 | -.074 | -.035 | .125 | .074 | .026 |
| P.4.7 | V42 | .007 | -.066 | .083 | .084 | .002 |
| P.4.8 | V43 | .090 | .044 | .182 | .153 | .012 |
| P.4.9 | V44 | .019 | -.026 | .222 | .134 | .046 |
| P.4.10 | V45 | .006 | -.003 | .052 | .118 | .017 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.6.1 | V47 | -.167 | -.088 | .021 | -.044 | .108 |
| P.6.2 | V48 | -.041 | .000 | .083 | .133 | -.042 |
| P.6.3 | V49 | -.036 | .033 | -.021 | .079 | -.048 |
| P.6.4 | V50 | -.005 | .061 | .176 | .150 | -.022 |
| P.6.5 | V51 | -.066 | .034 | -.015 | .013 | .000 |

| | | P.3.3<br>V35 | P.4.1<br>V36 | P.4.2<br>V37 | P.4.3<br>V38 | P.4.4<br>V39 |
|---|---|---|---|---|---|---|
| P.3.3 | V35 | .000 | | | | |
| P.4.1 | V36 | .141 | .000 | | | |
| P.4.2 | V37 | -.026 | .011 | .000 | | |
| P.4.3 | V38 | .047 | -.002 | .001 | .000 | |
| P.4.4 | V39 | -.038 | -.029 | -.003 | .002 | .000 |
| P.4.7 | V42 | -.047 | .002 | -.050 | -.077 | -.021 |
| P.4.8 | V43 | -.051 | .069 | .021 | -.003 | .051 |
| P.4.9 | V44 | -.039 | .022 | -.021 | -.015 | .052 |
| P.4.10 | V45 | .021 | .077 | .053 | .036 | .059 |
| P.6.1 | V47 | .047 | .043 | -.006 | -.004 | .054 |
| P.6.2 | V48 | -.002 | .068 | .007 | -.008 | .007 |
| P.6.3 | V49 | .022 | .010 | -.010 | .037 | .042 |
| P.6.4 | V50 | -.065 | .070 | .109 | .097 | .139 |
| P.6.5 | V51 | -.004 | .036 | -.023 | -.051 | -.002 |

| | | P.4.7<br>V42 | P.4.8<br>V43 | P.4.9<br>V44 | P.4.10<br>V45 | P.6.1<br>V47 |
|---|---|---|---|---|---|---|
| P.4.7 | V42 | .000 | | | | |
| P.4.8 | V43 | .107 | .000 | | | |
| P.4.9 | V44 | -.040 | -.035 | .000 | | |
| P.4.10 | V45 | -.068 | -.071 | .098 | .000 | |
| P.6.1 | V47 | -.029 | -.057 | .013 | -.037 | .000 |
| P.6.2 | V48 | -.036 | -.099 | -.043 | -.046 | .035 |
| P.6.3 | V49 | -.087 | -.094 | .002 | .020 | -.029 |
| P.6.4 | V50 | -.002 | -.049 | .015 | -.034 | .046 |
| P.6.5 | V51 | .031 | -.031 | .002 | .063 | -.027 |

```
                      P.6.2      P.6.3      P.6.4      P.6.5
                         V48        V49        V50        V51
 P.6.2    V48           .000
 P.6.3    V49           .025       .000
 P.6.4    V50          -.030      -.049       .000
 P.6.5    V51          -.028       .032       .026       .000
```

AVERAGE ABSOLUTE STANDARDIZED RESIDUALS = .0448

AVERAGE OFF-DIAGONAL ABSOLUTE STANDARDIZED RESIDUALS = .0498

LARGEST STANDARDIZED RESIDUALS:

| NO. | PARAMETER | ESTIMATE | NO. | PARAMETER | ESTIMATE |
|---|---|---|---|---|---|
| 1 | V44, V21 | .222 | 11 | V50, V39 | .139 |
| 2 | V43, V21 | .182 | 12 | V44, V23 | .134 |
| 3 | V50, V21 | .176 | 13 | V48, V23 | .133 |
| 4 | V47, V19 | -.167 | 14 | V39, V21 | .125 |
| 5 | V36, V33 | .163 | 15 | V38, V19 | -.122 |
| 6 | V36, V21 | .162 | 16 | V45, V23 | .118 |
| 7 | V23, V21 | .162 | 17 | V50, V37 | .109 |
| 8 | V43, V23 | .153 | 18 | V47, V33 | .108 |
| 9 | V50, V23 | .150 | 19 | V43, V42 | .107 |
| 10 | V36, V35 | .141 | 20 | V36, V23 | .102 |

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MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

DISTRIBUTION OF STANDARDIZED RESIDUALS

```
    ----------------------------------------
    !                                      !
100-                                       -
    !                                      !
    !                                      !
    !                *  *                  !
    !                 *  *                  !            RANGE        FREQ
PERCENT
 75-                 *  *                  -
    !                 *  *                  !     1    -0.5  -  --          0
.00%
    !                 *  *                  !     2    -0.4  -  -0.5        0
.00%
    !                 *  *                  !     3    -0.3  -  -0.4        0
.00%
    !                 *  *                  !     4    -0.2  -  -0.3        0
.00%
```

```
   50-                 *  *                 -    5   -0.1  -  -0.2     2
1.05%
     !                 *  *                 !    6    0.0  -  -0.1    83
43.68%
     !                 *  *                 !    7    0.1  -   0.0    87
45.79%
     !                 *  *                 !    8    0.2  -   0.1    17
8.95%
     !                 *  *                 !    9    0.3  -   0.2     1
.53%
   25-                 *  *                 -    A    0.4  -   0.3     0
.00%
     !                 *  *                 !    B    0.5  -   0.4     0
.00%
     !                 *  *  *              !    C     ++  -   0.5     0
.00%
     !                 *  *  *              !  -----------------------
-------
     !                 *  *  *              !         TOTAL       190
100.00%
     ----------------------------------------
        1  2  3  4  5  6  7  8  9  A  B  C       EACH "*" REPRESENTS  5
RESIDUALS


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)



  GOODNESS OF FIT SUMMARY FOR METHOD = ML

  INDEPENDENCE MODEL CHI-SQUARE        =    2305.727 ON   171 DEGREES OF
FREEDOM

  INDEPENDENCE AIC =  1963.72674   INDEPENDENCE CAIC =  1256.50520
         MODEL AIC =    25.64384          MODEL CAIC =  -569.91113

  CHI-SQUARE =      313.644 BASED ON     144 DEGREES OF FREEDOM
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00000

  THE   NORMAL   THEORY   RLS   CHI-SQUARE   FOR   THIS   ML   SOLUTION   IS
297.697.

  FIT INDICES
  -----------
  BENTLER-BONETT     NORMED FIT INDEX =      .864
  BENTLER-BONETT NON-NORMED FIT INDEX =      .906
  COMPARATIVE FIT INDEX (CFI)         =      .921
  BOLLEN   (IFI) FIT INDEX            =      .922
  MCDONALD (MFI) FIT INDEX            =      .607
  LISREL    GFI  FIT INDEX            =      .844
  LISREL   AGFI  FIT INDEX            =      .794
  ROOT MEAN-SQUARE RESIDUAL (RMR)     =      .341
  STANDARDIZED RMR                    =      .063
```

```
  ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .083
  90% CONFIDENCE INTERVAL OF RMSEA  (        .071,        .096)

  RELIABILITY COEFFICIENTS
  ------------------------
  CRONBACH'S ALPHA                    =      .907
  COEFFICIENT ALPHA FOR AN OPTIMAL SHORT SCALE                =      .959
  BASED ON THE FOLLOWING  3 VARIABLES
  P.4.2     P.4.3     P.4.4
  RELIABILITY COEFFICIENT RHO         =      .948
  GREATEST LOWER BOUND RELIABILITY                            =      .973
  GLB RELIABILITY FOR AN OPTIMAL SHORT SCALE                  =      .976
  BASED ON 16 VARIABLES, ALL EXCEPT:
  P.3.1     P.3.3     P.4.1
  BENTLER'S DIMENSION-FREE LOWER BOUND RELIABILITY            =      .973
  SHAPIRO'S LOWER BOUND RELIABILITY FOR A WEIGHTED COMPOSITE  =      .982
  WEIGHTS THAT ACHIEVE SHAPIRO'S LOWER BOUND:
  P.2.2     P.2.3     P.2.4     P.2.6     P.3.1     P.3.3
      .154      .153      .171      .168      .079      .123
  P.4.1     P.4.2     P.4.3     P.4.4     P.4.7     P.4.8
      .247      .384      .419      .360      .196      .232
  P.4.9     P.4.10    P.6.1     P.6.2     P.6.3     P.6.4
      .236      .226      .154      .165      .215      .179
  P.6.5
      .181


  GOODNESS OF FIT SUMMARY FOR METHOD = ROBUST

  ROBUST INDEPENDENCE MODEL CHI-SQUARE =    2087.596 ON   171 DEGREES OF
FREEDOM

  INDEPENDENCE AIC =  1745.59648   INDEPENDENCE CAIC =  1038.37494
         MODEL AIC =   -52.46509          MODEL CAIC =  -648.02006

  SATORRA-BENTLER SCALED CHI-SQUARE =     235.5349 ON      144 DEGREES OF
FREEDOM
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00000

  FIT INDICES
  -----------
  BENTLER-BONETT     NORMED FIT INDEX =      .887
  BENTLER-BONETT NON-NORMED FIT INDEX =      .943
  COMPARATIVE FIT INDEX (CFI)         =      .952
  BOLLEN   (IFI) FIT INDEX            =      .953
  MCDONALD (MFI) FIT INDEX            =      .764
  ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .061
  90% CONFIDENCE INTERVAL OF RMSEA  (        .047,        .075)


                       ITERATIVE SUMMARY

                    PARAMETER
  ITERATION         ABS CHANGE         ALPHA                FUNCTION
      1              1.885865          .50000               5.64763
      2               .838757         1.00000               1.88195
      3               .042515         1.00000               1.85902
```

```
      4              .016662         1.00000              1.85694
      5              .006332         1.00000              1.85625
      6              .003724         1.00000              1.85601
      7              .001992         1.00000              1.85592
      8              .001305         1.00000              1.85589
      9              .000734         1.00000              1.85588

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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
  (ROBUST STATISTICS IN PARENTHESES)


 P.2.2   =V19 =   1.000 F6    + 1.000 E19


 P.2.3   =V20 =    .902*F6    + 1.000 E20
                   .078
                 11.569@
              (    .075)
              (  12.029@

 P.2.4   =V21 =    .948*F6    + 1.000 E21
                   .107
                  8.894@
              (    .088)
              (  10.752@

 P.2.6   =V23 =    .912*F6    + 1.000 E23
                   .096
                  9.458@
              (    .088)
              (  10.370@

 P.3.1   =V33 =   1.000 F7    + 1.000 E33


 P.3.3   =V35 =   1.393*F7    + 1.000 E35
                   .408
                  3.417@
              (    .397)
              (   3.503@

 P.4.1   =V36 =   1.000 F8    + 1.000 E36
```

```
 P.4.2   =V37 =   1.300*F8    + 1.000 E37
                   .108
                 12.038@
               (   .119)
               ( 10.964@

 P.4.3   =V38 =   1.355*F8    + 1.000 E38
                   .110
                 12.313@
               (   .126)
               ( 10.763@

 P.4.4   =V39 =   1.288*F8    + 1.000 E39
                   .110
                 11.664@
               (   .122)
               ( 10.540@

 P.4.7   =V42 =   1.000 F9    + 1.000 E42



 P.4.8   =V43 =   1.052*F9    + 1.000 E43
                   .084
                 12.537@
               (   .074)
               ( 14.147@
```

MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS (CONTINUED)

```
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)
  (ROBUST STATISTICS IN PARENTHESES)

 P.4.9   =V44 =   1.115*F9    + 1.000 E44
                   .087
                 12.806@
               (   .078)
               ( 14.358@

 P.4.10  =V45 =    .983*F9    + 1.000 E45
                   .088
                 11.176@
               (   .083)
               ( 11.877@

 P.6.1   =V47 =   1.000 F10   + 1.000 E47
```

```
 P.6.2   =V48 =   1.005*F10   + 1.000 E48
                   .100
                 10.031@
               (   .089)
               ( 11.260@

 P.6.3   =V49 =   1.085*F10   + 1.000 E49
                   .104
                 10.446@
               (   .093)
               ( 11.622@

 P.6.4   =V50 =    .907*F10   + 1.000 E50
                   .099
                  9.193@
               (   .092)
               (  9.885@

 P.6.5   =V51 =   1.031*F10   + 1.000 E51
                   .102
                 10.151@
               (   .102)
               ( 10.119@


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  CONSTRUCT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
  (ROBUST STATISTICS IN PARENTHESES)



    F8   =F8  =   1.401*F11   + 1.000 D8
                   .177
                  7.930@
               (   .177)
               (  7.912@

    F9   =F9  =   1.326*F11   + 1.000 D9
                   .168
                  7.877@
               (   .153)
               (  8.683@
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)
```

```
  VARIANCES OF INDEPENDENT VARIABLES
  ----------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                V                                F
               ---                              ---
                              I F6  -   F6              3.144*I
                              I                          .504 I
                              I                         6.231@I
                              I                      (   .543)I
                              I                      (  5.792@I
                              I                               I
                              I F7  -   F7              1.961*I
                              I                          .717 I
                              I                         2.734@I
                              I                      (   .741)I
                              I                      (  2.648@I
                              I                               I
                              I F10 -   F10             3.023*I
                              I                          .555 I
                              I                         5.451@I
                              I                      (   .467)I
                              I                      (  6.476@I
                              I                               I
                              I F11 -   F11             1.000 I
                              I                               I
                              I                               I
                              I                               I
                              I                               I
                              I                               I
```



```
  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES
  ----------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                E                                D
               ---                              ---
 E19 -P.2.2               1.391*I D8  -   F8              1.025*I
                           .239 I                          .309 I
                          5.831@I                         3.312@I
                       (   .426)I                      (   .309)I
                       (  3.266@I                      (  3.315@I
                                I                               I
 E20 -P.2.3               1.018*I D9  -   F9              1.614*I
                           .185 I                          .348 I
                          5.494@I                         4.634@I
                       (   .256)I                      (   .375)I
                       (  3.973@I                      (  4.299@I
                                I                               I
 E21 -P.2.4               3.582*I                               I
                           .443 I                               I
                          8.087@I                               I
```

```
                        (   .503)I                               I
                        (  7.121@I                               I
                                 I                               I
E23 -P.2.6                 2.743*I                               I
                            .350 I                               I
                           7.845@I                               I
                        (   .495)I                               I
                        (  5.542@I                               I
                                 I                               I
E33 -P.3.1                 3.730*I                               I
                            .678 I                               I
                           5.498@I                               I
                        (   .773)I                               I
                        (  4.828@I                               I
                                 I                               I
E35 -P.3.3                 1.779*I                               I
                           1.072 I                               I
                           1.659 I                               I
                        (  1.114)I                               I
                        (  1.597)I                               I
                                 I                               I
E36 -P.4.1                 2.985*I                               I
                            .336 I                               I
                           8.880@I                               I
                        (   .471)I                               I
                        (  6.341@I                               I
                                 I                               I
E37 -P.4.2                  .619*I                               I
                            .100 I                               I
                           6.199@I                               I
                        (   .191)I                               I
                        (  3.237@I                               I
                                 I                               I
E38 -P.4.3                  .366*I                               I
                            .088 I                               I
                           4.177@I                               I
                        (   .276)I                               I
                        (  1.324)I                               I
                                 I                               I
E39 -P.4.4                  .980*I                               I
                            .131 I                               I
                           7.479@I                               I
                        (   .348)I                               I
                        (  2.817@I                               I
                                 I                               I
E42 -P.4.7                 1.746*I                               I
                            .240 I                               I
                           7.286@I                               I
                        (   .276)I                               I
                        (  6.337@I                               I
                                 I                               I
E43 -P.4.8                 1.429*I                               I
                            .217 I                               I
                           6.591@I                               I
                        (   .365)I                               I
                        (  3.918@I                               I
                                 I                               I
```

```
MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

VARIANCES OF INDEPENDENT VARIABLES (CONTINUED)
----------------------------------------------

E44 -P.4.9              1.409*I                                  I
                         .226 I                                  I
                        6.232@I                                  I
                     (   .350)I                                  I
                     (  4.020@I                                  I
                              I                                  I
E45 -P.4.10             2.112*I                                  I
                         .275 I                                  I
                        7.680@I                                  I
                     (   .291)I                                  I
                     (  7.257@I                                  I
                              I                                  I
E47 -P.6.1              2.398*I                                  I
                         .310 I                                  I
                        7.742@I                                  I
                     (   .426)I                                  I
                     (  5.622@I                                  I
                              I                                  I
E48 -P.6.2              1.893*I                                  I
                         .258 I                                  I
                        7.327@I                                  I
                     (   .436)I                                  I
                     (  4.345@I                                  I
                              I                                  I
E49 -P.6.3              1.765*I                                  I
                         .258 I                                  I
                        6.855@I                                  I
                     (   .361)I                                  I
                     (  4.884@I                                  I
                              I                                  I
E50 -P.6.4              2.270*I                                  I
                         .286 I                                  I
                        7.935@I                                  I
                     (   .326)I                                  I
                     (  6.963@I                                  I
                              I                                  I
E51 -P.6.5              1.871*I                                  I
                         .260 I                                  I
                        7.207@I                                  I
                     (   .324)I                                  I
                     (  5.768@I                                  I
                              I                                  I
```

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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  COVARIANCES AMONG INDEPENDENT VARIABLES
  ---------------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                V                                 F
               ---                               ---
                              I F7  -   F7              .257*I
                              I F6  -   F6              .249 I
                              I                        1.030 I
                              I                     (   .284)I
                              I                     (   .902)I
                              I                              I
                              I F10 -   F10            1.038*I
                              I F6  -   F6              .295 I
                              I                        3.512@I
                              I                     (   .287)I
                              I                     (  3.613@I
                              I                              I
                              I F11 -   F11             .887*I
                              I F6  -   F6              .169 I
                              I                        5.262@I
                              I                     (   .163)I
                              I                     (  5.430@I
                              I                              I
                              I F10 -   F10             .811*I
                              I F7  -   F7              .313 I
                              I                        2.594@I
                              I                     (   .353)I
                              I                     (  2.296@I
                              I                              I
                              I F11 -   F11             .607*I
                              I F7  -   F7              .202 I
                              I                        3.002@I
                              I                     (   .207)I
                              I                     (  2.934@I
                              I                              I
                              I F11 -   F11            1.084*I
                              I F10 -   F10             .169 I
                              I                        6.399@I
                              I                     (   .167)I
                              I                     (  6.489@I
                              I                              I


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  DECOMPOSITION OF EFFECTS WITH NONSTANDARDIZED VALUES
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

  PARAMETER TOTAL EFFECTS
```

```
 ----------------------

P.2.2   =V19 =   1.000 F6    + 1.000 E19



P.2.3   =V20 =    .902*F6    + 1.000 E20



P.2.4   =V21 =    .948*F6    + 1.000 E21



P.2.6   =V23 =    .912*F6    + 1.000 E23



P.3.1   =V33 =   1.000 F7    + 1.000 E33



P.3.3   =V35 =   1.393*F7    + 1.000 E35



P.4.1   =V36 =   1.000 F8    + 1.401 F11   + 1.000 E36   + 1.000 D8
                                 .177
                                7.930@
                             (   .177)
                             (  7.912@

P.4.2   =V37 =   1.300*F8    + 1.822 F11   + 1.000 E37   + 1.300 D8
                  .108           .187                        .108
                12.038@         9.732@                     12.038@
              (   .119)      (   .367)                   (   .119)
              ( 10.964@      (  4.959@                   ( 10.964@

P.4.3   =V38 =   1.355*F8    + 1.898 F11   + 1.000 E38   + 1.355 D8
                  .110           .192                        .110
                12.313@         9.902@                     12.313@
              (   .126)      (   .387)                   (   .126)
              ( 10.763@      (  4.899@                   ( 10.763@
```

```
P.4.4   =V39 =   1.288*F8    + 1.805 F11   + 1.000 E39   + 1.288 D8
                  .110          .189                        .110
                11.664@        9.531@                     11.664@
              (   .122)     (   .366)                   (   .122)
              ( 10.540@     (  4.932@                   ( 10.540@

P.4.7   =V42 =   1.000 F9    + 1.326 F11   + 1.000 E42   + 1.000 D9
                                .168
                               7.877@
                            (   .153)
                            (  8.683@

P.4.8   =V43 =   1.052*F9    + 1.394 F11   + 1.000 E43   + 1.052 D9
                  .084          .172                        .084
                12.537@        8.101@                     12.537@
              (   .074)     (   .208)                   (   .074)
              ( 14.147@     (  6.696@                   ( 14.147@

P.4.9   =V44 =   1.115*F9    + 1.478 F11   + 1.000 E44   + 1.115 D9
                  .087          .181                        .087
                12.806@        8.186@                     12.806@
              (   .078)     (   .227)                   (   .078)
              ( 14.358@     (  6.503@                   ( 14.358@

P.4.10  =V45 =    .983*F9    + 1.304 F11   + 1.000 E45   +  .983 D9
                  .088          .170                        .088
                11.176@        7.678@                     11.176@
              (   .083)     (   .206)                   (   .083)
              ( 11.877@     (  6.314@                   ( 11.877@

P.6.1   =V47 =   1.000 F10   + 1.000 E47

P.6.2   =V48 =   1.005*F10   + 1.000 E48

P.6.3   =V49 =   1.085*F10   + 1.000 E49

P.6.4   =V50 =    .907*F10   + 1.000 E50
```

```
 P.6.5   =V51 =   1.031*F10   + 1.000 E51



    F8   =F8  =   1.401*F11   + 1.000 D8



    F9   =F9  =   1.326*F11   + 1.000 D9
```



```
  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  DECOMPOSITION OF EFFECTS WITH NONSTANDARDIZED VALUES
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

  PARAMETER INDIRECT EFFECTS
  --------------------------

 P.4.1   =V36 =   1.401 F11   + 1.000 D8
                   .177
                  7.930@
               (   .177)
               (  7.912@

 P.4.2   =V37 =   1.822 F11   + 1.300 D8
                   .187          .108
                  9.732@       12.038@
               (   .367)     (   .119)
               (  4.959@     ( 10.964@

 P.4.3   =V38 =   1.898 F11   + 1.355 D8
                   .192          .110
                  9.902@       12.313@
               (   .387)     (   .126)
               (  4.899@     ( 10.763@

 P.4.4   =V39 =   1.805 F11   + 1.288 D8
                   .189          .110
                  9.531@       11.664@
               (   .366)     (   .122)
               (  4.932@     ( 10.540@

 P.4.7   =V42 =   1.326 F11   + 1.000 D9
                   .168
                  7.877@
```

```
              (    .153)
              (   8.683@

 P.4.8   =V43 =   1.394 F11   + 1.052 D9
                   .172          .084
                  8.101@       12.537@
              (    .208)     (    .074)
              (   6.696@     (  14.147@

 P.4.9   =V44 =   1.478 F11   + 1.115 D9
                   .181          .087
                  8.186@       12.806@
              (    .227)     (    .078)
              (   6.503@     (  14.358@

 P.4.10  =V45 =   1.304 F11   +  .983 D9
                   .170          .088
                  7.678@       11.176@
              (    .206)     (    .083)
              (   6.314@     (  11.877@


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  DECOMPOSITION OF EFFECTS WITH STANDARDIZED VALUES

  PARAMETER TOTAL EFFECTS
  -----------------------

 P.2.2   =V19 =    .833 F6    +  .554 E19

 P.2.3   =V20 =    .846*F6    +  .534 E20

 P.2.4   =V21 =    .664*F6    +  .748 E21

 P.2.6   =V23 =    .699*F6    +  .715 E23

 P.3.1   =V33 =    .587 F7    +  .810 E33

 P.3.3   =V35 =    .825*F7    +  .565 E35

 P.4.1   =V36 =    .707 F8    +  .573 F11   +  .707 E36   +  .414 D8

 P.4.2   =V37 =    .944*F8    +  .765 F11   +  .330 E37   +  .553 D8

 P.4.3   =V38 =    .968*F8    +  .785 F11   +  .250 E38   +  .567 D8

 P.4.4   =V39 =    .914*F8    +  .741 F11   +  .406 E39   +  .535 D8

 P.4.7   =V42 =    .812 F9    +  .586 F11   +  .584 E42   +  .562 D9

 P.4.8   =V43 =    .850*F9    +  .614 F11   +  .526 E43   +  .588 D9

 P.4.9   =V44 =    .865*F9    +  .625 F11   +  .502 E44   +  .599 D9
```

```
 P.4.10  =V45 =    .779*F9    +  .562 F11   +  .627 E45   +  .539 D9

 P.6.1   =V47 =    .747 F10   +  .665 E47

 P.6.2   =V48 =    .786*F10   +  .619 E48

 P.6.3   =V49 =    .818*F10   +  .576 E49

 P.6.4   =V50 =    .723*F10   +  .691 E50

 P.6.5   =V51 =    .795*F10   +  .607 E51

    F8   =F8  =    .811*F11   +  .586 D8

    F9   =F9  =    .722*F11   +  .692 D9


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  DECOMPOSITION OF EFFECTS WITH STANDARDIZED VALUES

  PARAMETER INDIRECT EFFECTS
  -------------------------

 P.4.1   =V36 =    .573 F11   +  .414 D8

 P.4.2   =V37 =    .765 F11   +  .553 D8

 P.4.3   =V38 =    .785 F11   +  .567 D8

 P.4.4   =V39 =    .741 F11   +  .535 D8

 P.4.7   =V42 =    .586 F11   +  .562 D9

 P.4.8   =V43 =    .614 F11   +  .588 D9

 P.4.9   =V44 =    .625 F11   +  .599 D9

 P.4.10  =V45 =    .562 F11   +  .539 D9


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  STANDARDIZED SOLUTION:                                             R-
SQUARED
```

```
 P.2.2           =V19    =          .833    F6             +    .554    E19
.693
 P.2.3            =V20    =          .846*F6               +    .534    E20
.715
 P.2.4            =V21    =          .664*F6               +    .748    E21
.441
 P.2.6            =V23    =          .699*F6               +    .715    E23
.488
 P.3.1           =V33    =          .587    F7             +    .810    E33
.345
 P.3.3            =V35    =          .825*F7               +    .565    E35
.681
 P.4.1           =V36    =          .707    F8             +    .707    E36
.500
 P.4.2            =V37    =          .944*F8               +    .330    E37
.891
 P.4.3            =V38    =          .968*F8               +    .250    E38
.937
 P.4.4            =V39    =          .914*F8               +    .406    E39
.835
 P.4.7           =V42    =          .812    F9             +    .584    E42
.659
 P.4.8            =V43    =          .850*F9               +    .526    E43
.723
 P.4.9            =V44    =          .865*F9               +    .502    E44
.748
 P.4.10        =V45    =          .779*F9                 +    .627    E45
.607
 P.6.1            =V47    =          .747    F10           +    .665    E47
.558
 P.6.2             =V48    =          .786*F10             +    .619    E48
.617
 P.6.3             =V49    =          .818*F10             +    .576    E49
.669
 P.6.4             =V50    =          .723*F10             +    .691    E50
.523
 P.6.5             =V51    =          .795*F10             +    .607    E51
.632
    F8            =F8        =          .811*F11            +    .586    D8
.657
    F9            =F9        =          .722*F11            +    .692    D9
.521


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  CORRELATIONS AMONG INDEPENDENT VARIABLES
  ---------------------------------------

                 V                                F
                ---                              ---
                               I F7  -   F7                .103*I
                               I F6  -   F6                    I
                               I                               I
                               I F10 -   F10               .337*I
```

```
I F6  -   F6                   I
I                              I
I F11 -   F11             .500*I
I F6  -   F6                   I
I                              I
I F10 -   F10             .333*I
I F7  -   F7                   I
I                              I
I F11 -   F11             .434*I
I F7  -   F7                   I
I                              I
I F11 -   F11             .623*I
I F10 -   F10                  I
I                              I
```

```
 ------------------------------------------------------------------------
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                          E N D   O F   M E T H O D
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MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

WALD TEST (FOR DROPPING PARAMETERS)
ROBUST INFORMATION MATRIX USED IN THIS WALD TEST
MULTIVARIATE WALD TEST BY SIMULTANEOUS PROCESS

| | CUMULATIVE MULTIVARIATE STATISTICS | | | UNIVARIATE INCREMENT | |
|---|---|---|---|---|---|
| STEP | PARAMETER | CHI-SQUARE | D.F. | PROBABILITY | CHI-SQUARE | PROBABILITY |
| 1 | F7,F6 | .814 | 1 | .367 | .814 | .367 |
| 2 | E38,E38 | 2.726 | 2 | .256 | 1.912 | .167 |
| 3 | E35,E35 | 4.205 | 3 | .240 | 1.479 | .224 |
| 4 | F10,F7 | 7.195 | 4 | .126 | 2.990 | .084 |

| | | | | | | |
|---|---|---|---|---|---|---|
| 5 | F7,F7 | 9.789 | 5 | .081 | 2.594 | .107 |
| 6 | F11,F7 | 11.437 | 6 | .076 | 1.648 | .199 |

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MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

LAGRANGE MULTIPLIER TEST (FOR ADDING PARAMETERS)

ORDERED UNIVARIATE TEST STATISTICS:

| NO | CODE | PARAMETER | CHI-SQUARE | PROB. | HANCOCK 144 DF PROB. | PARAMETER CHANGE | STANDARDIZED CHANGE |
|---|---|---|---|---|---|---|---|
| 1 | 2 12 | V36,F7 | 9.131 | .003 | 1.000 | .372 | .109 |
| 2 | 2 20 | V21,F9 | 7.164 | .007 | 1.000 | .260 | .056 |
| 3 | 2 12 | V21,F11 | 6.602 | .010 | 1.000 | .560 | .221 |
| 4 | 2 12 | V47,F6 | 5.904 | .015 | 1.000 | -.207 | -.050 |
| 5 | 2 12 | V19,F10 | 5.681 | .017 | 1.000 | -.180 | -.049 |
| 6 | 2 20 | V21,F8 | 5.498 | .019 | 1.000 | .240 | .055 |
| 7 | 2 20 | V50,F8 | 5.450 | .020 | 1.000 | .206 | .055 |
| 8 | 2 20 | V19,F8 | 4.947 | .026 | 1.000 | -.168 | -.046 |
| 9 | 2 12 | V36,F11 | 4.932 | .026 | 1.000 | .838 | .343 |
| 10 | 2 20 | V23,F9 | 4.886 | .027 | 1.000 | .191 | .045 |
| 11 | 2 12 | V23,F11 | 4.872 | .027 | 1.000 | .428 | .185 |
| 12 | 2 12 | V19,F11 | 4.675 | .031 | 1.000 | -.350 | -.164 |
| 13 | 2 12 | V37,F7 | 4.363 | .037 | 1.000 | -.136 | -.041 |
| 14 | 2 20 | V20,F9 | 4.323 | .038 | 1.000 | -.130 | -.038 |
| 15 | 2 12 | V43,F6 | 4.048 | .044 | 1.000 | .144 | .036 |
| 16 | 2 16 | F9,F6 | 3.850 | .050 | 1.000 | .221 | .068 |
| 17 | 2 16 | F8,F6 | 3.850 | .050 | 1.000 | -.234 | -.076 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 18 | 2 | 12 | V38,F7 | 3.573 | .059 | 1.000 | .114 | .034 |
| 19 | 2 | 12 | V38,F6 | 3.539 | .060 | 1.000 | -.085 | -.020 |
| 20 | 2 | 12 | V50,F6 | 3.532 | .060 | 1.000 | .154 | .040 |
| 21 | 2 | 20 | V42,F8 | 3.520 | .061 | 1.000 | -.165 | -.042 |
| 22 | 2 | 20 | V39,F9 | 3.332 | .068 | 1.000 | .113 | .025 |
| 23 | 2 | 12 | V42,F11 | 3.284 | .070 | 1.000 | -.424 | -.188 |
| 24 | 2 | 12 | V50,F11 | 3.115 | .078 | 1.000 | .365 | .167 |
| 25 | 2 | 12 | V23,F10 | 3.087 | .079 | 1.000 | .160 | .040 |
| 26 | 2 | 20 | V23,F8 | 3.033 | .082 | 1.000 | .158 | .040 |
| 27 | 2 | 12 | V43,F10 | 2.969 | .085 | 1.000 | -.133 | -.034 |
| 28 | 2 | 12 | V39,F11 | 2.904 | .088 | 1.000 | .403 | .165 |
| 29 | 2 | 20 | V38,F9 | 2.860 | .091 | 1.000 | -.085 | -.019 |
| 30 | 2 | 12 | V47,F7 | 2.520 | .112 | 1.000 | .188 | .058 |
| 31 | 2 | 16 | F8,F10 | 2.264 | .132 | 1.000 | .261 | .087 |
| 32 | 2 | 16 | F9,F10 | 2.264 | .132 | 1.000 | -.247 | -.077 |
| 33 | 2 | 12 | V38,F11 | 2.138 | .144 | 1.000 | -.285 | -.118 |
| 34 | 2 | 20 | V45,F8 | 2.005 | .157 | 1.000 | .133 | .033 |
| 35 | 2 | 12 | V36,F6 | 1.852 | .174 | 1.000 | .124 | .029 |
| 36 | 2 | 12 | V19,F7 | 1.848 | .174 | 1.000 | -.128 | -.043 |
| 37 | 2 | 20 | V51,F8 | 1.768 | .184 | 1.000 | -.113 | -.029 |
| 38 | 2 | 12 | V39,F10 | 1.750 | .186 | 1.000 | .081 | .019 |
| 39 | 2 | 12 | V45,F11 | 1.704 | .192 | 1.000 | .325 | .140 |
| 40 | 2 | 12 | V20,F11 | 1.703 | .192 | 1.000 | -.187 | -.099 |
| 41 | 2 | 20 | V20,F8 | 1.551 | .213 | 1.000 | -.083 | -.025 |
| 42 | 2 | 12 | V39,F7 | 1.398 | .237 | 1.000 | -.090 | -.026 |
| 43 | 2 | 12 | V42,F6 | 1.329 | .249 | 1.000 | -.087 | -.022 |
| 44 | 2 | 20 | V36,F9 | 1.324 | .250 | 1.000 | .114 | .025 |
| 45 | 2 | 12 | V50,F7 | 1.316 | .251 | 1.000 | -.130 | -.043 |
| 46 | 2 | 12 | V21,F10 | 1.239 | .266 | 1.000 | .114 | .026 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 47 | 2 | 12 | V39,F6 | 1.158 | .282 | 1.000 | .061 | .014 |
| 48 | 2 | 20 | V35,F9 | 1.124 | .289 | 1.000 | -.167 | -.039 |
| 49 | 2 | 20 | V48,F9 | 1.118 | .290 | 1.000 | -.084 | -.020 |
| 50 | 2 | 12 | V45,F7 | 1.059 | .303 | 1.000 | .112 | .035 |
| 51 | 2 | 20 | V33,F9 | 1.002 | .317 | 1.000 | .148 | .034 |
| 52 | 2 | 12 | V36,F10 | .860 | .354 | 1.000 | .091 | .021 |
| 53 | 2 | 20 | V51,F9 | .779 | .377 | 1.000 | .070 | .017 |
| 54 | 2 | 12 | V44,F10 | .650 | .420 | 1.000 | .064 | .015 |
| 55 | 2 | 12 | V37,F11 | .625 | .429 | 1.000 | -.162 | -.068 |
| 56 | 2 | 12 | V43,F7 | .568 | .451 | 1.000 | -.073 | -.023 |
| 57 | 2 | 16 | F8,F7 | .563 | .453 | 1.000 | .110 | .046 |
| 58 | 2 | 16 | F9,F7 | .563 | .453 | 1.000 | -.104 | -.041 |
| 59 | 2 | 12 | V20,F7 | .457 | .499 | 1.000 | .056 | .021 |
| 60 | 2 | 12 | V42,F7 | .414 | .520 | 1.000 | -.065 | -.021 |
| 61 | 2 | 20 | V43,F8 | .409 | .523 | 1.000 | .054 | .014 |
| 62 | 2 | 12 | V45,F10 | .392 | .531 | 1.000 | .054 | .013 |
| 63 | 2 | 12 | V38,F10 | .390 | .532 | 1.000 | -.031 | -.007 |
| 64 | 2 | 12 | V48,F11 | .360 | .549 | 1.000 | -.119 | -.053 |
| 65 | 2 | 12 | V33,F11 | .357 | .550 | 1.000 | .322 | .135 |
| 66 | 2 | 12 | V35,F11 | .357 | .550 | 1.000 | -.448 | -.190 |
| 67 | 2 | 20 | V49,F9 | .325 | .569 | 1.000 | -.045 | -.011 |
| 68 | 2 | 12 | V48,F6 | .316 | .574 | 1.000 | .044 | .011 |
| 69 | 2 | 12 | V51,F11 | .305 | .581 | 1.000 | -.110 | -.049 |
| 70 | 2 | 20 | V19,F9 | .289 | .591 | 1.000 | -.038 | -.010 |
| 71 | 2 | 12 | V35,F6 | .271 | .603 | 1.000 | -.076 | -.018 |
| 72 | 2 | 12 | V33,F6 | .271 | .603 | 1.000 | .055 | .013 |
| 73 | 2 | 12 | V21,F7 | .226 | .635 | 1.000 | .062 | .017 |
| 74 | 2 | 12 | V37,F10 | .212 | .645 | 1.000 | -.024 | -.006 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 75 | 2 | 12 | V23,F7 | .211 | .646 | 1.000 | .053 | .016 |
| 76 | 2 | 12 | V48,F7 | .189 | .664 | 1.000 | -.047 | -.015 |
| 77 | 2 | 12 | V47,F11 | .176 | .675 | 1.000 | -.090 | -.039 |
| 78 | 2 | 20 | V35,F8 | .162 | .688 | 1.000 | .090 | .022 |
| 79 | 2 | 12 | V44,F6 | .147 | .702 | 1.000 | .028 | .007 |
| 80 | 2 | 20 | V48,F8 | .140 | .709 | 1.000 | -.032 | -.008 |
| 81 | 2 | 12 | V42,F10 | .114 | .735 | 1.000 | -.027 | -.007 |
| 82 | 2 | 12 | V49,F6 | .106 | .744 | 1.000 | .025 | .006 |
| 83 | 2 | 12 | V51,F6 | .097 | .756 | 1.000 | -.024 | -.006 |
| 84 | 2 | 20 | V50,F9 | .087 | .769 | 1.000 | .024 | .006 |
| 85 | 2 | 12 | V43,F11 | .084 | .772 | 1.000 | .065 | .029 |
| 86 | 2 | 12 | V20,F10 | .079 | .779 | 1.000 | .019 | .006 |
| 87 | 2 | 20 | V49,F8 | .072 | .788 | 1.000 | .023 | .006 |
| 88 | 2 | 12 | V44,F11 | .066 | .797 | 1.000 | .060 | .025 |
| 89 | 2 | 12 | V45,F6 | .050 | .822 | 1.000 | -.018 | -.004 |
| 90 | 2 | 20 | V33,F8 | .034 | .854 | 1.000 | -.035 | -.009 |
| 91 | 2 | 20 | V37,F9 | .028 | .866 | 1.000 | -.009 | -.002 |
| 92 | 2 | 20 | V47,F8 | .028 | .866 | 1.000 | -.015 | -.004 |
| 93 | 2 | 12 | V33,F10 | .027 | .869 | 1.000 | -.029 | -.007 |
| 94 | 2 | 12 | V35,F10 | .027 | .869 | 1.000 | .040 | .010 |
| 95 | 2 | 20 | V47,F9 | .022 | .883 | 1.000 | -.013 | -.003 |
| 96 | 2 | 12 | V51,F7 | .017 | .897 | 1.000 | -.014 | -.004 |
| 97 | 2 | 20 | V44,F8 | .013 | .908 | 1.000 | -.010 | -.002 |
| 98 | 2 | 12 | V49,F7 | .010 | .920 | 1.000 | .011 | .003 |
| 99 | 2 | 12 | V37,F6 | .001 | .978 | 1.000 | .001 | .000 |
| 100 | 2 | 12 | V49,F11 | .000 | .985 | 1.000 | .004 | .002 |
| 101 | 2 | 12 | V44,F7 | .000 | .991 | 1.000 | -.001 | .000 |
| 102 | 2 | 22 | F8,F9 | .000 | 1.000 | 1.000 | .000 | .000 |
| 103 | 2 | 0 | V42,F9 | .000 | 1.000 | 1.000 | .000 | .000 |

```
  104     2    0        V36,F8         .000      1.000      1.000        .000
.000
  105     2    0        V47,F10        .000      1.000      1.000        .000
.000
  106     2    0        F11,F11        .000      1.000      1.000        .000
.000
  107     2    0        V33,F7         .000      1.000      1.000        .000
.000
  108     2    0        V19,F6         .000      1.000      1.000        .000
.000
  109     2   10         D9,D8         .000      1.000      1.000        .000
.000
  110     2   22         F9,F8         .000      1.000      1.000        .000
.000


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  MULTIVARIATE LAGRANGE MULTIPLIER TEST BY SIMULTANEOUS PROCESS IN STAGE
1

  PARAMETER SETS (SUBMATRICES) ACTIVE AT THIS STAGE ARE:

     PVV PFV PFF PDD GVV GVF GFV GFF BVF BFF


        CUMULATIVE MULTIVARIATE STATISTICS      UNIVARIATE INCREMENT
        ----------------------------------      -------------------------
-----

HANCOCK'S

SEQUENTIAL
 STEP   PARAMETER   CHI-SQUARE  D.F.   PROB.   CHI-SQUARE   PROB.  D.F.
PROB.
 ----  -----------  ----------  ----   -----   ----------   -----  ----
-----
    1      V36,F7        9.131     1    .003        9.131    .003   144
1.000
    2      V21,F9       16.282     2    .000        7.151    .007   143
1.000
    3      V23,F9       23.253     3    .000        6.971    .008   142
1.000
    4      V47,F6       29.156     4    .000        5.904    .015   141
1.000
    5      V50,F8       33.960     5    .000        4.803    .028   140
1.000

  LAGRANGIAN MULTIPLIER TEST REQUIRED    82102 WORDS OF MEMORY.
  PROGRAM ALLOCATES  2000000 WORDS.
1
  Execution begins at 13:07:06
  Execution ends   at 13:07:07
  Elapsed time =       1.00 seconds
```

# ANEXO XI

# ANALISIS FIABILIDAD INICIAL – RDOS

**Escala: ALL VARIABLES**

**Resumen de procesamiento de casos**

| | | N | % |
|---|---|---|---|
| Casos | Válido | 170 | 100,0 |
| | Excluido[a] | 0 | ,0 |
| | Total | 170 | 100,0 |

a. La eliminación por lista se basa en todas las variables del procedimiento.

**Estadísticas de fiabilidad**

| Alfa de Cronbach | Alfa de Cronbach basada en elementos estandarizados | N de elementos |
|---|---|---|
| ,879 | ,883 | 7 |

**Estadísticas de elemento**

| | Media | Desviación estándar | N |
|---|---|---|---|
| p.9.3 - [Cuenta con clientes satisfechos] | 6,1647 | 1,06418 | 170 |
| p.9.10 - [Innovaciones de producto y/o servicio] | 4,5118 | 1,91919 | 170 |
| p.9.12 - [Rentabilidad sobre ventas] | 4,8235 | 1,69004 | 170 |
| p.9.13 - [Resultado financiero global] | 4,4235 | 1,92693 | 170 |
| p.9.14 - [Relaciones con clientes] | 5,8059 | 1,45666 | 170 |
| p.9.15 - [Relaciones con proveedores] | 5,7588 | 1,46176 | 170 |

| | | | |
|---|---|---|---|
| p.9.9 - [Innovaciones de proceso] | 4,1824 | 1,99013 | 170 |

**Correlación entre elementos entre elementos**

| | p.9.3 - [Cuenta con clientes satisfechos] | p.9.10 - [Innovaciones de producto y/o servicio] | p.9.12 - [Rentabilidad sobre ventas] | p.9.13 - [Resultado financiero global] |
|---|---|---|---|---|
| p.9.3 - [Cuenta con clientes satisfechos] | 1,000 | ,500 | ,408 | ,358 |
| p.9.10 - [Innovaciones de producto y/o servicio] | ,500 | 1,000 | ,632 | ,599 |
| p.9.12 - [Rentabilidad sobre ventas] | ,408 | ,632 | 1,000 | ,806 |
| p.9.13 - [Resultado financiero global] | ,358 | ,599 | ,806 | 1,000 |
| p.9.14 - [Relaciones con clientes] | ,574 | ,559 | ,558 | ,493 |
| p.9.15 - [Relaciones con proveedores] | ,486 | ,403 | ,390 | ,349 |
| p.9.9 - [Innovaciones de proceso] | ,427 | ,733 | ,548 | ,521 |

**Correlación entre elementos entre elementos**

| | p.9.14 - [Relaciones con clientes] | p.9.15 - [Relaciones con proveedores] | p.9.9 - [Innovaciones de proceso] |
|---|---|---|---|
| p.9.3 - [Cuenta con clientes satisfechos] | ,574 | ,486 | ,427 |
| p.9.10 - [Innovaciones de producto y/o servicio] | ,559 | ,403 | ,733 |
| p.9.12 - [Rentabilidad sobre ventas] | ,558 | ,390 | ,548 |
| p.9.13 - [Resultado financiero global] | ,493 | ,349 | ,521 |
| p.9.14 - [Relaciones con clientes] | 1,000 | ,614 | ,474 |
| p.9.15 - [Relaciones con proveedores] | ,614 | 1,000 | ,465 |
| p.9.9 - [Innovaciones de proceso] | ,474 | ,465 | 1,000 |

**Estadísticas de total de elemento**

| | Media de escala si el elemento se ha suprimido | Varianza de escala si el elemento se ha suprimido | Correlación total de elementos corregida | Correlación múltiple al cuadrado |
|---|---|---|---|---|
| p.9.3 - [Cuenta con clientes satisfechos] | 29,5059 | 68,393 | ,573 | ,400 |
| p.9.10 - [Innovaciones de producto y/o servicio] | 31,1588 | 54,371 | ,761 | ,652 |
| p.9.12 - [Rentabilidad sobre ventas] | 30,8471 | 57,574 | ,748 | ,701 |
| p.9.13 - [Resultado financiero global] | 31,2471 | 56,010 | ,689 | ,665 |
| p.9.14 - [Relaciones con clientes] | 29,8647 | 61,703 | ,690 | ,565 |
| p.9.15 - [Relaciones con proveedores] | 29,9118 | 64,483 | ,553 | ,440 |
| p.9.9 - [Innovaciones de proceso] | 31,4882 | 55,103 | ,695 | ,580 |

**Estadísticas de total de elemento**

| | Alfa de Cronbach si el elemento se ha suprimido |
|---|---|
| p.9.3 - [Cuenta con clientes satisfechos] | ,876 |
| p.9.10 - [Innovaciones de producto y/o servicio] | ,849 |
| p.9.12 - [Rentabilidad sobre ventas] | ,851 |
| p.9.13 - [Resultado financiero global] | ,860 |
| p.9.14 - [Relaciones con clientes] | ,860 |
| p.9.15 - [Relaciones con proveedores] | ,875 |
| p.9.9 - [Innovaciones de proceso] | ,859 |

# ANEXO XII

# ANÁLISIS FACTORIAL EXPLORATORIO

# RDOS – PRIMER ORDEN

**Matriz de correlaciones**

| | | p.9.3 - [Cuenta con clientes satisfechos] | p.9.9 - [Innovaciones de proceso] | p.9.10 - [Innovaciones de producto y/o servicio] |
|---|---|---|---|---|
| Correlación | p.9.3 - [Cuenta con clientes satisfechos] | 1,000 | ,427 | ,500 |
| | p.9.9 - [Innovaciones de proceso] | ,427 | 1,000 | ,733 |
| | p.9.10 - [Innovaciones de producto y/o servicio] | ,500 | ,733 | 1,000 |
| | p.9.12 - [Rentabilidad sobre ventas] | ,408 | ,548 | ,632 |
| | p.9.13 - [Resultado financiero global] | ,358 | ,521 | ,599 |
| | p.9.14 - [Relaciones con clientes] | ,574 | ,474 | ,559 |
| | p.9.15 - [Relaciones con proveedores] | ,486 | ,465 | ,403 |
| Sig. (unilateral) | p.9.3 - [Cuenta con clientes satisfechos] | | ,000 | ,000 |
| | p.9.9 - [Innovaciones de proceso] | ,000 | | ,000 |
| | p.9.10 - [Innovaciones de producto y/o servicio] | ,000 | ,000 | |
| | p.9.12 - [Rentabilidad sobre ventas] | ,000 | ,000 | ,000 |
| | p.9.13 - [Resultado financiero global] | ,000 | ,000 | ,000 |
| | p.9.14 - [Relaciones con clientes] | ,000 | ,000 | ,000 |
| | p.9.15 - [Relaciones con proveedores] | ,000 | ,000 | ,000 |

**Matriz de correlaciones**

| | | p.9.12 - [Rentabilidad sobre ventas] | p.9.13 - [Resultado financiero global] | p.9.14 - [Relaciones con clientes] |
|---|---|---|---|---|
| Correlación | p.9.3 - [Cuenta con clientes satisfechos] | ,408 | ,358 | ,574 |
| | p.9.9 - [Innovaciones de proceso] | ,548 | ,521 | ,474 |
| | p.9.10 - [Innovaciones de producto y/o servicio] | ,632 | ,599 | ,559 |
| | p.9.12 - [Rentabilidad sobre ventas] | 1,000 | ,806 | ,558 |
| | p.9.13 - [Resultado financiero global] | ,806 | 1,000 | ,493 |
| | p.9.14 - [Relaciones con clientes] | ,558 | ,493 | 1,000 |
| | p.9.15 - [Relaciones con proveedores] | ,390 | ,349 | ,614 |
| Sig. (unilateral) | p.9.3 - [Cuenta con clientes satisfechos] | ,000 | ,000 | ,000 |
| | p.9.9 - [Innovaciones de proceso] | ,000 | ,000 | ,000 |
| | p.9.10 - [Innovaciones de producto y/o servicio] | ,000 | ,000 | ,000 |
| | p.9.12 - [Rentabilidad sobre ventas] | | ,000 | ,000 |
| | p.9.13 - [Resultado financiero global] | ,000 | | ,000 |
| | p.9.14 - [Relaciones con clientes] | ,000 | ,000 | |
| | p.9.15 - [Relaciones con proveedores] | ,000 | ,000 | ,000 |

**Matriz de correlaciones**

| | | p.9.15 - [Relaciones con proveedores] |
|---|---|---|
| Correlación | p.9.3 - [Cuenta con clientes satisfechos] | ,486 |

| | | |
|---|---|---|
| | p.9.9 - [Innovaciones de proceso] | ,465 |
| | p.9.10 - [Innovaciones de producto y/o servicio] | ,403 |
| | p.9.12 - [Rentabilidad sobre ventas] | ,390 |
| | p.9.13 - [Resultado financiero global] | ,349 |
| | p.9.14 - [Relaciones con clientes] | ,614 |
| | p.9.15 - [Relaciones con proveedores] | 1,000 |
| Sig. (unilateral) | p.9.3 - [Cuenta con clientes satisfechos] | ,000 |
| | p.9.9 - [Innovaciones de proceso] | ,000 |
| | p.9.10 - [Innovaciones de producto y/o servicio] | ,000 |
| | p.9.12 - [Rentabilidad sobre ventas] | ,000 |
| | p.9.13 - [Resultado financiero global] | ,000 |
| | p.9.14 - [Relaciones con clientes] | ,000 |
| | p.9.15 - [Relaciones con proveedores] | |

**Prueba de KMO y Bartlett**

| | | |
|---|---|---|
| Medida Kaiser-Meyer-Olkin de adecuación de muestreo | | ,829 |
| Prueba de esfericidad de Bartlett | Aprox. Chi-cuadrado | 653,646 |
| | gl | 21 |
| | Sig. | ,000 |

**Matrices anti-imagen**

| | | p.9.3 - [Cuenta con clientes satisfechos] | p.9.9 - [Innovaciones de proceso] |
|---|---|---|---|
| Covarianza anti-imagen | p.9.3 - [Cuenta con clientes satisfechos] | ,600 | -,008 |
| | p.9.9 - [Innovaciones de proceso] | -,008 | ,420 |
| | p.9.10 - [Innovaciones de producto y/o servicio] | -,083 | -,208 |
| | p.9.12 - [Rentabilidad sobre ventas] | -,008 | -,021 |
| | p.9.13 - [Resultado financiero global] | ,013 | -,020 |

| | | | |
|---|---|---|---|
| | p.9.14 - [Relaciones con clientes] | -,140 | ,029 |
| | p.9.15 - [Relaciones con proveedores] | -,104 | -,117 |
| Correlación anti-imagen | p.9.3 - [Cuenta con clientes satisfechos] | ,901[a] | -,017 |
| | p.9.9 - [Innovaciones de proceso] | -,017 | ,826[a] |
| | p.9.10 - [Innovaciones de producto y/o servicio] | -,181 | -,544 |
| | p.9.12 - [Rentabilidad sobre ventas] | -,018 | -,060 |
| | p.9.13 - [Resultado financiero global] | ,030 | -,055 |
| | p.9.14 - [Relaciones con clientes] | -,274 | ,067 |
| | p.9.15 - [Relaciones con proveedores] | -,180 | -,241 |

a. Medidas de adecuación de muestreo (MSA)

**Matriz de componente[a]**

| | Componente | | |
|---|---|---|---|
| | 1 | 2 | 3 |
| p.9.10 - [Innovaciones de producto y/o servicio] | ,834 | -,175 | -,353 |
| p.9.12 - [Rentabilidad sobre ventas] | ,819 | -,380 | ,277 |
| p.9.14 - [Relaciones con clientes] | ,793 | ,312 | ,232 |
| p.9.9 - [Innovaciones de proceso] | ,781 | -,115 | -,510 |
| p.9.13 - [Resultado financiero global] | ,778 | -,451 | ,294 |
| p.9.3 - [Cuenta con clientes satisfechos] | ,685 | ,438 | -,042 |
| p.9.15 - [Relaciones con proveedores] | ,673 | ,520 | ,122 |

Método de extracción: análisis de componentes principales.[a]

a. 3 componentes extraídos.

**Comunalidades**

| | Extracción |
|---|---|
| p.9.3 - [Cuenta con clientes satisfechos] | ,663 |
| p.9.9 - [Innovaciones de proceso] | ,883 |
| p.9.10 - [Innovaciones de producto y/o servicio] | ,851 |
| p.9.12 - [Rentabilidad sobre ventas] | ,892 |
| p.9.13 - [Resultado financiero global] | ,896 |
| p.9.14 - [Relaciones con clientes] | ,779 |
| p.9.15 - [Relaciones con proveedores] | ,739 |

Método de extracción: análisis de componentes principales.

**Varianza total explicada**

| Componente | Sumas de extracción de cargas al cuadrado | | | Sumas de rotación de cargas al cuadrado | |
|---|---|---|---|---|---|
| | Total | % de varianza | % acumulado | Total | % de varianza |
| 1 | 4,133 | 59,044 | 59,044 | 2,082 | 29,749 |
| 2 | ,952 | 13,595 | 72,639 | 1,945 | 27,784 |
| 3 | ,618 | 8,833 | 81,472 | 1,676 | 23,939 |

**Varianza total explicada**

| Componente | Sumas de rotación de cargas al cuadrado |
|---|---|
| | % acumulado |
| 1 | 29,749 |
| 2 | 57,533 |
| 3 | 81,472 |

Método de extracción: análisis de componentes principales.

**Matriz de componente rotado**[a]

| | Componente | | |
|---|---|---|---|
| | 1 | 2 | 3 |
| p.9.15 - [Relaciones con proveedores] | ,831 | ,144 | ,166 |
| p.9.14 - [Relaciones con clientes] | ,766 | ,400 | ,182 |
| p.9.3 - [Cuenta con clientes satisfechos] | ,740 | ,113 | ,321 |
| p.9.13 - [Resultado financiero global] | ,183 | ,887 | ,273 |
| p.9.12 - [Rentabilidad sobre ventas] | ,259 | ,859 | ,296 |
| p.9.9 - [Innovaciones de proceso] | ,270 | ,253 | ,864 |
| p.9.10 - [Innovaciones de producto y/o servicio] | ,290 | ,404 | ,777 |

Método de extracción: análisis de componentes principales.
Método de rotación: Varimax con normalización Kaiser.[a]
a. La rotación ha convergido en 5 iteraciones.

**Matriz de transformación de componente**

| Componente | 1 | 2 | 3 |
|---|---|---|---|
| 1 | ,600 | ,585 | ,545 |
| 2 | ,770 | -,607 | -,197 |
| 3 | ,215 | ,538 | -,815 |

Método de extracción: análisis de componentes principales.
Método de rotación: Varimax con normalización Kaiser.

# ANEXO XIII

# ANÁLISIS FACTORIAL CONFIRMATORIO

# RDOS – PRIMER ORDEN

```
  EQS, A STRUCTURAL EQUATION PROGRAM          MULTIVARIATE SOFTWARE, INC.
  COPYRIGHT BY P.M. BENTLER                   VERSION 6.1 (C) 1985 - 2005
(B85).


    PROGRAM CONTROL INFORMATION

        /TITLE
          master confirmatorio rdos
        /SPECIFICATIONS
        VARIABLES= 17 ; CASES= 170 ;
        DATAFILE='C:\tesis1\base rdos.ESS';
          MATRIX=RAW;METHOD=ML,robust;
        /LABELS
        V1=P.9.1; V2=P.9.2; V3=P.9.3; V4=P.9.4; V5=P.9.5;
        V6=P.9.6; V7=P.9.7; V8=P.9.8; V9=P.9.9; V10=P.9.10;
        V11=P.9.11;
        V12=P.9.12; V13=P.9.13; V14=P.9.14; V15=P.9.15;
        V16=P.9.16; V17=P.9.17;
        /EQUATIONS
        V15=F12+ E15;
        V14=*F12+E14;
        V3= F12+E3;
        V13=*F13+E13;
        V12=F13+E12;
        V9=F14+E9;
        V10=*F14+E10;
        /VARIANCES
        E14 TO E15=*; E3=*;
        E12 TO E13=*;
        E9 TO E10=*;
        /COVARIANZAS
        F12,F13=*;
        F12,F14=*;
        F13,F14=*;
        /TECHNICAL
        ITR=100
        /PRINT
        FIT=ALL;
        EFFECT=YES;
        /WTEST
        /LMTEST
        /END


       37 RECORDS OF INPUT MODEL FILE WERE READ


    DATA IS READ FROM C:\tesis1\base rdos.ESS
    THERE ARE  17 VARIABLES AND   170 CASES
    IT IS A RAW DATA ESS FILE
```

SAMPLE STATISTICS BASED ON COMPLETE CASES

UNIVARIATE STATISTICS
---------------------

| VARIABLE | P.9.3 V3 | P.9.9 V9 | P.9.10 V10 | P.9.12 V12 | P.9.13 V13 |
|---|---|---|---|---|---|
| MEAN | 6.1647 | 4.1824 | 4.5118 | 4.8235 | 4.4235 |
| SKEWNESS (G1) | -1.6316 | -.3570 | -.5772 | -.5256 | -.4133 |
| KURTOSIS (G2) | 2.6761 | -.7646 | -.3762 | -.2772 | -.6250 |
| STANDARD DEV. | 1.0642 | 1.9901 | 1.9192 | 1.6900 | 1.9269 |

| VARIABLE | P.9.14 V14 | P.9.15 V15 |
|---|---|---|
| MEAN | 5.8059 | 5.7588 |
| SKEWNESS (G1) | -1.4572 | -1.3098 |
| KURTOSIS (G2) | 2.0533 | 1.3013 |
| STANDARD DEV. | 1.4567 | 1.4618 |

MULTIVARIATE KURTOSIS
---------------------

MARDIA'S COEFFICIENT (G2,P) = 43.8074
NORMALIZED ESTIMATE = 25.4423

ELLIPTICAL THEORY KURTOSIS ESTIMATES
------------------------------------

MARDIA-BASED KAPPA = .6954 MEAN SCALED UNIVARIATE KURTOSIS = .1899

MARDIA-BASED KAPPA IS USED IN COMPUTATION. KAPPA= .6954

CASE NUMBERS WITH LARGEST CONTRIBUTION TO NORMALIZED MULTIVARIATE KURTOSIS:
---------------------------------------------------------------------------

CASE NUMBER 1 22 85 98 169

```
   ESTIMATE         589.6604      384.9274     1223.4268       416.5238
866.4043

24-May-17      PAGE :  3  EQS     Licensee:
  TITLE:    master confirmatorio rdos

  COVARIANCE  MATRIX TO BE ANALYZED:    7 VARIABLES (SELECTED FROM  17
VARIABLES)
  BASED ON   170 CASES.


                       P.9.3      P.9.9      P.9.10     P.9.12     P.9.13
                          V3         V9         V10        V12        V13
     P.9.3    V3        1.132
     P.9.9    V9         .905      3.961
     P.9.10   V10       1.022      2.800      3.683
     P.9.12   V12        .733      1.843      2.049      2.856
     P.9.13    V13           .735        1.999        2.214        2.625
3.713
     P.9.14    V14           .890        1.373        1.561        1.374
1.384
     P.9.15    V15           .756        1.352        1.130         .963
.984


                       P.9.14     P.9.15
                          V14        V15
     P.9.14   V14       2.122
     P.9.15   V15       1.308      2.137



  BENTLER-WEEKS STRUCTURAL REPRESENTATION:

        NUMBER OF DEPENDENT VARIABLES =  7
            DEPENDENT V'S :     3    9   10   12   13   14   15

        NUMBER OF INDEPENDENT VARIABLES = 10
            INDEPENDENT F'S :    12   13   14
            INDEPENDENT E'S :     3    9   10   12   13   14   15

        NUMBER OF FREE PARAMETERS =  16
        NUMBER OF FIXED NONZERO PARAMETERS =  11

 *** WARNING MESSAGES ABOVE, IF ANY, REFER TO THE MODEL PROVIDED.
     CALCULATIONS FOR INDEPENDENCE MODEL NOW BEGIN.

 *** WARNING MESSAGES ABOVE, IF ANY, REFER TO INDEPENDENCE MODEL.
     CALCULATIONS FOR USER'S MODEL NOW BEGIN.


  3RD STAGE OF COMPUTATION REQUIRED     14856 WORDS OF MEMORY.
  PROGRAM ALLOCATED 200000000 WORDS

  DETERMINANT OF INPUT MATRIX IS    .15425D+02

  PARAMETER ESTIMATES APPEAR IN ORDER,
  NO SPECIAL PROBLEMS WERE ENCOUNTERED DURING OPTIMIZATION.
```

RESIDUAL COVARIANCE MATRIX (S-SIGMA) :

| | | P.9.3 V3 | P.9.9 V9 | P.9.10 V10 | P.9.12 V12 | P.9.13 V13 |
|---|---|---|---|---|---|---|
| P.9.3 | V3 | -.126 | | | | |
| P.9.9 | V9 | -.046 | .000 | | | |
| P.9.10 | V10 | -.023 | .000 | .000 | | |
| P.9.12 | V12 | -.123 | -.029 | -.007 | .000 | |
| P.9.13 | V13 | -.172 | .018 | .037 | .000 | .000 |
| P.9.14 | V14 | -.138 | -.068 | -.022 | .077 | .012 |
| P.9.15 | V15 | .077 | .401 | .085 | .107 | .078 |

| | | P.9.14 V14 | P.9.15 V15 |
|---|---|---|---|
| P.9.14 | V14 | .000 | |
| P.9.15 | V15 | .279 | .260 |

AVERAGE ABSOLUTE COVARIANCE RESIDUALS = .0780
AVERAGE OFF-DIAGONAL ABSOLUTE COVARIANCE RESIDUALS = .0857

STANDARDIZED RESIDUAL MATRIX:

| | | P.9.3 V3 | P.9.9 V9 | P.9.10 V10 | P.9.12 V12 | P.9.13 V13 |
|---|---|---|---|---|---|---|
| P.9.3 | V3 | -.111 | | | | |
| P.9.9 | V9 | -.022 | .000 | | | |
| P.9.10 | V10 | -.011 | .000 | .000 | | |
| P.9.12 | V12 | -.068 | -.009 | -.002 | .000 | |
| P.9.13 | V13 | -.084 | .005 | .010 | .000 | .000 |
| P.9.14 | V14 | -.089 | -.023 | -.008 | .031 | .004 |
| P.9.15 | V15 | .050 | .138 | .030 | .043 | .028 |

| | | P.9.14 V14 | P.9.15 V15 |
|---|---|---|---|
| P.9.14 | V14 | .000 | |
| P.9.15 | V15 | .131 | .122 |

AVERAGE ABSOLUTE STANDARDIZED RESIDUALS = .0364

```
        AVERAGE  OFF-DIAGONAL  ABSOLUTE  STANDARDIZED  RESIDUALS        =
.0375


 24-May-17      PAGE :  4  EQS     Licensee:
  TITLE:    master confirmatorio rdos

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  LARGEST STANDARDIZED RESIDUALS:

      NO.    PARAMETER   ESTIMATE      NO.    PARAMETER   ESTIMATE
      ---    ---------   --------      ---    ---------   --------
       1     V15, V9         .138      11     V15, V10        .030
       2     V15, V14        .131      12     V15, V13        .028
       3     V15, V15        .122      13     V14, V9        -.023
       4     V3,  V3        -.111      14     V9,  V3        -.022
       5     V14, V3        -.089      15     V10, V3        -.011
       6     V13, V3        -.084      16     V13, V10        .010
       7     V12, V3        -.068      17     V12, V9        -.009
       8     V15, V3         .050      18     V14, V10       -.008
       9     V15, V12        .043      19     V13, V9         .005
      10     V14, V12        .031      20     V14, V13        .004



  DISTRIBUTION OF STANDARDIZED RESIDUALS


     ----------------------------------------
     !                                      !
   20-                                      -
     !                                      !
     !                                      !
     !                                      !
     !                                       !            RANGE       FREQ
PERCENT
   15-                                      -
     !                    *                  !    1    -0.5  -  --         0
.00%
     !                    *                  !    2    -0.4  -  -0.5       0
.00%
     !                    *                  !    3    -0.3  -  -0.4       0
.00%
     !                    *                  !    4    -0.2  -  -0.3       0
.00%
   10-                 *  *                  -    5    -0.1  -  -0.2       1
3.57%
     !                 *  *                  !    6     0.0  -  -0.1      10
35.71%
     !                 *  *                  !    7     0.1  -   0.0      14
50.00%
     !                 *  *                  !    8     0.2  -   0.1       3
10.71%
     !                 *  *                  !    9     0.3  -   0.2       0
.00%
```

```
   5-                 *  *                 -    A    0.4  -   0.3     0
.00%
     !                *  *                 !    B    0.5  -   0.4     0
.00%
     !                *  *  *              !    C     ++  -   0.5     0
.00%
     !                *  *  *              !    ------------------------
-------
     !             *  *  *  *              !           TOTAL        28
100.00%
     ----------------------------------------
        1  2  3  4  5  6  7  8  9  A  B  C      EACH "*" REPRESENTS  1
RESIDUALS

24-May-17      PAGE :  5  EQS     Licensee:
  TITLE:    master confirmatorio rdos

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)



  GOODNESS OF FIT SUMMARY FOR METHOD = ML

  INDEPENDENCE MODEL CHI-SQUARE        =     666.128 ON    21 DEGREES OF
FREEDOM

  INDEPENDENCE AIC =   624.12816   INDEPENDENCE CAIC =   537.27639
         MODEL AIC =    -2.19903          MODEL CAIC =   -51.82861

  CHI-SQUARE =       21.801 BASED ON      12 DEGREES OF FREEDOM
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .03981

  THE   NORMAL   THEORY   RLS   CHI-SQUARE   FOR   THIS   ML   SOLUTION   IS
20.634.

  FIT INDICES
  -----------
  BENTLER-BONETT     NORMED FIT INDEX =      .967
  BENTLER-BONETT NON-NORMED FIT INDEX =      .973
  COMPARATIVE FIT INDEX (CFI)         =      .985
  BOLLEN   (IFI) FIT INDEX            =      .985
  MCDONALD (MFI) FIT INDEX            =      .972
  LISREL    GFI  FIT INDEX            =      .966
  LISREL   AGFI  FIT INDEX            =      .921
  ROOT MEAN-SQUARE RESIDUAL (RMR)     =      .124
  STANDARDIZED RMR                    =      .057
  ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .070
  90% CONFIDENCE INTERVAL OF RMSEA  (        .015,        .115)

  RELIABILITY COEFFICIENTS
  ------------------------
  CRONBACH'S ALPHA                    =      .879
  COEFFICIENT ALPHA FOR AN OPTIMAL SHORT SCALE                =      .879
  BASED ON ALL VARIABLES
  RELIABILITY COEFFICIENT RHO         =      .928
  GREATEST LOWER BOUND RELIABILITY                            =      .941
  GLB RELIABILITY FOR AN OPTIMAL SHORT SCALE                  =      .941
  BASED ON ALL VARIABLES
```

```
  BENTLER'S DIMENSION-FREE LOWER BOUND RELIABILITY           =      .941
  SHAPIRO'S LOWER BOUND RELIABILITY FOR A WEIGHTED COMPOSITE  =      .945
  WEIGHTS THAT ACHIEVE SHAPIRO'S LOWER BOUND:
  P.9.3     P.9.9     P.9.10    P.9.12    P.9.13    P.9.14
      .192      .415      .447      .442      .457      .330
  P.9.15
      .279


  GOODNESS OF FIT SUMMARY FOR METHOD = ROBUST

  ROBUST INDEPENDENCE MODEL CHI-SQUARE =     475.035 ON    21 DEGREES OF
FREEDOM

  INDEPENDENCE AIC =   433.03454   INDEPENDENCE CAIC =   346.18277
         MODEL AIC =    -9.76015          MODEL CAIC =   -59.38973

  SATORRA-BENTLER SCALED CHI-SQUARE =     14.2399 ON      12 DEGREES OF
FREEDOM
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .28565

  RESIDUAL-BASED TEST STATISTIC                        =    16.166
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .18375

  YUAN-BENTLER RESIDUAL-BASED TEST STATISTIC           =    14.762
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .25470

  YUAN-BENTLER RESIDUAL-BASED F-STATISTIC     =      1.259
  DEGREES OF FREEDOM  =                          12,   158
  PROBABILITY VALUE FOR THE F-STATISTIC IS          .24785

  FIT INDICES
  -----------
  BENTLER-BONETT     NORMED FIT INDEX =      .970
  BENTLER-BONETT NON-NORMED FIT INDEX =      .991
  COMPARATIVE FIT INDEX (CFI)         =      .995
  BOLLEN   (IFI) FIT INDEX            =      .995
  MCDONALD (MFI) FIT INDEX            =      .993
  ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .033
  90% CONFIDENCE INTERVAL OF RMSEA  (       .000,       .088)


                       ITERATIVE SUMMARY

                   PARAMETER
  ITERATION        ABS CHANGE         ALPHA              FUNCTION
      1             1.293188        1.00000               .25663
      2              .181957        1.00000               .13512
      3              .026601        1.00000               .12915
      4              .002871        1.00000               .12901
      5              .001005        1.00000               .12900
      6              .000151        1.00000               .12900
```

MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
(ROBUST STATISTICS IN PARENTHESES)

```
P.9.3   =V3  =   1.000 F12   + 1.000 E3



P.9.9   =V9  =   1.000 F14   + 1.000 E9



P.9.10  =V10 =   1.099*F14   + 1.000 E10
                  .095
                11.571@
              (   .096)
              ( 11.416@

P.9.12  =V12 =   1.000 F13   + 1.000 E12



P.9.13  =V13 =   1.059*F13   + 1.000 E13
                  .078
                13.566@
              (   .086)
              ( 12.319@

P.9.14  =V14 =   1.515*F12   + 1.000 E14
                  .144
                10.517@
              (   .192)
              (  7.880@

P.9.15  =V15 =   1.000 F12   + 1.000 E15
```

```
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES
  ----------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                V                                F
               ---                              ---
                              I F12 -   F12              .679*I
                              I                          .116 I
                              I                         5.845@I
                              I                      (   .148)I
                              I                      (  4.577@I
                              I                               I
                              I F13 -   F13             2.480*I
                              I                          .335 I
                              I                         7.397@I
                              I                      (   .336)I
                              I                      (  7.371@I
                              I                               I
                              I F14 -   F14             2.548*I
                              I                          .431 I
                              I                         5.911@I
                              I                      (   .408)I
                              I                      (  6.250@I
                              I                               I

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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES
  ----------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                E                                D
               ---                              ---
 E3  -P.9.3               .580*I                              I
                          .081 I                              I
                         7.122@I                              I
                      (   .109)I                              I
                      (  5.325@I                              I
                               I                              I
 E9  -P.9.9              1.413*I                              I
                          .218 I                              I
                         6.487@I                              I
                      (   .380)I                              I
                      (  3.715@I                              I
                               I                              I
 E10 -P.9.10              .607*I                              I
                          .198 I                              I
                         3.072@I                              I
                      (   .188)I                              I
                      (  3.235@I                              I
```

```
                          I                                I
 E12 -P.9.12          .376*I                                I
                      .139 I                                I
                     2.715@I                                I
                   (   .193)I                               I
                   (  1.951)I                               I
                          I                                I
 E13 -P.9.13          .934*I                                I
                      .180 I                                I
                     5.192@I                                I
                   (   .318)I                               I
                   (  2.940@I                               I
                          I                                I
 E14 -P.9.14          .564*I                                I
                      .130 I                                I
                     4.325@I                                I
                   (   .184)I                               I
                   (  3.061@I                               I
                          I                                I
 E15 -P.9.15         1.198*I                                I
                      .144 I                                I
                     8.307@I                                I
                   (   .273)I                               I
                   (  4.391@I                               I
                          I                                I

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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  COVARIANCES AMONG INDEPENDENT VARIABLES
  ---------------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                  V                                F
                 ---                              ---
                          I F13 -   F13                .856*I
                          I F12 -   F12                .144 I
                          I                           5.954@I
                          I                         (   .151)I
                          I                         (  5.662@I
                          I                                I
                          I F14 -   F14                .951*I
                          I F12 -   F12                .163 I
                          I                           5.850@I
                          I                         (   .166)I
                          I                         (  5.719@I
                          I                                I
                          I F14 -   F14               1.872*I
                          I F13 -   F13                .290 I
                          I                           6.454@I
                          I                         (   .278)I
                          I                         (  6.739@I
                          I                                I

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```

```
 MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

 DECOMPOSITION OF EFFECTS WITH NONSTANDARDIZED VALUES
 STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

 PARAMETER TOTAL EFFECTS
 -----------------------

P.9.3   =V3  =   1.000 F12   + 1.000 E3


P.9.9   =V9  =   1.000 F14   + 1.000 E9


P.9.10  =V10 =   1.099*F14   + 1.000 E10


P.9.12  =V12 =   1.000 F13   + 1.000 E12


P.9.13  =V13 =   1.059*F13   + 1.000 E13


P.9.14  =V14 =   1.515*F12   + 1.000 E14


P.9.15  =V15 =   1.000 F12   + 1.000 E15


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 MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

 DECOMPOSITION OF EFFECTS WITH STANDARDIZED VALUES
```

```
  PARAMETER TOTAL EFFECTS
  -----------------------

 P.9.3   =V3  =    .734 F12   +  .679 E3

 P.9.9   =V9  =    .802 F14   +  .597 E9

 P.9.10  =V10 =    .914*F14   +  .406 E10

 P.9.12  =V12 =    .932 F13   +  .363 E12

 P.9.13  =V13 =    .865*F13   +  .501 E13

 P.9.14  =V14 =    .857*F12   +  .515 E14

 P.9.15  =V15 =    .601 F12   +  .799 E15

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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  STANDARDIZED SOLUTION:                                              R-
SQUARED



 P.9.3          =V3       =          .734    F12          +    .679    E3
.539
 P.9.9          =V9       =          .802    F14          +    .597    E9
.643
 P.9.10        =V10     =            .914*F14            +     .406     E10
.835
 P.9.12       =V12     =            .932     F13          +     .363     E12
.868
 P.9.13        =V13     =            .865*F13            +     .501     E13
.749
 P.9.14        =V14     =            .857*F12            +     .515     E14
.734
 P.9.15       =V15     =            .601     F12          +     .799     E15
.362

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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  CORRELATIONS AMONG INDEPENDENT VARIABLES
  ---------------------------------------

                V                                F
               ---                              ---
                            I F13 -   F13              .660*I
                            I F12 -   F12                   I
                            I                               I
                            I F14 -   F14              .723*I
                            I F12 -   F12                   I
```

```
                                            I                                I
                                            I F14 -   F14              .745*I
                                            I F13 -   F13                   I
                                            I                                I
```

```
 ------------------------------------------------------------------------
-------
                          E N D    O F    M E T H O D
 ------------------------------------------------------------------------
-------
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  WALD TEST (FOR DROPPING PARAMETERS)
  ROBUST INFORMATION MATRIX USED IN THIS WALD TEST
  MULTIVARIATE WALD TEST BY SIMULTANEOUS PROCESS



         CUMULATIVE  MULTIVARIATE  STATISTICS                   UNIVARIATE
INCREMENT
         ----------------------------------              ----------------
----

  STEP   PARAMETER    CHI-SQUARE   D.F.   PROBABILITY          CHI-SQUARE
PROBABILITY
  ---- -----------  ----------  ----  -----------       ----------  -----
------

    1     E12,E12        3.807       1        .051                3.807
.051

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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  LAGRANGE MULTIPLIER TEST (FOR ADDING PARAMETERS)


  ORDERED UNIVARIATE TEST STATISTICS:
                                                            HANCOCK
STANDAR-
                                 CHI-                    12  DF    PARAMETER
DIZED
   NO     CODE       PARAMETER        SQUARE       PROB.      PROB.      CHANGE
CHANGE
```

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 1 | 2 | 0 | V3,F12 | 6.554 | .010 | .886 | -.357 | -.386 |
| 2 | 2 | 0 | V15,F12 | 6.554 | .010 | .886 | .357 | .316 |
| 3 | 2 | 12 | V3,F13 | 4.140 | .042 | .981 | -.119 | -.067 |
| 4 | 2 | 12 | V14,F13 | 2.270 | .132 | .999 | .175 | .076 |
| 5 | 2 | 12 | V15,F14 | 2.262 | .133 | .999 | .100 | .046 |
| 6 | 2 | 12 | V15,F13 | .994 | .319 | 1.000 | .065 | .030 |
| 7 | 2 | 12 | V13,F12 | .869 | .351 | 1.000 | -.258 | -.163 |
| 8 | 2 | 12 | V12,F12 | .869 | .351 | 1.000 | .244 | .175 |
| 9 | 2 | 12 | V13,F14 | .869 | .351 | 1.000 | .295 | .096 |
| 10 | 2 | 12 | V12,F14 | .869 | .351 | 1.000 | -.278 | -.103 |
| 11 | 2 | 12 | V3,F14 | .845 | .358 | 1.000 | -.057 | -.032 |
| 12 | 2 | 12 | V14,F14 | .579 | .447 | 1.000 | -.114 | -.049 |
| 13 | 2 | 12 | V9,F13 | .081 | .776 | 1.000 | -.061 | -.020 |
| 14 | 2 | 12 | V9,F12 | .081 | .776 | 1.000 | .101 | .062 |
| 15 | 2 | 12 | V10,F12 | .081 | .776 | 1.000 | -.111 | -.070 |
| 16 | 2 | 12 | V10,F13 | .081 | .776 | 1.000 | .067 | .022 |
| 17 | 2 | 0 | V12,F13 | .000 | 1.000 | 1.000 | .000 | .000 |
| 18 | 2 | 0 | V9,F14 | .000 | 1.000 | 1.000 | .000 | .000 |



TITLE: master confirmatorio rdos

MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

MULTIVARIATE LAGRANGE MULTIPLIER TEST BY SIMULTANEOUS PROCESS IN STAGE 1

PARAMETER SETS (SUBMATRICES) ACTIVE AT THIS STAGE ARE:

PVV PFV PFF PDD GVV GVF GFV GFF BVF BFF

CUMULATIVE MULTIVARIATE STATISTICS UNIVARIATE INCREMENT

HANCOCK'S

```
SEQUENTIAL
 STEP   PARAMETER   CHI-SQUARE  D.F.   PROB.   CHI-SQUARE   PROB.  D.F.
PROB.
 ----  -----------  ----------  ----   -----   ----------   -----  ----
-----
    1       V3,F12       6.554     1    .010        6.554    .010    12
.886


  LAGRANGIAN MULTIPLIER TEST REQUIRED     5397 WORDS OF MEMORY.
  PROGRAM ALLOCATES ******** WORDS.
1
  Execution begins at 10:06:21
  Execution ends   at 10:06:21
```

# ANEXO XIV

# ANÁLISIS FACTORIAL CONFIRMATORIO

# RDOS – SEGUNDO ORDEN

```
EQS, A STRUCTURAL EQUATION PROGRAM          MULTIVARIATE SOFTWARE, INC.
  COPYRIGHT BY P.M. BENTLER                   VERSION 6.1 (C) 1985 - 2005
(B85).


    PROGRAM CONTROL INFORMATION

        /TITLE
          master confirmatorio rdos
        /SPECIFICATIONS
        VARIABLES= 17 ; CASES= 170 ;
        DATAFILE='C:\tesis1\base rdos.ESS';
          MATRIX=RAW;METHOD=ML,robust;
        /LABELS
        V1=P.9.1; V2=P.9.2; V3=P.9.3; V4=P.9.4; V5=P.9.5;
        V6=P.9.6; V7=P.9.7; V8=P.9.8; V9=P.9.9; V10=P.9.10;
        V11=P.9.11;
        V12=P.9.12; V13=P.9.13; V14=P.9.14; V15=P.9.15;
        V16=P.9.16; V17=P.9.17;

        /EQUATIONS
        V15=F12+ E15;
        V14=*F12+E14;
        V3= F12+E3;
        V13=*F13+E13;
        V12=F13+E12;
        V9=F14+E9;
        V10=*F14+E10;
        F12=*F15+D12;
        F13=*F15+D13;
        F14=F15+D14;

        /VARIANCES
        E14 TO E15=*; E3=*;
        E12 TO E13=*;
        E9 TO E10=*;
        D12 TO D14=*;
        F15=*;
        /COVARIANZAS
        /TECHNICAL
        ITR=100
        /PRINT
        FIT=ALL;
        EFFECT=YES;
        /WTEST
        /LMTEST
        /END


       40 RECORDS OF INPUT MODEL FILE WERE READ


    DATA IS READ FROM C:\tesis1\base rdos.ESS
    THERE ARE  17 VARIABLES AND   170 CASES
```

IT IS A RAW DATA ESS FILE

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SAMPLE STATISTICS BASED ON COMPLETE CASES

UNIVARIATE STATISTICS
---------------------

| VARIABLE | P.9.3 V3 | P.9.9 V9 | P.9.10 V10 | P.9.12 V12 | P.9.13 V13 |
|---|---|---|---|---|---|
| MEAN | 6.1647 | 4.1824 | 4.5118 | 4.8235 | 4.4235 |
| SKEWNESS (G1) | -1.6316 | -.3570 | -.5772 | -.5256 | -.4133 |
| KURTOSIS (G2) | 2.6761 | -.7646 | -.3762 | -.2772 | -.6250 |
| STANDARD DEV. | 1.0642 | 1.9901 | 1.9192 | 1.6900 | 1.9269 |

| VARIABLE | P.9.14 V14 | P.9.15 V15 |
|---|---|---|
| MEAN | 5.8059 | 5.7588 |
| SKEWNESS (G1) | -1.4572 | -1.3098 |
| KURTOSIS (G2) | 2.0533 | 1.3013 |
| STANDARD DEV. | 1.4567 | 1.4618 |

MULTIVARIATE KURTOSIS
---------------------

MARDIA'S COEFFICIENT (G2,P) = 43.8074
NORMALIZED ESTIMATE = 25.4423

ELLIPTICAL THEORY KURTOSIS ESTIMATES
------------------------------------

MARDIA-BASED KAPPA = .6954 MEAN SCALED UNIVARIATE KURTOSIS = .1899

MARDIA-BASED KAPPA IS USED IN COMPUTATION. KAPPA= .6954

CASE NUMBERS WITH LARGEST CONTRIBUTION TO NORMALIZED MULTIVARIATE KURTOSIS:
---------------------------------------------------------------------------

```
   CASE NUMBER         1           22           85           98
169

   ESTIMATE       589.6604     384.9274    1223.4268     416.5238
866.4043


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  COVARIANCE  MATRIX TO BE ANALYZED:   7 VARIABLES (SELECTED FROM  17
VARIABLES)
  BASED ON   170 CASES.


                       P.9.3      P.9.9      P.9.10     P.9.12     P.9.13
                          V3         V9         V10        V12        V13
     P.9.3    V3         1.132
     P.9.9    V9          .905      3.961
     P.9.10   V10        1.022      2.800      3.683
     P.9.12   V12         .733      1.843      2.049      2.856
     P.9.13   V13         .735      1.999      2.214      2.625
3.713
     P.9.14   V14         .890      1.373      1.561      1.374
1.384
     P.9.15   V15         .756      1.352      1.130       .963
.984


                       P.9.14     P.9.15
                          V14        V15
     P.9.14   V14        2.122
     P.9.15   V15        1.308      2.137



  BENTLER-WEEKS STRUCTURAL REPRESENTATION:

        NUMBER OF DEPENDENT VARIABLES = 10
            DEPENDENT V'S :     3    9   10   12   13   14   15
            DEPENDENT F'S :    12   13   14

        NUMBER OF INDEPENDENT VARIABLES = 11
            INDEPENDENT F'S :    15
            INDEPENDENT E'S :     3    9   10   12   13   14   15
            INDEPENDENT D'S :    12   13   14

        NUMBER OF FREE PARAMETERS =  16
        NUMBER OF FIXED NONZERO PARAMETERS =  15

 *** WARNING MESSAGES ABOVE, IF ANY, REFER TO THE MODEL PROVIDED.
     CALCULATIONS FOR INDEPENDENCE MODEL NOW BEGIN.

 *** WARNING MESSAGES ABOVE, IF ANY, REFER TO INDEPENDENCE MODEL.
     CALCULATIONS FOR USER'S MODEL NOW BEGIN.


  3RD STAGE OF COMPUTATION REQUIRED     15562 WORDS OF MEMORY.
```

PROGRAM ALLOCATED 200000000 WORDS

DETERMINANT OF INPUT MATRIX IS .15425D+02

PARAMETER ESTIMATES APPEAR IN ORDER,
NO SPECIAL PROBLEMS WERE ENCOUNTERED DURING OPTIMIZATION.

RESIDUAL COVARIANCE MATRIX (S-SIGMA) :

| | | P.9.3 V3 | P.9.9 V9 | P.9.10 V10 | P.9.12 V12 | P.9.13 V13 |
|---|---|---|---|---|---|---|
| P.9.3 | V3 | -.126 | | | | |
| P.9.9 | V9 | -.046 | .000 | | | |
| P.9.10 | V10 | -.023 | .000 | .000 | | |
| P.9.12 | V12 | -.123 | -.029 | -.007 | .000 | |
| P.9.13 | V13 | -.172 | .018 | .037 | .000 | .000 |
| P.9.14 | V14 | -.138 | -.068 | -.022 | .077 | .012 |
| P.9.15 | V15 | .077 | .401 | .085 | .107 | .078 |

| | | P.9.14 V14 | P.9.15 V15 |
|---|---|---|---|
| P.9.14 | V14 | .000 | |
| P.9.15 | V15 | .279 | .260 |

AVERAGE ABSOLUTE COVARIANCE RESIDUALS = .0781
AVERAGE OFF-DIAGONAL ABSOLUTE COVARIANCE RESIDUALS = .0857

STANDARDIZED RESIDUAL MATRIX:

| | | P.9.3 V3 | P.9.9 V9 | P.9.10 V10 | P.9.12 V12 | P.9.13 V13 |
|---|---|---|---|---|---|---|
| P.9.3 | V3 | -.111 | | | | |
| P.9.9 | V9 | -.022 | .000 | | | |
| P.9.10 | V10 | -.011 | .000 | .000 | | |
| P.9.12 | V12 | -.068 | -.009 | -.002 | .000 | |
| P.9.13 | V13 | -.084 | .005 | .010 | .000 | .000 |
| P.9.14 | V14 | -.089 | -.024 | -.008 | .031 | .004 |
| P.9.15 | V15 | .050 | .138 | .030 | .043 | .028 |

| | | P.9.14 V14 | P.9.15 V15 |
|---|---|---|---|
| P.9.14 | V14 | .000 | |

```
    P.9.15   V15         .131       .122


                   AVERAGE ABSOLUTE STANDARDIZED RESIDUALS     =
.0364
       AVERAGE OFF-DIAGONAL ABSOLUTE STANDARDIZED RESIDUALS     =
.0375


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  LARGEST STANDARDIZED RESIDUALS:

      NO.     PARAMETER   ESTIMATE      NO.     PARAMETER   ESTIMATE
      ---     ---------   --------      ---     ---------   --------
       1      V15, V9         .138      11      V15, V10        .030
       2      V15, V14        .131      12      V15, V13        .028
       3      V15, V15        .122      13      V14, V9        -.024
       4      V3,  V3        -.111      14      V9,  V3        -.022
       5      V14, V3        -.089      15      V10, V3        -.011
       6      V13, V3        -.084      16      V13, V10        .010
       7      V12, V3        -.068      17      V12, V9        -.009
       8      V15, V3         .050      18      V14, V10       -.008
       9      V15, V12        .043      19      V13, V9         .005
      10      V14, V12        .031      20      V14, V13        .004


  DISTRIBUTION OF STANDARDIZED RESIDUALS


     ----------------------------------------
     !                                      !
   20-                                      -
     !                                      !
     !                                      !
     !                                      !
     !                                      !            RANGE      FREQ
PERCENT
   15-                  *                   -
     !                  *                   !    1   -0.5  -  --        0
.00%
     !                  *                   !    2   -0.4  -  -0.5      0
.00%
     !                  *                   !    3   -0.3  -  -0.4      0
.00%
     !                  *                   !    4   -0.2  -  -0.3      0
.00%
   10-                  *                   -    5   -0.1  -  -0.2      1
3.57%
     !               *  *                   !    6    0.0  -  -0.1      9
32.14%
```

```
     !                 *  *                ! 7   0.1  -  0.0   15
53.57%
     !                 *  *                ! 8   0.2  -  0.1    3
10.71%
     !                 *  *                ! 9   0.3  -  0.2    0
.00%
    5-                 *  *                - A   0.4  -  0.3    0
.00%
     !                 *  *                ! B   0.5  -  0.4    0
.00%
     !                 *  *  *             ! C    ++  -  0.5    0
.00%
     !                 *  *  *             ! ------------------------
-------
     !              *  *  *  *             !         TOTAL     28
100.00%
     ----------------------------------------
        1  2  3  4  5  6  7  8  9  A  B  C     EACH "*" REPRESENTS  1
RESIDUALS


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)



  GOODNESS OF FIT SUMMARY FOR METHOD = ML

  INDEPENDENCE MODEL CHI-SQUARE        =     666.128 ON    21 DEGREES OF
FREEDOM

  INDEPENDENCE AIC =   624.12816   INDEPENDENCE CAIC =   537.27639
         MODEL AIC =    -2.19903           MODEL CAIC =   -51.82861

  CHI-SQUARE =       21.801 BASED ON      12 DEGREES OF FREEDOM
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .03981

  THE NORMAL THEORY RLS CHI-SQUARE FOR THIS ML SOLUTION IS
20.635.

  FIT INDICES
  -----------
  BENTLER-BONETT     NORMED FIT INDEX =      .967
  BENTLER-BONETT NON-NORMED FIT INDEX =      .973
  COMPARATIVE FIT INDEX (CFI)         =      .985
  BOLLEN   (IFI) FIT INDEX            =      .985
  MCDONALD (MFI) FIT INDEX            =      .972
  LISREL    GFI  FIT INDEX            =      .966
  LISREL   AGFI  FIT INDEX            =      .921
  ROOT MEAN-SQUARE RESIDUAL (RMR)     =      .124
  STANDARDIZED RMR                    =      .057
  ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .070
  90% CONFIDENCE INTERVAL OF RMSEA  (        .015,        .115)

  RELIABILITY COEFFICIENTS
  ------------------------
```

```
  CRONBACH'S ALPHA                      =     .879
  COEFFICIENT ALPHA FOR AN OPTIMAL SHORT SCALE               =      .879
  BASED ON ALL VARIABLES
  RELIABILITY COEFFICIENT RHO           =     .928
  GREATEST LOWER BOUND RELIABILITY                           =      .941
  GLB RELIABILITY FOR AN OPTIMAL SHORT SCALE                 =      .941
  BASED ON ALL VARIABLES
  BENTLER'S DIMENSION-FREE LOWER BOUND RELIABILITY           =      .941
  SHAPIRO'S LOWER BOUND RELIABILITY FOR A WEIGHTED COMPOSITE  =      .945
  WEIGHTS THAT ACHIEVE SHAPIRO'S LOWER BOUND:
  P.9.3     P.9.9     P.9.10    P.9.12    P.9.13    P.9.14
      .192      .415      .447      .442      .457      .330
  P.9.15
      .279



  GOODNESS OF FIT SUMMARY FOR METHOD = ROBUST

  ROBUST INDEPENDENCE MODEL CHI-SQUARE =     475.035 ON    21 DEGREES OF
FREEDOM

  INDEPENDENCE AIC =   433.03454   INDEPENDENCE CAIC =   346.18277
         MODEL AIC =    -9.76017          MODEL CAIC =   -59.38975

  SATORRA-BENTLER SCALED CHI-SQUARE =     14.2398 ON      12 DEGREES OF
FREEDOM
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .28566

  RESIDUAL-BASED TEST STATISTIC                        =    16.166
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .18377

  YUAN-BENTLER RESIDUAL-BASED TEST STATISTIC           =    14.762
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .25472

  YUAN-BENTLER RESIDUAL-BASED F-STATISTIC     =      1.259
  DEGREES OF FREEDOM  =                          12,   158
  PROBABILITY VALUE FOR THE F-STATISTIC IS         .24786

  FIT INDICES
  -----------
  BENTLER-BONETT     NORMED FIT INDEX =      .970
  BENTLER-BONETT NON-NORMED FIT INDEX =      .991
  COMPARATIVE FIT INDEX (CFI)         =      .995
  BOLLEN   (IFI) FIT INDEX            =      .995
  MCDONALD (MFI) FIT INDEX            =      .993
  ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .033
  90% CONFIDENCE INTERVAL OF RMSEA  (        .000,        .088)


                        ITERATIVE SUMMARY

                   PARAMETER
  ITERATION        ABS CHANGE         ALPHA               FUNCTION
      1             1.105032         1.00000               .90138
      2              .189620         1.00000               .44294
      3              .125061         1.00000               .13595
```

| | | | |
|---|---|---|---|
| 4 | .036134 | 1.00000 | .12917 |
| 5 | .005827 | 1.00000 | .12901 |
| 6 | .001292 | 1.00000 | .12900 |
| 7 | .000199 | 1.00000 | .12900 |

```
24-May-17      PAGE :  6  EQS     Licensee:
  TITLE:    master confirmatorio rdos

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
  (ROBUST STATISTICS IN PARENTHESES)


 P.9.3   =V3  =   1.000 F12   + 1.000 E3


 P.9.9   =V9  =   1.000 F14   + 1.000 E9


 P.9.10  =V10 =   1.099*F14   + 1.000 E10
                    .095
                  11.571@
               (    .096)
               (  11.416@

 P.9.12  =V12 =   1.000 F13   + 1.000 E12


 P.9.13  =V13 =   1.059*F13   + 1.000 E13
                    .078
                  13.566@
               (    .086)
               (  12.319@

 P.9.14  =V14 =   1.515*F12   + 1.000 E14
                    .144
                  10.517@
               (    .192)
               (   7.880@

 P.9.15  =V15 =   1.000 F12   + 1.000 E15
```

```
24-May-17      PAGE :  7  EQS     Licensee:
  TITLE:    master confirmatorio rdos

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  CONSTRUCT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
  (ROBUST STATISTICS IN PARENTHESES)



    F12  =F12 =    .457*F15   + 1.000 D12
                   .065
                  7.056@
               (   .077)
               (  5.956@

    F13  =F13 =    .900*F15   + 1.000 D13
                   .115
                  7.855@
               (   .115)
               (  7.842@

    F14  =F14 =   1.000 F15   + 1.000 D14
```

```
24-May-17      PAGE :  8  EQS     Licensee:
  TITLE:    master confirmatorio rdos

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES
  ----------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                  V                                F
                 ---                              ---
                              I F15 -   F15             2.080*I
                              I                          .440 I
                              I                         4.733@I
                              I                      (   .443)I
                              I                      (  4.692@I
                              I                               I
```

TITLE:    master confirmatorio rdos

MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

VARIANCES OF INDEPENDENT VARIABLES

STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

```
                E                               D
               ---                             ---
E3  -P.9.3                .580*I D12 -   F12              .244*I
                          .081 I                          .063 I
                         7.123@I                         3.898@I
                      (   .109)I                      (   .086)I
                      (  5.326@I                      (  2.821@I
                               I                               I
E9  -P.9.9               1.413*I D13 -   F13              .796*I
                          .218 I                          .200 I
                         6.487@I                         3.974@I
                      (   .380)I                      (   .272)I
                      (  3.715@I                      (  2.926@I
                               I                               I
E10 -P.9.10               .607*I D14 -   F14              .468*I
                          .198 I                          .210 I
                         3.072@I                         2.225@I
                      (   .188)I                      (   .342)I
                      (  3.235@I                      (  1.369)I
                               I                               I
E12 -P.9.12               .376*I                               I
                          .139 I                               I
                         2.715@I                               I
                      (   .193)I                               I
                      (  1.951)I                               I
                               I                               I
E13 -P.9.13               .934*I                               I
                          .180 I                               I
                         5.192@I                               I
                      (   .318)I                               I
                      (  2.940@I                               I
                               I                               I
E14 -P.9.14               .564*I                               I
                          .130 I                               I
                         4.324@I                               I
                      (   .184)I                               I
                      (  3.060@I                               I
                               I                               I
E15 -P.9.15              1.197*I                               I
                          .144 I                               I
                         8.307@I                               I
                      (   .273)I                               I
                      (  4.390@I                               I
                               I                               I
```

```
24-May-17      PAGE : 10  EQS     Licensee:
 TITLE:    master confirmatorio rdos

 MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

 DECOMPOSITION OF EFFECTS WITH NONSTANDARDIZED VALUES
 STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

 PARAMETER TOTAL EFFECTS
 -----------------------

P.9.3   =V3  =   1.000 F12   +  .457 F15   + 1.000 E3    + 1.000 D12
                                .065
                               7.056@
                            (   .077)
                            (  5.956@


P.9.9   =V9  =   1.000 F14   + 1.000 F15   + 1.000 E9    + 1.000 D14




P.9.10  =V10 =   1.099*F14   + 1.099 F15   + 1.000 E10   + 1.099 D14
                  .095          .095                        .095
                11.571@       11.571@                     11.571@
              (   .096)     (   .096)                   (   .096)
              ( 11.416@     ( 11.416@                   ( 11.416@


P.9.12  =V12 =   1.000 F13   +  .900 F15   + 1.000 E12   + 1.000 D13
                                .115
                               7.855@
                            (   .115)
                            (  7.842@


P.9.13  =V13 =   1.059*F13   +  .953 F15   + 1.000 E13   + 1.059 D13
                  .078          .129                        .078
                13.566@        7.400@                     13.566@
              (   .086)     (   .151)                   (   .086)
              ( 12.319@     (  6.302@                   ( 12.319@


P.9.14  =V14 =   1.515*F12   +  .693 F15   + 1.000 E14   + 1.515 D12
                  .144          .093                        .144
                10.517@        7.449@                     10.517@
              (   .192)     (   .172)                   (   .192)
              (  7.880@     (  4.025@                   (  7.880@


P.9.15  =V15 =   1.000 F12   +  .457 F15   + 1.000 E15   + 1.000 D12
                                .065
                               7.056@
                            (   .077)
                            (  5.956@
```

```
   F12  =F12 =    .457*F15   + 1.000 D12



   F13  =F13 =    .900*F15   + 1.000 D13



   F14  =F14 =   1.000 F15   + 1.000 D14
```

```
24-May-17      PAGE : 11  EQS     Licensee:
  TITLE:    master confirmatorio rdos

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  DECOMPOSITION OF EFFECTS WITH NONSTANDARDIZED VALUES
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

  PARAMETER INDIRECT EFFECTS
  --------------------------

 P.9.3   =V3  =    .457 F15   + 1.000 D12
                   .065
                  7.056@
              (    .077)
              (   5.956@

 P.9.9   =V9  =   1.000 F15   + 1.000 D14



 P.9.10  =V10 =   1.099 F15   + 1.099 D14
                   .095          .095
                 11.571@       11.571@
              (    .096)     (    .096)
              (  11.416@     (  11.416@

 P.9.12  =V12 =    .900 F15   + 1.000 D13
                   .115
                  7.855@
              (    .115)
              (   7.842@

 P.9.13  =V13 =    .953 F15   + 1.059 D13
                   .129          .078
```

```
                 7.400@       13.566@
              (   .151)     (   .086)
              (  6.302@     ( 12.319@

 P.9.14  =V14 =    .693 F15   + 1.515 D12
                  .093          .144
                 7.449@       10.517@
              (   .172)     (   .192)
              (  4.025@     (  7.880@

 P.9.15  =V15 =    .457 F15   + 1.000 D12
                  .065
                 7.056@
              (   .077)
              (  5.956@


24-May-17      PAGE : 12  EQS     Licensee:
  TITLE:    master confirmatorio rdos

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  DECOMPOSITION OF EFFECTS WITH STANDARDIZED VALUES

  PARAMETER TOTAL EFFECTS
  -----------------------

 P.9.3   =V3  =    .734 F12   +  .588 F15   +  .679 E3    +  .440 D12

 P.9.9   =V9  =    .802 F14   +  .725 F15   +  .597 E9    +  .344 D14

 P.9.10  =V10 =    .914*F14   +  .826 F15   +  .406 E10   +  .392 D14

 P.9.12  =V12 =    .932 F13   +  .768 F15   +  .363 E12   +  .528 D13

 P.9.13  =V13 =    .865*F13   +  .713 F15   +  .501 E13   +  .490 D13

 P.9.14  =V14 =    .857*F12   +  .686 F15   +  .515 E14   +  .514 D12

 P.9.15  =V15 =    .601 F12   +  .481 F15   +  .799 E15   +  .361 D12

    F12  =F12 =    .800*F15   +  .599 D12

    F13  =F13 =    .824*F15   +  .566 D13

    F14  =F14 =    .904 F15   +  .429 D14


24-May-17      PAGE : 13  EQS     Licensee:
  TITLE:    master confirmatorio rdos

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  DECOMPOSITION OF EFFECTS WITH STANDARDIZED VALUES

  PARAMETER INDIRECT EFFECTS
```

```
  -------------------------

 P.9.3   =V3  =    .588 F15   +  .440 D12

 P.9.9   =V9  =    .725 F15   +  .344 D14

 P.9.10  =V10 =    .826 F15   +  .392 D14

 P.9.12  =V12 =    .768 F15   +  .528 D13

 P.9.13  =V13 =    .713 F15   +  .490 D13

 P.9.14  =V14 =    .686 F15   +  .514 D12

 P.9.15  =V15 =    .481 F15   +  .361 D12


24-May-17      PAGE : 14  EQS     Licensee:
  TITLE:    master confirmatorio rdos

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  STANDARDIZED SOLUTION:                                          R-
SQUARED



 P.9.3   =V3  =   .734 F12   + .679 E3
.539
 P.9.9   =V9  =   .802 F14   + .597 E9
.643
 P.9.10  =V10 =   .914*F14   + .406 E10
.835
 P.9.12  =V12 =   .932 F13   + .363 E12
.868
 P.9.13  =V13 =   .865*F13   + .501 E13
.749
 P.9.14  =V14 =   .857*F12   + .515 E14
.734
 P.9.15  =V15 =   .601 F12   + .799 E15
.362
    F12  =F12 =   .800*F15   + .599 D12
.641
    F13  =F13 =   .824*F15   + .566 D13
.679
    F14  =F14 =   .904 F15   + .429 D14
.816
                          E N D   O F   M E T H O D
 ------------------------------------------------------------------------
-------
```

```
 24-May-17      PAGE : 15  EQS     Licensee:
  TITLE:    master confirmatorio rdos

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  WALD TEST (FOR DROPPING PARAMETERS)
  ROBUST INFORMATION MATRIX USED IN THIS WALD TEST
  MULTIVARIATE WALD TEST BY SIMULTANEOUS PROCESS



         CUMULATIVE MULTIVARIATE STATISTICS              UNIVARIATE
INCREMENT
         ----------------------------------              ----------------
----

  STEP  PARAMETER   CHI-SQUARE  D.F.  PROBABILITY       CHI-SQUARE
PROBABILITY
  ---- -----------  ----------  ----  -----------       ----------  -----
------

    1    D14,D14       1.874      1       .171             1.874
.171


24-May-17      PAGE : 16  EQS     Licensee:
  TITLE:    master confirmatorio rdos

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  LAGRANGE MULTIPLIER TEST (FOR ADDING PARAMETERS)


  ORDERED UNIVARIATE TEST STATISTICS:
                                                     HANCOCK
STANDAR-
                                             CHI-              12 DF   PARAMETER
DIZED
   NO    CODE     PARAMETER      SQUARE      PROB.    PROB.    CHANGE
CHANGE
   --   ------    ---------      ------      -----  -------- ---------   --
------
    1    2   0       V15,F12      6.555       .010      .886       .357
.316
    2    2   0        V3,F12      6.555       .010      .886     -.357
-.386
    3    2  20        V3,F13      4.140       .042      .981     -.119
-.067
    4    2  12        V3,F15      2.993       .084      .996     -.127
-.079
    5    2  12       V15,F15      2.957       .086      .996       .133
.067
    6    2  20       V14,F13      2.270       .132      .999       .175
.076
    7    2  20       V15,F14      2.262       .133      .999       .100
.046
```

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 8 | 2 | 20 | V15,F13 | .994 | .319 | 1.000 | .065 | .030 |
| 9 | 2 | 20 | V13,F14 | .869 | .351 | 1.000 | .295 | .096 |
| 10 | 2 | 20 | V13,F12 | .869 | .351 | 1.000 | -.258 | -.163 |
| 11 | 2 | 20 | V12,F12 | .869 | .351 | 1.000 | .244 | .175 |
| 12 | 2 | 20 | V12,F14 | .869 | .351 | 1.000 | -.278 | -.103 |
| 13 | 2 | 20 | V3,F14 | .845 | .358 | 1.000 | -.057 | -.032 |
| 14 | 2 | 20 | V14,F14 | .579 | .447 | 1.000 | -.114 | -.049 |
| 15 | 2 | 20 | V9,F13 | .081 | .776 | 1.000 | -.061 | -.020 |
| 16 | 2 | 20 | V10,F13 | .081 | .776 | 1.000 | .067 | .022 |
| 17 | 2 | 20 | V10,F12 | .081 | .776 | 1.000 | -.111 | -.070 |
| 18 | 2 | 20 | V9,F12 | .081 | .776 | 1.000 | .101 | .062 |
| 19 | 2 | 12 | V14,F15 | .042 | .837 | 1.000 | .050 | .024 |
| 20 | 2 | 22 | F13,F12 | .000 | 1.000 | 1.000 | .000 | .000 |
| 21 | 2 | 22 | F14,F12 | .000 | 1.000 | 1.000 | .000 | .000 |
| 22 | 2 | 22 | F12,F14 | .000 | 1.000 | 1.000 | .000 | .000 |
| 23 | 2 | 22 | F12,F13 | .000 | 1.000 | 1.000 | .000 | .000 |
| 24 | 2 | 22 | F13,F14 | .000 | 1.000 | 1.000 | .000 | .000 |
| 25 | 2 | 0 | V12,F13 | .000 | 1.000 | 1.000 | .000 | .000 |
| 26 | 2 | 10 | D13,D12 | .000 | 1.000 | 1.000 | .000 | .000 |
| 27 | 2 | 0 | V9,F14 | .000 | 1.000 | 1.000 | .000 | .000 |
| 28 | 2 | 0 | F14,F15 | .000 | 1.000 | 1.000 | .000 | .000 |
| 29 | 2 | 12 | V13,F15 | .000 | 1.000 | 1.000 | .000 | .000 |
| 30 | 2 | 12 | V12,F15 | .000 | 1.000 | 1.000 | .000 | .000 |
| 31 | 2 | 12 | V10,F15 | .000 | 1.000 | 1.000 | .000 | .000 |
| 32 | 2 | 12 | V9,F15 | .000 | 1.000 | 1.000 | .000 | .000 |
| 33 | 2 | 10 | D14,D13 | .000 | 1.000 | 1.000 | .000 | .000 |
| 34 | 2 | 10 | D14,D12 | .000 | 1.000 | 1.000 | .000 | .000 |
| 35 | 2 | 22 | F14,F13 | .000 | 1.000 | 1.000 | .000 | .000 |

```
 24-May-17      PAGE : 17  EQS     Licensee:
  TITLE:    master confirmatorio rdos

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  MULTIVARIATE LAGRANGE MULTIPLIER TEST BY SIMULTANEOUS PROCESS IN STAGE
1

  PARAMETER SETS (SUBMATRICES) ACTIVE AT THIS STAGE ARE:

     PVV PFV PFF PDD GVV GVF GFV GFF BVF BFF



        CUMULATIVE MULTIVARIATE STATISTICS      UNIVARIATE INCREMENT
        ----------------------------------      -------------------------
-----

HANCOCK'S

SEQUENTIAL
 STEP   PARAMETER   CHI-SQUARE  D.F.   PROB.   CHI-SQUARE   PROB.  D.F.
PROB.
 ----  -----------  ----------  ----   -----   ----------   -----  ----
-----
    1       V3,F12       6.555     1    .010        6.555    .010    12
.886


  LAGRANGIAN MULTIPLIER TEST REQUIRED     8209 WORDS OF MEMORY.
  PROGRAM ALLOCATES ******** WORDS.
1
  Execution begins at 12:39:12
  Execution ends   at 12:39:12
```

# ANEXO XV

# MODELOS DE ECUACIONES ESTRUCTURALES

# TIC-FLEX

```
      1
        EQS,  A  STRUCTURAL  EQUATION  PROGRAM                 MULTIVARIATE
SOFTWARE, INC.
        COPYRIGHT BY P.M. BENTLER                    VERSION 6.1 (C) 1985
- 2005 (B85).


          PROGRAM CONTROL INFORMATION

           1  /TITLE
           2  master confirmatorio la 5 sobre la 6, 7, 10 y 11 y la 4
sobre la 10 y 7
           3  /SPECIFICATIONS
           4  VARIABLES= 58 ; CASES= 170 ;
           5  DATAFILE='C:\tesis1\base brasilticflex.ESS';
           6   MATRIX=RAW;METHOD=ML,robust;
           7  /LABELS
           8  V1=P.1.1; V2=P.1.2; V3=P.1.3; V4=P.1.4; V5=P.1.5; V6=P.1.6;
V7=P.1.7;
           9  V8=P.1.8; V9=P.1.9; V10=P.1.10; V11=P.1.11; V12=P.1.12;
          10  V13=P.1.13; V14=P.1.14; V15=P.1.15; V16=P.1.16;
          11   V17=P.1.17;  V18=P.2.1;  V19=P.2.2;  V20=P.2.3;  V21=P.2.4;
V22=P.2.5;
          12   V23=P.2.6;  V24=P.2.7;  V25=P.2.8;  V26=P.2.9;  V27=P.2.10;
V28=P.2.11; V29=P.2.12;
          13   V30=P.2.13;  V31=P.2.14;  V32=P.2.15;  V33=P.3.1;  V34=P.3.2;
V35=P.3.3; V36=P.4.1;
          14    V37=P.4.2;  V38=P.4.3;  V39=P.4.4;  V40=P.4.5;  V41=P.4.6;
V42=P.4.7; V43=P.4.8;
          15  V44=P.4.9; V45=P.4.10; V46=P.4.11;
          16    V47=P.6.1;  V48=P.6.2;  V49=P.6.3;  V50=P.6.4;  V51=P.6.5;
V52=P.6.6; V53=P.6.7;
          17      V54=P.6.8;    V55=P.6.9;    V56=P.6.10;    V57=P.11.2LI;
V58=P.11.3LI;
          18  /EQUATIONS
          19  V1=F1+ E1;
          20  V8=*F1+E8;
          21  V2=*F1+E2;
          22  V3=*F1+E3;
          23  V10=F2+E10;
          24  V16=*F2+E16;
          25  V17=*F2+E17;
          26  V11=*F2+E11;
          27  V6=F3+E6;
          28  V5=*F3+E5;
          29  V9=F4+E9;
          30  V12=*F4+E12;
          31  F1=*F5+D1;
          32  F2=F5+D2;
          33  F3=*F5+D3;
          34  V19=F6+E19;
          35  V20=*F6+E20;
          36  V21=*F6+E21;
          37  V23=*F6+E23;
          38  V33=F7+E33;
          39  V35=*F7+E35;
```

```
V36=F8+E36;
V37=*F8+E37;
V38=*F8+E38;
V39=*F8+E39;
V42=F9+E42;
V43=*F9+E43;
V44=*F9+E44;
V45=*F9+E45;
V47=F10+E47;
V48=*F10+E48;
V49=*F10+E49;
V50=*F10+E50;
V51=*F10+E51;
```

29-Jun-17 PAGE : 2 EQS Licensee:
TITLE: master confirmatorio la 5 sobre la 6, 7, 10 y 11 y la 4 sob

```
F8=F11+D8;
F9=*F11+D9;
F11=*F5+D11;
F10=*F4+D10;
F7= *F4+*F5+D7;
F6=*F5+D6;

/VARIANCES
E1 TO E3=*; E5 TO E6=*;
E8 TO E12=*;
E16 TO E17=*;
D1 TO D3=*;
F5=*;
E19 TO E21=*;
E23=*;
E35 TO E39=*;
E33=*;
E42 TO E45=*;
E47 TO E51=*;
D8 TO D9=*;
F4=*;
D11=*;
D10=*;
D7=*;
D6=*;
/COVARIANCES
F4,F5=*;
/TECHNICAL
ITR=100
/PRINT
FIT=ALL;
EFFECT=YES;
/WTEST
/LMTEST
/END
```

87 RECORDS OF INPUT MODEL FILE WERE READ

```
          DATA IS READ FROM C:\tesis1\base brasilticflex.ESS
          THERE ARE  58 VARIABLES AND   170 CASES
          IT IS A RAW DATA ESS FILE


      29-Jun-17      PAGE :  3  EQS     Licensee:
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sob


        SAMPLE STATISTICS BASED ON COMPLETE CASES


                                   UNIVARIATE STATISTICS
                                   ---------------------


         VARIABLE          P.1.1        P.1.2        P.1.3        P.1.5
P.1.6
                           V1            V2            V3            V5
V6

         MEAN                3.6941       4.0059       3.4235       4.8765
4.4000

         SKEWNESS (G1)     -.1427      -.3284      -.0187      -.8703     -
.5597

         KURTOSIS (G2)    -1.6839     -1.4951     -1.5302      -.8141     -
1.3132

         STANDARD DEV.      2.9694       2.7873       2.7126       2.6540
2.7914


         VARIABLE          P.1.8        P.1.9        P.1.10       P.1.11
P.1.12
                           V8            V9            V10           V11
V12

         MEAN                2.1353       2.3647       4.7059       3.5059
2.3706

         SKEWNESS  (G1)        .8348         .6639        -.7765         -
.0322      .6738

         KURTOSIS (G2)     -.8715     -1.0669     -1.1465     -1.6572     -
1.2320

         STANDARD DEV.      2.5971       2.6147       2.8939       2.9053
2.8385


         VARIABLE          P.1.16       P.1.17       P.2.2        P.2.3
P.2.4
                           V16           V17           V19           V20
V21
```

MEAN 4.6235 4.6176 1.8765 1.4588
2.9471

SKEWNESS (G1) -.7038 -.6901 1.2422
1.5942 .4243

KURTOSIS (G2) -1.0836 -1.0056 .3913 1.6513 -
1.3650

STANDARD DEV. 2.7217 2.6110 2.1295 1.8908
2.5309

VARIABLE P.2.6 P.3.1 P.3.3 P.4.1
P.4.2
V23 V33 V35 V36
V37

MEAN 2.0882 2.2059 1.9000 2.7294
2.8235

SKEWNESS (G1) 1.0549 .8539
1.1054 .4621 .2998

KURTOSIS (G2) -.2638 -.6331 -.1092 -1.1132 -
1.2121

STANDARD DEV. 2.3150 2.3856 2.3626 2.4441
2.3818

VARIABLE P.4.3 P.4.4 P.4.7 P.4.8
P.4.9
V38 V39 V42 V43
V44

MEAN 2.6882 2.6647 3.4059 4.0471
3.5353

SKEWNESS (G1) .4307 .4202 .1232 -.2498 -
.0173

KURTOSIS (G2) -1.1559 -1.1980 -1.1944 -1.1031 -
1.3026

STANDARD DEV. 2.4185 2.4372 2.2624 2.2710
2.3663

VARIABLE P.4.10 P.6.1 P.6.2 P.6.3
P.6.4
V45 V47 V48 V49
V50

MEAN 2.7706 2.8294 2.9235 2.5529
2.3765

SKEWNESS
(G1) .4803 .3455 .2227 .5477 .4525

```
        KURTOSIS (G2)     -1.0218    -1.0645    -1.0536     -.9088     -
.9277

        STANDARD DEV.        2.3180       2.3282       2.2241       2.3077
2.1810


        VARIABLE        P.6.5
                          V51

        MEAN              2.1118

        SKEWNESS (G1)       .8085

        KURTOSIS (G2)      -.5685

        STANDARD DEV.     2.2544


                                 MULTIVARIATE KURTOSIS
                                 ---------------------

        MARDIA'S COEFFICIENT (G2,P) =    179.3099
        NORMALIZED ESTIMATE =             25.8432


                          ELLIPTICAL THEORY KURTOSIS ESTIMATES
                          ------------------------------------

        MARDIA-BASED KAPPA =       .1753 MEAN SCALED UNIVARIATE KURTOSIS
=     -.3124

        MARDIA-BASED     KAPPA     IS     USED     IN     COMPUTATION.
KAPPA=            .1753


        CASE   NUMBERS   WITH   LARGEST   CONTRIBUTION   TO   NORMALIZED
MULTIVARIATE KURTOSIS:
        -------------------------------------------------------------
-----------

        CASE NUMBER         21             61             85            150
156

        ESTIMATE        742.1016      426.5545    1308.4114      610.1216
404.2348


      29-Jun-17      PAGE :  4  EQS     Licensee:
       TITLE:   master confirmatorio la 5 sobre la 6, 7, 10 y 11 y la 4
sob

       COVARIANCE  MATRIX TO BE ANALYZED:  31 VARIABLES (SELECTED FROM
58 VARIABLES)
       BASED ON   170 CASES.
```

| | | P.1.1 | P.1.2 | P.1.3 | P.1.5 | P.1.6 |
|---|---|---|---|---|---|---|
| | | V1 | V2 | V3 | V5 | V6 |
| P.1.1 | V1 | 8.817 | | | | |
| P.1.2 | V2 | 5.617 | 7.769 | | | |
| P.1.3 | V3 | 4.781 | 4.938 | 7.358 | | |
| P.1.5 | V5 | 4.287 | 3.800 | 3.810 | 7.044 | |
| P.1.6 | V6 | 3.147 | 3.353 | 2.978 | 5.417 | 7.792 |
| P.1.8 | V8 | 3.917 | 3.981 | 4.392 | 2.242 | 2.336 |
| P.1.9 | V9 | 1.757 | 2.838 | 1.892 | .957 | 1.717 |
| P.1.10 | V10 | 3.389 | 3.451 | 3.741 | 3.247 | 2.006 |
| P.1.11 | V11 | 3.327 | 3.399 | 3.441 | 3.282 | 3.004 |
| P.1.12 | V12 | 3.558 | 3.838 | 3.611 | 2.863 | 3.040 |
| P.1.16 | V16 | 3.269 | 3.576 | 3.657 | 3.308 | 2.595 |
| P.1.17 | V17 | 2.823 | 3.061 | 3.305 | 3.621 | 2.822 |
| P.2.2 | V19 | .370 | .385 | 1.017 | .434 | .073 |
| P.2.3 | V20 | .520 | .725 | .941 | .453 | .472 |
| P.2.4 | V21 | .635 | .568 | .691 | .248 | -.535 |
| P.2.6 | V23 | 1.311 | 1.201 | 1.128 | .484 | -.053 |
| P.3.1 | V33 | -.682 | -.196 | .226 | -1.199 | -1.237 |
| P.3.3 | V35 | .111 | .385 | .214 | -.669 | -.676 |
| P.4.1 | V36 | .544 | 1.303 | .701 | .073 | .292 |
| P.4.2 | V37 | 1.295 | 1.758 | 1.430 | .795 | 1.195 |
| P.4.3 | V38 | 1.170 | 1.771 | 1.074 | .772 | 1.256 |
| P.4.4 | V39 | 1.394 | 1.653 | 1.107 | .757 | 1.277 |
| P.4.7 | V42 | .746 | 1.441 | 1.312 | .151 | .375 |
| P.4.8 | V43 | 1.352 | 2.183 | 1.773 | .787 | .863 |
| P.4.9 | V44 | .745 | 1.423 | 1.275 | .611 | .560 |
| P.4.10 | V45 | .977 | 1.463 | 1.334 | .758 | 1.288 |
| P.6.1 | V47 | 1.782 | 1.989 | 2.161 | 1.174 | 1.134 |
| P.6.2 | V48 | 1.332 | 1.279 | 1.364 | 1.251 | 1.504 |
| P.6.3 | V49 | 2.217 | 1.932 | 2.244 | 2.223 | 2.269 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.6.4 | V50 | 1.406 | 1.169 | 1.508 | 1.035 | 1.115 |
| P.6.5 | V51 | 2.188 | 2.124 | 2.006 | 1.606 | 1.570 |

| | | P.1.8 | P.1.9 | P.1.10 | P.1.11 | P.1.12 |
|---|---|---|---|---|---|---|
| | | V8 | V9 | V10 | V11 | V12 |
| P.1.8 | V8 | 6.745 | | | | |
| P.1.9 | V9 | 2.134 | 6.837 | | | |
| P.1.10 | V10 | 2.016 | 1.179 | 8.375 | | |
| P.1.11 | V11 | 3.316 | 2.140 | 3.724 | 8.441 | |
| P.1.12 | V12 | 3.772 | 3.704 | 2.956 | 3.770 | 8.057 |
| P.1.16 | V16 | 2.886 | 1.706 | 3.528 | 3.795 | 3.566 |
| P.1.17 | V17 | 2.129 | 1.904 | 3.106 | 3.147 | 3.048 |
| P.2.2 | V19 | .875 | .359 | .301 | .755 | .715 |
| P.2.3 | V20 | 1.299 | 1.086 | .219 | .843 | 1.119 |
| P.2.4 | V21 | .806 | 1.079 | .475 | .145 | 1.428 |
| P.2.6 | V23 | 1.603 | 1.317 | .979 | 1.298 | 1.713 |
| P.3.1 | V33 | -.016 | .711 | -1.756 | -.324 | -.195 |
| P.3.3 | V35 | .203 | .806 | -1.024 | .069 | .173 |
| P.4.1 | V36 | 1.226 | 1.383 | .387 | 1.138 | 1.687 |
| P.4.2 | V37 | 1.793 | 1.538 | .829 | .954 | 2.249 |
| P.4.3 | V38 | 1.853 | 2.026 | .440 | 1.348 | 2.495 |
| P.4.4 | V39 | 1.933 | 2.076 | .422 | 1.543 | 2.232 |
| P.4.7 | V42 | 1.223 | .543 | .233 | 1.285 | 1.257 |
| P.4.8 | V43 | 1.390 | .782 | .493 | 1.739 | 1.456 |
| P.4.9 | V44 | 1.330 | 1.413 | -.155 | 1.325 | 1.493 |
| P.4.10 | V45 | 1.729 | 1.049 | .080 | 1.099 | 1.304 |
| P.6.1 | V47 | 2.059 | 2.145 | 1.056 | 1.998 | 2.614 |
| P.6.2 | V48 | 1.543 | 1.430 | 1.060 | 1.690 | 2.484 |
| P.6.3 | V49 | 2.605 | 2.347 | 1.004 | 2.452 | 3.285 |
| P.6.4 | V50 | 1.576 | 1.891 | .703 | 1.104 | 2.262 |
| P.6.5 | V51 | 1.878 | 1.995 | 1.370 | 1.955 | 2.615 |

| | | P.1.16 V16 | P.1.17 V17 | P.2.2 V19 | P.2.3 V20 | P.2.4 V21 |
|---|---|---|---|---|---|---|
| P.1.16 | V16 | 7.408 | | | | |
| P.1.17 | V17 | 3.832 | 6.817 | | | |
| P.2.2 | V19 | 1.042 | .787 | 4.535 | | |
| P.2.3 | V20 | .771 | .833 | 3.051 | 3.575 | |
| P.2.4 | V21 | 1.199 | 1.364 | 2.804 | 2.356 | 6.405 |
| P.2.6 | V23 | 1.075 | 1.016 | 2.561 | 2.462 | 3.667 |
| P.3.1 | V33 | -.591 | -.447 | .375 | .461 | .573 |
| P.3.3 | V35 | -.245 | .068 | .088 | .395 | .279 |
| P.4.1 | V36 | .578 | .985 | 1.173 | 1.113 | 2.181 |
| P.4.2 | V37 | .620 | 1.021 | 1.292 | 1.123 | 1.979 |
| P.4.3 | V38 | .799 | 1.211 | 1.056 | 1.197 | 2.019 |
| P.4.4 | V39 | .636 | 1.019 | 1.219 | 1.285 | 2.290 |
| P.4.7 | V42 | .674 | .908 | 1.210 | .777 | 1.590 |
| P.4.8 | V43 | .888 | 1.503 | 1.674 | 1.304 | 2.221 |
| P.4.9 | V44 | 1.138 | 1.466 | 1.410 | 1.067 | 2.573 |
| P.4.10 | V45 | 1.026 | 1.498 | 1.185 | 1.029 | 1.402 |
| P.6.1 | V47 | 2.012 | 1.627 | .210 | .546 | 1.109 |
| P.6.2 | V48 | 1.805 | .858 | .848 | .941 | 1.457 |
| P.6.3 | V49 | 2.363 | 1.704 | .950 | 1.159 | .947 |
| P.6.4 | V50 | 1.148 | .813 | .917 | 1.098 | 1.866 |
| P.6.5 | V51 | 2.161 | 1.570 | .754 | 1.108 | .929 |

| | | P.2.6 V23 | P.3.1 V33 | P.3.3 V35 | P.4.1 V36 | P.4.2 V37 |
|---|---|---|---|---|---|---|
| P.2.6 | V23 | 5.359 | | | | |
| P.3.1 | V33 | -.101 | 5.691 | | | |
| P.3.3 | V35 | .488 | 2.731 | 5.582 | | |
| P.4.1 | V36 | 1.710 | 1.802 | 1.996 | 5.974 | |
| P.4.2 | V37 | 1.743 | .924 | 1.396 | 3.952 | 5.673 |
| P.4.3 | V38 | 1.750 | 1.136 | 1.874 | 4.033 | 5.270 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.4.4 | V39 | 1.882 | 1.247 | 1.309 | 3.678 | 4.988 |
| P.4.7 | V42 | 1.514 | .815 | .869 | 1.868 | 2.149 |
| P.4.8 | V43 | 1.931 | .913 | .904 | 2.338 | 2.653 |
| P.4.9 | V44 | 1.929 | 1.155 | 1.030 | 2.199 | 2.574 |
| P.4.10 | V45 | 1.689 | .888 | 1.220 | 2.263 | 2.669 |
| P.6.1 | V47 | .707 | 1.408 | 1.385 | 1.764 | 1.940 |
| P.6.2 | V48 | 1.634 | .590 | 1.122 | 1.896 | 2.022 |
| P.6.3 | V49 | 1.448 | .613 | 1.346 | 1.707 | 2.086 |
| P.6.4 | V50 | 1.617 | .620 | .689 | 1.753 | 2.357 |
| P.6.5 | V51 | 1.043 | .835 | 1.141 | 1.764 | 1.913 |

| | | P.4.3 | P.4.4 | P.4.7 | P.4.8 | P.4.9 |
|---|---|---|---|---|---|---|
| | | V38 | V39 | V42 | V43 | V44 |
| P.4.3 | V38 | 5.849 | | | | |
| P.4.4 | V39 | 5.226 | 5.940 | | | |
| P.4.7 | V42 | 2.098 | 2.279 | 5.118 | | |
| P.4.8 | V43 | 2.630 | 2.797 | 4.093 | 5.158 | |
| P.4.9 | V44 | 2.718 | 2.968 | 3.545 | 3.768 | 5.599 |
| P.4.10 | V45 | 2.674 | 2.686 | 2.958 | 3.111 | 4.236 |
| P.6.1 | V47 | 2.035 | 2.262 | 1.283 | 1.209 | 1.672 |
| P.6.2 | V48 | 2.023 | 2.004 | 1.262 | 1.021 | 1.384 |
| P.6.3 | V49 | 2.440 | 2.358 | 1.106 | 1.145 | 1.750 |
| P.6.4 | V50 | 2.378 | 2.512 | 1.296 | 1.130 | 1.531 |
| P.6.5 | V51 | 1.840 | 2.008 | 1.641 | 1.397 | 1.662 |

| | | P.4.10 | P.6.1 | P.6.2 | P.6.3 | P.6.4 |
|---|---|---|---|---|---|---|
| | | V45 | V47 | V48 | V49 | V50 |
| P.4.10 | V45 | 5.373 | | | | |
| P.6.1 | V47 | 1.215 | 5.420 | | | |
| P.6.2 | V48 | 1.184 | 3.218 | 4.947 | | |
| P.6.3 | V49 | 1.642 | 3.124 | 3.427 | 5.326 | |
| P.6.4 | V50 | 1.111 | 2.976 | 2.609 | 2.731 | 4.757 |
| P.6.5 | V51 | 1.783 | 2.972 | 2.991 | 3.547 | 2.952 |

```
                    P.6.5
                       V51
         P.6.5    V51        5.082


      BENTLER-WEEKS STRUCTURAL REPRESENTATION:

            NUMBER OF DEPENDENT VARIABLES = 40
                DEPENDENT V'S :      1     2     3     5     6     8     9
10   11   12
                DEPENDENT V'S :     16    17    19    20    21    23    33
35   36   37
                DEPENDENT V'S :     38    39    42    43    44    45    47
48   49   50
                DEPENDENT V'S :    51
                DEPENDENT F'S :      1     2     3     6     7     8     9
10   11

            NUMBER OF INDEPENDENT VARIABLES = 42
                INDEPENDENT F'S :     4     5
                INDEPENDENT E'S :      1     2     3     5     6     8     9
10   11   12
                INDEPENDENT E'S :     16    17    19    20    21    23    33
35   36   37
                INDEPENDENT E'S :     38    39    42    43    44    45    47
48   49   50
                INDEPENDENT E'S :    51
                INDEPENDENT D'S :      1     2     3     6     7     8     9
10   11

            NUMBER OF FREE PARAMETERS =  73
            NUMBER OF FIXED NONZERO PARAMETERS =  51

     *** WARNING MESSAGES ABOVE, IF ANY, REFER TO THE MODEL PROVIDED.
         CALCULATIONS FOR INDEPENDENCE MODEL NOW BEGIN.

     *** WARNING MESSAGES ABOVE, IF ANY, REFER TO INDEPENDENCE MODEL.
         CALCULATIONS FOR USER'S MODEL NOW BEGIN.


      3RD STAGE OF COMPUTATION REQUIRED   2854283 WORDS OF MEMORY.
      PROGRAM ALLOCATED 200000000 WORDS

      DETERMINANT OF INPUT MATRIX IS    .82950D+15

     *** NOTE *** RESIDUAL-BASED STATISTICS CANNOT BE
                  CALCULATED BECAUSE OF PIVOTING PROBLEMS.

      PARAMETER ESTIMATES APPEAR IN ORDER,
      NO SPECIAL PROBLEMS WERE ENCOUNTERED DURING OPTIMIZATION.


      RESIDUAL COVARIANCE MATRIX  (S-SIGMA) :
```

| | | P.1.1 | P.1.2 | P.1.3 | P.1.5 | P.1.6 |
|---|---|---|---|---|---|---|
| | | V1 | V2 | V3 | V5 | V6 |
| P.1.1 | V1 | .000 | | | | |
| P.1.2 | V2 | .442 | .000 | | | |
| P.1.3 | V3 | -.207 | -.141 | .000 | | |
| P.1.5 | V5 | .741 | .189 | .330 | .000 | |
| P.1.6 | V6 | .064 | .214 | -.048 | .000 | .000 |
| P.1.8 | V8 | -.213 | -.224 | .339 | -.640 | -.169 |
| P.1.9 | V9 | -.680 | .356 | -.500 | -1.254 | -.204 |
| P.1.10 | V10 | .179 | .183 | .591 | .336 | -.525 |
| P.1.11 | V11 | -.180 | -.172 | -.001 | .100 | .238 |
| P.1.12 | V12 | -.047 | .167 | .073 | -.407 | .198 |
| P.1.16 | V16 | -.342 | -.100 | .114 | .033 | -.252 |
| P.1.17 | V17 | -.410 | -.231 | .132 | .689 | .273 |
| P.2.2 | V19 | -.669 | -.673 | -.003 | -.509 | -.746 |
| P.2.3 | V20 | -.422 | -.234 | .016 | -.401 | -.270 |
| P.2.4 | V21 | -.300 | -.383 | -.226 | -.600 | -1.272 |
| P.2.6 | V23 | .401 | .274 | .235 | -.341 | -.771 |
| P.3.1 | V33 | -.409 | .081 | .494 | -.952 | -1.022 |
| P.3.3 | V35 | .359 | .637 | .457 | -.445 | -.481 |
| P.4.1 | V36 | -.622 | .116 | -.443 | -.985 | -.627 |
| P.4.2 | V37 | -.228 | .208 | -.064 | -.587 | -.005 |
| P.4.3 | V38 | -.415 | .157 | -.482 | -.666 | .006 |
| P.4.4 | V39 | -.113 | .119 | -.371 | -.610 | .089 |
| P.4.7 | V42 | -.522 | .150 | .068 | -.999 | -.624 |
| P.4.8 | V43 | .013 | .820 | .459 | -.427 | -.192 |
| P.4.9 | V44 | -.648 | .004 | -.092 | -.653 | -.538 |
| P.4.10 | V45 | -.254 | .210 | .127 | -.358 | .318 |
| P.6.1 | V47 | -.214 | -.043 | .203 | -.636 | -.440 |
| P.6.2 | V48 | -.646 | -.735 | -.577 | -.543 | -.055 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.6.3 | V49 | .010 | -.316 | .077 | .220 | .528 |
| P.6.4 | V50 | -.361 | -.629 | -.225 | -.567 | -.278 |
| P.6.5 | V51 | .124 | .021 | -.021 | -.267 | -.057 |

| | | P.1.8 | P.1.9 | P.1.10 | P.1.11 | P.1.12 |
|---|---|---|---|---|---|---|
| | | V8 | V9 | V10 | V11 | V12 |
| P.1.8 | V8 | .000 | | | | |
| P.1.9 | V9 | .153 | .000 | | | |
| P.1.10 | V10 | -.592 | -.822 | .000 | | |
| P.1.11 | V11 | .466 | -.047 | .269 | .000 | |
| P.1.12 | V12 | .843 | .259 | -.004 | .536 | .000 |
| P.1.16 | V16 | -.049 | -.545 | -.029 | -.092 | .237 |
| P.1.17 | V17 | -.498 | -.112 | -.079 | -.333 | .067 |
| P.2.2 | V19 | .030 | -.289 | -.553 | -.177 | -.244 |
| P.2.3 | V20 | .533 | .499 | -.555 | -.002 | .250 |
| P.2.4 | V21 | .047 | .496 | -.292 | -.693 | .566 |
| P.2.6 | V23 | .864 | .749 | .232 | .482 | .873 |
| P.3.1 | V33 | .206 | .265 | -1.532 | -.079 | -.856 |
| P.3.3 | V35 | .404 | .401 | -.821 | .290 | -.425 |
| P.4.1 | V36 | .279 | .656 | -.570 | .092 | .612 |
| P.4.2 | V37 | .556 | .589 | -.421 | -.413 | .845 |
| P.4.3 | V38 | .565 | 1.038 | -.861 | -.074 | 1.033 |
| P.4.4 | V39 | .709 | 1.136 | -.816 | .192 | .842 |
| P.4.7 | V42 | .193 | -.247 | -.808 | .147 | .088 |
| P.4.8 | V43 | .303 | -.053 | -.606 | .539 | .222 |
| P.4.9 | V44 | .198 | .545 | -1.299 | .075 | .208 |
| P.4.10 | V45 | .730 | .282 | -.930 | -.005 | .170 |
| P.6.1 | V47 | .437 | .238 | -.582 | .208 | -.207 |
| P.6.2 | V48 | -.064 | -.460 | -.563 | -.085 | -.311 |
| P.6.3 | V49 | .811 | .238 | -.808 | .472 | .165 |
| P.6.4 | V50 | .141 | .203 | -.747 | -.480 | -.235 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.6.5 | V51 | .201 | .021 | -.325 | .103 | -.303 |

| | | P.1.16 | P.1.17 | P.2.2 | P.2.3 | P.2.4 |
|---|---|---|---|---|---|---|
| | | V16 | V17 | V19 | V20 | V21 |
| P.1.16 | V16 | .000 | | | | |
| P.1.17 | V17 | .248 | .000 | | | |
| P.2.2 | V19 | .082 | -.073 | .000 | | |
| P.2.3 | V20 | -.099 | .054 | .124 | .000 | |
| P.2.4 | V21 | .336 | .591 | -.100 | -.276 | .000 |
| P.2.6 | V23 | .234 | .263 | -.267 | -.100 | 1.125 |
| P.3.1 | V33 | -.339 | -.222 | .447 | .527 | .638 |
| P.3.3 | V35 | -.017 | .273 | .154 | .455 | .338 |
| P.4.1 | V36 | -.499 | .020 | .863 | .832 | 1.902 |
| P.4.2 | V37 | -.787 | -.239 | .887 | .756 | 1.615 |
| P.4.3 | V38 | -.665 | -.099 | .635 | .815 | 1.640 |
| P.4.4 | V39 | -.755 | -.227 | .818 | .922 | 1.930 |
| P.4.7 | V42 | -.497 | -.141 | .873 | .472 | 1.287 |
| P.4.8 | V43 | -.348 | .396 | 1.319 | .981 | 1.901 |
| P.4.9 | V44 | -.149 | .314 | 1.039 | .731 | 2.240 |
| P.4.10 | V45 | -.111 | .480 | .857 | .733 | 1.108 |
| P.6.1 | V47 | .169 | -.024 | -.321 | .065 | .632 |
| P.6.2 | V48 | -.021 | -.777 | .323 | .464 | .985 |
| P.6.3 | V49 | .324 | -.122 | .363 | .627 | .419 |
| P.6.4 | V50 | -.483 | -.647 | .447 | .673 | 1.444 |
| P.6.5 | V51 | .254 | -.138 | .205 | .611 | .435 |

| | | P.2.6 | P.3.1 | P.3.3 | P.4.1 | P.4.2 |
|---|---|---|---|---|---|---|
| | | V23 | V33 | V35 | V36 | V37 |
| P.2.6 | V23 | .000 | | | | |
| P.3.1 | V33 | -.038 | .000 | | | |
| P.3.3 | V35 | .546 | .000 | .000 | | |
| P.4.1 | V36 | 1.439 | 1.883 | 2.070 | .000 | |
| P.4.2 | V37 | 1.389 | 1.030 | 1.493 | .076 | .000 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.4.3 | V38 | 1.381 | 1.246 | 1.974 | .000 | .001 |
| P.4.4 | V39 | 1.531 | 1.352 | 1.405 | -.157 | -.021 |
| P.4.7 | V42 | 1.219 | .904 | .949 | .008 | -.281 |
| P.4.8 | V43 | 1.619 | 1.007 | .989 | .375 | .089 |
| P.4.9 | V44 | 1.605 | 1.253 | 1.118 | .155 | -.095 |
| P.4.10 | V45 | 1.403 | .974 | 1.297 | .458 | .311 |
| P.6.1 | V47 | .243 | 1.042 | 1.054 | 1.169 | 1.163 |
| P.6.2 | V48 | 1.174 | .227 | .794 | 1.307 | 1.251 |
| P.6.3 | V49 | .934 | .209 | .979 | 1.048 | 1.226 |
| P.6.4 | V50 | 1.206 | .297 | .395 | 1.227 | 1.669 |
| P.6.5 | V51 | .563 | .457 | .799 | 1.148 | 1.109 |

| | | P.4.3 V38 | P.4.4 V39 | P.4.7 V42 | P.4.8 V43 | P.4.9 V44 |
|---|---|---|---|---|---|---|
| P.4.3 | V38 | .000 | | | | |
| P.4.4 | V39 | .013 | .000 | | | |
| P.4.7 | V42 | -.431 | -.125 | .000 | | |
| P.4.8 | V43 | -.039 | .260 | .492 | .000 | |
| P.4.9 | V44 | -.060 | .326 | -.203 | -.189 | .000 |
| P.4.10 | V45 | .220 | .353 | -.353 | -.383 | .599 |
| P.6.1 | V47 | 1.226 | 1.493 | .635 | .526 | .961 |
| P.6.2 | V48 | 1.222 | 1.242 | .621 | .344 | .680 |
| P.6.3 | V49 | 1.545 | 1.507 | .390 | .390 | .963 |
| P.6.4 | V50 | 1.662 | 1.831 | .723 | .525 | .902 |
| P.6.5 | V51 | 1.003 | 1.212 | .971 | .690 | .926 |

| | | P.4.10 V45 | P.6.1 V47 | P.6.2 V48 | P.6.3 V49 | P.6.4 V50 |
|---|---|---|---|---|---|---|
| P.4.10 | V45 | .000 | | | | |
| P.6.1 | V47 | .587 | .000 | | | |
| P.6.2 | V48 | .561 | .219 | .000 | | |
| P.6.3 | V49 | .948 | -.223 | .110 | .000 | |
| P.6.4 | V50 | .555 | .297 | -.046 | -.231 | .000 |

```
          P.6.5       V51             1.133          -.159          -
.112       .084       .181


                            P.6.5
                               V51
          P.6.5    V51         .000


                          AVERAGE   ABSOLUTE    COVARIANCE    RESIDUALS
=          .4839
             AVERAGE   OFF-DIAGONAL   ABSOLUTE    COVARIANCE    RESIDUALS
=          .5162


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sob

       MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)



       STANDARDIZED RESIDUAL MATRIX:


                            P.1.1        P.1.2        P.1.3        P.1.5
P.1.6
                               V1           V2           V3           V5
V6
          P.1.1    V1          .000
          P.1.2    V2          .053       .000
          P.1.3    V3         -.026      -.019       .000
          P.1.5    V5          .094       .026       .046       .000
          P.1.6       V6                 .008            .028           -
.006       .000       .000
          P.1.8     V8          -.028       -.031        .048       -.093
-.023
          P.1.9     V9          -.088        .049       -.070       -.181
-.028
          P.1.10    V10          .021        .023        .075        .044
-.065
          P.1.11         V11                        -.021               -
.021       .000       .013       .029
          P.1.12    V12          -.006         .021         .010         -
.054       .025
          P.1.16    V16         -.042       -.013        .015        .005
-.033
          P.1.17         V17                        -.053               -
.032       .019       .099       .038
          P.2.2     V19         -.106       -.113       -.001       -.090
-.126
          P.2.3     V20         -.075       -.044        .003       -.080
-.051
          P.2.4     V21         -.040       -.054       -.033       -.089
-.180
          P.2.6     V23          .058        .042        .037       -.056
-.119
```

| | | | | | | |
|---|---|---|---|---|---|---|
| P.3.1 | V33 | -.058 | .012 | .076 | -.150 | -.153 |
| P.3.3 | V35 | .051 | .097 | .071 | -.071 | -.073 |
| P.4.1 | V36 | -.086 | .017 | -.067 | -.152 | -.092 |
| P.4.2 | V37 | -.032 | .031 | -.010 | -.093 | -.001 |
| P.4.3 | V38 | -.058 | .023 | -.073 | -.104 | .001 |
| P.4.4 | V39 | -.016 | .017 | -.056 | -.094 | .013 |
| P.4.7 | V42 | -.078 | .024 | .011 | -.166 | -.099 |
| P.4.8 | V43 | .002 | .130 | .075 | -.071 | -.030 |
| P.4.9 | V44 | -.092 | .001 | -.014 | -.104 | -.082 |
| P.4.10 | V45 | -.037 | .033 | .020 | -.058 | .049 |
| P.6.1 | V47 | -.031 | -.007 | .032 | -.103 | -.068 |
| P.6.2 | V48 | -.098 | -.119 | -.096 | -.092 | -.009 |
| P.6.3 | V49 | .001 | -.049 | .012 | .036 | .082 |
| P.6.4 | V50 | -.056 | -.103 | -.038 | -.098 | -.046 |
| P.6.5 | V51 | .018 | .003 | -.003 | -.045 | -.009 |

| | | P.1.8 | P.1.9 | P.1.10 | P.1.11 | P.1.12 |
|---|---|---|---|---|---|---|
| | | V8 | V9 | V10 | V11 | V12 |
| P.1.8 | V8 | .000 | | | | |
| P.1.9 | V9 | .023 | .000 | | | |
| P.1.10 | V10 | -.079 | -.109 | .000 | | |
| P.1.11 | V11 | .062 | -.006 | .032 | .000 | |
| P.1.12 | V12 | .114 | .035 | .000 | .065 | .000 |
| P.1.16 | V16 | -.007 | -.077 | -.004 | -.012 | .031 |
| P.1.17 | V17 | -.073 | -.016 | -.010 | -.044 | .009 |
| P.2.2 | V19 | .005 | -.052 | -.090 | -.029 | -.040 |
| P.2.3 | V20 | .109 | .101 | -.101 | .000 | .047 |
| P.2.4 | V21 | .007 | .075 | -.040 | -.094 | .079 |
| P.2.6 | V23 | .144 | .124 | .035 | .072 | .133 |
| P.3.1 | V33 | .033 | .042 | -.222 | -.011 | -.126 |
| P.3.3 | V35 | .066 | .065 | -.120 | .042 | -.063 |

P.4.1 V36 .044 .103 -
.081 .013 .088
P.4.2 V37 .090 .095 -.061 -
.060 .125
P.4.3 V38 .090 .164 -.123 -
.011 .151
P.4.4 V39 .112 .178 -
.116 .027 .122
P.4.7 V42 .033 -.042 -
.123 .022 .014
P.4.8 V43 .051 -.009 -
.092 .082 .034
P.4.9 V44 .032 .088 -
.190 .011 .031
P.4.10 V45 .121 .046 -.139 -
.001 .026
P.6.1 V47 .072 .039 -.086 .031
-.031
P.6.2 V48 -.011 -.079 -.088 -.013
-.049
P.6.3 V49 .135 .039 -
.121 .070 .025
P.6.4 V50 .025 .036 -.118 -.076
-.038
P.6.5 V51 .034 .004 -.050 .016
-.047

P.1.16 P.1.17 P.2.2 P.2.3
P.2.4
V16 V17 V19 V20
V21
P.1.16 V16 .000
P.1.17 V17 .035 .000
P.2.2 V19 .014 -.013 .000
P.2.3 V20 -.019 .011 .031 .000
P.2.4 V21 .049 .089 -.019 -
.058 .000
P.2.6 V23 .037 .044 -.054 -
.023 .192
P.3.1 V33 -.052 -
.036 .088 .117 .106
P.3.3 V35 -
.003 .044 .031 .102 .056
P.4.1 V36 -
.075 .003 .166 .180 .307
P.4.2 V37 -.121 -
.038 .175 .168 .268
P.4.3 V38 -.101 -
.016 .123 .178 .268
P.4.4 V39 -.114 -
.036 .158 .200 .313
P.4.7 V42 -.081 -
.024 .181 .110 .225
P.4.8 V43 -
.056 .067 .273 .229 .331
P.4.9 V44 -
.023 .051 .206 .163 .374

| | | | | | | |
|---|---|---|---|---|---|---|
| P.4.10 | V45 | -.018 | .079 | .174 | .167 | .189 |
| P.6.1 | V47 | .027 | -.004 | -.065 | .015 | .107 |
| P.6.2 | V48 | -.004 | -.134 | .068 | .110 | .175 |
| P.6.3 | V49 | .052 | -.020 | .074 | .144 | .072 |
| P.6.4 | V50 | -.081 | -.114 | .096 | .163 | .262 |
| P.6.5 | V51 | .041 | -.023 | .043 | .143 | .076 |

| | | P.2.6 | P.3.1 | P.3.3 | P.4.1 | P.4.2 |
|---|---|---|---|---|---|---|
| | | V23 | V33 | V35 | V36 | V37 |
| P.2.6 | V23 | .000 | | | | |
| P.3.1 | V33 | -.007 | .000 | | | |
| P.3.3 | V35 | .100 | .000 | .000 | | |
| P.4.1 | V36 | .254 | .323 | .359 | .000 | |
| P.4.2 | V37 | .252 | .181 | .265 | .013 | .000 |
| P.4.3 | V38 | .247 | .216 | .346 | .000 | .000 |
| P.4.4 | V39 | .271 | .233 | .244 | -.026 | -.004 |
| P.4.7 | V42 | .233 | .167 | .178 | .001 | -.052 |
| P.4.8 | V43 | .308 | .186 | .184 | .068 | .016 |
| P.4.9 | V44 | .293 | .222 | .200 | .027 | -.017 |
| P.4.10 | V45 | .261 | .176 | .237 | .081 | .056 |
| P.6.1 | V47 | .045 | .188 | .192 | .205 | .210 |
| P.6.2 | V48 | .228 | .043 | .151 | .240 | .236 |
| P.6.3 | V49 | .175 | .038 | .180 | .186 | .223 |
| P.6.4 | V50 | .239 | .057 | .077 | .230 | .321 |
| P.6.5 | V51 | .108 | .085 | .150 | .208 | .207 |

| | | P.4.3 | P.4.4 | P.4.7 | P.4.8 | P.4.9 |
|---|---|---|---|---|---|---|
| | | V38 | V39 | V42 | V43 | V44 |
| P.4.3 | V38 | .000 | | | | |
| P.4.4 | V39 | .002 | .000 | | | |
| P.4.7 | V42 | -.079 | -.023 | .000 | | |
| P.4.8 | V43 | -.007 | .047 | .096 | .000 | |
| P.4.9 | V44 | -.010 | .057 | -.038 | -.035 | .000 |

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           P.4.10    V45            .039          .063          -.067         -
.073        .109
           P.6.1
V47         .218        .263        .121        .099        .174
           P.6.2
V48         .227        .229        .123        .068        .129
           P.6.3
V49         .277        .268        .075        .074        .176
           P.6.4
V50         .315        .344        .147        .106        .175
           P.6.5
V51         .184        .221        .190        .135        .174


                              P.4.10       P.6.1        P.6.2         P.6.3
P.6.4
                                 V45          V47          V48           V49
V50
           P.4.10   V45          .000
           P.6.1    V47          .109        .000
           P.6.2    V48          .109        .042        .000
           P.6.3    V49          .177       -.042        .021        .000
           P.6.4     V50            .110          .059          -.009         -
.046        .000
           P.6.5       V51                   .217          -.030              -
.022        .016       .037


                              P.6.5
                                 V51
           P.6.5    V51          .000


                            AVERAGE    ABSOLUTE    STANDARDIZED    RESIDUALS
=          .0827
              AVERAGE   OFF-DIAGONAL   ABSOLUTE    STANDARDIZED    RESIDUALS
=          .0882


        LARGEST STANDARDIZED RESIDUALS:

            NO.     PARAMETER   ESTIMATE      NO.     PARAMETER   ESTIMATE
            ---     ---------   --------      ---     ---------   --------
             1      V44, V21        .374       11      V36, V21        .307
             2      V36, V35        .359       12      V44, V23        .293
             3      V38, V35        .346       13      V49, V38        .277
             4      V50, V39        .344       14      V43, V19        .273
             5      V43, V21        .331       15      V39, V23        .271
             6      V36, V33        .323       16      V49, V39        .268
             7      V50, V37        .321       17      V38, V21        .268
             8      V50, V38        .315       18      V37, V21        .268
             9      V39, V21        .313       19      V37, V35        .265
            10      V43, V23        .308       20      V47, V39        .263
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sob

        MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


        DISTRIBUTION OF STANDARDIZED RESIDUALS


           ----------------------------------------
           !                                      !
        180-                    *                 -
           !                    *                 !
           !                 *  *                 !
           !                 *  *                 !
           !                   *  *                   !              RANGE
FREQ PERCENT
        135-                 *  *                 -
           !                  *  *                  !    1    -0.5   -  --
0     .00%
           !                  *  *                !    2    -0.4   -  -0.5
0     .00%
           !                  *  *                !    3    -0.3   -  -0.4
0     .00%
           !                  *  *                !    4    -0.2   -  -0.3
1     .20%
         90-                  *  *                -    5    -0.1   -  -0.2
31    6.25%
           !                  *  *                !    6     0.0   -  -0.1
160   32.26%
           !                  *  *  *             !    7     0.1   -   0.0
183   36.90%
           !                  *  *  *             !    8     0.2   -   0.1
70   14.11%
           !                  *  *  *             !    9     0.3   -   0.2
40    8.06%
         45-                  *  *  *             -    A     0.4   -   0.3
11    2.22%
           !                  *  *  *  *          !    B     0.5   -   0.4
0     .00%
           !               *  *  *  *  *          !    C      ++   -   0.5
0     .00%
           !              *  *  *  *  *           !    -----------------
-------------
           !                *  *  *  *  *  *          !              TOTAL
496 100.00%
           ----------------------------------------
              1  2  3  4  5  6  7  8  9  A  B  C     EACH "*" REPRESENTS
9 RESIDUALS
```

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sob

       MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)



       GOODNESS OF FIT SUMMARY FOR METHOD = ML

       INDEPENDENCE MODEL CHI-SQUARE          =     3658.720 ON    465
DEGREES OF FREEDOM

       INDEPENDENCE AIC =  2728.71971   INDEPENDENCE CAIC =   805.57344
              MODEL AIC =   -79.68568          MODEL CAIC = -1829.12842

       CHI-SQUARE =      766.314 BASED ON     423 DEGREES OF FREEDOM
       PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00000

       THE NORMAL THEORY RLS CHI-SQUARE FOR THIS ML SOLUTION IS
735.739.

       FIT INDICES
       -----------
       BENTLER-BONETT     NORMED FIT INDEX =      .791
       BENTLER-BONETT NON-NORMED FIT INDEX =      .882
       COMPARATIVE FIT INDEX (CFI)         =      .893
       BOLLEN   (IFI) FIT INDEX            =      .894
       MCDONALD (MFI) FIT INDEX            =      .364
       LISREL    GFI  FIT INDEX            =      .781
       LISREL   AGFI  FIT INDEX            =      .743
       ROOT MEAN-SQUARE RESIDUAL (RMR)     =      .655
       STANDARDIZED RMR                    =      .114
       ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .069
       90% CONFIDENCE INTERVAL OF RMSEA  (        .061,        .077)

       RELIABILITY COEFFICIENTS
       ------------------------
       CRONBACH'S ALPHA                    =      .918
       COEFFICIENT ALPHA FOR AN OPTIMAL SHORT SCALE
=      .959
       BASED ON THE FOLLOWING  3 VARIABLES
       P.4.2     P.4.3     P.4.4
       RELIABILITY COEFFICIENT RHO         =      .950
       GREATEST LOWER BOUND RELIABILITY
=      .978
       GLB RELIABILITY FOR AN OPTIMAL SHORT SCALE
=      .979
       BASED ON 29 VARIABLES, ALL EXCEPT:
       P.3.1     P.3.3
       BENTLER'S DIMENSION-FREE LOWER BOUND RELIABILITY
=      .978
       SHAPIRO'S LOWER BOUND RELIABILITY FOR A WEIGHTED COMPOSITE
=      .986
       WEIGHTS THAT ACHIEVE SHAPIRO'S LOWER BOUND:
       P.1.1     P.1.2     P.1.3     P.1.5     P.1.6     P.1.8
           .120      .161      .130      .103      .124      .152
```

```
        P.1.9      P.1.10     P.1.11     P.1.12     P.1.16     P.1.17
            .123       .065       .126       .166       .097       .105
        P.2.2      P.2.3      P.2.4      P.2.6      P.3.1      P.3.3
            .137       .135       .155       .154       .060       .101
        P.4.1      P.4.2      P.4.3      P.4.4      P.4.7      P.4.8
            .213       .340       .364       .319       .176       .207
        P.4.9      P.4.10     P.6.1      P.6.2      P.6.3      P.6.4
            .215       .209       .154       .156       .203       .173
        P.6.5
            .185


        GOODNESS OF FIT SUMMARY FOR METHOD = ROBUST

        ROBUST  INDEPENDENCE  MODEL  CHI-SQUARE  =      3486.497  ON     465
DEGREES OF FREEDOM

        INDEPENDENCE AIC =  2556.49747   INDEPENDENCE CAIC =   633.35120
               MODEL AIC =  -216.92186          MODEL CAIC = -1966.36460

        SATORRA-BENTLER  SCALED  CHI-SQUARE  =      629.0781  ON        423
DEGREES OF FREEDOM
        PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00000

        FIT INDICES
        -----------
        BENTLER-BONETT     NORMED FIT INDEX =      .820
        BENTLER-BONETT NON-NORMED FIT INDEX =      .925
        COMPARATIVE FIT INDEX (CFI)         =      .932
        BOLLEN   (IFI) FIT INDEX            =      .933
        MCDONALD (MFI) FIT INDEX            =      .545
        ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .054
        90% CONFIDENCE INTERVAL OF RMSEA  (        .045,        .062)


                               ITERATIVE SUMMARY

                           PARAMETER
        ITERATION                      ABS   CHANGE                    ALPHA
FUNCTION
            1                             1.941457                   1.00000
5.89757
            2                               .308884                  1.00000
4.85579
            3                              .282689                    .50000
4.64303
            4                               .086042                  1.00000
4.55178
            5                               .041239                  1.00000
4.53792
            6                               .019997                  1.00000
4.53516
            7                               .009886                  1.00000
4.53458
            8                               .004981                  1.00000
4.53445
```

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          9                              .002487               1.00000
4.53442
         10                              .001318               1.00000
4.53441
         11                              .000693               1.00000
4.53440


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       MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


       MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
       STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
       (ROBUST STATISTICS IN PARENTHESES)


      P.1.1   =V1  =   1.000 F1    + 1.000 E1




      P.1.2   =V2  =   1.018*F1    + 1.000 E2
                        .095
                      10.727@
                    (   .070)
                    ( 14.525@

      P.1.3   =V3  =    .981*F1    + 1.000 E3
                        .092
                      10.623@
                    (   .072)
                    ( 13.619@

      P.1.5   =V5  =   1.150*F3    + 1.000 E5
                        .119
                       9.643@
                    (   .099)
                    ( 11.641@

      P.1.6   =V6  =   1.000 F3    + 1.000 E6




      P.1.8   =V8  =    .813*F1    + 1.000 E8
                        .089
                       9.083@
                    (   .077)
                    ( 10.592@

      P.1.9   =V9  =   1.000 F4    + 1.000 E9
```

```
P.1.10  =V10 =   1.000 F2    + 1.000 E10



P.1.11  =V11 =   1.093*F2    + 1.000 E11
                   .159
                  6.869@
              (    .128)
              (   8.533@

P.1.12  =V12 =   1.479*F4    + 1.000 E12
                   .214
                  6.907@
              (    .197)
              (   7.494@

P.1.16  =V16 =   1.125*F2    + 1.000 E16
                   .154
                  7.328@
              (    .120)
              (   9.345@

P.1.17  =V17 =   1.007*F2    + 1.000 E17
                   .144
                  6.994@

              (    .124)
              (   8.092@
```

MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS (CONTINUED)

29-Jun-17 PAGE : 9 EQS Licensee:
TITLE: master confirmatorio la 5 sobre la 6, 7, 10 y 11 y la 4 sob

MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)
(ROBUST STATISTICS IN PARENTHESES)

```
P.2.2   =V19 =   1.000 F6    + 1.000 E19



P.2.3   =V20 =    .906*F6    + 1.000 E20
                   .077
                 11.799@
              (    .082)
```

```
                ( 11.039@

P.2.4   =V21 =    .899*F6    + 1.000 E21
                  .105
                 8.580@
                (   .085)
                ( 10.626@

P.2.6   =V23 =    .876*F6    + 1.000 E23
                  .095
                 9.262@
                (   .086)
                ( 10.135@

P.3.1   =V33 =   1.000 F7    + 1.000 E33




P.3.3   =V35 =    .906*F7    + 1.000 E35
                  .391
                 2.320@
                (   .435)
                (  2.085@

P.4.1   =V36 =   1.000 F8    + 1.000 E36




P.4.2   =V37 =   1.306*F8    + 1.000 E37
                  .109
                11.972@
                (   .120)
                ( 10.894@

P.4.3   =V38 =   1.359*F8    + 1.000 E38
                  .111
                12.229@
                (   .127)
                ( 10.683@

P.4.4   =V39 =   1.292*F8    + 1.000 E39
                  .112
                11.589@
                (   .123)
                ( 10.477@

P.4.7   =V42 =   1.000 F9    + 1.000 E42




P.4.8   =V43 =   1.056*F9    + 1.000 E43
                  .083
```

```
                      12.785@
                    (   .075)
                    ( 14.141@


        MEASUREMENT  EQUATIONS  WITH  STANDARD  ERRORS  AND  TEST  STATISTICS
(CONTINUED)


      29-Jun-17      PAGE : 10  EQS     Licensee:
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sob

        MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)
        (ROBUST STATISTICS IN PARENTHESES)

       P.4.9   =V44 =   1.099*F9    + 1.000 E44
                         .086
                       12.768@
                    (   .080)
                    ( 13.783@

       P.4.10  =V45 =    .970*F9    + 1.000 E45
                         .087
                       11.134@
                    (   .083)
                    ( 11.752@

       P.6.1   =V47 =   1.000 F10   + 1.000 E47




       P.6.2   =V48 =    .991*F10   + 1.000 E48
                         .100
                        9.942@
                    (   .091)
                    ( 10.948@

       P.6.3   =V49 =   1.106*F10   + 1.000 E49
                         .103
                       10.717@
                    (   .092)
                    ( 12.001@

       P.6.4   =V50 =    .885*F10   + 1.000 E50
                         .098
                        9.002@
                    (   .091)
                    (  9.681@

       P.6.5   =V51 =   1.035*F10   + 1.000 E51
                         .101
                       10.254@
                    (   .102)
                    ( 10.114@
```

```
    29-Jun-17      PAGE : 11  EQS     Licensee:
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sob

      MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


      CONSTRUCT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
      STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
      (ROBUST STATISTICS IN PARENTHESES)



 F1   =F1  =   1.218*F5    + 1.000 D1
                .185
               6.576@
            (   .155)
            (  7.846@

 F2   =F2  =   1.000 F5    + 1.000 D2




 F3   =F3  =    .960*F5    + 1.000 D3
                .167
               5.736@
            (   .142)
            (  6.750@

 F6   =F6  =    .324*F5    + 1.000 D6
                .104
               3.122@
            (   .102)
            (  3.190@

 F7   =F7  =    .762*F4    -   .663*F5    + 1.000 D7
                .342            .311
               2.226@         -2.135@
            (   .416)      (    .381)
            (  1.829)      (  -1.743)

 F8   =F8  =   1.000 F11   + 1.000 D8




 F9   =F9  =   1.087*F11   + 1.000 D9
                .278
               3.905@
            (   .244)
            (  4.458@

 F10  =F10 =    .819*F4    + 1.000 D10
                .139
               5.873@
```

```
                (   .127)
                (  6.466@

     F11  =F11 =    .363*F5    + 1.000 D11
                    .099
                   3.654@
                (   .106)
                (  3.422@


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sob

     MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

     VARIANCES OF INDEPENDENT VARIABLES
     ----------------------------------
     STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                    V                                F
                   ---                              ---
                                 I F4  -   F4              2.329*I
                                 I                          .619 I
                                 I                         3.764@I
                                 I                      (   .573)I
                                 I                      (  4.067@I
                                 I                               I
                                 I F5  -   F5              2.635*I
                                 I                          .692 I
                                 I                         3.810@I
                                 I                      (   .626)I
                                 I                      (  4.211@I
                                 I                               I


   29-Jun-17      PAGE : 13  EQS     Licensee:
     TITLE:   master confirmatorio la 5 sobre la 6, 7, 10 y 11 y la 4
sob

     MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

     VARIANCES OF INDEPENDENT VARIABLES
     ----------------------------------
     STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                    E                                D
                   ---                              ---
   E1  -P.1.1              3.734*I D1  -   F1              1.173*I
                            .492 I                          .365 I
                           7.597@I                         3.216@I
                        (   .590)I                      (   .442)I
                        (  6.327@I                      (  2.653@I
                                 I                               I
   E2  -P.1.2              2.500*I D2  -   F2               .527*I
                            .373 I                          .260 I
                           6.700@I                         2.026@I
                        (   .424)I                      (   .276)I
```

```
                           (  5.896@I                          (  1.911)I
                                    I                                   I
 E3  -P.1.3                   2.462*I D3  -   F3                  2.278*I
                               .360 I                              .453 I
                              6.842@I                             5.029@I
                           (   .443)I                          (   .464)I
                           (  5.556@I                          (  4.909@I
                                    I                                   I
 E5  -P.1.5                    .812*I D6  -   F6                  2.954*I
                               .514 I                              .474 I
                              1.579 I                             6.231@I
                           (   .535)I                          (   .507)I
                           (  1.520)I                          (  5.825@I
                                    I                                   I
 E6  -P.1.6                   3.084*I D7  -   F7                  2.524*I
                               .509 I                             1.239 I
                              6.058@I                             2.038@I
                           (   .619)I                          (  1.346)I
                           (  4.978@I                          (  1.876)I
                                    I                                   I
 E8  -P.1.8                   3.389*I D8  -   F8                  1.257*I
                               .421 I                              .457 I
                              8.040@I                             2.748@I
                           (   .442)I                          (   .435)I
                           (  7.664@I                          (  2.891@I
                                    I                                   I
 E9  -P.1.9                   4.507*I D9  -   F9                  1.389*I
                               .557 I                              .517 I
                              8.086@I                             2.686@I
                           (   .543)I                          (   .532)I
                           (  8.294@I                          (  2.610@I
                                    I                                   I
 E10 -P.1.10                  5.213*I D10 -   F10                 1.465*I
                               .639 I                              .321 I
                              8.159@I                             4.558@I
                           (   .645)I                          (   .280)I
                           (  8.088@I                          (  5.225@I
                                    I                                   I
 E11 -P.1.11                  4.665*I D11 -   F11                 1.363*I
                               .598 I                              .459 I
                              7.801@I                             2.970@I
                           (   .559)I                          (   .449)I
                           (  8.339@I                          (  3.037@I
                                    I                                   I
 E12 -P.1.12                  2.961*I                                   I
                               .554 I                                   I
                              5.347@I                                   I
                           (   .591)I                                   I
                           (  5.009@I                                   I
                                    I                                   I
 E16 -P.1.16                  3.406*I                                   I
                               .477 I                                   I
                              7.139@I                                   I
                           (   .499)I                                   I
                           (  6.823@I                                   I
                                    I                                   I
 E17 -P.1.17                  3.609*I                                   I
                               .471 I                                   I
```

```
                        7.659@I                                I
                     (   .609)I                                I
                     (  5.928@I                                I
                              I                                I
```



MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

VARIANCES OF INDEPENDENT VARIABLES (CONTINUED)

```
 E19 -P.2.2             1.305*I                                I
                         .239 I                                I
                        5.463@I                                I
                     (   .432)I                                I
                     (  3.022@I                                I
                              I                                I
 E20 -P.2.3              .923*I                                I
                         .186 I                                I
                        4.967@I                                I
                     (   .288)I                                I
                     (  3.203@I                                I
                              I                                I
 E21 -P.2.4             3.794*I                                I
                         .460 I                                I
                        8.256@I                                I
                     (   .517)I                                I
                     (  7.334@I                                I
                              I                                I
 E23 -P.2.6             2.883*I                                I
                         .360 I                                I
                        8.014@I                                I
                     (   .529)I                                I
                     (  5.449@I                                I
                              I                                I
 E33 -P.3.1             2.678*I                                I
                        1.310 I                                I
                        2.045@I                                I
                     (  1.566)I                                I
                     (  1.710)I                                I
                              I                                I
 E35 -P.3.3             3.107*I                                I
                        1.102 I                                I
                        2.818@I                                I
                     (  1.200)I                                I
                     (  2.589@I                                I
                              I                                I

 E36 -P.4.1             3.006*I                                I
                         .338 I                                I
                        8.883@I                                I
                     (   .471)I                                I
                     (  6.388@I                                I
                              I                                I
 E37 -P.4.2              .610*I                                I
```

```
                              .100 I                               I
                             6.106@I                               I
                          (   .187)I                               I
                          (  3.260@I                               I
                                   I                               I
 E38 -P.4.3                   .366*I                               I
                              .089 I                               I
                             4.129@I                               I
                          (   .280)I                               I
                          (  1.305)I                               I
                                   I                               I
 E39 -P.4.4                   .984*I                               I
                              .132 I                               I
                             7.476@I                               I
                          (   .349)I                               I
                          (  2.818@I                               I
                                   I                               I
 E42 -P.4.7                  1.707*I                               I
                              .237 I                               I
                             7.205@I                               I
                          (   .280)I                               I
                          (  6.095@I                               I
                                   I                               I
 E43 -P.4.8                  1.356*I                               I
                              .213 I                               I
                             6.380@I                               I
                          (   .362)I                               I
                          (  3.743@I                               I
                                   I                               I


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES (CONTINUED)
  ----------------------------------------------

 E44 -P.4.9                  1.481*I                               I
                              .231 I                               I
                             6.403@I                               I
                          (   .368)I                               I
                          (  4.023@I                               I
                                   I                               I
 E45 -P.4.10                 2.160*I                               I
                              .280 I                               I
                             7.728@I                               I
                          (   .295)I                               I
                          (  7.331@I                               I
                                   I                               I
 E47 -P.6.1                  2.394*I                               I
                              .307 I                               I
                             7.794@I                               I
                          (   .441)I                               I
                          (  5.428@I                               I
                                   I                               I
```

```
 E48 -P.6.2                1.975*I                                I
                            .263 I                                I
                           7.521@I                                I
                        (   .409)I                                I
                        (  4.823@I                                I
                                 I                                I
 E49 -P.6.3                1.623*I                                I
                            .244 I                                I
                           6.649@I                                I
                        (   .323)I                                I
                        (  5.029@I                                I
                                 I                                I
 E50 -P.6.4                2.386*I                                I
                            .295 I                                I
                           8.098@I                                I
                        (   .344)I                                I
                        (  6.937@I                                I
                                 I                                I
 E51 -P.6.5                1.843*I                                I
                            .255 I                                I
                           7.235@I                                I
                        (   .319)I                                I
                        (  5.775@I                                I
                                 I                                I
```

```
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  COVARIANCES AMONG INDEPENDENT VARIABLES
  ---------------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                  V                                 F
                 ---                               ---
                                 I F5   -   F5                2.001*I
                                 I F4   -   F4                 .430 I
                                 I                            4.658@I
                                 I                         (   .361)I
                                 I                         (  5.542@I
                                 I                                  I
```

```
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sob

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  DECOMPOSITION OF EFFECTS WITH NONSTANDARDIZED VALUES
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

  PARAMETER TOTAL EFFECTS
  -----------------------
```

```
     P.1.1   =V1  =   1.000 F1    + 1.218 F5    + 1.000 E1    + 1.000
D1
                                     .185
                                    6.576@
                                  (   .155)
                                  (  7.846@

     P.1.2   =V2  =   1.018*F1    + 1.240 F5    + 1.000 E2    + 1.018
D1
                      .095           .181                        .095
                    10.727@         6.841@                     10.727@
                  (   .070)       (   .206)                  (   .070)
                  ( 14.525@       (  6.023@                  ( 14.525@

     P.1.3   =V3  =    .981*F1    + 1.195 F5    + 1.000 E3    +  .981
D1
                      .092           .176                        .092
                    10.623@         6.810@                     10.623@
                  (   .072)       (   .199)                  (   .072)
                  ( 13.619@       (  6.010@                  ( 13.619@

     P.1.5   =V5  =   1.150*F3    + 1.105 F5    + 1.000 E5    + 1.150
D3
                      .119           .168                        .119
                     9.643@         6.564@                      9.643@
                  (   .099)       (   .233)                  (   .099)
                  ( 11.641@       (  4.734@                  ( 11.641@

     P.1.6   =V6  =   1.000 F3    +  .960 F5    + 1.000 E6    + 1.000
D3
                                     .167
                                    5.736@
                                  (   .142)
                                  (  6.750@

     P.1.8   =V8  =    .813*F1    +  .990 F5    + 1.000 E8    +  .813
D1
                      .089           .156                        .089
                     9.083@         6.330@                      9.083@
                  (   .077)       (   .163)                  (   .077)
                  ( 10.592@       (  6.063@                  ( 10.592@

     P.1.9   =V9  =   1.000 F4    + 1.000 E9


     P.1.10  =V10 =   1.000 F2    + 1.000 F5    + 1.000 E10   + 1.000
D2
```

```
 P.1.11  =V11 =   1.093*F2    + 1.093 F5    + 1.000 E11   + 1.093
D2
                   .159         .159                        .159
                  6.869@       6.869@                      6.869@
               (   .128)    (   .128)                   (   .128)
               (  8.533@    (  8.533@                   (  8.533@

 P.1.12  =V12 =   1.479*F4    + 1.000 E12



 P.1.16  =V16 =   1.125*F2    + 1.125 F5    + 1.000 E16   + 1.125
D2
                   .154         .154                        .154
                  7.328@       7.328@                      7.328@
               (   .120)    (   .120)                   (   .120)
               (  9.345@    (  9.345@                   (  9.345@

 P.1.17  =V17 =   1.007*F2    + 1.007 F5    + 1.000 E17   + 1.007
D2
                   .144         .144                        .144
                  6.994@       6.994@                      6.994@
               (   .124)    (   .124)                   (   .124)
               (  8.092@    (  8.092@                   (  8.092@

 P.2.2   =V19 =   1.000 F6    +  .324 F5    + 1.000 E19   + 1.000
D6
                                .104
                               3.122@
                            (   .102)
                            (  3.190@

 P.2.3   =V20 =    .906*F6    +  .293 F5    + 1.000 E20   +  .906
D6
                   .077         .094                        .077
                 11.799@       3.129@                     11.799@
               (   .082)    (   .098)                   (   .082)
               ( 11.039@    (  2.988@                   ( 11.039@

 P.2.4   =V21 =    .899*F6    +  .291 F5    + 1.000 E21   +  .899
D6
                   .105         .096                        .105
                  8.580@       3.021@                      8.580@
               (   .085)    (   .099)                   (   .085)
               ( 10.626@    (  2.939@                   ( 10.626@
```

```
      P.2.6   =V23 =    .876*F6    +  .284 F5    + 1.000 E23   +  .876
D6
                       .095          .093                        .095
                      9.262@        3.049@                      9.262@
                    (  .086)      (  .094)                    (  .086)
                    ( 10.135@     (  3.021@                   ( 10.135@


      P.3.1   =V33 =   1.000 F7    +  .762 F4    -  .663 F5    + 1.000
E33
                                     .342          .311
                                    2.226@       -2.135@
                                  (  .416)      (  .381)
                                  (  1.829)     ( -1.743)

                     + 1.000 D7




      P.3.3   =V35 =    .906*F7    +  .690 F4    -  .601 F5    + 1.000
E35
                       .391          .334          .301
                      2.320@        2.069@       -1.995@
                    (  .435)      (  .612)      (  .546)
                    (  2.085@     (  1.128)     ( -1.102)

                     +  .906 D7
                       .391
                      2.320@
                    (  .435)
                    (  2.085@
      P.4.1   =V36 =   1.000 F8    + 1.000 F11   +  .363 F5    + 1.000
E36
                                                   .099
                                                  3.654@
                                                (  .106)
                                                (  3.422@

                     + 1.000 D8    + 1.000 D11




      P.4.2   =V37 =   1.306*F8    + 1.306 F11   +  .475 F5    + 1.000
E37
                       .109          .109          .125
                     11.972@       11.972@        3.794@
                    (  .120)      (  .120)      (  .152)
                    ( 10.894@     ( 10.894@     (  3.124@

                     + 1.306 D8    + 1.306 D11
                       .109          .109
                     11.972@       11.972@
                    (  .120)      (  .120)
```

```
                    ( 10.894@     ( 10.894@

     P.4.3   =V38 =   1.359*F8    + 1.359 F11   +  .494 F5    + 1.000
E38
                        .111          .111          .130
                      12.229@       12.229@       3.804@
                    (   .127)     (   .127)     (   .160)
                    ( 10.683@     ( 10.683@     (  3.079@

                     + 1.359 D8    + 1.359 D11
                        .111          .111
                      12.229@       12.229@
                    (   .127)     (   .127)
                    ( 10.683@     ( 10.683@

     P.4.4   =V39 =   1.292*F8    + 1.292 F11   +  .469 F5    + 1.000
E39
                        .112          .112          .124
                      11.589@       11.589@       3.782@
                    (   .123)     (   .123)     (   .150)
                    ( 10.477@     ( 10.477@     (  3.130@

                     + 1.292 D8    + 1.292 D11
                        .112          .112
                      11.589@       11.589@
                    (   .123)     (   .123)
                    ( 10.477@     ( 10.477@

     P.4.7   =V42 =   1.000 F9    + 1.087 F11   +  .395 F5    + 1.000
E42
                                      .278          .108
                                     3.905@       3.669@
                                  (   .244)     (   .165)
                                  (  4.458@     (  2.394@

                     + 1.000 D9    + 1.087 D11
                                      .278
                                     3.905@
                                  (   .244)
                                  (  4.458@

     P.4.8   =V43 =   1.056*F9    + 1.148 F11   +  .417 F5    + 1.000
E43
                        .083          .292          .113
                      12.785@        3.934@       3.692@
                    (   .075)     (   .261)     (   .175)
                    ( 14.141@     (  4.396@     (  2.383@

                     + 1.056 D9    + 1.148 D11
                        .083          .292
                      12.785@        3.934@
                    (   .075)     (   .261)
                    ( 14.141@     (  4.396@

     P.4.9   =V44 =   1.099*F9    + 1.195 F11   +  .434 F5    + 1.000
E44
                        .086          .304          .118
                      12.768@        3.933@       3.692@
                    (   .080)     (   .270)     (   .182)
```

```
                    ( 13.783@     (  4.425@     (  2.380@

                     + 1.099 D9    + 1.195 D11
                        .086          .304
                      12.768@        3.933@
                    (   .080)     (   .270)
                    ( 13.783@     (  4.425@

      P.4.10  =V45 =    .970*F9    + 1.055 F11   +  .383 F5    + 1.000
E45
                        .087          .273          .105
                      11.134@        3.872@        3.641@
                    (   .083)     (   .246)     (   .162)
                    ( 11.752@     (  4.291@     (  2.367@

                     +  .970 D9    + 1.055 D11
                        .087          .273
                      11.134@        3.872@
                    (   .083)     (   .246)
                    ( 11.752@     (  4.291@

      P.6.1   =V47 =   1.000 F10   +  .819 F4    + 1.000 E47   + 1.000
D10
                                      .139
                                     5.873@
                                  (   .127)
                                  (  6.466@


      P.6.2   =V48 =    .991*F10   +  .811 F4    + 1.000 E48   +  .991
D10
                        .100          .136                        .100
                       9.942@        5.960@                      9.942@
                    (   .091)     (   .159)                   (   .091)
                    ( 10.948@     (  5.089@                   ( 10.948@


      P.6.3   =V49 =   1.106*F10   +  .906 F4    + 1.000 E49   + 1.106
D10
                        .103          .148                        .103
                      10.717@        6.127@                     10.717@
                    (   .092)     (   .173)                   (   .092)
                    ( 12.001@     (  5.227@                   ( 12.001@


      P.6.4   =V50 =    .885*F10   +  .725 F4    + 1.000 E50   +  .885
D10
                        .098          .126                        .098
                       9.002@        5.734@                      9.002@
                    (   .091)     (   .154)                   (   .091)
                    (  9.681@     (  4.707@                   (  9.681@


      P.6.5   =V51 =   1.035*F10   +  .847 F4    + 1.000 E51   + 1.035
D10
                        .101          .141                        .101
                      10.254@        6.028@                     10.254@
                    (   .102)     (   .173)                   (   .102)
```

```
                  ( 10.114@     (   4.908@                   ( 10.114@

          F1   =F1  =   1.218*F5    + 1.000 D1



          F2   =F2  =   1.000 F5    + 1.000 D2



          F3   =F3  =    .960*F5    + 1.000 D3



          F6   =F6  =    .324*F5    + 1.000 D6



          F7   =F7  =    .762*F4    -   .663*F5    + 1.000 D7



          F8   =F8  =   1.000 F11   +   .363 F5    + 1.000 D8    + 1.000
D11
                                       .099
                                      3.654@
                                (      .106)
                                (     3.422@

          F9   =F9  =   1.087*F11   +   .395 F5    + 1.000 D9    + 1.087
D11
                       .278            .108                     .278
                      3.905@          3.654@                   3.905@
                 (     .244)    (      .165)              (     .244)
                 (    4.458@    (     2.394@              (    4.458@

          F10  =F10 =    .819*F4    + 1.000 D10



          F11  =F11 =    .363*F5    + 1.000 D11
```

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     29-Jun-17      PAGE : 18  EQS     Licensee:
       TITLE:   master confirmatorio la 5 sobre la 6, 7, 10 y 11 y la 4
sob

       MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

       DECOMPOSITION OF EFFECTS WITH NONSTANDARDIZED VALUES
       STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

       PARAMETER INDIRECT EFFECTS
       --------------------------

      P.1.1   =V1  =   1.218 F5    + 1.000 D1
                        .185
                       6.576@
                    (   .155)
                    (  7.846@

      P.1.2   =V2  =   1.240 F5    + 1.018 D1
                        .181           .095
                       6.841@        10.727@
                    (   .206)     (   .070)
                    (  6.023@     ( 14.525@

      P.1.3   =V3  =   1.195 F5    +  .981 D1
                        .176           .092
                       6.810@        10.623@
                    (   .199)     (   .072)
                    (  6.010@     ( 13.619@

      P.1.5   =V5  =   1.105 F5    + 1.150 D3
                        .168           .119
                       6.564@         9.643@
                    (   .233)     (   .099)
                    (  4.734@     ( 11.641@

      P.1.6   =V6  =    .960 F5    + 1.000 D3
                        .167
                       5.736@
                    (   .142)
                    (  6.750@

      P.1.8   =V8  =    .990 F5    +  .813 D1
                        .156           .089
                       6.330@         9.083@
                    (   .163)     (   .077)
                    (  6.063@     ( 10.592@

      P.1.10  =V10 =   1.000 F5    + 1.000 D2



      P.1.11  =V11 =   1.093 F5    + 1.093 D2
                        .159           .159
                       6.869@         6.869@
                    (   .128)     (   .128)
```

```
                 (  8.533@     (  8.533@

P.1.16  =V16 =   1.125 F5    + 1.125 D2
                  .154          .154
                 7.328@        7.328@
                 (   .120)     (   .120)
                 (  9.345@     (  9.345@

P.1.17  =V17 =   1.007 F5    + 1.007 D2
                  .144          .144
                 6.994@        6.994@
                 (   .124)     (   .124)
                 (  8.092@     (  8.092@

P.2.2   =V19 =    .324 F5    + 1.000 D6
                  .104
                 3.122@
                 (   .102)
                 (  3.190@

P.2.3   =V20 =    .293 F5    +  .906 D6
                  .094          .077
                 3.129@       11.799@
                 (   .098)     (   .082)
                 (  2.988@     ( 11.039@

P.2.4   =V21 =    .291 F5    +  .899 D6
                  .096          .105
                 3.021@        8.580@
                 (   .099)     (   .085)
                 (  2.939@     ( 10.626@

P.2.6   =V23 =    .284 F5    +  .876 D6
                  .093          .095
                 3.049@        9.262@
                 (   .094)     (   .086)
                 (  3.021@     ( 10.135@

P.3.1   =V33 =    .762 F4    -  .663 F5    + 1.000 D7
                  .342          .311
                 2.226@       -2.135@
                 (   .416)     (   .381)
                 (  1.829)     ( -1.743)

P.3.3   =V35 =    .690 F4    -  .601 F5    +  .906 D7
                  .334          .301          .391
                 2.069@       -1.995@        2.320@
                 (   .612)     (   .546)     (   .435)
                 (  1.128)     ( -1.102)     (  2.085@

P.4.1   =V36 =   1.000 F11   +  .363 F5    + 1.000 D8    + 1.000
D11
                                .099
                               3.654@
                               (   .106)
                               (  3.422@
```

```
      P.4.2   =V37 =   1.306 F11   + .475 F5    + 1.306 D8    + 1.306
D11
                        .109          .125          .109          .109
                      11.972@        3.794@       11.972@       11.972@
                    (   .120)     (   .152)     (   .120)     (   .120)
                    ( 10.894@     (  3.124@     ( 10.894@     ( 10.894@


      P.4.3   =V38 =   1.359 F11   + .494 F5    + 1.359 D8    + 1.359
D11
                        .111          .130          .111          .111
                      12.229@        3.804@       12.229@       12.229@
                    (   .127)     (   .160)     (   .127)     (   .127)
                    ( 10.683@     (  3.079@     ( 10.683@     ( 10.683@


      P.4.4   =V39 =   1.292 F11   + .469 F5    + 1.292 D8    + 1.292
D11
                        .112          .124          .112          .112
                      11.589@        3.782@       11.589@       11.589@
                    (   .123)     (   .150)     (   .123)     (   .123)
                    ( 10.477@     (  3.130@     ( 10.477@     ( 10.477@


      P.4.7   =V42 =   1.087 F11   + .395 F5    + 1.000 D9    + 1.087
D11
                        .278          .108                        .278
                       3.905@        3.669@                      3.905@
                    (   .244)     (   .165)                   (   .244)
                    (  4.458@     (  2.394@                   (  4.458@


      P.4.8   =V43 =   1.148 F11   + .417 F5    + 1.056 D9    + 1.148
D11
                        .292          .113          .083          .292
                       3.934@        3.692@       12.785@        3.934@
                    (   .261)     (   .175)     (   .075)     (   .261)
                    (  4.396@     (  2.383@     ( 14.141@     (  4.396@


      P.4.9   =V44 =   1.195 F11   + .434 F5    + 1.099 D9    + 1.195
D11
                        .304          .118          .086          .304
                       3.933@        3.692@       12.768@        3.933@
                    (   .270)     (   .182)     (   .080)     (   .270)
                    (  4.425@     (  2.380@     ( 13.783@     (  4.425@


      P.4.10  =V45 =   1.055 F11   + .383 F5    +  .970 D9    + 1.055
D11
                        .273          .105          .087          .273
                       3.872@        3.641@       11.134@        3.872@
                    (   .246)     (   .162)     (   .083)     (   .246)
                    (  4.291@     (  2.367@     ( 11.752@     (  4.291@


      P.6.1   =V47 =    .819 F4    + 1.000 D10
                        .139
```

```
                   5.873@
                (   .127)
                (  6.466@

 P.6.2   =V48 =    .811 F4    +  .991 D10
                   .136          .100
                  5.960@        9.942@
                (   .159)    (   .091)
                (  5.089@    ( 10.948@

 P.6.3   =V49 =    .906 F4    + 1.106 D10
                   .148          .103
                  6.127@       10.717@
                (   .173)    (   .092)
                (  5.227@    ( 12.001@

 P.6.4   =V50 =    .725 F4    +  .885 D10
                   .126          .098
                  5.734@        9.002@
                (   .154)    (   .091)
                (  4.707@    (  9.681@

 P.6.5   =V51 =    .847 F4    + 1.035 D10
                   .141          .101
                  6.028@       10.254@
                (   .173)    (   .102)
                (  4.908@    ( 10.114@

    F8   =F8  =    .363 F5    + 1.000 D11
                   .099
                  3.654@
                (   .106)
                (  3.422@

    F9   =F9  =    .395 F5    + 1.087 D11
                   .108          .278
                  3.669@        3.905@
                (   .165)    (   .244)
                (  2.394@    (  4.458@
```

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sob

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  DECOMPOSITION OF EFFECTS WITH STANDARDIZED VALUES

  PARAMETER TOTAL EFFECTS
  -----------------------

 P.1.1   =V1  =    .759 F1    +  .666 F5    +  .651 E1    +  .365
D1

 P.1.2   =V2  =    .824*F1    +  .722 F5    +  .567 E2    +  .396
D1
```

```
      P.1.3   =V3   =    .816*F1    +  .715 F5    + .578 E3     +  .392
D1
      P.1.5   =V5   =    .941*F3    +  .676 F5    + .340 E5     +  .654
D3
      P.1.6   =V6   =    .777 F3    +  .558 F5    + .629 E6     +  .541
D3
      P.1.8   =V8   =    .705*F1    +  .619 F5    + .709 E8     +  .339
D1
      P.1.9   =V9  =    .584 F4    +  .812 E9
      P.1.10  =V10 =    .614 F2    +  .561 F5    + .789 E10    +  .251
D2
      P.1.11  =V11 =    .669*F2    +  .611 F5    + .743 E11    +  .273
D2
      P.1.12  =V12 =    .795*F4    +  .606 E12
      P.1.16  =V16 =    .735*F2    +  .671 F5    + .678 E16    +  .300
D2
      P.1.17  =V17 =    .686*F2    +  .626 F5    + .728 E17    +  .280
D2
      P.2.2   =V19 =    .844 F6    +  .247 F5    + .536 E19    +  .807
D6
      P.2.3   =V20 =    .861*F6    +  .252 F5    + .508 E20    +  .824
D6
      P.2.4   =V21 =    .638*F6    +  .187 F5    + .770 E21    +  .611
D6
      P.2.6   =V23 =    .680*F6    +  .199 F5    + .733 E23    +  .650
D6
      P.3.1   =V33 =    .728 F7    +  .487 F4    - .451 F5     +  .686
E33
                   +  .666 D7
      P.3.3   =V35 =    .666*F7    +  .446 F4    - .413 F5     +  .746
E35
                   +  .610 D7
      P.4.1   =V36 =    .705 F8    +  .535 F11   + .241 F5     +  .709
E36
                   +  .459 D8    + .478 D11
      P.4.2   =V37 =    .945*F8    +  .717 F11   + .323 F5     +  .328
E37
                   +  .615 D8    + .640 D11
      P.4.3   =V38 =    .968*F8    +  .735 F11   + .331 F5     +  .250
E38
```

```
                  +  .630 D8    +  .656 D11

      P.4.4   =V39 =    .913*F8    +  .693 F11   +  .313 F5    +  .407
E39
                  +  .594 D8    +  .619 D11

      P.4.7   =V42 =    .816 F9    +  .629 F11   +  .283 F5    +  .578
E42
                  +  .521 D9    +  .561 D11

      P.4.8   =V43 =    .858*F9    +  .661 F11   +  .298 F5    +  .513
E43
                  +  .548 D9    +  .590 D11

      P.4.9   =V44 =    .858*F9    +  .660 F11   +  .298 F5    +  .514
E44
                  +  .547 D9    +  .589 D11

      P.4.10  =V45 =    .773*F9    +  .595 F11   +  .268 F5    +  .634
E45
                  +  .493 D9    +  .531 D11

      P.6.1   =V47 =    .747 F10   +  .537 F4    +  .665 E47   +  .520
D10

      P.6.2   =V48 =    .775*F10   +  .557 F4    +  .632 E48   +  .539
D10

      P.6.3   =V49 =    .834*F10   +  .599 F4    +  .552 E49   +  .580
D10

      P.6.4   =V50 =    .706*F10   +  .507 F4    +  .708 E50   +  .491
D10

      P.6.5   =V51 =    .798*F10   +  .573 F4    +  .602 E51   +  .555
D10

         F1   =F1  =    .877*F5    +  .480 D1

         F2   =F2  =    .913 F5    +  .408 D2

         F3   =F3  =    .718*F5    +  .696 D3

         F6   =F6  =    .293*F5    +  .956 D6

         F7   =F7  =    .670*F4    -  .620*F5    +  .915 D7

         F8   =F8  =    .759 F11   +  .342 F5    +  .651 D8    +  .678
D11

         F9   =F9  =    .770*F11   +  .347 F5    +  .638 D9    +  .687
D11

         F10  =F10 =    .718*F4    +  .696 D10

         F11  =F11 =    .451*F5    +  .893 D11

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        TITLE:   master confirmatorio la 5 sobre la 6, 7, 10 y 11 y la 4
sob

        MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

        DECOMPOSITION OF EFFECTS WITH STANDARDIZED VALUES

        PARAMETER INDIRECT EFFECTS
        --------------------------

       P.1.1   =V1  =    .666 F5    +  .365 D1

       P.1.2   =V2  =    .722 F5    +  .396 D1

       P.1.3   =V3  =    .715 F5    +  .392 D1

       P.1.5   =V5  =    .676 F5    +  .654 D3

       P.1.6   =V6  =    .558 F5    +  .541 D3

       P.1.8   =V8  =    .619 F5    +  .339 D1

       P.1.10  =V10 =    .561 F5    +  .251 D2

       P.1.11  =V11 =    .611 F5    +  .273 D2

       P.1.16  =V16 =    .671 F5    +  .300 D2

       P.1.17  =V17 =    .626 F5    +  .280 D2

       P.2.2   =V19 =    .247 F5    +  .807 D6

       P.2.3   =V20 =    .252 F5    +  .824 D6

       P.2.4   =V21 =    .187 F5    +  .611 D6

       P.2.6   =V23 =    .199 F5    +  .650 D6

       P.3.1   =V33 =    .487 F4    -  .451 F5    +  .666 D7

       P.3.3   =V35 =    .446 F4    -  .413 F5    +  .610 D7

       P.4.1   =V36 =    .535 F11   +  .241 F5    +  .459 D8    +  .478
D11

       P.4.2   =V37 =    .717 F11   +  .323 F5    +  .615 D8    +  .640
D11

       P.4.3   =V38 =    .735 F11   +  .331 F5    +  .630 D8    +  .656
D11

       P.4.4   =V39 =    .693 F11   +  .313 F5    +  .594 D8    +  .619
D11

       P.4.7   =V42 =    .629 F11   +  .283 F5    +  .521 D9    +  .561
D11
```

```
      P.4.8   =V43 =    .661 F11   +  .298 F5    +  .548 D9    +  .590
D11

      P.4.9   =V44 =    .660 F11   +  .298 F5    +  .547 D9    +  .589
D11

      P.4.10  =V45 =    .595 F11   +  .268 F5    +  .493 D9    +  .531
D11

      P.6.1   =V47 =    .537 F4    +  .520 D10

      P.6.2   =V48 =    .557 F4    +  .539 D10

      P.6.3   =V49 =    .599 F4    +  .580 D10

      P.6.4   =V50 =    .507 F4    +  .491 D10

      P.6.5   =V51 =    .573 F4    +  .555 D10

         F8   =F8  =    .342 F5    +  .678 D11

         F9   =F9  =    .347 F5    +  .687 D11


     29-Jun-17      PAGE : 21  EQS     Licensee:
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       MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


       STANDARDIZED                                             SOLUTION:
R-SQUARED



      P.1.1          =V1       =          .759   F1             +   .651
E1                                      .576
      P.1.2           =V2       =          .824*F1             +   .567
E2                                      .678
      P.1.3           =V3       =          .816*F1             +   .578
E3                                      .665
      P.1.5           =V5       =          .941*F3             +   .340
E5                                      .885
      P.1.6          =V6       =          .777   F3             +   .629
E6                                      .604
      P.1.8           =V8       =          .705*F1             +   .709
E8                                      .498
      P.1.9          =V9       =          .584   F4             +   .812
E9                                      .341
      P.1.10       =V10    =          .614   F2             +   .789
E10                                     .378
      P.1.11        =V11    =          .669*F2             +   .743
E11                                     .447
      P.1.12        =V12    =          .795*F4             +   .606
E12                                     .632
      P.1.16        =V16    =          .735*F2             +   .678
E16                                     .540
```

```
      P.1.17        =V17    =           .686*F2                + .728
E17                                   .471
      P.2.2          =V19   =          .844   F6               + .536
E19                                   .712
      P.2.3           =V20   =          .861*F6                + .508
E20                                   .742
      P.2.4           =V21   =          .638*F6                + .770
E21                                   .408
      P.2.6           =V23   =          .680*F6                + .733
E23                                   .462
      P.3.1          =V33   =          .728   F7               + .686
E33                                   .529
      P.3.3           =V35   =          .666*F7                + .746
E35                                   .443
      P.4.1          =V36   =          .705   F8               + .709
E36                                   .497
      P.4.2           =V37   =          .945*F8                + .328
E37                                   .893
      P.4.3           =V38   =          .968*F8                + .250
E38                                   .937
      P.4.4           =V39   =          .913*F8                + .407
E39                                   .834
      P.4.7          =V42   =          .816   F9               + .578
E42                                   .666
      P.4.8           =V43   =          .858*F9                + .513
E43                                   .737
      P.4.9           =V44   =          .858*F9                + .514
E44                                   .735
      P.4.10        =V45    =           .773*F9                + .634
E45                                   .598
      P.6.1           =V47   =          .747   F10             + .665
E47                                   .558
      P.6.2            =V48   =          .775*F10              + .632
E48                                   .601
      P.6.3            =V49   =          .834*F10              + .552
E49                                   .695
      P.6.4            =V50   =          .706*F10              + .708
E50                                   .498
      P.6.5            =V51   =          .798*F10              + .602
E51                                   .637
         F1          =F1      =         .877*F5                + .480
D1                                    .769
         F2         =F2      =         .913   F5               + .408
D2                                    .833
         F3          =F3      =         .718*F5                + .696
D3                                    .516
         F6          =F6      =         .293*F5                + .956
D6                                    .086
         F7      =F7    =      .670*F4       -  .620*F5        + .915
D7                      .162
         F8          =F8      =         .759   F11             + .651
D8                                    .576
         F9           =F9      =         .770*F11              + .638
D9                                    .593
```

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       STANDARDIZED                                           SOLUTION:
R-SQUARED
```

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      29-Jun-17      PAGE : 22  EQS     Licensee:
        TITLE:   master confirmatorio la 5 sobre la 6, 7, 10 y 11 y la 4
sob

        MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

          F10        =F10    =            .718*F4                +    .696
D10                                    .516
          F11        =F11    =            .451*F5                +    .893
D11                                    .203


      29-Jun-17      PAGE : 23  EQS     Licensee:
        TITLE:   master confirmatorio la 5 sobre la 6, 7, 10 y 11 y la 4
sob

        MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

        CORRELATIONS AMONG INDEPENDENT VARIABLES
        ---------------------------------------

                       V                                 F
                      ---                               ---
                                   I F5  -   F5                .808*I
                                   I F4  -   F4                     I
                                   I                                I



       ------------------------------------------------------------------
-------------
                                 E N D    O F    M E T H O D
       ------------------------------------------------------------------
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      29-Jun-17      PAGE : 24  EQS     Licensee:
        TITLE:   master confirmatorio la 5 sobre la 6, 7, 10 y 11 y la 4
sob

        MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


        WALD TEST (FOR DROPPING PARAMETERS)
        ROBUST INFORMATION MATRIX USED IN THIS WALD TEST
        MULTIVARIATE WALD TEST BY SIMULTANEOUS PROCESS


               CUMULATIVE MULTIVARIATE STATISTICS              UNIVARIATE
INCREMENT
               ----------------------------------              ----------
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```

```
        STEP   PARAMETER    CHI-SQUARE   D.F.   PROBABILITY        CHI-SQUARE
PROBABILITY
        ---- -----------   ----------   ----   -----------        ----------
-----------

          1        E38,E38             1.704           1              .192
1.704        .192
          2        E33,E33             3.716           2              .156
2.012        .156
          3          E5,E5              6.266           3              .099
2.550        .110


      29-Jun-17      PAGE : 25  EQS     Licensee:
        TITLE:   master confirmatorio la 5 sobre la 6, 7, 10 y 11 y la 4
sob

        MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


        LAGRANGE MULTIPLIER TEST (FOR ADDING PARAMETERS)


        ORDERED UNIVARIATE TEST STATISTICS:
                                                          HANCOCK
STANDAR-
                                             CHI-                       423  DF
PARAMETER   DIZED
         NO      CODE       PARAMETER        SQUARE       PROB.      PROB.
CHANGE    CHANGE
         --    ------    ---------      ------     -----   -------- -------
--  --------
          1        2    22            F11,F10        27.036            .000
1.000      .471      .207
          2        2    22            F11,F7         24.003            .000
1.000      .391      .172
          3        2    16             F8,F4          23.729            .000
1.000      .881      .335
          4        2    16            F11,F4         23.307            .000
1.000      .888      .445
          5        2    22             F8,F10        19.996            .000
1.000      .399      .133
          6        2    22            F11,F6         19.472            .000
1.000      .313      .133
          7        2    10            D11,D6         19.472            .000
1.000      .924      .461
          8        2    22             F6,F11        19.472            .000
1.000      .678      .288
          9        2    22             F6,F9          18.575            .000
1.000      .382      .115
         10        2    10            D11,D10        16.778            .000
1.000      .684      .484
         11        2    22            F10,F8         16.133            .000
1.000      .289      .096
         12        2    10            D11,D7         15.002            .000
1.000      .915      .493
         13        2    22             F7,F11        15.002            .000
1.000      .671      .296
```

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 14 | 2 | 22 | F10,F11 | 14.349 | .000 | 1.000 | .450 | .198 |
| 15 | 2 | 20 | V12,F7 | 14.186 | .000 | 1.000 | -.539 | -.109 |
| 16 | 2 | 12 | V5,F4 | 13.700 | .000 | 1.000 | -.791 | -.195 |
| 17 | 2 | 22 | F6,F8 | 12.046 | .001 | 1.000 | .317 | .102 |
| 18 | 2 | 22 | F7,F10 | 11.712 | .001 | 1.000 | .615 | .204 |
| 19 | 2 | 10 | D10,D7 | 11.712 | .001 | 1.000 | .901 | .469 |
| 20 | 2 | 22 | F7,F8 | 11.708 | .001 | 1.000 | .352 | .118 |
| 21 | 2 | 22 | F7,F9 | 11.617 | .001 | 1.000 | .340 | .106 |
| 22 | 2 | 20 | V10,F7 | 11.406 | .001 | 1.000 | -.444 | -.088 |
| 23 | 2 | 22 | F8,F7 | 11.174 | .001 | 1.000 | .263 | .088 |
| 24 | 2 | 20 | V36,F7 | 10.807 | .001 | 1.000 | .315 | .074 |
| 25 | 2 | 10 | D10,D8 | 9.967 | .002 | 1.000 | .521 | .384 |
| 26 | 2 | 22 | F10,F7 | 9.878 | .002 | 1.000 | .277 | .092 |
| 27 | 2 | 16 | F3,F4 | 9.144 | .002 | 1.000 | -.727 | -.219 |
| 28 | 2 | 20 | V21,F11 | 9.143 | .002 | 1.000 | .433 | .131 |
| 29 | 2 | 20 | V21,F9 | 9.017 | .003 | 1.000 | .270 | .058 |
| 30 | 2 | 22 | F3,F7 | 8.637 | .003 | 1.000 | -.295 | -.078 |
| 31 | 2 | 12 | V12,F5 | 8.632 | .003 | 1.000 | 1.161 | .252 |
| 32 | 2 | 22 | F9,F6 | 8.377 | .004 | 1.000 | .226 | .068 |
| 33 | 2 | 10 | D9,D6 | 8.377 | .004 | 1.000 | .667 | .329 |
| 34 | 2 | 22 | F10,F9 | 8.366 | .004 | 1.000 | .201 | .063 |
| 35 | 2 | 20 | V35,F8 | 8.044 | .005 | 1.000 | .270 | .066 |
| 36 | 2 | 20 | V23,F11 | 8.020 | .005 | 1.000 | .358 | .118 |
| 37 | 2 | 20 | V9,F3 | 7.811 | .005 | 1.000 | -.328 | -.058 |
| 38 | 2 | 20 | V12,F2 | 7.766 | .005 | 1.000 | .785 | .156 |
| 39 | 2 | 20 | V21,F8 | 7.571 | .006 | 1.000 | .256 | .059 |
| 40 | 2 | 20 | V10,F9 | 7.454 | .006 | 1.000 | -.310 | -.058 |
| 41 | 2 | 20 | V49,F3 | 7.381 | .007 | 1.000 | .171 | .034 |
| 42 | 2 | 20 | V5,F11 | 7.266 | .007 | 1.000 | -.370 | -.107 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 43 | 2 | 20 | V5,F2 | 7.181 | .007 | 1.000 | 1.027 | .218 |
| 44 | 2 | 20 | V50,F8 | 7.092 | .008 | 1.000 | .202 | .054 |
| 45 | 2 | 20 | V23,F9 | 7.000 | .008 | 1.000 | .210 | .049 |
| 46 | 2 | 20 | V35,F11 | 6.882 | .009 | 1.000 | .388 | .126 |
| 47 | 2 | 20 | V5,F8 | 6.537 | .011 | 1.000 | -.208 | -.046 |
| 48 | 2 | 20 | V47,F7 | 6.279 | .012 | 1.000 | .229 | .057 |
| 49 | 2 | 22 | F6,F10 | 6.188 | .013 | 1.000 | .287 | .092 |
| 50 | 2 | 22 | F2,F8 | 6.153 | .013 | 1.000 | -.179 | -.058 |
| 51 | 2 | 20 | V10,F11 | 6.050 | .014 | 1.000 | -.480 | -.127 |
| 52 | 2 | 20 | V35,F10 | 5.976 | .015 | 1.000 | .280 | .068 |
| 53 | 2 | 12 | V19,F4 | 5.795 | .016 | 1.000 | -.200 | -.062 |
| 54 | 2 | 20 | V8,F3 | 5.655 | .017 | 1.000 | -.247 | -.044 |
| 55 | 2 | 22 | F3,F11 | 5.594 | .018 | 1.000 | -.356 | -.125 |
| 56 | 2 | 10 | D11,D3 | 5.594 | .018 | 1.000 | -.485 | -.275 |
| 57 | 2 | 22 | F11,F3 | 5.594 | .018 | 1.000 | -.213 | -.075 |
| 58 | 2 | 20 | V48,F1 | 5.500 | .019 | 1.000 | -.162 | -.032 |
| 59 | 2 | 22 | F7,F3 | 5.415 | .020 | 1.000 | -.304 | -.081 |
| 60 | 2 | 10 | D7,D3 | 5.415 | .020 | 1.000 | -.693 | -.289 |
| 61 | 2 | 10 | D8,D2 | 5.284 | .022 | 1.000 | -.372 | -.457 |
| 62 | 2 | 22 | F8,F2 | 5.284 | .022 | 1.000 | -.706 | -.230 |
| 63 | 2 | 12 | V23,F4 | 5.210 | .022 | 1.000 | .241 | .068 |
| 64 | 2 | 20 | V23,F8 | 5.171 | .023 | 1.000 | .187 | .047 |
| 65 | 2 | 22 | F3,F9 | 5.160 | .023 | 1.000 | -.197 | -.049 |
| 66 | 2 | 20 | V43,F6 | 5.038 | .025 | 1.000 | .141 | .035 |
| 67 | 2 | 12 | V8,F4 | 5.004 | .025 | 1.000 | .429 | .108 |
| 68 | 2 | 12 | V9,F5 | 4.832 | .028 | 1.000 | -.643 | -.151 |
| 69 | 2 | 20 | V5,F9 | 4.830 | .028 | 1.000 | -.174 | -.035 |
| 70 | 2 | 20 | V17,F3 | 4.807 | .028 | 1.000 | .263 | .046 |
| 71 | 2 | 20 | V42,F11 | 4.757 | .029 | 1.000 | -.513 | -.173 |

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|---|---|---|---|---|---|---|---|---|
| 72 | 2 | 12 | V10,F4 | 4.571 | .033 | 1.000 | -.568 | -.128 |
| 73 | 2 | 12 | V49,F4 | 4.565 | .033 | 1.000 | .320 | .091 |
| 74 | 2 | 20 | V10,F10 | 4.448 | .035 | 1.000 | -.304 | -.060 |
| 75 | 2 | 10 | D10,D6 | 4.422 | .035 | 1.000 | .448 | .215 |
| 76 | 2 | 22 | F3,F6 | 4.405 | .036 | 1.000 | -.185 | -.047 |
| 77 | 2 | 10 | D6,D3 | 4.405 | .036 | 1.000 | -.546 | -.210 |
| 78 | 2 | 22 | F6,F3 | 4.405 | .036 | 1.000 | -.240 | -.061 |
| 79 | 2 | 20 | V23,F10 | 4.223 | .040 | 1.000 | .177 | .044 |
| 80 | 2 | 20 | V8,F10 | 4.154 | .042 | 1.000 | .230 | .051 |
| 81 | 2 | 16 | F6,F4 | 4.121 | .042 | 1.000 | .474 | .173 |
| 82 | 2 | 10 | D8,D7 | 4.099 | .043 | 1.000 | .472 | .265 |
| 83 | 2 | 10 | D11,D2 | 4.080 | .043 | 1.000 | -.335 | -.396 |
| 84 | 2 | 22 | F2,F11 | 4.080 | .043 | 1.000 | -.246 | -.106 |
| 85 | 2 | 22 | F11,F2 | 4.080 | .043 | 1.000 | -.637 | -.274 |
| 86 | 2 | 20 | V9,F2 | 4.060 | .044 | 1.000 | -.447 | -.096 |
| 87 | 2 | 12 | V48,F4 | 4.047 | .044 | 1.000 | -.306 | -.090 |
| 88 | 2 | 20 | V8,F8 | 3.992 | .046 | 1.000 | .188 | .042 |
| 89 | 2 | 22 | F10,F6 | 3.939 | .047 | 1.000 | .142 | .045 |
| 90 | 2 | 20 | V42,F8 | 3.935 | .047 | 1.000 | -.174 | -.045 |
| 91 | 2 | 20 | V16,F8 | 3.893 | .048 | 1.000 | -.198 | -.042 |
| 92 | 2 | 20 | V42,F3 | 3.877 | .049 | 1.000 | -.112 | -.023 |
| 93 | 2 | 12 | V48,F5 | 3.871 | .049 | 1.000 | -.211 | -.058 |
| 94 | 2 | 20 | V50,F6 | 3.768 | .052 | 1.000 | .148 | .038 |
| 95 | 2 | 12 | V23,F5 | 3.704 | .054 | 1.000 | .190 | .051 |
| 96 | 2 | 20 | V47,F6 | 3.690 | .055 | 1.000 | -.149 | -.036 |
| 97 | 2 | 22 | F3,F8 | 3.582 | .058 | 1.000 | -.169 | -.045 |
| 98 | 2 | 20 | V50,F2 | 3.572 | .059 | 1.000 | -.185 | -.048 |
| 99 | 2 | 12 | V49,F5 | 3.569 | .059 | 1.000 | .197 | .053 |
| 100 | 2 | 20 | V1,F3 | 3.514 | .061 | 1.000 | .212 | .033 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 101 | 2 | 20 | V23,F1 | 3.480 | .062 | 1.000 | .128 | .025 |
| 102 | 2 | 20 | V35,F9 | 3.476 | .062 | 1.000 | .171 | .039 |
| 103 | 2 | 22 | F3,F2 | 3.472 | .062 | 1.000 | .850 | .220 |
| 104 | 2 | 22 | F2,F3 | 3.472 | .062 | 1.000 | .197 | .051 |
| 105 | 2 | 10 | D3,D2 | 3.472 | .062 | 1.000 | .448 | .409 |
| 106 | 2 | 20 | V33,F3 | 3.428 | .064 | 1.000 | -.164 | -.032 |
| 107 | 2 | 10 | D9,D7 | 3.380 | .066 | 1.000 | .477 | .255 |
| 108 | 2 | 20 | V43,F1 | 3.329 | .068 | 1.000 | .099 | .019 |
| 109 | 2 | 20 | V12,F10 | 3.306 | .069 | 1.000 | -.487 | -.099 |
| 110 | 2 | 20 | V12,F1 | 3.256 | .071 | 1.000 | .335 | .052 |
| 111 | 2 | 20 | V39,F9 | 3.250 | .071 | 1.000 | .111 | .025 |
| 112 | 2 | 20 | V5,F7 | 3.237 | .072 | 1.000 | -.163 | -.035 |
| 113 | 2 | 20 | V19,F10 | 3.219 | .073 | 1.000 | -.120 | -.032 |
| 114 | 2 | 20 | V8,F6 | 3.211 | .073 | 1.000 | .168 | .036 |
| 115 | 2 | 22 | F7,F1 | 3.109 | .078 | 1.000 | .444 | .113 |
| 116 | 2 | 10 | D7,D1 | 3.109 | .078 | 1.000 | .521 | .303 |
| 117 | 2 | 12 | V6,F4 | 3.097 | .078 | 1.000 | .422 | .099 |
| 118 | 2 | 20 | V38,F7 | 3.067 | .080 | 1.000 | .080 | .019 |
| 119 | 2 | 20 | V5,F10 | 3.047 | .081 | 1.000 | -.182 | -.039 |
| 120 | 2 | 20 | V8,F11 | 3.021 | .082 | 1.000 | .270 | .080 |
| 121 | 2 | 20 | V39,F11 | 3.008 | .083 | 1.000 | .288 | .090 |
| 122 | 2 | 20 | V16,F11 | 2.996 | .083 | 1.000 | -.291 | -.082 |
| 123 | 2 | 20 | V50,F11 | 2.992 | .084 | 1.000 | .207 | .073 |
| 124 | 2 | 20 | V23,F2 | 2.979 | .084 | 1.000 | .155 | .038 |
| 125 | 2 | 22 | F7,F2 | 2.924 | .087 | 1.000 | -.799 | -.259 |
| 126 | 2 | 10 | D7,D2 | 2.924 | .087 | 1.000 | -.421 | -.365 |
| 127 | 2 | 22 | F1,F7 | 2.888 | .089 | 1.000 | .168 | .043 |
| 128 | 2 | 20 | V48,F2 | 2.869 | .090 | 1.000 | -.157 | -.040 |
| 129 | 2 | 20 | V38,F9 | 2.844 | .092 | 1.000 | -.084 | -.019 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 130 | 2 | 22 | F2,F7 | 2.806 | .094 | 1.000 | -.138 | -.045 |
| 131 | 2 | 20 | V37,F7 | 2.784 | .095 | 1.000 | -.083 | -.020 |
| 132 | 2 | 20 | V1,F9 | 2.767 | .096 | 1.000 | -.164 | -.030 |
| 133 | 2 | 22 | F6,F7 | 2.706 | .100 | 1.000 | .167 | .054 |
| 134 | 2 | 20 | V6,F2 | 2.705 | .100 | 1.000 | -.682 | -.137 |
| 135 | 2 | 20 | V10,F8 | 2.626 | .105 | 1.000 | -.189 | -.038 |
| 136 | 2 | 12 | V19,F5 | 2.485 | .115 | 1.000 | -.124 | -.036 |
| 137 | 2 | 20 | V19,F1 | 2.480 | .115 | 1.000 | -.086 | -.018 |
| 138 | 2 | 20 | V38,F11 | 2.472 | .116 | 1.000 | -.212 | -.067 |
| 139 | 2 | 20 | V1,F11 | 2.443 | .118 | 1.000 | -.262 | -.068 |
| 140 | 2 | 20 | V49,F2 | 2.408 | .121 | 1.000 | .140 | .034 |
| 141 | 2 | 22 | F8,F6 | 2.357 | .125 | 1.000 | .108 | .035 |
| 142 | 2 | 10 | D8,D6 | 2.357 | .125 | 1.000 | .318 | .165 |
| 143 | 2 | 22 | F9,F7 | 2.331 | .127 | 1.000 | .134 | .042 |
| 144 | 2 | 20 | V36,F3 | 2.300 | .129 | 1.000 | -.103 | -.019 |
| 145 | 2 | 20 | V45,F11 | 2.277 | .131 | 1.000 | .383 | .126 |
| 146 | 2 | 20 | V51,F9 | 2.271 | .132 | 1.000 | .102 | .025 |
| 147 | 2 | 20 | V45,F8 | 2.254 | .133 | 1.000 | .142 | .036 |
| 148 | 2 | 20 | V5,F1 | 2.240 | .134 | 1.000 | .310 | .052 |
| 149 | 2 | 10 | D9,D3 | 2.183 | .139 | 1.000 | -.332 | -.186 |
| 150 | 2 | 22 | F9,F3 | 2.183 | .139 | 1.000 | -.146 | -.036 |
| 151 | 2 | 20 | V33,F9 | 2.175 | .140 | 1.000 | .138 | .031 |
| 152 | 2 | 20 | V20,F7 | 2.101 | .147 | 1.000 | .095 | .029 |
| 153 | 2 | 20 | V33,F2 | 2.064 | .151 | 1.000 | -.173 | -.041 |
| 154 | 2 | 20 | V3,F8 | 2.012 | .156 | 1.000 | -.123 | -.026 |
| 155 | 2 | 20 | V2,F6 | 2.008 | .156 | 1.000 | -.124 | -.025 |
| 156 | 2 | 20 | V10,F6 | 1.990 | .158 | 1.000 | -.164 | -.031 |
| 157 | 2 | 20 | V6,F8 | 1.922 | .166 | 1.000 | .129 | .027 |
| 158 | 2 | 12 | V50,F5 | 1.914 | .167 | 1.000 | -.156 | -.044 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 159 | 2 | 20 | V39,F10 | 1.911 | .167 | 1.000 | .072 | .017 |
| 160 | 2 | 12 | V11,F4 | 1.863 | .172 | 1.000 | .356 | .080 |
| 161 | 2 | 20 | V47,F3 | 1.850 | .174 | 1.000 | -.096 | -.019 |
| 162 | 2 | 22 | F3,F1 | 1.832 | .176 | 1.000 | .336 | .069 |
| 163 | 2 | 10 | D3,D1 | 1.832 | .176 | 1.000 | .394 | .241 |
| 164 | 2 | 22 | F1,F3 | 1.832 | .176 | 1.000 | .173 | .035 |
| 165 | 2 | 20 | V3,F2 | 1.818 | .178 | 1.000 | .287 | .059 |
| 166 | 2 | 20 | V1,F6 | 1.788 | .181 | 1.000 | -.135 | -.025 |
| 167 | 2 | 20 | V36,F6 | 1.728 | .189 | 1.000 | .107 | .024 |
| 168 | 2 | 20 | V2,F10 | 1.710 | .191 | 1.000 | -.140 | -.029 |
| 169 | 2 | 12 | V1,F4 | 1.683 | .195 | 1.000 | -.272 | -.060 |
| 170 | 2 | 20 | V35,F1 | 1.668 | .196 | 1.000 | .109 | .020 |
| 171 | 2 | 20 | V49,F1 | 1.664 | .197 | 1.000 | .087 | .017 |
| 172 | 2 | 20 | V50,F3 | 1.601 | .206 | 1.000 | -.087 | -.018 |
| 173 | 2 | 12 | V42,F5 | 1.596 | .207 | 1.000 | -.104 | -.028 |
| 174 | 2 | 20 | V43,F10 | 1.588 | .208 | 1.000 | -.083 | -.021 |
| 175 | 2 | 20 | V9,F7 | 1.575 | .209 | 1.000 | .161 | .036 |
| 176 | 2 | 12 | V43,F5 | 1.563 | .211 | 1.000 | .098 | .027 |
| 177 | 2 | 20 | V21,F10 | 1.534 | .216 | 1.000 | .121 | .027 |
| 178 | 2 | 20 | V3,F7 | 1.522 | .217 | 1.000 | .121 | .026 |
| 179 | 2 | 20 | V50,F1 | 1.480 | .224 | 1.000 | -.089 | -.018 |
| 180 | 2 | 20 | V9,F1 | 1.465 | .226 | 1.000 | -.185 | -.031 |
| 181 | 2 | 12 | V33,F5 | 1.427 | .232 | 1.000 | -.157 | -.040 |
| 182 | 2 | 12 | V35,F5 | 1.427 | .232 | 1.000 | .142 | .037 |
| 183 | 2 | 12 | V33,F4 | 1.427 | .232 | 1.000 | -.180 | -.049 |
| 184 | 2 | 12 | V35,F4 | 1.427 | .232 | 1.000 | .163 | .045 |
| 185 | 2 | 20 | V19,F2 | 1.410 | .235 | 1.000 | -.085 | -.022 |
| 186 | 2 | 20 | V2,F9 | 1.405 | .236 | 1.000 | .101 | .020 |
| 187 | 2 | 20 | V43,F2 | 1.392 | .238 | 1.000 | .084 | .021 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 188 | 2 | 20 | V6,F6 | 1.385 | .239 | 1.000 | -.108 | -.022 |
| 189 | 2 | 20 | V42,F2 | 1.364 | .243 | 1.000 | -.087 | -.022 |
| 190 | 2 | 20 | V17,F9 | 1.354 | .245 | 1.000 | .113 | .023 |
| 191 | 2 | 20 | V39,F6 | 1.343 | .246 | 1.000 | .058 | .013 |
| 192 | 2 | 22 | F3,F10 | 1.343 | .247 | 1.000 | -.134 | -.035 |
| 193 | 2 | 20 | V44,F1 | 1.307 | .253 | 1.000 | -.064 | -.012 |
| 194 | 2 | 20 | V48,F3 | 1.297 | .255 | 1.000 | -.074 | -.015 |
| 195 | 2 | 10 | D7,D6 | 1.296 | .255 | 1.000 | .342 | .125 |
| 196 | 2 | 22 | F7,F6 | 1.296 | .255 | 1.000 | .116 | .037 |
| 197 | 2 | 20 | V44,F10 | 1.271 | .260 | 1.000 | .078 | .019 |
| 198 | 2 | 20 | V8,F9 | 1.240 | .265 | 1.000 | .102 | .021 |
| 199 | 2 | 20 | V17,F10 | 1.208 | .272 | 1.000 | -.137 | -.030 |
| 200 | 2 | 20 | V6,F10 | 1.189 | .276 | 1.000 | .128 | .026 |
| 201 | 2 | 20 | V36,F9 | 1.175 | .278 | 1.000 | .107 | .024 |
| 202 | 2 | 20 | V2,F11 | 1.171 | .279 | 1.000 | .158 | .043 |
| 203 | 2 | 20 | V6,F11 | 1.161 | .281 | 1.000 | .169 | .046 |
| 204 | 2 | 22 | F2,F9 | 1.159 | .282 | 1.000 | -.075 | -.023 |
| 205 | 2 | 20 | V1,F8 | 1.145 | .285 | 1.000 | -.109 | -.021 |
| 206 | 2 | 20 | V16,F9 | 1.141 | .285 | 1.000 | -.104 | -.021 |
| 207 | 2 | 22 | F10,F1 | 1.106 | .293 | 1.000 | -.118 | -.030 |
| 208 | 2 | 20 | V20,F9 | 1.094 | .295 | 1.000 | -.056 | -.016 |
| 209 | 2 | 20 | V44,F7 | 1.087 | .297 | 1.000 | .080 | .020 |
| 210 | 2 | 22 | F10,F2 | 1.085 | .298 | 1.000 | -.172 | -.056 |
| 211 | 2 | 20 | V20,F10 | 1.084 | .298 | 1.000 | .061 | .019 |
| 212 | 2 | 20 | V38,F6 | 1.058 | .304 | 1.000 | -.040 | -.009 |
| 213 | 2 | 20 | V1,F2 | 1.058 | .304 | 1.000 | -.244 | -.046 |
| 214 | 2 | 12 | V42,F4 | 1.036 | .309 | 1.000 | -.089 | -.026 |
| 215 | 2 | 20 | V17,F1 | 1.010 | .315 | 1.000 | -.189 | -.032 |
| 216 | 2 | 20 | V35,F2 | 1.006 | .316 | 1.000 | .110 | .026 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 217 | 2 | 10 | D9,D1 | .996 | .318 | 1.000 | .214 | .168 |
| 218 | 2 | 22 | F9,F1 | .996 | .318 | 1.000 | .182 | .044 |
| 219 | 2 | 20 | V9,F8 | .989 | .320 | 1.000 | .107 | .024 |
| 220 | 2 | 20 | V1,F7 | .958 | .328 | 1.000 | -.112 | -.022 |
| 221 | 2 | 20 | V49,F8 | .931 | .334 | 1.000 | .066 | .017 |
| 222 | 2 | 12 | V21,F4 | .926 | .336 | 1.000 | .115 | .030 |
| 223 | 2 | 20 | V33,F11 | .908 | .341 | 1.000 | .145 | .046 |
| 224 | 2 | 16 | F10,F5 | .882 | .348 | 1.000 | -.208 | -.074 |
| 225 | 2 | 12 | V20,F4 | .853 | .356 | 1.000 | .068 | .023 |
| 226 | 2 | 20 | V50,F9 | .841 | .359 | 1.000 | .067 | .017 |
| 227 | 2 | 20 | V48,F6 | .839 | .360 | 1.000 | .066 | .016 |
| 228 | 2 | 20 | V45,F3 | .829 | .362 | 1.000 | .056 | .011 |
| 229 | 2 | 12 | V38,F4 | .829 | .362 | 1.000 | .046 | .013 |
| 230 | 2 | 10 | D10,D9 | .828 | .363 | 1.000 | .167 | .117 |
| 231 | 2 | 20 | V16,F10 | .825 | .364 | 1.000 | .114 | .024 |
| 232 | 2 | 12 | V50,F4 | .822 | .365 | 1.000 | -.144 | -.043 |
| 233 | 2 | 12 | V11,F5 | .808 | .369 | 1.000 | .590 | .125 |
| 234 | 2 | 20 | V11,F9 | .805 | .369 | 1.000 | .098 | .018 |
| 235 | 2 | 22 | F1,F2 | .783 | .376 | 1.000 | -.504 | -.126 |
| 236 | 2 | 22 | F2,F1 | .783 | .376 | 1.000 | -.226 | -.056 |
| 237 | 2 | 10 | D2,D1 | .783 | .376 | 1.000 | -.265 | -.338 |
| 238 | 2 | 22 | F8,F3 | .779 | .378 | 1.000 | -.078 | -.021 |
| 239 | 2 | 10 | D8,D3 | .779 | .378 | 1.000 | -.178 | -.105 |
| 240 | 2 | 20 | V43,F11 | .762 | .383 | 1.000 | .197 | .066 |
| 241 | 2 | 20 | V8,F7 | .738 | .390 | 1.000 | .092 | .020 |
| 242 | 2 | 20 | V11,F10 | .726 | .394 | 1.000 | .119 | .024 |
| 243 | 2 | 22 | F2,F10 | .724 | .395 | 1.000 | -.083 | -.027 |
| 244 | 2 | 20 | V19,F8 | .718 | .397 | 1.000 | -.054 | -.015 |
| 245 | 2 | 20 | V49,F6 | .709 | .400 | 1.000 | .058 | .014 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 246 | 2 | 20 | V45,F10 | .705 | .401 | 1.000 | .064 | .016 |
| 247 | 2 | 20 | V42,F6 | .703 | .402 | 1.000 | -.056 | -.014 |
| 248 | 2 | 20 | V45,F7 | .688 | .407 | 1.000 | .071 | .018 |
| 249 | 2 | 20 | V49,F11 | .678 | .410 | 1.000 | .089 | .029 |
| 250 | 2 | 20 | V3,F3 | .677 | .411 | 1.000 | .081 | .014 |
| 251 | 2 | 20 | V42,F1 | .674 | .412 | 1.000 | -.047 | -.009 |
| 252 | 2 | 20 | V36,F11 | .666 | .414 | 1.000 | .218 | .068 |
| 253 | 2 | 22 | F1,F9 | .661 | .416 | 1.000 | .068 | .016 |
| 254 | 2 | 20 | V21,F3 | .642 | .423 | 1.000 | -.063 | -.011 |
| 255 | 2 | 16 | F2,F4 | .629 | .428 | 1.000 | -.170 | -.063 |
| 256 | 2 | 20 | V43,F3 | .614 | .433 | 1.000 | .042 | .009 |
| 257 | 2 | 20 | V36,F10 | .612 | .434 | 1.000 | .066 | .016 |
| 258 | 2 | 20 | V5,F6 | .596 | .440 | 1.000 | -.062 | -.013 |
| 259 | 2 | 22 | F1,F6 | .590 | .443 | 1.000 | -.065 | -.016 |
| 260 | 2 | 10 | D6,D1 | .590 | .443 | 1.000 | -.191 | -.103 |
| 261 | 2 | 22 | F6,F1 | .590 | .443 | 1.000 | -.163 | -.040 |
| 262 | 2 | 20 | V2,F8 | .584 | .445 | 1.000 | .067 | .014 |
| 263 | 2 | 20 | V19,F3 | .576 | .448 | 1.000 | -.041 | -.009 |
| 264 | 2 | 12 | V1,F5 | .567 | .452 | 1.000 | -.282 | -.058 |
| 265 | 2 | 20 | V21,F7 | .558 | .455 | 1.000 | .083 | .019 |
| 266 | 2 | 20 | V38,F1 | .545 | .460 | 1.000 | -.025 | -.004 |
| 267 | 2 | 16 | F1,F4 | .533 | .465 | 1.000 | .190 | .055 |
| 268 | 2 | 10 | D10,D1 | .531 | .466 | 1.000 | -.148 | -.113 |
| 269 | 2 | 20 | V51,F1 | .521 | .471 | 1.000 | .049 | .010 |
| 270 | 2 | 12 | V16,F5 | .517 | .472 | 1.000 | -.468 | -.106 |
| 271 | 2 | 20 | V12,F9 | .510 | .475 | 1.000 | -.071 | -.013 |
| 272 | 2 | 12 | V3,F5 | .509 | .476 | 1.000 | .243 | .055 |
| 273 | 2 | 20 | V10,F1 | .503 | .478 | 1.000 | .148 | .023 |
| 274 | 2 | 20 | V33,F6 | .496 | .481 | 1.000 | .068 | .016 |

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|---|---|---|---|---|---|---|---|---|
| 275 | 2 | 20 | V11,F7 | .490 | .484 | 1.000 | .089 | .018 |
| 276 | 2 | 12 | V39,F4 | .482 | .488 | 1.000 | .044 | .012 |
| 277 | 2 | 20 | V51,F11 | .479 | .489 | 1.000 | .077 | .026 |
| 278 | 2 | 20 | V37,F1 | .469 | .493 | 1.000 | .024 | .005 |
| 279 | 2 | 20 | V51,F2 | .457 | .499 | 1.000 | .062 | .015 |
| 280 | 2 | 20 | V6,F7 | .455 | .500 | 1.000 | -.070 | -.014 |
| 281 | 2 | 22 | F9,F10 | .448 | .503 | 1.000 | .067 | .021 |
| 282 | 2 | 20 | V17,F11 | .445 | .505 | 1.000 | .112 | .033 |
| 283 | 2 | 10 | D10,D2 | .440 | .507 | 1.000 | -.113 | -.128 |
| 284 | 2 | 20 | V2,F7 | .439 | .508 | 1.000 | .066 | .014 |
| 285 | 2 | 20 | V44,F6 | .422 | .516 | 1.000 | .043 | .010 |
| 286 | 2 | 20 | V6,F1 | .410 | .522 | 1.000 | -.143 | -.023 |
| 287 | 2 | 20 | V33,F1 | .402 | .526 | 1.000 | -.058 | -.011 |
| 288 | 2 | 20 | V3,F11 | .396 | .529 | 1.000 | -.090 | -.025 |
| 289 | 2 | 20 | V11,F11 | .389 | .533 | 1.000 | .118 | .031 |
| 290 | 2 | 20 | V33,F8 | .370 | .543 | 1.000 | .059 | .014 |
| 291 | 2 | 12 | V37,F4 | .352 | .553 | 1.000 | -.032 | -.009 |
| 292 | 2 | 20 | V19,F7 | .330 | .566 | 1.000 | -.043 | -.012 |
| 293 | 2 | 20 | V36,F1 | .309 | .578 | 1.000 | -.038 | -.007 |
| 294 | 2 | 22 | F8,F1 | .301 | .583 | 1.000 | -.090 | -.023 |
| 295 | 2 | 10 | D8,D1 | .301 | .583 | 1.000 | -.106 | -.087 |
| 296 | 2 | 12 | V45,F4 | .299 | .584 | 1.000 | .052 | .015 |
| 297 | 2 | 20 | V1,F10 | .299 | .584 | 1.000 | -.067 | -.013 |
| 298 | 2 | 12 | V51,F5 | .298 | .585 | 1.000 | .058 | .016 |
| 299 | 2 | 20 | V47,F11 | .294 | .587 | 1.000 | .066 | .022 |
| 300 | 2 | 20 | V48,F8 | .294 | .588 | 1.000 | .039 | .010 |
| 301 | 2 | 12 | V44,F5 | .283 | .595 | 1.000 | -.044 | -.011 |
| 302 | 2 | 20 | V47,F8 | .280 | .596 | 1.000 | .041 | .010 |
| 303 | 2 | 20 | V43,F8 | .274 | .600 | 1.000 | .044 | .011 |

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|---|---|---|---|---|---|---|---|---|
| 304 | 2 | 20 | V20,F11 | .271 | .602 | 1.000 | -.045 | -.018 |
| 305 | 2 | 20 | V6,F9 | .271 | .603 | 1.000 | .047 | .009 |
| 306 | 2 | 12 | V45,F5 | .268 | .604 | 1.000 | .046 | .012 |
| 307 | 2 | 20 | V44,F3 | .264 | .607 | 1.000 | -.029 | -.006 |
| 308 | 2 | 20 | V47,F1 | .258 | .611 | 1.000 | .038 | .007 |
| 309 | 2 | 20 | V47,F9 | .253 | .615 | 1.000 | .038 | .009 |
| 310 | 2 | 20 | V51,F7 | .250 | .617 | 1.000 | .041 | .011 |
| 311 | 2 | 20 | V16,F3 | .239 | .625 | 1.000 | -.060 | -.010 |
| 312 | 2 | 20 | V17,F6 | .238 | .626 | 1.000 | .048 | .010 |
| 313 | 2 | 12 | V36,F5 | .229 | .632 | 1.000 | -.047 | -.012 |
| 314 | 2 | 20 | V3,F6 | .202 | .653 | 1.000 | .039 | .008 |
| 315 | 2 | 20 | V16,F1 | .199 | .656 | 1.000 | -.088 | -.014 |
| 316 | 2 | 12 | V47,F4 | .194 | .660 | 1.000 | .072 | .020 |
| 317 | 2 | 22 | F11,F1 | .193 | .661 | 1.000 | .074 | .025 |
| 318 | 2 | 22 | F1,F11 | .193 | .661 | 1.000 | .064 | .022 |
| 319 | 2 | 10 | D11,D1 | .193 | .661 | 1.000 | .087 | .069 |
| 320 | 2 | 20 | V19,F9 | .192 | .661 | 1.000 | .027 | .007 |
| 321 | 2 | 20 | V2,F3 | .191 | .662 | 1.000 | .044 | .007 |
| 322 | 2 | 12 | V39,F5 | .183 | .668 | 1.000 | .026 | .007 |
| 323 | 2 | 20 | V19,F11 | .182 | .670 | 1.000 | -.042 | -.015 |
| 324 | 2 | 12 | V44,F4 | .179 | .672 | 1.000 | .036 | .010 |
| 325 | 2 | 20 | V2,F2 | .176 | .674 | 1.000 | -.092 | -.019 |
| 326 | 2 | 20 | V45,F2 | .176 | .675 | 1.000 | .034 | .008 |
| 327 | 2 | 20 | V45,F1 | .171 | .679 | 1.000 | .026 | .005 |
| 328 | 2 | 20 | V12,F3 | .171 | .679 | 1.000 | .050 | .008 |
| 329 | 2 | 20 | V35,F6 | .171 | .679 | 1.000 | .040 | .009 |
| 330 | 2 | 20 | V44,F2 | .161 | .688 | 1.000 | -.030 | -.007 |
| 331 | 2 | 20 | V8,F2 | .151 | .698 | 1.000 | -.083 | -.018 |
| 332 | 2 | 20 | V12,F8 | .148 | .700 | 1.000 | .039 | .008 |

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|---|---|---|---|---|---|---|---|---|
| 333 | 2 | 20 | V37,F6 | .140 | .708 | 1.000 | .016 | .004 |
| 334 | 2 | 10 | D6,D2 | .139 | .709 | 1.000 | -.078 | -.062 |
| 335 | 2 | 22 | F2,F6 | .139 | .709 | 1.000 | -.026 | -.008 |
| 336 | 2 | 22 | F6,F2 | .139 | .709 | 1.000 | -.148 | -.046 |
| 337 | 2 | 12 | V17,F4 | .139 | .709 | 1.000 | -.087 | -.022 |
| 338 | 2 | 20 | V43,F7 | .132 | .716 | 1.000 | -.027 | -.007 |
| 339 | 2 | 20 | V9,F6 | .122 | .727 | 1.000 | .037 | .008 |
| 340 | 2 | 22 | F1,F10 | .119 | .730 | 1.000 | -.040 | -.010 |
| 341 | 2 | 20 | V51,F8 | .119 | .730 | 1.000 | -.024 | -.006 |
| 342 | 2 | 10 | D9,D2 | .116 | .734 | 1.000 | .061 | .071 |
| 343 | 2 | 22 | F9,F2 | .116 | .734 | 1.000 | .116 | .035 |
| 344 | 2 | 12 | V10,F5 | .115 | .734 | 1.000 | -.217 | -.046 |
| 345 | 2 | 20 | V16,F6 | .102 | .749 | 1.000 | .032 | .006 |
| 346 | 2 | 20 | V39,F1 | .101 | .751 | 1.000 | .013 | .002 |
| 347 | 2 | 20 | V10,F3 | .097 | .756 | 1.000 | .043 | .007 |
| 348 | 2 | 20 | V37,F2 | .096 | .756 | 1.000 | -.014 | -.003 |
| 349 | 2 | 20 | V21,F2 | .090 | .764 | 1.000 | .030 | .007 |
| 350 | 2 | 22 | F10,F3 | .089 | .765 | 1.000 | -.024 | -.006 |
| 351 | 2 | 20 | V38,F10 | .086 | .769 | 1.000 | .012 | .003 |
| 352 | 2 | 12 | V36,F4 | .086 | .770 | 1.000 | .030 | .008 |
| 353 | 2 | 20 | V16,F7 | .083 | .773 | 1.000 | -.033 | -.007 |
| 354 | 2 | 20 | V35,F3 | .082 | .775 | 1.000 | .024 | .005 |
| 355 | 2 | 20 | V9,F10 | .070 | .791 | 1.000 | .051 | .011 |
| 356 | 2 | 20 | V37,F3 | .070 | .792 | 1.000 | .009 | .002 |
| 357 | 2 | 20 | V20,F2 | .069 | .793 | 1.000 | -.017 | -.005 |
| 358 | 2 | 20 | V23,F7 | .066 | .797 | 1.000 | -.025 | -.006 |
| 359 | 2 | 20 | V9,F11 | .066 | .797 | 1.000 | .045 | .013 |
| 360 | 2 | 20 | V51,F6 | .065 | .799 | 1.000 | .018 | .004 |
| 361 | 2 | 12 | V21,F5 | .064 | .800 | 1.000 | .028 | .007 |

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|---|---|---|---|---|---|---|---|---|
| 362 | 2 | 20 | V9,F9 | .064 | .801 | 1.000 | -.026 | -.005 |
| 363 | 2 | 20 | V17,F7 | .060 | .806 | 1.000 | .028 | .006 |
| 364 | 2 | 20 | V21,F1 | .053 | .817 | 1.000 | -.018 | -.003 |
| 365 | 2 | 20 | V47,F2 | .051 | .822 | 1.000 | .023 | .005 |
| 366 | 2 | 12 | V38,F5 | .050 | .823 | 1.000 | -.011 | -.003 |
| 367 | 2 | 20 | V20,F1 | .050 | .824 | 1.000 | .011 | .003 |
| 368 | 2 | 20 | V39,F2 | .049 | .825 | 1.000 | .012 | .003 |
| 369 | 2 | 20 | V3,F9 | .048 | .827 | 1.000 | .018 | .004 |
| 370 | 2 | 12 | V8,F5 | .045 | .832 | 1.000 | .071 | .017 |
| 371 | 2 | 20 | V39,F3 | .042 | .838 | 1.000 | .009 | .002 |
| 372 | 2 | 20 | V11,F1 | .042 | .839 | 1.000 | .043 | .007 |
| 373 | 2 | 12 | V3,F4 | .040 | .841 | 1.000 | -.037 | -.009 |
| 374 | 2 | 20 | V12,F6 | .038 | .846 | 1.000 | -.020 | -.004 |
| 375 | 2 | 12 | V2,F5 | .037 | .848 | 1.000 | -.067 | -.015 |
| 376 | 2 | 20 | V11,F3 | .034 | .853 | 1.000 | .025 | .004 |
| 377 | 2 | 20 | V49,F9 | .031 | .861 | 1.000 | .012 | .003 |
| 378 | 2 | 20 | V11,F6 | .030 | .861 | 1.000 | -.020 | -.004 |
| 379 | 2 | 12 | V17,F5 | .027 | .870 | 1.000 | .098 | .023 |
| 380 | 2 | 20 | V20,F3 | .026 | .872 | 1.000 | .008 | .002 |
| 381 | 2 | 20 | V50,F7 | .026 | .873 | 1.000 | -.014 | -.004 |
| 382 | 2 | 20 | V11,F8 | .024 | .877 | 1.000 | .018 | .004 |
| 383 | 2 | 20 | V48,F9 | .023 | .880 | 1.000 | -.010 | -.003 |
| 384 | 2 | 20 | V36,F2 | .023 | .881 | 1.000 | -.013 | -.003 |
| 385 | 2 | 20 | V49,F7 | .020 | .887 | 1.000 | .011 | .003 |
| 386 | 2 | 20 | V48,F7 | .020 | .888 | 1.000 | .012 | .003 |
| 387 | 2 | 20 | V23,F3 | .019 | .891 | 1.000 | .009 | .002 |
| 388 | 2 | 16 | F9,F4 | .016 | .898 | 1.000 | -.026 | -.009 |
| 389 | 2 | 20 | V42,F7 | .016 | .899 | 1.000 | -.010 | -.003 |
| 390 | 2 | 20 | V44,F11 | .016 | .900 | 1.000 | -.030 | -.010 |

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|---|---|---|---|---|---|---|---|---|
| 391 | 2 | 20 | V42,F10 | .015 | .902 | 1.000 | -.009 | -.002 |
| 392 | 2 | 20 | V37,F9 | .014 | .906 | 1.000 | -.006 | -.001 |
| 393 | 2 | 20 | V37,F10 | .012 | .912 | 1.000 | -.005 | -.001 |
| 394 | 2 | 12 | V2,F4 | .011 | .915 | 1.000 | .020 | .005 |
| 395 | 2 | 20 | V38,F3 | .008 | .928 | 1.000 | -.003 | -.001 |
| 396 | 2 | 20 | V51,F3 | .007 | .934 | 1.000 | .005 | .001 |
| 397 | 2 | 20 | V37,F11 | .006 | .936 | 1.000 | -.011 | -.004 |
| 398 | 2 | 12 | V37,F5 | .006 | .936 | 1.000 | .004 | .001 |
| 399 | 2 | 20 | V3,F10 | .006 | .938 | 1.000 | -.008 | -.002 |
| 400 | 2 | 20 | V45,F6 | .005 | .942 | 1.000 | .005 | .001 |
| 401 | 2 | 12 | V20,F5 | .005 | .942 | 1.000 | .005 | .002 |
| 402 | 2 | 20 | V38,F2 | .005 | .942 | 1.000 | -.003 | -.001 |
| 403 | 2 | 12 | V47,F5 | .003 | .955 | 1.000 | -.007 | -.002 |
| 404 | 2 | 12 | V16,F4 | .003 | .956 | 1.000 | .013 | .003 |
| 405 | 2 | 20 | V44,F8 | .003 | .959 | 1.000 | .004 | .001 |
| 406 | 2 | 22 | F1,F8 | .002 | .962 | 1.000 | -.004 | -.001 |
| 407 | 2 | 20 | V12,F11 | .002 | .962 | 1.000 | -.008 | -.002 |
| 408 | 2 | 12 | V51,F4 | .002 | .963 | 1.000 | -.007 | -.002 |
| 409 | 2 | 20 | V20,F8 | .002 | .967 | 1.000 | .002 | .001 |
| 410 | 2 | 20 | V33,F10 | .002 | .968 | 1.000 | -.005 | -.001 |
| 411 | 2 | 10 | D10,D3 | .001 | .971 | 1.000 | .008 | .004 |
| 412 | 2 | 20 | V48,F11 | .001 | .978 | 1.000 | -.003 | -.001 |
| 413 | 2 | 20 | V39,F7 | .000 | .996 | 1.000 | .000 | .000 |
| 414 | 2 | 20 | V17,F8 | .000 | .996 | 1.000 | .000 | .000 |
| 415 | 2 | 12 | V43,F4 | .000 | .998 | 1.000 | .000 | .000 |
| 416 | 2 | 0 | V19,F6 | .000 | 1.000 | 1.000 | .000 | .000 |
| 417 | 2 | 0 | V33,F7 | .000 | 1.000 | 1.000 | .000 | .000 |
| 418 | 2 | 10 | D9,D8 | .000 | 1.000 | 1.000 | .000 | .000 |
| 419 | 2 | 22 | F11,F8 | .000 | 1.000 | 1.000 | .000 | .000 |

| | | | | | | | |
|---|---|---|---|---|---|---|---|
| 420 | 2 | 0 | V36,F8 | .000 | 1.000 | | |
| 1.000 | .000 | .000 | | | | | |
| 421 | 2 | 22 | F11,F9 | .000 | 1.000 | | |
| 1.000 | .000 | .000 | | | | | |
| 422 | 2 | 10 | D11,D8 | .000 | 1.000 | | |
| 1.000 | .000 | .000 | | | | | |
| 423 | 2 | 22 | F9,F8 | .000 | 1.000 | | |
| 1.000 | .000 | .000 | | | | | |
| 424 | 2 | 0 | F2,F5 | .000 | 1.000 | | |
| 1.000 | .000 | .000 | | | | | |
| 425 | 2 | 16 | F8,F5 | .000 | 1.000 | | |
| 1.000 | .000 | .000 | | | | | |
| 426 | 2 | 16 | F9,F5 | .000 | 1.000 | | |
| 1.000 | .000 | .000 | | | | | |
| 427 | 2 | 0 | V1,F1 | .000 | 1.000 | | |
| 1.000 | .000 | .000 | | | | | |
| 428 | 2 | 0 | V47,F10 | .000 | 1.000 | | |
| 1.000 | .000 | .000 | | | | | |
| 429 | 2 | 0 | V9,F4 | .000 | 1.000 | | |
| 1.000 | .000 | .000 | | | | | |
| 430 | 2 | 12 | V6,F5 | .000 | 1.000 | | |
| 1.000 | .000 | .000 | | | | | |
| 431 | 2 | 0 | V10,F2 | .000 | 1.000 | | |
| 1.000 | .000 | .000 | | | | | |
| 432 | 2 | 12 | V5,F5 | .000 | 1.000 | | |
| 1.000 | .000 | .000 | | | | | |
| 433 | 2 | 22 | F8,F9 | .000 | 1.000 | | |
| 1.000 | .000 | .000 | | | | | |
| 434 | 2 | 0 | V42,F9 | .000 | 1.000 | | |
| 1.000 | .000 | .000 | | | | | |
| 435 | 2 | 0 | F8,F11 | .000 | 1.000 | | |
| 1.000 | .000 | .000 | | | | | |
| 436 | 2 | 10 | D11,D9 | .000 | 1.000 | | |
| 1.000 | .000 | .000 | | | | | |
| 437 | 2 | 0 | V6,F3 | .000 | 1.000 | | |
| 1.000 | .000 | .000 | | | | | |

29-Jun-17 PAGE : 26 EQS Licensee:
TITLE: master confirmatorio la 5 sobre la 6, 7, 10 y 11 y la 4 sob

MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

MULTIVARIATE LAGRANGE MULTIPLIER TEST BY SIMULTANEOUS PROCESS IN STAGE 1

PARAMETER SETS (SUBMATRICES) ACTIVE AT THIS STAGE ARE:

PVV PFV PFF PDD GVV GVF GFV GFF BVF BFF

CUMULATIVE MULTIVARIATE STATISTICS UNIVARIATE INCREMENT
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HANCOCK'S

SEQUENTIAL

| STEP | PARAMETER | CHI-SQUARE | D.F. | PROB. | CHI-SQUARE | PROB. | D.F. | PROB. |
|---|---|---|---|---|---|---|---|---|
| 1 | F11,F10 | 27.036 | 1 | .000 | 27.036 | .000 | 423 | 1.000 |
| 2 | F11,F6 | 48.225 | 2 | .000 | 21.189 | .000 | 422 | 1.000 |
| 3 | V12,F7 | 62.704 | 3 | .000 | 14.479 | .000 | 421 | 1.000 |
| 4 | F11,F7 | 75.641 | 4 | .000 | 12.937 | .000 | 420 | 1.000 |
| 5 | V5,F4 | 87.260 | 5 | .000 | 11.619 | .001 | 419 | 1.000 |
| 6 | V10,F7 | 98.291 | 6 | .000 | 11.031 | .001 | 418 | 1.000 |
| 7 | V36,F7 | 108.431 | 7 | .000 | 10.141 | .001 | 417 | 1.000 |
| 8 | V49,F3 | 117.599 | 8 | .000 | 9.167 | .002 | 416 | 1.000 |
| 9 | F6,F10 | 125.225 | 9 | .000 | 7.627 | .006 | 415 | 1.000 |
| 10 | V19,F4 | 132.082 | 10 | .000 | 6.856 | .009 | 414 | 1.000 |
| 11 | V8,F3 | 138.648 | 11 | .000 | 6.566 | .010 | 413 | 1.000 |
| 12 | V8,F4 | 146.350 | 12 | .000 | 7.702 | .006 | 412 | 1.000 |
| 13 | V5,F11 | 152.726 | 13 | .000 | 6.376 | .012 | 411 | 1.000 |
| 14 | V10,F9 | 159.085 | 14 | .000 | 6.359 | .012 | 410 | 1.000 |
| 15 | F8,F4 | 165.117 | 15 | .000 | 6.032 | .014 | 409 | 1.000 |
| 16 | V21,F9 | 170.758 | 16 | .000 | 5.641 | .018 | 408 | 1.000 |
| 17 | V23,F11 | 176.198 | 17 | .000 | 5.439 | .020 | 407 | 1.000 |
| 18 | V50,F8 | 181.502 | 18 | .000 | 5.304 | .021 | 406 | 1.000 |
| 19 | V42,F11 | 186.258 | 19 | .000 | 4.757 | .029 | 405 | 1.000 |
| 20 | V8,F8 | 190.952 | 20 | .000 | 4.693 | .030 | 404 | 1.000 |

```
  LAGRANGIAN MULTIPLIER TEST REQUIRED   571647 WORDS OF MEMORY.
  PROGRAM ALLOCATES ******** WORDS.
1
  Execution begins at 13:25:46
  Execution ends   at 13:25:53
  Elapsed time =       7.00 seconds
```

# ANEXO XVI

# MODELOS DE ECUACIONES ESTRUCTURALES

# FLEX-RDOS

```
1
    EQS, A STRUCTURAL EQUATION PROGRAM          MULTIVARIATE SOFTWARE, INC.
    COPYRIGHT BY P.M. BENTLER                   VERSION 6.1 (C) 1985 - 2005 (B85).


      PROGRAM CONTROL INFORMATION

  /TITLE
   master confirmatorio la 5 sobre la 6, 7, 10 y 11 y la 4 sobre la 10 y 7
  /SPECIFICATIONS
  VARIABLES= 33 ; CASES= 170 ;
  DATAFILE='C:\tesis1\ticflexrdoscontrol.ESS';
   MATRIX=RAW;METHOD=ML,robust;
  /LABELS
  V1=P.2.2; V2=P.2.3; V3=P.2.4; V4=P.2.6; V5=P.3.1; V6=P.3.3; V7=P.4.1;
  V8=P.4.2; V9=P.4.3; V10=P.4.4; V11=P.4.7; V12=P.4.8;
  V13=P.4.9; V14=P.4.10; V15=P.6.1; V16=P.6.2; V17=P.6.3; V18=P.6.4; V19=P.6.5;
  V20=P.9.3; V21=P.9.9; V22=P.9.10;
  V23=P.9.12; V24=P.9.13; V25=P.9.14; V26=P.9.15;
  V27=P.11.1; V28=ANTIGUED; V29=LOGANTIG; V30=RAIZANTI; V31=P.10.1;
  V32=LOGTAMA; V33=RAIZTAMA;

  /EQUATIONS
  V1=F6+E1;
  V2=*F6+E2;
  V3=*F6+E3;
  V4=*F6+E4;
  V5=F7+E5;
  V6=*F7+E6;
  V7=F8+E7;
  V8=*F8+E8;
  V9=*F8+E9;
  V10=*F8+E10;
  V11=F9+E11;
  V12=*F9+E12;
  V13=*F9+E13;
  V14=*F9+E14;
  V15=F10+E15;
  V16=*F10+E16;
  V17=*F10+E17;
  V18=*F10+E18;
  V19=*F10+E19;
  F8=F11+D8;
  F9=*F11+D9;
  V26=*F12+ E26;
  V25=*F12+E25;
  V20= F12+E20;
  V24=*F13+E24;
  V23=F13+E23;
  V21=F14+E21;
```

```
V22=*F14+E22;
V29=F17+E29;
V32=F16+E32;
F12=*F15+D12;
F13=*F15+D13;
F14= F15+D14;
F15=*F6+*F7+*F11+*F10+*F16+*F17+D15;
```

```
24-Jul-17      PAGE :  2  EQS     Licensee:
  TITLE:   master confirmatorio la 5 sobre la 6, 7, 10 y 11 y la 4
sob
```

```
/VARIANCES
E1 TO E26=*;
E29=0;
E32=0;
D8 TO D9=*;
D12 TO D14=*;
F11=*;
F6=*;
F7=*;
F10=*;
F16=*;
F17=*;
D15=*;

/COVARIANCES
F6,F7=*;
F6,F11=*;
F6,F10=*;
F7,F11=*;
F7,F10=*;
F10,F11=*;
F16,F6=*;
F16,F7=*;
F16,F10=*;
F16,F11=*;
F17,F6=*;
F17,F7=*;
F17,F10=*;
F17,F11=*;
F16,F17=*;


/TECHNICAL
ITR=100
/PRINT
FIT=ALL;
EFFECT=YES;
/WTEST
/LMTEST
/END
```

```
92 RECORDS OF INPUT MODEL FILE WERE READ
```

```
          DATA IS READ FROM C:\tesis1\ticflexrdoscontrol.ESS
          THERE ARE  33 VARIABLES AND   170 CASES
          IT IS A RAW DATA ESS FILE


      24-Jul-17      PAGE :  3  EQS     Licensee:
        TITLE:   master confirmatorio la 5 sobre la 6, 7, 10 y 11 y la 4
sob


        SAMPLE STATISTICS BASED ON COMPLETE CASES


                                   UNIVARIATE STATISTICS
                                   ---------------------


         VARIABLE         P.2.2      P.2.3      P.2.4      P.2.6
P.3.1
                             V1         V2         V3         V4
V5

         MEAN               1.8765     1.4588     2.9471     2.0882
2.2059

         SKEWNESS (G1)      1.2422     1.5942      .4243
1.0549     .8539

         KURTOSIS (G2)       .3913     1.6513    -1.3650     -.2638     -
.6331

         STANDARD DEV.      2.1295     1.8908     2.5309     2.3150
2.3856


         VARIABLE         P.3.3      P.4.1      P.4.2      P.4.3
P.4.4
                             V6         V7         V8         V9
V10

         MEAN               1.9000     2.7294     2.8235     2.6882
2.6647

         SKEWNESS (G1)
1.1054     .4621      .2998      .4307      .4202

         KURTOSIS (G2)      -.1092    -1.1132    -1.2121    -1.1559    -
1.1980

         STANDARD DEV.      2.3626     2.4441     2.3818     2.4185
2.4372


         VARIABLE         P.4.7      P.4.8      P.4.9      P.4.10
P.6.1
                             V11        V12        V13        V14
V15
```

| | | | | | |
|---|---|---|---|---|---|
| MEAN | 3.4059 | 4.0471 | 3.5353 | 2.7706 | 2.8294 |
| SKEWNESS (G1) | .1232 | -.2498 | -.0173 | .4803 | .3455 |
| KURTOSIS (G2) | -1.1944 | -1.1031 | -1.3026 | -1.0218 | -1.0645 |
| STANDARD DEV. | 2.2624 | 2.2710 | 2.3663 | 2.3180 | 2.3282 |

| VARIABLE | P.6.2 | P.6.3 | P.6.4 | P.6.5 | P.9.3 |
|---|---|---|---|---|---|
| | V16 | V17 | V18 | V19 | V20 |
| MEAN | 2.9235 | 2.5529 | 2.3765 | 2.1118 | 6.1647 |
| SKEWNESS (G1) | .2227 | .5477 | .4525 | .8085 | -1.6316 |
| KURTOSIS (G2) | -1.0536 | -.9088 | -.9277 | -.5685 | 2.6761 |
| STANDARD DEV. | 2.2241 | 2.3077 | 2.1810 | 2.2544 | 1.0642 |

| VARIABLE | P.9.9 | P.9.10 | P.9.12 | P.9.13 | P.9.14 |
|---|---|---|---|---|---|
| | V21 | V22 | V23 | V24 | V25 |
| MEAN | 4.1824 | 4.5118 | 4.8235 | 4.4235 | 5.8059 |
| SKEWNESS (G1) | -.3570 | -.5772 | -.5256 | -.4133 | -1.4572 |
| KURTOSIS (G2) | -.7646 | -.3762 | -.2772 | -.6250 | 2.0533 |
| STANDARD DEV. | 1.9901 | 1.9192 | 1.6900 | 1.9269 | 1.4567 |

| VARIABLE | P.9.15 | LOGANTIG | LOGTAMA |
|---|---|---|---|
| | V26 | V29 | V32 |
| MEAN | 5.7588 | 1.2075 | 1.2278 |
| SKEWNESS (G1) | -1.3098 | -.7551 | .7711 |
| KURTOSIS (G2) | 1.3013 | 1.3199 | 1.2529 |

STANDARD DEV. 1.4618 .3556 .6087

MULTIVARIATE KURTOSIS
---------------------

MARDIA'S COEFFICIENT (G2,P) = 172.5597
NORMALIZED ESTIMATE = 27.4460

ELLIPTICAL THEORY KURTOSIS ESTIMATES
------------------------------------

MARDIA-BASED KAPPA = .2054 MEAN SCALED UNIVARIATE KURTOSIS = -.0904

MARDIA-BASED KAPPA IS USED IN COMPUTATION. KAPPA= .2054

CASE NUMBERS WITH LARGEST CONTRIBUTION TO NORMALIZED MULTIVARIATE KURTOSIS:
---------------------------------------------------------------------------

| | | | | | |
|---|---|---|---|---|---|
| CASE NUMBER | 21 | 58 | 85 | 139 | 150 |
| ESTIMATE | 773.2405 | 470.5727 | 1786.2369 | 412.7335 | 762.3372 |

24-Jul-17 PAGE : 4 EQS Licensee:
TITLE: master confirmatorio la 5 sobre la 6, 7, 10 y 11 y la 4 sob

COVARIANCE MATRIX TO BE ANALYZED: 28 VARIABLES (SELECTED FROM 33 VARIABLES)
BASED ON 170 CASES.

| | | P.2.2 | P.2.3 | P.2.4 | P.2.6 | P.3.1 |
|---|---|---|---|---|---|---|
| | | V1 | V2 | V3 | V4 | V5 |
| P.2.2 | V1 | 4.535 | | | | |
| P.2.3 | V2 | 3.051 | 3.575 | | | |
| P.2.4 | V3 | 2.804 | 2.356 | 6.405 | | |
| P.2.6 | V4 | 2.561 | 2.462 | 3.667 | 5.359 | |
| P.3.1 | V5 | .375 | .461 | .573 | -.101 | 5.691 |
| P.3.3 | V6 | .088 | .395 | .279 | .488 | 2.731 |
| P.4.1 | V7 | 1.173 | 1.113 | 2.181 | 1.710 | 1.802 |
| P.4.2 | V8 | 1.292 | 1.123 | 1.979 | 1.743 | .924 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.4.3 | V9 | 1.056 | 1.197 | 2.019 | 1.750 | 1.136 |
| P.4.4 | V10 | 1.219 | 1.285 | 2.290 | 1.882 | 1.247 |
| P.4.7 | V11 | 1.210 | .777 | 1.590 | 1.514 | .815 |
| P.4.8 | V12 | 1.674 | 1.304 | 2.221 | 1.931 | .913 |
| P.4.9 | V13 | 1.410 | 1.067 | 2.573 | 1.929 | 1.155 |
| P.4.10 | V14 | 1.185 | 1.029 | 1.402 | 1.689 | .888 |
| P.6.1 | V15 | .210 | .546 | 1.109 | .707 | 1.408 |
| P.6.2 | V16 | .848 | .941 | 1.457 | 1.634 | .590 |
| P.6.3 | V17 | .950 | 1.159 | .947 | 1.448 | .613 |
| P.6.4 | V18 | .917 | 1.098 | 1.866 | 1.617 | .620 |
| P.6.5 | V19 | .754 | 1.108 | .929 | 1.043 | .835 |
| P.9.3 | V20 | .228 | .220 | .234 | .252 | -.028 |
| P.9.9 | V21 | .549 | .815 | .584 | 1.280 | .175 |
| P.9.10 | V22 | .206 | .592 | .501 | .848 | .515 |
| P.9.12 | V23 | .724 | .584 | .707 | .542 | .344 |
| P.9.13 | V24 | .893 | .775 | .762 | .661 | .468 |
| P.9.14 | V25 | .579 | .397 | .493 | .544 | .318 |
| P.9.15 | V26 | .260 | .176 | .419 | .211 | .482 |
| LOGANTIG | V29 | .082 | .034 | .124 | .083 | -.056 |
| LOGTAMA | V32 | .075 | .081 | .281 | .181 | .095 |

| | | P.3.3 | P.4.1 | P.4.2 | P.4.3 | P.4.4 |
|---|---|---|---|---|---|---|
| | | V6 | V7 | V8 | V9 | V10 |
| P.3.3 | V6 | 5.582 | | | | |
| P.4.1 | V7 | 1.996 | 5.974 | | | |
| P.4.2 | V8 | 1.396 | 3.952 | 5.673 | | |
| P.4.3 | V9 | 1.874 | 4.033 | 5.270 | 5.849 | |
| P.4.4 | V10 | 1.309 | 3.678 | 4.988 | 5.226 | 5.940 |
| P.4.7 | V11 | .869 | 1.868 | 2.149 | 2.098 | 2.279 |
| P.4.8 | V12 | .904 | 2.338 | 2.653 | 2.630 | 2.797 |
| P.4.9 | V13 | 1.030 | 2.199 | 2.574 | 2.718 | 2.968 |

P.4.10 V14 1.220 2.263 2.669 2.674
2.686
P.6.1 V15 1.385 1.764 1.940 2.035
2.262
P.6.2 V16 1.122 1.896 2.022 2.023
2.004
P.6.3 V17 1.346 1.707 2.086 2.440
2.358
P.6.4 V18 .689 1.753 2.357 2.378
2.512
P.6.5 V19 1.141 1.764 1.913 1.840
2.008
P.9.3
V20 .159 .429 .556 .703 .777
P.9.9 V21 .575 1.020 1.506 1.477
1.576
P.9.10 V22 .478 1.370 1.523 1.468
1.853
P.9.12 V23 .195 .828 1.087 .939
1.153
P.9.13 V24 .125 .819 1.247 1.133
1.415
P.9.14 V25 -
.085 .415 .468 .371 .645
P.9.15
V26 .343 .496 .484 .741 .759
LOGANTIG V29 -.105 -.023 -.014 -.047
-.041
LOGTAMA
V32 .047 .287 .208 .212 .235

P.4.7 P.4.8 P.4.9 P.4.10
P.6.1
V11 V12 V13 V14
V15
P.4.7 V11 5.118
P.4.8 V12 4.093 5.158
P.4.9 V13 3.545 3.768 5.599
P.4.10 V14 2.958 3.111 4.236 5.373
P.6.1 V15 1.283 1.209 1.672 1.215
5.420
P.6.2 V16 1.262 1.021 1.384 1.184
3.218
P.6.3 V17 1.106 1.145 1.750 1.642
3.124
P.6.4 V18 1.296 1.130 1.531 1.111
2.976
P.6.5 V19 1.641 1.397 1.662 1.783
2.972
P.9.3
V20 .737 .856 .692 .541 .312
P.9.9 V21 1.571 1.281 1.517 1.699
1.469
P.9.10 V22 1.330 1.313 1.429 1.491
1.532
P.9.12 V23 1.368 1.316 1.397
1.444 .804

P.9.13 V24 1.614 1.483 1.583 1.660
1.173
P.9.14 V25 1.073
1.045 .998 .914 .730
P.9.15 V26 1.246 1.077
1.083 .885 .734
LOGANTIG V29 -.119 -.031 -.082 -
.105 .006
LOGTAMA V32 -
.055 .100 .194 .075 .256

P.6.2 P.6.3 P.6.4 P.6.5
P.9.3
V16 V17 V18 V19
V20
P.6.2 V16 4.947
P.6.3 V17 3.427 5.326
P.6.4 V18 2.609 2.731 4.757
P.6.5 V19 2.991 3.547 2.952 5.082
P.9.3 V20 .415 .488 .198 .337
1.132
P.9.9 V21 1.943 1.916 1.097
1.772 .905
P.9.10 V22 1.797 1.348 .990 1.303
1.022
P.9.12
V23 .910 .962 .540 .848 .733
P.9.13 V24 1.098 .912 .934
1.083 .735
P.9.14
V25 .944 .552 .322 .507 .890
P.9.15
V26 .881 .803 .476 .642 .756
LOGANTIG V29 .003 -.079 -
.032 .002 .004
LOGTAMA V32 .261 .283 .220 .237
-.052

P.9.9 P.9.10 P.9.12 P.9.13
P.9.14
V21 V22 V23 V24
V25
P.9.9 V21 3.961
P.9.10 V22 2.800 3.683
P.9.12 V23 1.843 2.049 2.856
P.9.13 V24 1.999 2.214 2.625 3.713
P.9.14 V25 1.373 1.561 1.374 1.384
2.122
P.9.15 V26 1.352 1.130 .963 .984
1.308
LOGANTIG V29 .010 -.042 -.030 -.035
-.008
LOGTAMA
V32 .160 .116 .035 .079 .010

P.9.15 LOGANTIG LOGTAMA

```
                              V26         V29         V32
           P.9.15   V26      2.137
           LOGANTIG V29      -.022        .126
           LOGTAMA  V32       .042        .096        .370


        BENTLER-WEEKS STRUCTURAL REPRESENTATION:

              NUMBER OF DEPENDENT VARIABLES = 34
                  DEPENDENT V'S :     1    2    3    4    5    6    7
8    9   10
                  DEPENDENT V'S :    11   12   13   14   15   16   17
18   19   20
                  DEPENDENT V'S :    21   22   23   24   25   26   29
32
                  DEPENDENT F'S :     8    9   12   13   14   15

              NUMBER OF INDEPENDENT VARIABLES = 40
                  INDEPENDENT F'S :     6    7   10   11   16   17
                  INDEPENDENT E'S :     1    2    3    4    5    6    7
8    9   10
                  INDEPENDENT E'S :    11   12   13   14   15   16   17
18   19   20
                  INDEPENDENT E'S :    21   22   23   24   25   26   29
32
                  INDEPENDENT D'S :     8    9   12   13   14   15


              NUMBER OF FREE PARAMETERS =  80
              NUMBER OF FIXED NONZERO PARAMETERS =  46

       *** WARNING MESSAGES ABOVE, IF ANY, REFER TO THE MODEL PROVIDED.
           CALCULATIONS FOR INDEPENDENCE MODEL NOW BEGIN.

       *** WARNING MESSAGES ABOVE, IF ANY, REFER TO INDEPENDENCE MODEL.
           CALCULATIONS FOR USER'S MODEL NOW BEGIN.


        3RD STAGE OF COMPUTATION REQUIRED   1964574 WORDS OF MEMORY.
        PROGRAM ALLOCATED 200000000 WORDS

        DETERMINANT OF INPUT MATRIX IS    .65513D+07

       IN ITERATION #  1, MATRIX W_CFUNCT MAY NOT BE POSITIVE DEFINITE.
        YOU HAVE BAD START VALUES TO BEGIN WITH.
        IF ABOVE MESSAGE APPEARS ON EVERY ITERATION, PLEASE PROVIDE
BETTER START VALUES AND RE-RUN THE JOB.

       *** NOTE *** RESIDUAL-BASED STATISTICS CANNOT BE
                    CALCULATED BECAUSE OF PIVOTING PROBLEMS.

        PARAMETER ESTIMATES APPEAR IN ORDER,
        NO SPECIAL PROBLEMS WERE ENCOUNTERED DURING OPTIMIZATION.


        RESIDUAL COVARIANCE MATRIX  (S-SIGMA) :
```

```
                              P.2.2       P.2.3       P.2.4       P.2.6
P.3.1
                                 V1          V2          V3          V4
V5
          P.2.2    V1           .000
          P.2.3    V2           .242        .000
          P.2.4    V3          -.203       -.336        .000
          P.2.6    V4          -.324       -.120        .904        .000
          P.3.1    V5           .126        .239        .335       -
.330       .000
          P.3.3    V6          -.266        .078       -
.060       .163       .000
          P.4.1    V7          -.030        .036       1.028        .605
1.045
          P.4.2    V8          -.274       -.278        .479        .304
-.060
          P.4.3    V9          -.573       -
.261       .458       .252       .111
          P.4.4    V10         -.333       -
.104       .803       .456       .271
          P.4.7    V11         -.126       -.419        .310        .286
-.025
          P.4.8
V12         .272       .049       .878       .642       .032
          P.4.9    V13         -.081       -.268
1.144       .558       .218
          P.4.10   V14         -.134       -
.151       .139       .477       .059
          P.6.1    V15         -.829       -.383        .115       -
.247       .610
          P.6.2    V16         -.204       -.001        .450        .667
-.219
          P.6.3    V17         -.178        .149       -.135        .411
-.254
          P.6.4    V18         -.013        .266        .976        .763
-.094
          P.6.5    V19         -.313        .154       -
.093       .063       .015
          P.9.3    V20         -.033       -.013       -.016        .012
-.133
          P.9.9    V21         -.140        .198       -.077        .646
-.102
          P.9.10   V22         -.524       -.061       -
.198       .177       .221
          P.9.12
V23         .149       .070       .156       .014       .113
          P.9.13
V24         .275       .222       .170       .093       .220
          P.9.14
V25         .139       .003       .071       .139       .141
          P.9.15   V26         -.108       -.153        .067       -
.127       .334
          LOGANTIG V29          .009       -
.031       .054       .016       .014
          LOGTAMA  V32         -.052       -
.033       .159       .064       .051
```

| | | P.3.3 V6 | P.4.1 V7 | P.4.2 V8 | P.4.3 V9 | P.4.4 V10 |
|---|---|---|---|---|---|---|
| P.3.3 | V6 | .000 | | | | |
| P.4.1 | V7 | .920 | .000 | | | |
| P.4.2 | V8 | -.005 | .066 | .000 | | |
| P.4.3 | V9 | .416 | -.010 | .008 | .000 | |
| P.4.4 | V10 | -.079 | -.173 | -.024 | .010 | .000 |
| P.4.7 | V11 | -.327 | .011 | -.268 | -.418 | -.117 |
| P.4.8 | V12 | -.351 | .389 | .117 | -.010 | .283 |
| P.4.9 | V13 | -.305 | .126 | -.123 | -.089 | .294 |
| P.4.10 | V14 | .039 | .430 | .284 | .191 | .322 |
| P.6.1 | V15 | .249 | .386 | .147 | .169 | .484 |
| P.6.2 | V16 | -.029 | .500 | .205 | .132 | .203 |
| P.6.3 | V17 | .110 | .209 | .137 | .411 | .426 |
| P.6.4 | V18 | -.328 | .520 | .751 | .708 | .920 |
| P.6.5 | V19 | -.026 | .349 | .071 | -.077 | .182 |
| P.9.3 | V20 | .009 | -.011 | -.017 | .106 | .210 |
| P.9.9 | V21 | .179 | -.145 | -.010 | -.101 | .073 |
| P.9.10 | V22 | .059 | .137 | -.082 | -.202 | .262 |
| P.9.12 | V23 | -.134 | -.144 | -.178 | -.377 | -.100 |
| P.9.13 | V24 | -.229 | -.225 | -.112 | -.282 | .068 |
| P.9.14 | V25 | -.337 | -.330 | -.500 | -.637 | -.316 |
| P.9.15 | V26 | .132 | -.125 | -.325 | -.100 | -.042 |
| LOGANTIG | V29 | -.004 | .025 | .049 | .018 | .021 |
| LOGTAMA | V32 | -.016 | .165 | .050 | .048 | .078 |

| | | P.4.7 V11 | P.4.8 V12 | P.4.9 V13 | P.4.10 V14 | P.6.1 V15 |
|---|---|---|---|---|---|---|
| P.4.7 | V11 | .000 | | | | |
| P.4.8 | V12 | .558 | .000 | | | |
| P.4.9 | V13 | -.215 | -.178 | .000 | | |
| P.4.10 | V14 | -.367 | -.377 | .526 | .000 | |

P.6.1 V15 -.248 -.397 -.036 -
.295 .000
P.6.2 V16 -.289 -.606 -.347 -
.347 .151
P.6.3 V17 -.558 -.601 -.107 .001
-.166
P.6.4 V18 -.074 -.308 .002 -
.242 .266
P.6.5 V19 .069 -.253 -.093 .232
-.137
P.9.3 V20 .248 .343 .147 .058
-.162
P.9.9 V21 .277 -
.077 .073 .422 .214
P.9.10 V22 -.040 -.124 -
.100 .139 .203
P.9.12 V23 .289 .184 .192 .379
-.243
P.9.13
V24 .454 .266 .288 .515 .048
P.9.14 V25 .247 .177 .075 .098
-.072
P.9.15
V26 .557 .353 .313 .204 .064
LOGANTIG V29 -.065 .026 -.022 -
.052 .028
LOGTAMA V32 -.190 -.041 .044 -
.058 .005

P.6.2 P.6.3 P.6.4 P.6.5
P.9.3
V16 V17 V18 V19
V20
P.6.2 V16 .000
P.6.3 V17 .093 .000
P.6.4 V18 -.137 -.214 .000
P.6.5 V19 -.159 .168 .169 .000
P.9.3 V20 -.066 -.027 -.227 -
.151 .000
P.9.9 V21 .671 .552 -
.027 .483 .034
P.9.10 V22 .450 -.096 -.200 -
.062 .100
P.9.12 V23 -.151 -.176 -.397 -
.227 .007
P.9.13 V24 -.043 -.311 -.073 -.073
-.046
P.9.14 V25 .131 -.320 -.396 -.317
-.019
P.9.15 V26 .203 .075 -.123 -.045
-.003
LOGANTIG V29 .025 -.055 -
.012 .024 .013
LOGTAMA V32 .007 .010 -.004 -.020
-.085

```
                             P.9.9      P.9.10     P.9.12     P.9.13
P.9.14
                                V21        V22        V23        V24
V25
           P.9.9    V21         .000
           P.9.10   V22         .000       .000
           P.9.12   V23        -.079       .014       .000
           P.9.13   V24        -.067       .027       .000       .000
           P.9.14   V25        -
.100       .002       .146       .064       .000
           P.9.15   V26         .123      -.171      -.062      -
.117       .026
           LOGANTIG V29         .036      -.015      -.009      -
.013       .008
           LOGTAMA  V32         .075       .027      -.035       .003
-.044


                             P.9.15     LOGANTIG   LOGTAMA
                                V26        V29        V32
           P.9.15   V26         .000
           LOGANTIG V29        -.009       .000
           LOGTAMA  V32        -.003       .000       .000


                           AVERAGE ABSOLUTE  COVARIANCE  RESIDUALS
=          .1892
              AVERAGE OFF-DIAGONAL ABSOLUTE  COVARIANCE  RESIDUALS
=          .2033


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        MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


        STANDARDIZED RESIDUAL MATRIX:


                             P.2.2      P.2.3      P.2.4      P.2.6
P.3.1
                                V1         V2         V3         V4
V5
           P.2.2    V1          .000
           P.2.3    V2          .060       .000
           P.2.4    V3         -.038      -.070       .000
           P.2.6    V4         -.066      -.027       .154       .000
           P.3.1    V5          .025       .053       .055      -
.060       .000
           P.3.3    V6         -.053       .018      -
.010       .030       .000
           P.4.1    V7         -
.006       .008       .166       .107       .179
           P.4.2    V8         -.054      -.062       .079       .055
-.011
```

P.4.3 V9 -.111 -
.057 .075 .045 .019
P.4.4 V10 -.064 -
.023 .130 .081 .047
P.4.7 V11 -.026 -.098 .054 .055
-.005
P.4.8
V12 .056 .011 .153 .122 .006
P.4.9 V13 -.016 -
.060 .191 .102 .039
P.4.10 V14 -.027 -
.035 .024 .089 .011
P.6.1 V15 -.167 -.087 .019 -
.046 .110
P.6.2 V16 -.043 .000 .080 .130
-.041
P.6.3 V17 -.036 .034 -.023 .077
-.046
P.6.4 V18 -.003 .065 .177 .151
-.018
P.6.5 V19 -.065 .036 -
.016 .012 .003
P.9.3 V20 -.015 -.007 -.006 .005
-.052
P.9.9 V21 -.033 .053 -.015 .140
-.022
P.9.10 V22 -.128 -.017 -
.041 .040 .048
P.9.12
V23 .041 .022 .036 .004 .028
P.9.13
V24 .067 .061 .035 .021 .048
P.9.14
V25 .045 .001 .019 .041 .041
P.9.15 V26 -.035 -.055 .018 -
.038 .096
LOGANTIG V29 .012 -
.047 .060 .019 .017
LOGTAMA V32 -.040 -
.029 .103 .045 .035

P.3.3 P.4.1 P.4.2 P.4.3
P.4.4
V6 V7 V8 V9
V10
P.3.3 V6 .000
P.4.1 V7 .159 .000
P.4.2 V8 -.001 .011 .000
P.4.3 V9 .073 -.002 .001 .000
P.4.4 V10 -.014 -.029 -
.004 .002 .000
P.4.7 V11 -.061 .002 -.050 -.076
-.021
P.4.8 V12 -.065 .070 .022 -
.002 .051
P.4.9 V13 -.054 .022 -.022 -
.016 .051

P.4.10
V14 .007 .076 .051 .034 .057
P.6.1
V15 .045 .068 .026 .030 .085
P.6.2 V16 -
.006 .092 .039 .025 .037
P.6.3
V17 .020 .037 .025 .074 .076
P.6.4 V18 -
.064 .097 .145 .134 .173
P.6.5 V19 -.005 .063 .013 -
.014 .033
P.9.3 V20 .004 -.004 -
.007 .041 .081
P.9.9 V21 .038 -.030 -.002 -
.021 .015
P.9.10 V22 .013 .029 -.018 -
.044 .056
P.9.12 V23 -.034 -.035 -.044 -.092
-.024
P.9.13 V24 -.050 -.048 -.024 -
.060 .014
P.9.14 V25 -.098 -.093 -.144 -.181
-.089
P.9.15 V26 .038 -.035 -.093 -.028
-.012
LOGANTIG V29 -
.005 .029 .058 .021 .024
LOGTAMA V32 -
.011 .111 .035 .033 .053

P.4.7 P.4.8 P.4.9 P.4.10
P.6.1
V11 V12 V13 V14
V15
P.4.7 V11 .000
P.4.8 V12 .109 .000
P.4.9 V13 -.040 -.033 .000
P.4.10 V14 -.070 -.072 .096 .000
P.6.1 V15 -.047 -.075 -.007 -
.055 .000
P.6.2 V16 -.057 -.120 -.066 -
.067 .029
P.6.3 V17 -.107 -.115 -.020 .000
-.031
P.6.4 V18 -.015 -.062 .000 -
.048 .052
P.6.5 V19 .013 -.049 -.017 .044
-.026
P.9.3 V20 .103 .142 .058 .024
-.065
P.9.9 V21 .061 -
.017 .015 .091 .046
P.9.10 V22 -.009 -.029 -
.022 .031 .045
P.9.12 V23 .076 .048 .048 .097
-.062

```
          P.9.13
V24        .104      .061      .063      .115      .011
          P.9.14   V25        .075      .054      .022      .029
-.021
          P.9.15
V26        .168      .106      .090      .060      .019
          LOGANTIG V29       -.081      .032     -.027      -
.063       .034
          LOGTAMA  V32       -.138     -.030      .030      -
.041       .004


                             P.6.2     P.6.3     P.6.4     P.6.5
P.9.3
                              V16       V17       V18       V19
V20
          P.6.2    V16        .000
          P.6.3    V17        .018      .000
          P.6.4    V18       -.028     -.042      .000
          P.6.5    V19       -.032      .032      .034      .000
          P.9.3    V20       -.028     -.011     -.098      -
.063       .000
          P.9.9    V21        .152      .120      -
.006       .108      .016
          P.9.10   V22        .105     -.022     -.048      -
.014       .049
          P.9.12   V23       -.040     -.045     -.108      -
.060       .004
          P.9.13   V24       -.010     -.070     -.017     -.017
-.023
          P.9.14   V25        .040     -.095     -.125     -.096
-.012
          P.9.15   V26        .062      .022     -.039     -.014
-.002
          LOGANTIG V29        .032     -.067      -
.016       .030      .034
          LOGTAMA  V32        .005      .007     -.003     -.015
-.130


                             P.9.9     P.9.10    P.9.12    P.9.13
P.9.14
                              V21       V22       V23       V24
V25
          P.9.9    V21        .000
          P.9.10   V22        .000      .000
          P.9.12   V23       -.024      .004      .000
          P.9.13   V24       -.017      .007      .000      .000
          P.9.14   V25       -
.034       .001      .059      .023      .000
          P.9.15   V26        .042     -.061     -.025      -
.042       .012
          LOGANTIG V29        .050     -.022     -.015      -
.018       .016
          LOGTAMA  V32        .062      .023     -.034      .003
-.049


                             P.9.15    LOGANTIG  LOGTAMA
```

```
                              V26          V29          V32
P.9.15   V26                  .000
LOGANTIG V29                 -.017         .000
LOGTAMA  V32                 -.003         .000         .000


                     AVERAGE ABSOLUTE STANDARDIZED RESIDUALS
=          .0447
             AVERAGE OFF-DIAGONAL ABSOLUTE STANDARDIZED RESIDUALS
=          .0480


       LARGEST STANDARDIZED RESIDUALS:

           NO.    PARAMETER    ESTIMATE      NO.    PARAMETER    ESTIMATE
           ---    ---------    --------      ---    ---------    --------
            1     V13,  V3       .191        11     V12,  V3       .153
            2     V25,  V9      -.181        12     V21,  V16      .152
            3     V7,   V5       .179        13     V18,  V4       .151
            4     V18,  V3       .177        14     V18,  V8       .145
            5     V18,  V10      .173        15     V25,  V8      -.144
            6     V26,  V11      .168        16     V20,  V12      .142
            7     V15,  V1      -.167        17     V21,  V4       .140
            8     V7,   V3       .166        18     V32,  V11     -.138
            9     V7,   V6       .159        19     V18,  V9       .134
           10     V4,   V3       .154        20     V32,  V20     -.130


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       MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


       DISTRIBUTION OF STANDARDIZED RESIDUALS


          ----------------------------------------
          !                                      !
       200-                                      -
          !                 *                    !
          !                 *                    !
          !              *  *                    !
          !              *  *                    !          RANGE
FREQ PERCENT
       150-              *  *                    -
          !              *  *                    !    1   -0.5  -  --
0    .00%
          !              *  *                    !    2   -0.4  -  -0.5
0    .00%
          !              *  *                    !    3   -0.3  -  -0.4
0    .00%
          !              *  *                    !    4   -0.2  -  -0.3
0    .00%
```

```
       100-                 *  *                  -    5   -0.1  -  -0.2
12   2.96%
          !                 *  *                  !    6    0.0  -  -0.1
169  41.63%
          !                 *  *                  !    7    0.1  -   0.0
194  47.78%
          !                 *  *                  !    8    0.2  -   0.1
31   7.64%
          !                 *  *                  !    9    0.3  -   0.2
0    .00%
        50-                 *  *                  -    A    0.4  -   0.3
0    .00%
          !                 *  *                  !    B    0.5  -   0.4
0    .00%
          !                 *  *  *               !    C     ++  -   0.5
0    .00%
          !                 *  *  *               !    ------------------
-------------
          !              *  *  *  *               !           TOTAL
406 100.00%
          ----------------------------------------
             1  2  3  4  5  6  7  8  9  A  B  C       EACH "*" REPRESENTS
10 RESIDUALS


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       MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)



       GOODNESS OF FIT SUMMARY FOR METHOD = ML

       INDEPENDENCE MODEL CHI-SQUARE        =    3311.841 ON   380
DEGREES OF FREEDOM

       INDEPENDENCE AIC =  2551.84145   INDEPENDENCE CAIC =   980.23804
              MODEL AIC =   -89.83219          MODEL CAIC = -1438.10248

       CHI-SQUARE =      562.168 BASED ON     326 DEGREES OF FREEDOM
       PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00000

       THE NORMAL THEORY RLS CHI-SQUARE FOR THIS ML SOLUTION IS
532.938.

       FIT INDICES
       -----------
       BENTLER-BONETT     NORMED FIT INDEX =      .830
       BENTLER-BONETT NON-NORMED FIT INDEX =      .906
       COMPARATIVE FIT INDEX (CFI)         =      .919
       BOLLEN   (IFI) FIT INDEX            =      .921
       MCDONALD (MFI) FIT INDEX            =      .499
       LISREL    GFI  FIT INDEX            =      .816
       LISREL   AGFI  FIT INDEX            =      .771
       ROOT MEAN-SQUARE RESIDUAL (RMR)     =      .278
       STANDARDIZED RMR                    =      .060
```

```
        ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .065
        90% CONFIDENCE INTERVAL OF RMSEA  (        .056,        .074)

        RELIABILITY COEFFICIENTS
        ------------------------
        CRONBACH'S ALPHA                   =      .915
        COEFFICIENT ALPHA FOR AN OPTIMAL SHORT SCALE
=      .922
        BASED ON 24 VARIABLES, ALL EXCEPT:
        P.3.1     P.3.3     LOGANTIG  LOGTAMA
        RELIABILITY COEFFICIENT RHO        =      .958
        GREATEST LOWER BOUND RELIABILITY
=      .981
        GLB RELIABILITY FOR AN OPTIMAL SHORT SCALE
=      .982
        BASED ON 26 VARIABLES, ALL EXCEPT:
        P.3.1     P.3.3
        BENTLER'S DIMENSION-FREE LOWER BOUND RELIABILITY
=      .980
        SHAPIRO'S LOWER BOUND RELIABILITY FOR A WEIGHTED COMPOSITE
COULD NOT BE
        CALCULATED BECAUSE OF FAILURE TO CONVERGE IN 500 ITERATIONS.


        GOODNESS OF FIT SUMMARY FOR METHOD = ROBUST

        ROBUST INDEPENDENCE MODEL CHI-SQUARE =    3066.030 ON   380
DEGREES OF FREEDOM

        INDEPENDENCE AIC =  2306.03012   INDEPENDENCE CAIC =   734.42671
               MODEL AIC =  -203.10347          MODEL CAIC = -1551.37376

        SATORRA-BENTLER SCALED CHI-SQUARE =    448.8965 ON     326
DEGREES OF FREEDOM
        PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00001

        FIT INDICES
        -----------
        BENTLER-BONETT     NORMED FIT INDEX =      .854
        BENTLER-BONETT NON-NORMED FIT INDEX =      .947
        COMPARATIVE FIT INDEX (CFI)        =      .954
        BOLLEN   (IFI) FIT INDEX           =      .955
        MCDONALD (MFI) FIT INDEX           =      .697
        ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .047
        90% CONFIDENCE INTERVAL OF RMSEA  (        .036,        .057)


                               ITERATIVE SUMMARY

                           PARAMETER
        ITERATION          ABS CHANGE         ALPHA
FUNCTION
            1               1.666932          .50000
10.45537
            2                .809663         1.00000
5.32508
```

```
           3                .398948          .50000
5.23836
           4                .153451         1.00000
4.52912
           5                .131590         1.00000
3.54724
           6                .034840         1.00000
3.35658
           7                .018463         1.00000
3.32764
           8                .005241         1.00000
3.32656
           9                .001885         1.00000
3.32645
          10                .000815         1.00000
3.32644

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        MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


        MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
        STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
        (ROBUST STATISTICS IN PARENTHESES)



       P.2.2   =V1  =   1.000 F6    + 1.000 E1




       P.2.3   =V2  =    .895*F6    + 1.000 E2
                         .078
                       11.500@
                     (   .075)
                     ( 11.868@

       P.2.4   =V3  =    .958*F6    + 1.000 E3
                         .107
                        8.990@
                     (   .089)
                     ( 10.773@

       P.2.6   =V4  =    .919*F6    + 1.000 E4
                         .097
                        9.522@
                     (   .088)
                     ( 10.471@

       P.3.1   =V5  =   1.000 F7    + 1.000 E5
```

```
P.3.3   =V6  =   1.423*F7    + 1.000 E6
                  .404
                 3.526@
              (   .384)
              (  3.708@

P.4.1   =V7  =   1.000 F8    + 1.000 E7



P.4.2   =V8  =   1.301*F8    + 1.000 E8
                  .108
                12.030@
              (   .119)
              ( 10.957@

P.4.3   =V9  =   1.354*F8    + 1.000 E9
                  .110
                12.294@
              (   .126)
              ( 10.737@

P.4.4   =V10 =   1.290*F8    + 1.000 E10
                  .111
                11.662@
              (   .122)
              ( 10.548@

P.4.7   =V11 =   1.000 F9    + 1.000 E11



P.4.8   =V12 =   1.049*F9    + 1.000 E12
                  .084
                12.520@
              (   .073)
              ( 14.309@
```

MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS (CONTINUED)

```
 MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)
 (ROBUST STATISTICS IN PARENTHESES)

P.4.9   =V13 =   1.116*F9    + 1.000 E13
                   .087
                 12.847@
               (   .077)
               ( 14.567@

P.4.10  =V14 =    .987*F9    + 1.000 E14
                   .088
                 11.236@
               (   .082)
               ( 12.041@

P.6.1   =V15 =   1.000 F10   + 1.000 E15



P.6.2   =V16 =   1.013*F10   + 1.000 E16
                   .100
                 10.158@
               (   .088)
               ( 11.491@

P.6.3   =V17 =   1.087*F10   + 1.000 E17
                   .103
                 10.511@
               (   .093)
               ( 11.652@

P.6.4   =V18 =    .895*F10   + 1.000 E18
                   .098
                  9.098@
               (   .091)
               (  9.820@

P.6.5   =V19 =   1.027*F10   + 1.000 E19
                   .101
                 10.158@
               (   .100)
               ( 10.255@

P.9.3   =V20 =   1.000 F12   + 1.000 E20



P.9.9   =V21 =   1.000 F14   + 1.000 E21
```

```
P.9.10  =V22 =   1.059*F14   + 1.000 E22
                   .087
                 12.163@
               (   .091)
               ( 11.630@

P.9.12  =V23 =   1.000 F13   + 1.000 E23



P.9.13  =V24 =   1.075*F13   + 1.000 E24
                   .079
                 13.662@
               (   .085)
               ( 12.595@


   MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
(CONTINUED)


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   MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)
   (ROBUST STATISTICS IN PARENTHESES)

P.9.14  =V25 =   1.691*F12   + 1.000 E25
                   .191
                  8.852@
               (   .239)
               (  7.064@

P.9.15  =V26 =   1.411*F12   + 1.000 E26
                   .178
                  7.945@
               (   .211)
               (  6.678@

LOGANTIG=V29 =   1.000 F17   + 1.000 E29



LOGTAMA =V32 =   1.000 F16   + 1.000 E32
```

TITLE:   master confirmatorio la 5 sobre la 6, 7, 10 y 11 y la 4 sob

MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

CONSTRUCT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
(ROBUST STATISTICS IN PARENTHESES)

```
F8   =F8  =   1.000 F11   + 1.000 D8


F9   =F9  =   1.111*F11   + 1.000 D9
               .177
              6.286@
           (   .178)
           (  6.227@

F12  =F12 =    .378*F15   + 1.000 D12
               .056
              6.745@
           (   .067)
           (  5.656@

F13  =F13 =    .834*F15   + 1.000 D13
               .098
              8.501@
           (   .089)
           (  9.338@

F14  =F14 =   1.000 F15   + 1.000 D14


F15  =F15 =   -.099*F6    -  .194*F7    +  .184*F10
+  .716*F11
               .098          .121          .105          .230
             -1.010        -1.596         1.745         3.119@
           (   .100)     (   .133)     (   .107)     (   .204)
           (  -.993)     ( -1.459)     (  1.718)     (  3.507@

            -  .109*F16   +  .138*F17   + 1.000 D15
               .221          .385
              -.492          .359
           (   .213)     (   .390)
           (  -.512)     (   .355)
```

```
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       MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

       VARIANCES OF INDEPENDENT VARIABLES
       ----------------------------------
       STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                       V                                F
                      ---                              ---
                              I F6  -   F6              3.139*I
                              I                          .504 I
                              I                         6.229@I
                              I                       (  .543)I
                              I                       ( 5.778@I
                              I                               I
                              I F7  -   F7              1.918*I
                              I                          .691 I
                              I                         2.777@I
                              I                       (  .703)I
                              I                       ( 2.730@I
                              I                               I
                              I F10 -   F10             3.027*I
                              I                          .554 I
                              I                         5.463@I
                              I                       (  .463)I
                              I                       ( 6.537@I
                              I                               I
                              I F11 -   F11             1.672*I
                              I                          .431 I
                              I                         3.881@I
                              I                       (  .448)I
                              I                       ( 3.736@I
                              I                               I
                              I F16 -   F16              .370*I
                              I                          .040 I
                              I                         9.192@I
                              I                       (  .051)I
                              I                       ( 7.251@I
                              I                               I
                              I F17 -   F17              .126*I
                              I                          .014 I
                              I                         9.192@I
                              I                       (  .018)I
                              I                       ( 7.177@I
                              I                               I


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       MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

       VARIANCES OF INDEPENDENT VARIABLES
       ----------------------------------
```

STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

```
                 E                                  D
                ---                                ---
E1  -P.2.2              1.396*I D8  -   F8                  1.314*I
                         .238 I                              .308 I
                        5.867@I                             4.267@I
                     (   .415)I                          (   .297)I
                     (  3.368@I                          (  4.426@I
                              I                                   I
E2  -P.2.3              1.060*I D9  -   F9                  1.306*I
                         .186 I                              .314 I
                        5.698@I                             4.153@I
                     (   .258)I                          (   .379)I
                     (  4.111@I                          (  3.446@I
                              I                                   I
E3  -P.2.4              3.525*I D12 -   F12                  .208*I
                         .438 I                              .056 I
                        8.042@I                             3.724@I
                     (   .501)I                          (   .076)I
                     (  7.032@I                          (  2.760@I
                              I                                   I
E4  -P.2.6              2.707*I D13 -   F13                  .840*I
                         .347 I                              .188 I
                        7.803@I                             4.477@I
                     (   .486)I                          (   .229)I
                     (  5.572@I                          (  3.661@I
                              I                                   I
E5  -P.3.1              3.773*I D14 -   F14                  .340*I
                         .656 I                              .196 I
                        5.748@I                             1.732 I
                     (   .732)I                          (   .284)I
                     (  5.156@I                          (  1.196)I
                              I                                   I
E6  -P.3.3              1.694*I D15 -   F15                 1.375*I
                        1.054 I                              .318 I
                        1.608 I                             4.320@I
                     (  1.023)I                          (   .327)I
                     (  1.656)I                          (  4.202@I
                              I                                   I
E7  -P.4.1              2.988*I                                   I
                         .337 I                                   I
                        8.878@I                                   I
                     (   .471)I                                   I
                     (  6.345@I                                   I
                              I                                   I
E8  -P.4.2               .616*I                                   I
                         .100 I                                   I
                        6.170@I                                   I
                     (   .191)I                                   I
                     (  3.226@I                                   I
                              I                                   I
E9  -P.4.3               .372*I                                   I
                         .088 I                                   I
                        4.226@I                                   I
                     (   .285)I                                   I
                     (  1.305)I                                   I
                              I                                   I
E10 -P.4.4               .973*I                                   I
```

```
                          .131 I                               I
                         7.453@I                               I
                      (   .346)I                               I
                      (  2.810@I                               I
                               I                               I
 E11 -P.4.7              1.750*I                               I
                          .239 I                               I
                         7.330@I                               I
                      (   .271)I                               I
                      (  6.453@I                               I
                               I                               I
 E12 -P.4.8              1.448*I                               I
                          .216 I                               I
                         6.692@I                               I
                      (   .362)I                               I
                      (  4.004@I                               I
                               I                               I


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   MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

   VARIANCES OF INDEPENDENT VARIABLES (CONTINUED)
   ----------------------------------------------

 E13 -P.4.9              1.403*I                               I
                          .223 I                               I
                         6.277@I                               I
                      (   .347)I                               I
                      (  4.047@I                               I
                               I                               I
 E14 -P.4.10             2.092*I                               I
                          .272 I                               I
                         7.686@I                               I
                      (   .284)I                               I
                      (  7.376@I                               I
                               I                               I
 E15 -P.6.1              2.394*I                               I
                          .308 I                               I
                         7.771@I                               I
                      (   .420)I                               I
                      (  5.701@I                               I
                               I                               I
 E16 -P.6.2              1.839*I                               I
                          .253 I                               I
                         7.283@I                               I
                      (   .430)I                               I
                      (  4.281@I                               I
                               I                               I
 E17 -P.6.3              1.749*I                               I
                          .254 I                               I
                         6.878@I                               I
                      (   .374)I                               I
                      (  4.677@I                               I
                               I                               I
```

```
E18 -P.6.4              2.331*I                                I
                          .290 I                                I
                        8.027@I                                I
                     (    .329)I                                I
                     (  7.087@I                                I
                               I                                I
E19 -P.6.5              1.889*I                                I
                          .259 I                                I
                        7.283@I                                I
                     (    .318)I                                I
                     (  5.946@I                                I
                               I                                I
E20 -P.9.3                .595*I                                I
                          .078 I                                I
                        7.583@I                                I
                     (    .097)I                                I
                     (  6.151@I                                I
                               I                                I
E21 -P.9.9              1.316*I                                I
                          .205 I                                I
                        6.412@I                                I
                     (    .364)I                                I
                     (  3.611@I                                I
                               I                                I
E22 -P.9.10               .720*I                                I
                          .182 I                                I
                        3.944@I                                I
                     (    .194)I                                I
                     (  3.715@I                                I
                               I                                I
E23 -P.9.12               .413*I                                I
                          .137 I                                I
                        3.018@I                                I
                     (    .189)I                                I
                     (  2.185@I                                I
                               I                                I
E24 -P.9.13               .891*I                                I
                          .178 I                                I
                        5.004@I                                I
                     (    .316)I                                I
                     (  2.817@I                                I
                               I                                I
```

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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES (CONTINUED)
  ----------------------------------------------
```

```
E25 -P.9.14               .585*I                                I
                          .127 I                                I
                        4.603@I                                I
                     (    .201)I                                I
                     (  2.908@I                                I
                               I                                I
```

```
       E26 -P.9.15             1.067*I                               I
                                .144 I                               I
                               7.389@I                               I
                            (   .279)I                               I
                            (  3.826@I                               I
                                     I                               I


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        MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

        COVARIANCES AMONG INDEPENDENT VARIABLES
        ---------------------------------------
        STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                        V                                F
                       ---                              ---
                                     I F7  -   F7                .249*I
                                     I F6  -   F6                .244 I
                                     I                          1.018 I
                                     I                       (   .279)I
                                     I                       (   .893)I
                                     I                                I
                                     I F10 -   F10              1.038*I
                                     I F6  -   F6                .296 I
                                     I                          3.513@I
                                     I                       (   .287)I
                                     I                       (  3.619@I
                                     I                                I
                                     I F11 -   F11              1.203*I
                                     I F6  -   F6                .279 I
                                     I                          4.316@I
                                     I                       (   .279)I
                                     I                       (  4.313@I
                                     I                                I
                                     I F16 -   F16               .127*I
                                     I F6  -   F6                .090 I
                                     I                          1.415 I
                                     I                       (   .088)I
                                     I                       (  1.451)I
                                     I                                I
                                     I F17 -   F17               .073*I
                                     I F6  -   F6                .053 I
                                     I                          1.387 I
                                     I                       (   .049)I
                                     I                       (  1.473)I
                                     I                                I
                                     I F10 -   F10               .798*I
                                     I F7  -   F7                .306 I
                                     I                          2.608@I
                                     I                       (   .342)I
                                     I                       (  2.332@I
                                     I                                I
                                     I F11 -   F11               .756*I
                                     I F7  -   F7                .277 I
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```
I                                2.734@I
I                              (   .304)I
I                              (  2.488@I
I                                       I
I F16 -   F16                    .044*I
I F7  -   F7                     .076 I
I                                .579 I
I                              (   .079)I
I                              (   .559)I
I                                       I
I F17 -   F17                   -.071*I
I F7  -   F7                     .047 I
I                              -1.491 I
I                              (   .043)I
I                              ( -1.631)I
I                                       I
I F11 -   F11                   1.378*I
I F10 -   F10                    .295 I
I                                4.664@I
I                              (   .289)I
I                              (  4.775@I
I                                       I
I F16 -   F16                    .250*I
I F10 -   F10                    .090 I
I                                2.773@I
I                              (   .087)I
I                              (  2.868@I
I                                       I
I F17 -   F17                   -.022*I
I F10 -   F10                    .051 I
I                                -.437 I
I                              (   .054)I
I                              (  -.410)I
I                                       I
```



MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

COVARIANCES AMONG INDEPENDENT VARIABLES (CONTINUED)

---------------------------------------------------

```
I F16 -   F16                    .121*I
I F11 -   F11                    .074 I
I                                1.647 I
I                              (   .076)I
I                              (  1.601)I
I                                       I
I F17 -   F17                   -.048*I
I F11 -   F11                    .043 I
I                              -1.138 I
I                              (   .046)I
I                              ( -1.052)I
I                                       I
I F17 -   F17                    .096*I
I F16 -   F16                    .018 I
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                                          I                       5.276@I
                                          I                    (   .019)I
                                          I                    (  5.136@I
                                          I                             I


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        MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

        DECOMPOSITION OF EFFECTS WITH NONSTANDARDIZED VALUES
        STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

        PARAMETER TOTAL EFFECTS
        -----------------------

       P.2.2   =V1  =   1.000 F6    + 1.000 E1



       P.2.3   =V2  =    .895*F6    + 1.000 E2



       P.2.4   =V3  =    .958*F6    + 1.000 E3



       P.2.6   =V4  =    .919*F6    + 1.000 E4



       P.3.1   =V5  =   1.000 F7    + 1.000 E5



       P.3.3   =V6  =   1.423*F7    + 1.000 E6



       P.4.1   =V7  =   1.000 F8    + 1.000 F11   + 1.000 E7    + 1.000
D8
```

```
      P.4.2   =V8  =   1.301*F8    + 1.301 F11   + 1.000 E8    + 1.301
D8
                         .108          .108                          .108
                       12.030@       12.030@                       12.030@
                     (   .119)     (   .119)                     (   .119)
                     ( 10.957@     ( 10.957@                     ( 10.957@

      P.4.3   =V9  =   1.354*F8    + 1.354 F11   + 1.000 E9    + 1.354
D8
                         .110          .110                          .110
                       12.294@       12.294@                       12.294@
                     (   .126)     (   .126)                     (   .126)
                     ( 10.737@     ( 10.737@                     ( 10.737@

      P.4.4   =V10 =   1.290*F8    + 1.290 F11   + 1.000 E10   + 1.290
D8
                         .111          .111                          .111
                       11.662@       11.662@                       11.662@
                     (   .122)     (   .122)                     (   .122)
                     ( 10.548@     ( 10.548@                     ( 10.548@

      P.4.7   =V11 =   1.000 F9    + 1.111 F11   + 1.000 E11   + 1.000
D9
                                       .177
                                      6.286@
                                   (   .178)
                                   (  6.227@

      P.4.8   =V12 =   1.049*F9    + 1.165 F11   + 1.000 E12   + 1.049
D9
                         .084          .182                          .084
                       12.520@        6.393@                       12.520@
                     (   .073)     (   .214)                     (   .073)
                     ( 14.309@     (  5.453@                     ( 14.309@

      P.4.9   =V13 =   1.116*F9    + 1.240 F11   + 1.000 E13   + 1.116
D9
                         .087          .192                          .087
                       12.847@        6.443@                       12.847@
                     (   .077)     (   .231)                     (   .077)
                     ( 14.567@     (  5.368@                     ( 14.567@

      P.4.10  =V14 =    .987*F9    + 1.096 F11   + 1.000 E14   +  .987
D9
                         .088          .177                          .088
                       11.236@        6.192@                       11.236@
                     (   .082)     (   .213)                     (   .082)
                     ( 12.041@     (  5.155@                     ( 12.041@
```

```
        P.6.1   =V15 =   1.000 F10   + 1.000 E15



        P.6.2   =V16 =   1.013*F10   + 1.000 E16



        P.6.3   =V17 =   1.087*F10   + 1.000 E17



        P.6.4   =V18 =    .895*F10   + 1.000 E18



        P.6.5   =V19 =   1.027*F10   + 1.000 E19



        P.9.3   =V20 =   1.000 F12   +  .378 F15   -  .037 F6    -  .073
F7
                                        .056          .037          .046
                                       6.745@       -1.005        -1.577
                                    (   .067)     (   .038)     (   .053)
                                    (  5.656@     (  -.990)     ( -1.373)

                       +  .069 F10   +  .271 F11   -  .041 F16   +  .052
F17
                          .040          .091          .084          .145
                         1.721         2.989@        -.492          .359
                      (   .045)     (   .091)     (   .080)     (   .147)
                      (  1.544)     (  2.973@     (  -.511)     (   .355)

                       + 1.000 E20   + 1.000 D12   +  .378 D15
                                                      .056
                                                     6.745@
                                                  (   .067)
                                                  (  5.656@

        P.9.9   =V21 =   1.000 F14   + 1.000 F15   -  .099 F6    -  .194
F7
                                                      .098          .121
                                                    -1.010        -1.596
                                                  (   .100)     (   .133)
                                                  (  -.993)     ( -1.459)
```

```
                        +  .184 F10   +  .716 F11   -  .109 F16   +  .138
F17
                           .105          .230          .221          .385
                          1.745         3.119@         -.492          .359
                       (   .107)     (   .204)     (   .213)     (   .390)
                       (  1.718)     (  3.507@     (  -.512)     (   .355)

                        + 1.000 E21   + 1.000 D14   + 1.000 D15



      P.9.10  =V22 =   1.059*F14   + 1.059 F15   -  .105 F6    -  .205
F7
                           .087          .087          .104          .128
                         12.163@       12.163@       -1.011        -1.600
                       (   .091)     (   .091)     (   .105)     (   .142)
                       ( 11.630@     ( 11.630@     (  -.996)     ( -1.446)

                        +  .195 F10   +  .758 F11   -  .115 F16   +  .146
F17
                           .111          .240          .234          .407
                          1.751         3.154@         -.492          .359
                       (   .117)     (   .230)     (   .225)     (   .413)
                       (  1.661)     (  3.300@     (  -.511)     (   .354)

                        + 1.000 E22   + 1.059 D14   + 1.059 D15
                                         .087          .087
                                       12.163@       12.163@
                                     (   .091)     (   .091)
                                     ( 11.630@     ( 11.630@

      P.9.12  =V23 =   1.000 F13   +  .834 F15   -  .083 F6    -  .161
F7
                                         .098          .082          .101
                                        8.501@       -1.010        -1.594
                                     (   .089)     (   .083)     (   .111)
                                     (  9.338@     (  -.993)     ( -1.451)

                        +  .153 F10   +  .597 F11   -  .091 F16   +  .115
F17
                           .088          .192          .184          .321
                          1.743         3.108@         -.492          .359
                       (   .093)     (   .185)     (   .178)     (   .325)
                       (  1.642)     (  3.234@     (  -.511)     (   .355)

                        + 1.000 E23   + 1.000 D13   +  .834 D15
                                                       .098
                                                      8.501@
                                                   (   .089)
                                                   (  9.338@

      P.9.13  =V24 =   1.075*F13   +  .896 F15   -  .089 F6    -  .174
F7
                           .079          .111          .088          .109
                         13.662@        8.043@       -1.009        -1.591
                       (   .085)     (   .109)     (   .090)     (   .121)
                       ( 12.595@     (  8.247@     (  -.988)     ( -1.435)
```

```
                     +  .165 F10   +  .642 F11   -  .097 F16   +  .124
F17
                         .095         .208         .198         .345
                        1.739        3.084@       -.492         .359
                    (    .100)   (    .205)   (    .191)   (    .351)
                    (   1.643)   (   3.128@   (   -.510)   (    .353)

                     + 1.000 E24   + 1.075 D13   +  .896 D15
                                      .079         .111
                                    13.662@       8.043@
                                 (    .085)   (    .109)
                                 (  12.595@   (   8.247@

       P.9.14  =V25 =   1.691*F12   +  .639 F15   -  .063 F6    -  .124
F7
                         .191         .082         .063         .078
                        8.852@       7.834@      -1.008       -1.589
                    (    .239)   (    .093)   (    .065)   (    .086)
                    (   7.064@   (   6.835@   (   -.973)   (  -1.442)

                     +  .117 F10   +  .457 F11   -  .069 F16   +  .088
F17
                         .068         .149         .141         .246
                        1.736        3.068@       -.492         .359
                    (    .073)   (    .152)   (    .137)   (    .250)
                    (   1.620)   (   3.002@   (   -.509)   (    .354)

                     + 1.000 E25   + 1.691 D12   +  .639 D15
                                      .191         .082
                                     8.852@       7.834@
                                 (    .239)   (    .093)
                                 (   7.064@   (   6.835@

       P.9.15  =V26 =   1.411*F12   +  .533 F15   -  .053 F6    -  .103
F7
                         .178         .078         .053         .065
                        7.945@       6.862@      -1.006       -1.579
                    (    .211)   (    .074)   (    .053)   (    .074)
                    (   6.678@   (   7.248@   (   -.988)   (  -1.401)

                     +  .098 F10   +  .382 F11   -  .058 F16   +  .074
F17
                         .057         .127         .118         .205
                        1.723        2.999@       -.492         .359
                    (    .059)   (    .126)   (    .114)   (    .208)
                    (   1.657)   (   3.033@   (   -.507)   (    .354)

                     + 1.000 E26   + 1.411 D12   +  .533 D15
                                      .178         .078
                                     7.945@       6.862@
                                 (    .211)   (    .074)
                                 (   6.678@   (   7.248@

       LOGANTIG=V29 =   1.000 F17   + 1.000 E29
```

```
LOGTAMA =V32 =   1.000 F16   + 1.000 E32



F8   =F8  =   1.000 F11   + 1.000 D8



F9   =F9  =   1.111*F11   + 1.000 D9



F12  =F12 =    .378*F15   -  .037 F6    -  .073 F7    +  .069
F10
               .056          .037          .046          .040
              6.745@       -1.005        -1.577         1.721
           (   .067)     (   .038)     (   .053)     (   .045)
           (  5.656@     (  -.990)     ( -1.373)     (  1.544)

             +  .271 F11   -  .041 F16   +  .052 F17   + 1.000
D12
               .091          .084          .145
              2.989@        -.492          .359
           (   .091)     (   .080)     (   .147)
           (  2.973@     (  -.511)     (   .355)

             +  .378 D15
               .056
              6.745@
           (   .067)
           (  5.656@

F13  =F13 =    .834*F15   -  .083 F6    -  .161 F7    +  .153
F10
               .098          .082          .101          .088
              8.501@       -1.010        -1.594         1.743
           (   .089)     (   .083)     (   .111)     (   .093)
           (  9.338@     (  -.993)     ( -1.451)     (  1.642)

             +  .597 F11   -  .091 F16   +  .115 F17   + 1.000
D13
               .192          .184          .321
              3.108@        -.492          .359
           (   .185)     (   .178)     (   .325)
           (  3.234@     (  -.511)     (   .355)

             +  .834 D15
               .098
              8.501@
           (   .089)
           (  9.338@
```

```
         F14  =F14 =   1.000 F15   -  .099 F6    -  .194 F7    +  .184
F10
                                       .098          .121          .105
                                     -1.010        -1.596         1.745
                                   (   .100)     (   .133)     (   .107)
                                   (  -.993)     ( -1.459)     (  1.718)

                       +  .716 F11   -  .109 F16   +  .138 F17   + 1.000
D14
                          .230          .221          .385
                         3.119@        -.492          .359
                      (   .204)     (   .213)     (   .390)
                      (  3.507@     (  -.512)     (   .355)

                       + 1.000 D15



         F15  =F15 =   -.099*F6    -  .194*F7    +  .184*F10
+  .716*F11



                       -  .109*F16   +  .138*F17   + 1.000 D15



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       MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

       DECOMPOSITION OF EFFECTS WITH NONSTANDARDIZED VALUES
       STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

       PARAMETER INDIRECT EFFECTS
       --------------------------

      P.4.1   =V7  =   1.000 F11   + 1.000 D8



      P.4.2   =V8  =   1.301 F11   + 1.301 D8
                        .108          .108
                      12.030@       12.030@
                    (   .119)     (   .119)
```

```
                 ( 10.957@     ( 10.957@

 P.4.3   =V9  =   1.354 F11   + 1.354 D8
                   .110          .110
                 12.294@       12.294@
                 (   .126)     (   .126)
                 ( 10.737@     ( 10.737@

 P.4.4   =V10 =   1.290 F11   + 1.290 D8
                   .111          .111
                 11.662@       11.662@
                 (   .122)     (   .122)
                 ( 10.548@     ( 10.548@

 P.4.7   =V11 =   1.111 F11   + 1.000 D9
                   .177
                  6.286@
                 (   .178)
                 (  6.227@

 P.4.8   =V12 =   1.165 F11   + 1.049 D9
                   .182          .084
                  6.393@       12.520@
                 (   .214)     (   .073)
                 (  5.453@     ( 14.309@

 P.4.9   =V13 =   1.240 F11   + 1.116 D9
                   .192          .087
                  6.443@       12.847@
                 (   .231)     (   .077)
                 (  5.368@     ( 14.567@

 P.4.10  =V14 =   1.096 F11   +  .987 D9
                   .177          .088
                  6.192@       11.236@
                 (   .213)     (   .082)
                 (  5.155@     ( 12.041@

 P.9.3   =V20 =    .378 F15   -  .037 F6    -  .073 F7    +  .069
F10
                   .056          .037          .046          .040
                  6.745@       -1.005        -1.577         1.721
                 (   .067)     (   .038)     (   .053)     (   .045)
                 (  5.656@     (  -.990)     ( -1.373)     (  1.544)

                  +  .271 F11   -  .041 F16   +  .052 F17   + 1.000
D12
                   .091          .084          .145
                  2.989@        -.492          .359
                 (   .091)     (   .080)     (   .147)
                 (  2.973@     (  -.511)     (   .355)

                  +  .378 D15
                   .056
                  6.745@
                 (   .067)
                 (  5.656@
```

```
     P.9.9   =V21 =   1.000 F15   -  .099 F6    -  .194 F7    +  .184
F10
                                     .098          .121          .105
                                   -1.010        -1.596         1.745
                                 (   .100)     (   .133)     (   .107)
                                 (  -.993)     ( -1.459)     (  1.718)

                    +  .716 F11   -  .109 F16   +  .138 F17   + 1.000
D14
                       .230          .221          .385
                      3.119@        -.492          .359
                   (   .204)     (   .213)     (   .390)
                   (  3.507@     (  -.512)     (   .355)

                    + 1.000 D15




     P.9.10  =V22 =   1.059 F15   -  .105 F6    -  .205 F7    +  .195
F10
                       .087          .104          .128          .111
                     12.163@       -1.011        -1.600         1.751
                   (   .091)     (   .105)     (   .142)     (   .117)
                   ( 11.630@     (  -.996)     ( -1.446)     (  1.661)

                    +  .758 F11   -  .115 F16   +  .146 F17   + 1.059
D14
                       .240          .234          .407          .087
                      3.154@        -.492          .359        12.163@
                   (   .230)     (   .225)     (   .413)     (   .091)
                   (  3.300@     (  -.511)     (   .354)     ( 11.630@

                    + 1.059 D15
                       .087
                     12.163@
                   (   .091)
                   ( 11.630@

     P.9.12  =V23 =    .834 F15   -  .083 F6    -  .161 F7    +  .153
F10
                       .098          .082          .101          .088
                      8.501@       -1.010        -1.594         1.743
                   (   .089)     (   .083)     (   .111)     (   .093)
                   (  9.338@     (  -.993)     ( -1.451)     (  1.642)

                    +  .597 F11   -  .091 F16   +  .115 F17   + 1.000
D13
                       .192          .184          .321
                      3.108@        -.492          .359
                   (   .185)     (   .178)     (   .325)
                   (  3.234@     (  -.511)     (   .355)

                    +  .834 D15
                       .098
                      8.501@
                   (   .089)
```

```
                   (  9.338@

     P.9.13  =V24 =    .896 F15   -  .089 F6    -  .174 F7    +  .165
F10
                       .111          .088          .109          .095
                      8.043@       -1.009        -1.591         1.739
                   (   .109)    (   .090)    (   .121)    (   .100)
                   (  8.247@    (  -.988)    ( -1.435)    (  1.643)

                    +  .642 F11   -  .097 F16   +  .124 F17   + 1.075
D13
                       .208          .198          .345          .079
                      3.084@        -.492          .359        13.662@
                   (   .205)    (   .191)    (   .351)    (   .085)
                   (  3.128@    (  -.510)    (   .353)    ( 12.595@

                    +  .896 D15
                       .111
                      8.043@
                   (   .109)
                   (  8.247@

     P.9.14  =V25 =    .639 F15   -  .063 F6    -  .124 F7    +  .117
F10
                       .082          .063          .078          .068
                      7.834@       -1.008        -1.589         1.736
                   (   .093)    (   .065)    (   .086)    (   .073)
                   (  6.835@    (  -.973)    ( -1.442)    (  1.620)

                    +  .457 F11   -  .069 F16   +  .088 F17   + 1.691
D12
                       .149          .141          .246          .191
                      3.068@        -.492          .359         8.852@
                   (   .152)    (   .137)    (   .250)    (   .239)
                   (  3.002@    (  -.509)    (   .354)    (  7.064@

                    +  .639 D15
                       .082
                      7.834@
                   (   .093)
                   (  6.835@

     P.9.15  =V26 =    .533 F15   -  .053 F6    -  .103 F7    +  .098
F10
                       .078          .053          .065          .057
                      6.862@       -1.006        -1.579         1.723
                   (   .074)    (   .053)    (   .074)    (   .059)
                   (  7.248@    (  -.988)    ( -1.401)    (  1.657)

                    +  .382 F11   -  .058 F16   +  .074 F17   + 1.411
D12
                       .127          .118          .205          .178
                      2.999@        -.492          .359         7.945@
                   (   .126)    (   .114)    (   .208)    (   .211)
                   (  3.033@    (  -.507)    (   .354)    (  6.678@

                    +  .533 D15
                       .078
                      6.862@
```

```
                  (    .074)
                  (   7.248@

         F12  =F12 =    -.037 F6    -  .073 F7    +  .069 F10   +  .271
F11
                         .037          .046          .040          .091
                       -1.005        -1.577         1.721         2.989@
                  (    .038)     (    .053)     (    .045)     (    .091)
                  (   -.990)     (  -1.373)     (   1.544)     (   2.973@

                    -   .041 F16   +  .052 F17   +  .378 D15
                         .084          .145          .056
                        -.492          .359         6.745@
                  (    .080)     (    .147)     (    .067)
                  (   -.511)     (    .355)     (   5.656@

         F13  =F13 =    -.083 F6    -  .161 F7    +  .153 F10   +  .597
F11
                         .082          .101          .088          .192
                       -1.010        -1.594         1.743         3.108@
                  (    .083)     (    .111)     (    .093)     (    .185)
                  (   -.993)     (  -1.451)     (   1.642)     (   3.234@

                    -   .091 F16   +  .115 F17   +  .834 D15
                         .184          .321          .098
                        -.492          .359         8.501@
                  (    .178)     (    .325)     (    .089)
                  (   -.511)     (    .355)     (   9.338@

         F14  =F14 =    -.099 F6    -  .194 F7    +  .184 F10   +  .716
F11
                         .098          .121          .105          .230
                       -1.010        -1.596         1.745         3.119@
                  (    .100)     (    .133)     (    .107)     (    .204)
                  (   -.993)     (  -1.459)     (   1.718)     (   3.507@

                    -   .109 F16   +  .138 F17   + 1.000 D15
                         .221          .385
                        -.492          .359
                  (    .213)     (    .390)
                  (   -.512)     (    .355)


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        MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

        DECOMPOSITION OF EFFECTS WITH STANDARDIZED VALUES

        PARAMETER TOTAL EFFECTS
        -----------------------

       P.2.2   =V1  =    .832 F6    +  .555 E1

       P.2.3   =V2  =    .839*F6    +  .545 E2
```

P.2.4 =V3 = .671*F6 + .742 E3

P.2.6 =V4 = .703*F6 + .711 E4

P.3.1 =V5 = .581 F7 + .814 E5

P.3.3 =V6 = .835*F7 + .551 E6

P.4.1 =V7 = .707 F8 + .529 F11 + .707 E7 + .469
D8

P.4.2 =V8 = .944*F8 + .707 F11 + .330 E8 + .626
D8

P.4.3 =V9 = .968*F8 + .724 F11 + .252 E9 + .642
D8

P.4.4 =V10 = .914*F8 + .684 F11 + .405 E10 + .607
D8

P.4.7 =V11 = .811 F9 + .635 F11 + .585 E11 + .505
D9

P.4.8 =V12 = .848*F9 + .664 F11 + .530 E12 + .528
D9

P.4.9 =V13 = .866*F9 + .677 F11 + .501 E13 + .539
D9

P.4.10 =V14 = .781*F9 + .611 F11 + .624 E14 + .487
D9

P.6.1 =V15 = .747 F10 + .665 E15

P.6.2 =V16 = .793*F10 + .610 E16

P.6.3 =V17 = .819*F10 + .573 E17

P.6.4 =V18 = .714*F10 + .700 E18

P.6.5 =V19 = .793*F10 + .610 E19

P.9.3 =V20 = .689 F12 + .539 F15 - .062 F6 - .095
F7
+ .114 F10 + .329 F11 - .024 F16 + .017
F17
+ .725 E20 + .429 D12 + .416 D15

P.9.9 =V21 = .817 F14 + .763 F15 - .088 F6 - .135
F7
+ .161 F10 + .465 F11 - .033 F16 + .025
F17
+ .576 E21 + .293 D14 + .589 D15

P.9.10 =V22 = .897*F14 + .837 F15 - .097 F6 - .148
F7
+ .176 F10 + .511 F11 - .037 F16 + .027
F17

```
                    +  .442 E22   +  .322 D14   +  .647 D15

      P.9.12  =V23 =   .925 F13   +  .749 F15   -  .087 F6    -  .132
F7
                    +  .158 F10   +  .457 F11   -  .033 F16   +  .024
F17
                    +  .380 E23   +  .542 D13   +  .579 D15

      P.9.13  =V24 =   .872*F13   +  .706 F15   -  .082 F6    -  .125
F7
                    +  .149 F10   +  .431 F11   -  .031 F16   +  .023
F17
                    +  .490 E24   +  .511 D13   +  .545 D15

      P.9.14  =V25 =   .851*F12   +  .666 F15   -  .077 F6    -  .118
F7
                    +  .140 F10   +  .406 F11   -  .029 F16   +  .022
F17
                    +  .525 E25   +  .530 D12   +  .514 D15

      P.9.15  =V26 =   .708*F12   +  .554 F15   -  .064 F6    -  .098
F7
                    +  .117 F10   +  .338 F11   -  .024 F16   +  .018
F17
                    +  .707 E26   +  .441 D12   +  .428 D15

      LOGANTIG=V29 =  1.000 F17   +  .000 E29

      LOGTAMA =V32 =  1.000 F16   +  .000 E32

         F8   =F8  =   .748 F11   +  .663 D8

         F9   =F9  =   .783*F11   +  .623 D9

         F12  =F12 =   .782*F15   -  .090 F6    -  .138 F7    +  .165
F10
                    +  .477 F11   -  .034 F16   +  .025 F17   +  .623
D12
                    +  .604 D15

         F13  =F13 =   .810*F15   -  .094 F6    -  .143 F7    +  .171
F10
                    +  .494 F11   -  .035 F16   +  .026 F17   +  .586
D13
                    +  .626 D15

         F14  =F14 =   .934 F15   -  .108 F6    -  .165 F7    +  .197
F10
                    +  .569 F11   -  .041 F16   +  .030 F17   +  .358
D14
                    +  .721 D15

         F15  =F15 =  -.116*F6    -  .177*F7    +  .211*F10
+  .610*F11
                    -  .044*F16   +  .032*F17   +  .772 D15
```

MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

DECOMPOSITION OF EFFECTS WITH STANDARDIZED VALUES

PARAMETER INDIRECT EFFECTS
--------------------------

```
P.4.1   =V7  =    .529 F11   +  .469 D8

P.4.2   =V8  =    .707 F11   +  .626 D8

P.4.3   =V9  =    .724 F11   +  .642 D8

P.4.4   =V10 =    .684 F11   +  .607 D8

P.4.7   =V11 =    .635 F11   +  .505 D9

P.4.8   =V12 =    .664 F11   +  .528 D9

P.4.9   =V13 =    .677 F11   +  .539 D9

P.4.10  =V14 =    .611 F11   +  .487 D9

P.9.3   =V20 =    .539 F15   -  .062 F6    -  .095 F7    +  .114
F10
                +  .329 F11   -  .024 F16   +  .017 F17   +  .429
D12
                +  .416 D15

P.9.9   =V21 =    .763 F15   -  .088 F6    -  .135 F7    +  .161
F10
                +  .465 F11   -  .033 F16   +  .025 F17   +  .293
D14
                +  .589 D15

P.9.10  =V22 =    .837 F15   -  .097 F6    -  .148 F7    +  .176
F10
                +  .511 F11   -  .037 F16   +  .027 F17   +  .322
D14
                +  .647 D15

P.9.12  =V23 =    .749 F15   -  .087 F6    -  .132 F7    +  .158
F10
                +  .457 F11   -  .033 F16   +  .024 F17   +  .542
D13
                +  .579 D15

P.9.13  =V24 =    .706 F15   -  .082 F6    -  .125 F7    +  .149
F10
                +  .431 F11   -  .031 F16   +  .023 F17   +  .511
D13
                +  .545 D15

P.9.14  =V25 =    .666 F15   -  .077 F6    -  .118 F7    +  .140
F10
```

```
                      +  .406 F11   -  .029 F16   +  .022 F17   +  .530
D12
                      +  .514 D15

       P.9.15  =V26 =    .554 F15   -  .064 F6    -  .098 F7    +  .117
F10
                      +  .338 F11   -  .024 F16   +  .018 F17   +  .441
D12
                      +  .428 D15

          F12  =F12 =   -.090 F6    -  .138 F7    +  .165 F10   +  .477
F11
                      -  .034 F16   +  .025 F17   +  .604 D15

          F13  =F13 =   -.094 F6    -  .143 F7    +  .171 F10   +  .494
F11
                      -  .035 F16   +  .026 F17   +  .626 D15

          F14  =F14 =   -.108 F6    -  .165 F7    +  .197 F10   +  .569
F11
                      -  .041 F16   +  .030 F17   +  .721 D15


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        MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


        STANDARDIZED SOLUTION:
R-SQUARED



       P.2.2   =V1  =   .832 F6    + .555
E1                                      .692
       P.2.3   =V2  =   .839*F6    + .545
E2                                      .703
       P.2.4   =V3  =   .671*F6    + .742
E3                                      .450
       P.2.6   =V4  =   .703*F6    + .711
E4                                      .495
       P.3.1   =V5  =   .581 F7    + .814
E5                                      .337
       P.3.3   =V6  =   .835*F7    + .551
E6                                      .696
       P.4.1   =V7  =   .707 F8    + .707
E7                                      .500
       P.4.2   =V8  =   .944*F8    + .330
E8                                      .891
       P.4.3   =V9  =   .968*F8    + .252
E9                                      .936
       P.4.4   =V10 =   .914*F8    + .405
E10                                     .836
       P.4.7   =V11 =   .811 F9    + .585
E11                                     .658
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       P.4.8   =V12 =   .848*F9    + .530
E12                                    .719
       P.4.9   =V13 =   .866*F9    + .501
E13                                    .749
       P.4.10  =V14 =   .781*F9    + .624
E14                                    .611
       P.6.1   =V15 =   .747 F10   + .665
E15                                    .558
       P.6.2   =V16 =   .793*F10   + .610
E16                                    .628
       P.6.3   =V17 =   .819*F10   + .573
E17                                    .672
       P.6.4   =V18 =   .714*F10   + .700
E18                                    .510
       P.6.5   =V19 =   .793*F10   + .610
E19                                    .628
       P.9.3   =V20 =   .689 F12   + .725
E20                                    .475
       P.9.9   =V21 =   .817 F14   + .576
E21                                    .668
       P.9.10  =V22 =   .897*F14   + .442
E22                                    .805
       P.9.12  =V23 =   .925 F13   + .380
E23                                    .855
       P.9.13  =V24 =   .872*F13   + .490
E24                                    .760
       P.9.14  =V25 =   .851*F12   + .525
E25                                    .724
       P.9.15  =V26 =   .708*F12   + .707
E26                                    .501
       LOGANTIG=V29 =  1.000 F17   + .000 E29
1.000
       LOGTAMA =V32 =  1.000 F16   + .000 E32
1.000
          F8   =F8  =   .748 F11   + .663
D8                                     .560
          F9   =F9  =   .783*F11   + .623
D9                                     .612
          F12  =F12 =   .782*F15   + .623
D12                                    .612
          F13  =F13 =   .810*F15   + .586
D13                                    .656
          F14  =F14 =   .934 F15   + .358
D14                                    .872
          F15  =F15 =  -.116*F6    - .177*F7    + .211*F10   + .610*F11
                      - .044*F16   + .032*F17   + .772
D15                       .404


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        MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

        CORRELATIONS AMONG INDEPENDENT VARIABLES
        ---------------------------------------

                        V                                F
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                                 I F7  -   F7              .101*I
                                 I F6  -   F6                   I
                                 I                              I
                                 I F10 -   F10             .337*I
                                 I F6  -   F6                   I
                                 I                              I
                                 I F11 -   F11             .525*I
                                 I F6  -   F6                   I
                                 I                              I
                                 I F16 -   F16             .118*I
                                 I F6  -   F6                   I
                                 I                              I
                                 I F17 -   F17             .116*I
                                 I F6  -   F6                   I
                                 I                              I
                                 I F10 -   F10             .331*I
                                 I F7  -   F7                   I
                                 I                              I
                                 I F11 -   F11             .422*I
                                 I F7  -   F7                   I
                                 I                              I
                                 I F16 -   F16             .052*I
                                 I F7  -   F7                   I
                                 I                              I
                                 I F17 -   F17            -.143*I
                                 I F7  -   F7                   I
                                 I                              I
                                 I F11 -   F11             .613*I
                                 I F10 -   F10                  I
                                 I                              I
                                 I F16 -   F16             .236*I
                                 I F10 -   F10                  I
                                 I                              I
                                 I F17 -   F17            -.036*I
                                 I F10 -   F10                  I
                                 I                              I
                                 I F16 -   F16             .154*I
                                 I F11 -   F11                  I
                                 I                              I
                                 I F17 -   F17            -.105*I
                                 I F11 -   F11                  I
                                 I                              I
                                 I F17 -   F17             .444*I
                                 I F16 -   F16                  I
                                 I                              I



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                             E N D    O F    M E T H O D
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TITLE: master confirmatorio la 5 sobre la 6, 7, 10 y 11 y la 4 sob

MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

WALD TEST (FOR DROPPING PARAMETERS)
ROBUST INFORMATION MATRIX USED IN THIS WALD TEST
MULTIVARIATE WALD TEST BY SIMULTANEOUS PROCESS

| | CUMULATIVE MULTIVARIATE STATISTICS | | | | UNIVARIATE INCREMENT | |
|---|---|---|---|---|---|---|
| STEP | PARAMETER | CHI-SQUARE | D.F. | PROBABILITY | CHI-SQUARE | PROBABILITY |
| 1 | F15,F17 | .126 | 1 | .723 | .126 | .723 |
| 2 | F15,F16 | .285 | 2 | .867 | .159 | .690 |
| 3 | F17,F10 | .497 | 3 | .920 | .212 | .646 |
| 4 | F16,F7 | .828 | 4 | .935 | .331 | .565 |
| 5 | F7,F6 | 1.559 | 5 | .906 | .731 | .392 |
| 6 | F15,F6 | 2.453 | 6 | .874 | .894 | .344 |
| 7 | F17,F11 | 3.511 | 7 | .834 | 1.058 | .304 |
| 8 | F15,F7 | 4.920 | 8 | .766 | 1.409 | .235 |
| 9 | E9,E9 | 5.998 | 9 | .740 | 1.078 | .299 |
| 10 | F16,F6 | 7.756 | 10 | .653 | 1.758 | .185 |
| 11 | E6,E6 | 9.458 | 11 | .580 | 1.702 | .192 |
| 12 | F17,F7 | 11.447 | 12 | .491 | 1.989 | .158 |
| 13 | F15,F10 | 13.149 | 13 | .436 | 1.701 | .192 |
| 14 | F10,F7 | 14.447 | 14 | .417 | 1.299 | .254 |
| 15 | F11,F7 | 14.805 | 15 | .466 | .358 | .550 |
| 16 | F17,F6 | 16.895 | 16 | .392 | 2.090 | .148 |
| 17 | F7,F7 | 18.864 | 17 | .336 | 1.968 | .161 |
| 18 | D14,D14 | 21.615 | 18 | .250 | 2.752 | .097 |

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MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

LAGRANGE MULTIPLIER TEST (FOR ADDING PARAMETERS)

ORDERED UNIVARIATE TEST STATISTICS:

| NO | CODE | | PARAMETER | CHI-SQUARE | PROB. | HANCOCK 326 DF PROB. | PARAMETER CHANGE | STANDARDIZED CHANGE |
|---|---|---|---|---|---|---|---|---|
| 1 | 2 | 20 | V25,F8 | 9.595 | .002 | 1.000 | -.157 | -.063 |
| 2 | 2 | 12 | V7,F7 | 8.996 | .003 | 1.000 | .364 | .107 |
| 3 | 2 | 22 | F9,F12 | 8.572 | .003 | 1.000 | .727 | .540 |
| 4 | 2 | 12 | V21,F10 | 7.737 | .005 | 1.000 | .210 | .061 |
| 5 | 2 | 12 | V11,F16 | 7.578 | .006 | 1.000 | -.516 | -.375 |
| 6 | 2 | 16 | F9,F10 | 7.113 | .008 | 1.000 | -.382 | -.120 |
| 7 | 2 | 16 | F8,F10 | 7.113 | .008 | 1.000 | .344 | .115 |
| 8 | 2 | 22 | F8,F12 | 6.676 | .010 | 1.000 | -.582 | -.459 |
| 9 | 2 | 16 | F14,F10 | 6.643 | .010 | 1.000 | .204 | .072 |
| 10 | 2 | 10 | D12,D9 | 6.505 | .011 | 1.000 | .185 | .355 |
| 11 | 2 | 20 | V3,F9 | 6.461 | .011 | 1.000 | .254 | .055 |
| 12 | 2 | 20 | V9,F13 | 6.105 | .013 | 1.000 | -.119 | -.032 |
| 13 | 2 | 20 | V18,F8 | 6.009 | .014 | 1.000 | .210 | .056 |
| 14 | 2 | 22 | F9,F13 | 5.989 | .014 | 1.000 | .280 | .098 |
| 15 | 2 | 12 | V1,F10 | 5.831 | .016 | 1.000 | -.182 | -.049 |
| 16 | 2 | 20 | V10,F15 | 5.701 | .017 | 1.000 | .163 | .044 |
| 17 | 2 | 12 | V15,F6 | 5.629 | .018 | 1.000 | -.203 | -.049 |
| 18 | 2 | 20 | V9,F15 | 5.509 | .019 | 1.000 | -.128 | -.035 |
| 19 | 2 | 20 | V10,F14 | 5.439 | .020 | 1.000 | .142 | .036 |

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|---|---|---|---|---|---|---|---|---|
| 20 | 2 | 22 | F15,F9 | 5.294 | .021 | 1.000 | .407 | .146 |
| 21 | 2 | 22 | F15,F8 | 5.294 | .021 | 1.000 | -.364 | -.139 |
| 22 | 2 | 10 | D15,D9 | 5.294 | .021 | 1.000 | .531 | .396 |
| 23 | 2 | 10 | D15,D8 | 5.294 | .021 | 1.000 | -.478 | -.356 |
| 24 | 2 | 20 | V3,F8 | 5.132 | .023 | 1.000 | .229 | .052 |
| 25 | 2 | 20 | V16,F14 | 5.003 | .025 | 1.000 | .200 | .055 |
| 26 | 2 | 20 | V1,F8 | 4.923 | .026 | 1.000 | -.165 | -.045 |
| 27 | 2 | 20 | V9,F14 | 4.833 | .028 | 1.000 | -.107 | -.027 |
| 28 | 2 | 12 | V10,F11 | 4.771 | .029 | 1.000 | .296 | .094 |
| 29 | 2 | 12 | V3,F11 | 4.680 | .031 | 1.000 | .366 | .112 |
| 30 | 2 | 20 | V2,F9 | 4.630 | .031 | 1.000 | -.141 | -.041 |
| 31 | 2 | 12 | V4,F11 | 4.545 | .033 | 1.000 | .322 | .107 |
| 32 | 2 | 10 | D14,D9 | 4.530 | .033 | 1.000 | -.307 | -.461 |
| 33 | 2 | 12 | V1,F11 | 4.515 | .034 | 1.000 | -.269 | -.098 |
| 34 | 2 | 20 | V10,F12 | 4.511 | .034 | 1.000 | .285 | .159 |
| 35 | 2 | 20 | V4,F9 | 4.468 | .035 | 1.000 | .188 | .044 |
| 36 | 2 | 12 | V9,F7 | 4.379 | .036 | 1.000 | .124 | .037 |
| 37 | 2 | 10 | D12,D8 | 4.289 | .038 | 1.000 | -.137 | -.262 |
| 38 | 2 | 12 | V7,F11 | 4.170 | .041 | 1.000 | .443 | .140 |
| 39 | 2 | 20 | V16,F12 | 4.143 | .042 | 1.000 | .393 | .241 |
| 40 | 2 | 12 | V8,F7 | 4.032 | .045 | 1.000 | -.128 | -.039 |
| 41 | 2 | 12 | V22,F6 | 3.990 | .046 | 1.000 | -.119 | -.035 |
| 42 | 2 | 22 | F8,F13 | 3.972 | .046 | 1.000 | -.207 | -.077 |
| 43 | 2 | 12 | V25,F7 | 3.851 | .050 | 1.000 | -.127 | -.063 |
| 44 | 2 | 12 | V12,F10 | 3.847 | .050 | 1.000 | -.155 | -.039 |
| 45 | 2 | 20 | V1,F14 | 3.817 | .051 | 1.000 | -.151 | -.043 |
| 46 | 2 | 12 | V3,F16 | 3.813 | .051 | 1.000 | .500 | .325 |
| 47 | 2 | 10 | D13,D9 | 3.726 | .054 | 1.000 | .272 | .259 |
| 48 | 2 | 12 | V12,F6 | 3.675 | .055 | 1.000 | .142 | .035 |

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|---|---|---|---|---|---|---|---|---|
| 49 | 2 | 12 | V20,F16 | 3.673 | .055 | 1.000 | -.202 | -.312 |
| 50 | 2 | 20 | V16,F15 | 3.672 | .055 | 1.000 | .193 | .057 |
| 51 | 2 | 20 | V20,F8 | 3.647 | .056 | 1.000 | .079 | .043 |
| 52 | 2 | 12 | V18,F6 | 3.636 | .057 | 1.000 | .158 | .041 |
| 53 | 2 | 20 | V25,F13 | 3.581 | .058 | 1.000 | .186 | .082 |
| 54 | 2 | 12 | V25,F11 | 3.550 | .060 | 1.000 | -.165 | -.088 |
| 55 | 2 | 20 | V10,F9 | 3.497 | .061 | 1.000 | .115 | .026 |
| 56 | 2 | 12 | V13,F16 | 3.483 | .062 | 1.000 | .336 | .233 |
| 57 | 2 | 20 | V11,F8 | 3.449 | .063 | 1.000 | -.163 | -.042 |
| 58 | 2 | 22 | F9,F15 | 3.363 | .067 | 1.000 | .285 | .102 |
| 59 | 2 | 22 | F8,F15 | 3.363 | .067 | 1.000 | -.256 | -.098 |
| 60 | 2 | 12 | V9,F11 | 3.182 | .074 | 1.000 | -.200 | -.064 |
| 61 | 2 | 12 | V17,F17 | 3.105 | .078 | 1.000 | -.588 | -.717 |
| 62 | 2 | 12 | V9,F6 | 3.049 | .081 | 1.000 | -.078 | -.018 |
| 63 | 2 | 12 | V4,F10 | 3.033 | .082 | 1.000 | .158 | .039 |
| 64 | 2 | 20 | V10,F13 | 2.911 | .088 | 1.000 | .103 | .027 |
| 65 | 2 | 20 | V9,F9 | 2.885 | .089 | 1.000 | -.086 | -.019 |
| 66 | 2 | 20 | V18,F12 | 2.852 | .091 | 1.000 | -.349 | -.218 |
| 67 | 2 | 20 | V4,F8 | 2.806 | .094 | 1.000 | .151 | .038 |
| 68 | 2 | 20 | V4,F14 | 2.786 | .095 | 1.000 | .156 | .041 |
| 69 | 2 | 22 | F12,F8 | 2.737 | .098 | 1.000 | -.055 | -.044 |
| 70 | 2 | 12 | V23,F10 | 2.687 | .101 | 1.000 | -.087 | -.030 |
| 71 | 2 | 12 | V26,F7 | 2.621 | .105 | 1.000 | .118 | .058 |
| 72 | 2 | 16 | F13,F10 | 2.590 | .108 | 1.000 | -.116 | -.043 |
| 73 | 2 | 20 | V9,F12 | 2.529 | .112 | 1.000 | -.169 | -.096 |
| 74 | 2 | 20 | V22,F9 | 2.502 | .114 | 1.000 | -.102 | -.029 |
| 75 | 2 | 12 | V7,F16 | 2.441 | .118 | 1.000 | .350 | .235 |
| 76 | 2 | 12 | V12,F17 | 2.439 | .118 | 1.000 | .472 | .585 |
| 77 | 2 | 20 | V11,F12 | 2.366 | .124 | 1.000 | .285 | .172 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 78 | 2 | 20 | V18,F14 | 2.364 | .124 | 1.000 | -.146 | -.041 |
| 79 | 2 | 16 | F14,F16 | 2.295 | .130 | 1.000 | .252 | .255 |
| 80 | 2 | 12 | V11,F11 | 2.237 | .135 | 1.000 | -.323 | -.110 |
| 81 | 2 | 12 | V15,F7 | 2.202 | .138 | 1.000 | .176 | .054 |
| 82 | 2 | 16 | F8,F7 | 2.162 | .141 | 1.000 | .187 | .078 |
| 83 | 2 | 16 | F9,F7 | 2.162 | .141 | 1.000 | -.207 | -.082 |
| 84 | 2 | 12 | V11,F17 | 2.162 | .141 | 1.000 | -.469 | -.583 |
| 85 | 2 | 12 | V25,F10 | 2.150 | .143 | 1.000 | -.080 | -.031 |
| 86 | 2 | 20 | V6,F9 | 2.134 | .144 | 1.000 | -.255 | -.059 |
| 87 | 2 | 12 | V10,F10 | 2.118 | .146 | 1.000 | .085 | .020 |
| 88 | 2 | 20 | V18,F15 | 2.100 | .147 | 1.000 | -.155 | -.047 |
| 89 | 2 | 20 | V26,F9 | 2.095 | .148 | 1.000 | .080 | .030 |
| 90 | 2 | 12 | V14,F11 | 2.040 | .153 | 1.000 | .326 | .109 |
| 91 | 2 | 20 | V23,F12 | 2.006 | .157 | 1.000 | .343 | .277 |
| 92 | 2 | 12 | V2,F17 | 1.995 | .158 | 1.000 | -.400 | -.595 |
| 93 | 2 | 20 | V32,F12 | 1.991 | .158 | 1.000 | -.173 | -.387 |
| 94 | 2 | 12 | V7,F6 | 1.934 | .164 | 1.000 | .126 | .029 |
| 95 | 2 | 20 | V14,F8 | 1.920 | .166 | 1.000 | .130 | .032 |
| 96 | 2 | 20 | V1,F15 | 1.863 | .172 | 1.000 | -.116 | -.036 |
| 97 | 2 | 20 | V14,F13 | 1.816 | .178 | 1.000 | .121 | .033 |
| 98 | 2 | 12 | V1,F7 | 1.815 | .178 | 1.000 | -.128 | -.043 |
| 99 | 2 | 12 | V11,F6 | 1.813 | .178 | 1.000 | -.105 | -.026 |
| 100 | 2 | 16 | F12,F16 | 1.806 | .179 | 1.000 | -.108 | -.242 |
| 101 | 2 | 22 | F13,F9 | 1.780 | .182 | 1.000 | .089 | .031 |
| 102 | 2 | 16 | F12,F10 | 1.758 | .185 | 1.000 | -.048 | -.038 |
| 103 | 2 | 20 | V4,F15 | 1.725 | .189 | 1.000 | .135 | .038 |
| 104 | 2 | 12 | V21,F6 | 1.677 | .195 | 1.000 | .084 | .024 |
| 105 | 2 | 12 | V8,F17 | 1.654 | .198 | 1.000 | .257 | .303 |
| 106 | 2 | 20 | V14,F14 | 1.631 | .202 | 1.000 | .116 | .031 |

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|---|---|---|---|---|---|---|---|---|
| 107 | 2 | 12 | V21,F17 | 1.614 | .204 | 1.000 | .363 | .514 |
| 108 | 2 | 20 | V20,F14 | 1.603 | .206 | 1.000 | .108 | .062 |
| 109 | 2 | 10 | D13,D8 | 1.599 | .206 | 1.000 | -.162 | -.154 |
| 110 | 2 | 22 | F14,F9 | 1.593 | .207 | 1.000 | -.091 | -.030 |
| 111 | 2 | 20 | V26,F13 | 1.549 | .213 | 1.000 | -.116 | -.051 |
| 112 | 2 | 20 | V21,F13 | 1.523 | .217 | 1.000 | -.231 | -.074 |
| 113 | 2 | 12 | V21,F16 | 1.505 | .220 | 1.000 | .206 | .170 |
| 114 | 2 | 22 | F12,F9 | 1.504 | .220 | 1.000 | .041 | .030 |
| 115 | 2 | 22 | F8,F14 | 1.449 | .229 | 1.000 | -.144 | -.051 |
| 116 | 2 | 12 | V21,F11 | 1.424 | .233 | 1.000 | .151 | .059 |
| 117 | 2 | 20 | V7,F9 | 1.414 | .234 | 1.000 | .118 | .026 |
| 118 | 2 | 20 | V16,F9 | 1.412 | .235 | 1.000 | -.095 | -.023 |
| 119 | 2 | 10 | D14,D8 | 1.389 | .239 | 1.000 | .155 | .232 |
| 120 | 2 | 20 | V14,F15 | 1.382 | .240 | 1.000 | .120 | .034 |
| 121 | 2 | 12 | V1,F16 | 1.380 | .240 | 1.000 | -.220 | -.170 |
| 122 | 2 | 16 | F9,F16 | 1.364 | .243 | 1.000 | -.279 | -.250 |
| 123 | 2 | 16 | F8,F16 | 1.364 | .243 | 1.000 | .251 | .239 |
| 124 | 2 | 12 | V10,F7 | 1.338 | .247 | 1.000 | -.087 | -.026 |
| 125 | 2 | 16 | F14,F7 | 1.327 | .249 | 1.000 | .099 | .044 |
| 126 | 2 | 20 | V2,F8 | 1.294 | .255 | 1.000 | -.075 | -.023 |
| 127 | 2 | 12 | V3,F17 | 1.294 | .255 | 1.000 | .499 | .554 |
| 128 | 2 | 12 | V10,F6 | 1.273 | .259 | 1.000 | .063 | .015 |
| 129 | 2 | 20 | V32,F14 | 1.254 | .263 | 1.000 | .174 | .176 |
| 130 | 2 | 12 | V18,F11 | 1.233 | .267 | 1.000 | .174 | .062 |
| 131 | 2 | 16 | F13,F6 | 1.144 | .285 | 1.000 | .065 | .023 |
| 132 | 2 | 20 | V5,F9 | 1.127 | .288 | 1.000 | .158 | .036 |
| 133 | 2 | 12 | V2,F11 | 1.117 | .291 | 1.000 | -.119 | -.048 |
| 134 | 2 | 20 | V8,F12 | 1.108 | .292 | 1.000 | -.120 | -.069 |
| 135 | 2 | 20 | V6,F12 | 1.099 | .295 | 1.000 | -.327 | -.189 |

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|---|---|---|---|---|---|---|---|---|
| 136 | 2 | 20 | V19,F8 | 1.081 | .299 | 1.000 | -.084 | -.022 |
| 137 | 2 | 10 | D15,D14 | 1.080 | .299 | 1.000 | -.291 | -.426 |
| 138 | 2 | 10 | D13,D12 | 1.080 | .299 | 1.000 | .092 | .219 |
| 139 | 2 | 22 | F13,F12 | 1.080 | .299 | 1.000 | .440 | .384 |
| 140 | 2 | 22 | F12,F13 | 1.080 | .299 | 1.000 | .109 | .095 |
| 141 | 2 | 22 | F15,F14 | 1.080 | .299 | 1.000 | -.856 | -.347 |
| 142 | 2 | 20 | V6,F13 | 1.079 | .299 | 1.000 | -.149 | -.040 |
| 143 | 2 | 12 | V3,F10 | 1.069 | .301 | 1.000 | .106 | .024 |
| 144 | 2 | 20 | V18,F13 | 1.066 | .302 | 1.000 | -.097 | -.028 |
| 145 | 2 | 16 | F14,F6 | 1.047 | .306 | 1.000 | -.067 | -.023 |
| 146 | 2 | 12 | V7,F10 | 1.032 | .310 | 1.000 | .096 | .023 |
| 147 | 2 | 12 | V18,F7 | 1.031 | .310 | 1.000 | -.117 | -.039 |
| 148 | 2 | 12 | V24,F6 | 1.026 | .311 | 1.000 | .055 | .016 |
| 149 | 2 | 20 | V24,F9 | 1.025 | .311 | 1.000 | .059 | .017 |
| 150 | 2 | 12 | V20,F11 | 1.011 | .315 | 1.000 | .070 | .051 |
| 151 | 2 | 20 | V20,F15 | 1.005 | .316 | 1.000 | .111 | .068 |
| 152 | 2 | 12 | V26,F10 | .983 | .322 | 1.000 | .059 | .023 |
| 153 | 2 | 20 | V20,F9 | .975 | .323 | 1.000 | .041 | .021 |
| 154 | 2 | 12 | V22,F17 | .948 | .330 | 1.000 | -.254 | -.372 |
| 155 | 2 | 20 | V5,F12 | .920 | .338 | 1.000 | .242 | .138 |
| 156 | 2 | 12 | V14,F17 | .919 | .338 | 1.000 | -.328 | -.397 |
| 157 | 2 | 22 | F14,F8 | .896 | .344 | 1.000 | .067 | .024 |
| 158 | 2 | 12 | V12,F7 | .880 | .348 | 1.000 | -.092 | -.029 |
| 159 | 2 | 20 | V26,F15 | .868 | .351 | 1.000 | -.143 | -.065 |
| 160 | 2 | 20 | V19,F12 | .862 | .353 | 1.000 | -.182 | -.110 |
| 161 | 2 | 20 | V11,F13 | .854 | .355 | 1.000 | .078 | .022 |
| 162 | 2 | 16 | F9,F17 | .852 | .356 | 1.000 | -.373 | -.572 |
| 163 | 2 | 16 | F8,F17 | .852 | .356 | 1.000 | .336 | .547 |
| 164 | 2 | 12 | V23,F16 | .847 | .357 | 1.000 | -.110 | -.107 |

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        165    2  12        V14,F7        .842       .359
1.000      .101      .031
        166    2  12        V24,F11       .841       .359
1.000      .095      .038
        167    2  20        V26,F14       .836       .361      1.000      -
.108     -.045
        168    2  12         V4,F16       .822       .365
1.000      .207      .147
        169    2  20        V23,F8        .821       .365      1.000      -
.045     -.015
        170    2  12        V26,F11       .820       .365
1.000      .085      .045
        171    2  22         F9,F14       .814       .367
1.000      .120      .040
        172    2  12         V6,F11       .803       .370      1.000      -
.341     -.112
        173    2  12         V5,F11       .803       .370
1.000      .240      .078
        174    2  20         V5,F13       .787       .375
1.000      .101      .027
        175    2  12        V22,F11       .771       .380      1.000      -
.103     -.042
        176    2  12         V2,F16       .750       .386      1.000      -
.143     -.125
        177    2  20        V24,F12       .749       .387      1.000      -
.237     -.168
        178    2  20        V12,F12       .740       .390
1.000      .152      .091
        179    2  20        V29,F8        .732       .392
1.000      .026      .043
        180    2  20        V29,F9        .732       .392      1.000      -
.029     -.045
        181    2  20        V29,F12       .719       .396
1.000      .061      .234
        182    2  20        V11,F15       .708       .400
1.000      .081      .023
        183    2  16         F9,F6        .666       .414
1.000      .094      .029
        184    2  16         F8,F6        .666       .414      1.000      -
.085     -.028
        185    2  20         V1,F9        .657       .418      1.000      -
.060     -.015
        186    2  20        V19,F9        .644       .422
1.000      .065      .016
        187    2  20        V22,F13       .643       .423
1.000      .150      .050
        188    2  12        V26,F6        .626       .429      1.000      -
.043     -.017
        189    2  12         V8,F11       .607       .436      1.000      -
.092     -.030
        190    2  12        V16,F17       .588       .443
1.000      .255      .322
        191    2  22        F13,F8        .534       .465      1.000      -
.048     -.018
        192    2  12        V19,F17       .533       .465
1.000      .246      .307
        193    2  12        V11,F7        .532       .466      1.000      -
.075     -.024
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|---|---|---|---|---|---|---|---|---|
| 194 | 2 | 12 | V15,F17 | .525 | .469 | 1.000 | .265 | .320 |
| 195 | 2 | 16 | F12,F7 | .524 | .469 | 1.000 | -.030 | -.029 |
| 196 | 2 | 20 | V25,F9 | .520 | .471 | 1.000 | -.036 | -.014 |
| 197 | 2 | 12 | V25,F6 | .518 | .472 | 1.000 | .035 | .013 |
| 198 | 2 | 12 | V9,F17 | .505 | .477 | 1.000 | -.132 | -.153 |
| 199 | 2 | 12 | V2,F7 | .486 | .486 | 1.000 | .059 | .022 |
| 200 | 2 | 20 | V12,F8 | .461 | .497 | 1.000 | .058 | .015 |
| 201 | 2 | 20 | V12,F14 | .454 | .501 | 1.000 | -.055 | -.015 |
| 202 | 2 | 20 | V17,F9 | .453 | .501 | 1.000 | -.054 | -.013 |
| 203 | 2 | 12 | V23,F11 | .447 | .504 | 1.000 | -.059 | -.027 |
| 204 | 2 | 20 | V6,F15 | .444 | .505 | 1.000 | -.121 | -.034 |
| 205 | 2 | 20 | V5,F15 | .444 | .505 | 1.000 | .085 | .023 |
| 206 | 2 | 10 | D14,D13 | .430 | .512 | 1.000 | -.175 | -.327 |
| 207 | 2 | 10 | D15,D12 | .430 | .512 | 1.000 | .079 | .148 |
| 208 | 2 | 22 | F14,F13 | .430 | .512 | 1.000 | -.208 | -.082 |
| 209 | 2 | 22 | F15,F12 | .430 | .512 | 1.000 | .380 | .341 |
| 210 | 2 | 22 | F13,F14 | .430 | .512 | 1.000 | -.515 | -.203 |
| 211 | 2 | 16 | F13,F7 | .427 | .513 | 1.000 | -.053 | -.024 |
| 212 | 2 | 12 | V20,F10 | .402 | .526 | 1.000 | -.028 | -.015 |
| 213 | 2 | 12 | V6,F16 | .394 | .530 | 1.000 | -.244 | -.170 |
| 214 | 2 | 12 | V5,F16 | .394 | .530 | 1.000 | .172 | .118 |
| 215 | 2 | 12 | V13,F10 | .382 | .537 | 1.000 | .050 | .012 |
| 216 | 2 | 20 | V11,F14 | .370 | .543 | 1.000 | .052 | .014 |
| 217 | 2 | 12 | V16,F7 | .361 | .548 | 1.000 | -.065 | -.021 |
| 218 | 2 | 20 | V21,F9 | .350 | .554 | 1.000 | .041 | .011 |
| 219 | 2 | 12 | V26,F16 | .348 | .555 | 1.000 | .084 | .095 |
| 220 | 2 | 12 | V10,F16 | .335 | .563 | 1.000 | .080 | .054 |
| 221 | 2 | 20 | V4,F12 | .333 | .564 | 1.000 | .121 | .071 |
| 222 | 2 | 12 | V24,F16 | .328 | .567 | 1.000 | .081 | .069 |

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        223    2  20        V6,F8         .318       .573
1.000      .093       .023
        224    2  12       V21,F7         .317       .574
1.000      .049       .018
        225    2  20       V16,F13        .310       .578
1.000      .049       .014
        226    2  12       V16,F6         .305       .581
1.000      .043       .011
        227    2  20        V8,F13        .302       .583
1.000      .028       .008
        228    2  12        V6,F6         .300       .584      1.000      -
.081     -.019
        229    2  12        V5,F6         .300       .584
1.000      .057       .013
        230    2  20        V2,F14        .299       .584
1.000      .037       .012
        231    2  12       V20,F17        .286       .593
1.000      .096       .255
        232    2  12       V11,F10        .281       .596      1.000      -
.044     -.011
        233    2  16       F13,F16        .273       .601      1.000      -
.082     -.086
        234    2  20       V29,F13        .269       .604      1.000      -
.018     -.032
        235    2  12       V22,F7         .261       .610
1.000      .040       .015
        236    2  16       F12,F11        .251       .616      1.000      -
.030     -.032
        237    2  12       V24,F10        .241       .623
1.000      .031       .009
        238    2  22       F12,F14        .241       .623      1.000      -
.161     -.135
        239    2  22       F15,F13        .241       .623
1.000      .144       .061
        240    2  10       D14,D12        .241       .623      1.000      -
.055     -.206
        241    2  22       F14,F12        .241       .623      1.000      -
.263     -.220
        242    2  10       D15,D13        .241       .623
1.000      .121       .113
        243    2  12       V14,F10        .227       .634
1.000      .042       .010
        244    2  20       V23,F14        .225       .635      1.000      -
.171     -.062
        245    2  12       V26,F17        .222       .637      1.000      -
.115     -.221
        246    2  20       V17,F8         .206       .650
1.000      .037       .009
        247    2  12        V4,F7         .205       .651
1.000      .052       .016
        248    2  20       V25,F14        .204       .651      1.000      -
.063     -.027
        249    2  12       V14,F6         .204       .652      1.000      -
.037     -.009
        250    2  12       V15,F11        .204       .652      1.000      -
.073     -.024
        251    2  12        V9,F10        .195       .659      1.000      -
.021     -.005
```

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 252 | 2 | 12 | V9,F16 | .193 | .660 | 1.000 | -.048 | -.032 |
| 253 | 2 | 20 | V17,F13 | .193 | .660 | 1.000 | -.039 | -.011 |
| 254 | 2 | 20 | V21,F8 | .191 | .662 | 1.000 | .031 | .009 |
| 255 | 2 | 20 | V5,F14 | .191 | .662 | 1.000 | .050 | .013 |
| 256 | 2 | 20 | V19,F15 | .190 | .663 | 1.000 | -.044 | -.013 |
| 257 | 2 | 20 | V17,F15 | .188 | .665 | 1.000 | -.044 | -.013 |
| 258 | 2 | 20 | V22,F8 | .185 | .667 | 1.000 | .028 | .008 |
| 259 | 2 | 20 | V17,F12 | .184 | .668 | 1.000 | -.083 | -.049 |
| 260 | 2 | 12 | V3,F7 | .183 | .669 | 1.000 | .056 | .016 |
| 261 | 2 | 16 | F13,F17 | .165 | .684 | 1.000 | -.108 | -.195 |
| 262 | 2 | 20 | V13,F14 | .165 | .684 | 1.000 | -.034 | -.009 |
| 263 | 2 | 20 | V2,F12 | .161 | .689 | 1.000 | -.061 | -.044 |
| 264 | 2 | 20 | V24,F8 | .155 | .693 | 1.000 | .023 | .007 |
| 265 | 2 | 12 | V4,F17 | .144 | .704 | 1.000 | .148 | .180 |
| 266 | 2 | 20 | V17,F14 | .140 | .708 | 1.000 | -.034 | -.009 |
| 267 | 2 | 12 | V19,F16 | .136 | .712 | 1.000 | -.075 | -.055 |
| 268 | 2 | 20 | V12,F15 | .135 | .713 | 1.000 | -.034 | -.010 |
| 269 | 2 | 12 | V8,F10 | .132 | .716 | 1.000 | -.018 | -.004 |
| 270 | 2 | 12 | V2,F10 | .122 | .727 | 1.000 | .023 | .007 |
| 271 | 2 | 12 | V1,F17 | .120 | .729 | 1.000 | .111 | .147 |
| 272 | 2 | 20 | V13,F15 | .116 | .734 | 1.000 | -.032 | -.009 |
| 273 | 2 | 20 | V19,F14 | .112 | .738 | 1.000 | -.030 | -.008 |
| 274 | 2 | 12 | V14,F16 | .111 | .739 | 1.000 | -.067 | -.047 |
| 275 | 2 | 20 | V32,F8 | .110 | .740 | 1.000 | .017 | .016 |
| 276 | 2 | 20 | V32,F9 | .110 | .740 | 1.000 | -.019 | -.017 |
| 277 | 2 | 12 | V25,F16 | .106 | .745 | 1.000 | -.041 | -.046 |
| 278 | 2 | 12 | V18,F17 | .103 | .748 | 1.000 | -.114 | -.147 |
| 279 | 2 | 12 | V19,F11 | .101 | .751 | 1.000 | -.048 | -.016 |
| 280 | 2 | 20 | V7,F14 | .101 | .751 | 1.000 | .031 | .008 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 281 | 2 | 12 | V6,F17 | .099 | .753 | 1.000 | -.221 | -.263 |
| 282 | 2 | 12 | V5,F17 | .099 | .753 | 1.000 | .155 | .183 |
| 283 | 2 | 20 | V26,F8 | .092 | .762 | 1.000 | .017 | .007 |
| 284 | 2 | 20 | V13,F12 | .083 | .774 | 1.000 | -.051 | -.030 |
| 285 | 2 | 16 | F12,F17 | .082 | .775 | 1.000 | .039 | .151 |
| 286 | 2 | 12 | V22,F10 | .081 | .776 | 1.000 | -.020 | -.006 |
| 287 | 2 | 20 | V15,F12 | .080 | .777 | 1.000 | .060 | .035 |
| 288 | 2 | 20 | V18,F9 | .072 | .788 | 1.000 | .023 | .006 |
| 289 | 2 | 20 | V20,F13 | .070 | .792 | 1.000 | -.018 | -.011 |
| 290 | 2 | 20 | V6,F14 | .069 | .792 | 1.000 | -.042 | -.011 |
| 291 | 2 | 12 | V23,F7 | .069 | .792 | 1.000 | -.016 | -.007 |
| 292 | 2 | 12 | V24,F7 | .068 | .795 | 1.000 | -.019 | -.007 |
| 293 | 2 | 12 | V22,F16 | .067 | .796 | 1.000 | .040 | .034 |
| 294 | 2 | 20 | V15,F14 | .065 | .798 | 1.000 | .025 | .007 |
| 295 | 2 | 12 | V19,F6 | .065 | .799 | 1.000 | -.020 | -.005 |
| 296 | 2 | 20 | V1,F13 | .063 | .802 | 1.000 | .019 | .006 |
| 297 | 2 | 20 | V16,F8 | .061 | .805 | 1.000 | -.020 | -.005 |
| 298 | 2 | 12 | V16,F11 | .061 | .806 | 1.000 | -.036 | -.013 |
| 299 | 2 | 20 | V3,F12 | .060 | .806 | 1.000 | .058 | .031 |
| 300 | 2 | 20 | V15,F9 | .059 | .807 | 1.000 | -.022 | -.005 |
| 301 | 2 | 20 | V7,F15 | .057 | .811 | 1.000 | .026 | .007 |
| 302 | 2 | 12 | V25,F17 | .056 | .814 | 1.000 | .051 | .098 |
| 303 | 2 | 16 | F13,F11 | .055 | .814 | 1.000 | .029 | .014 |
| 304 | 2 | 12 | V17,F6 | .055 | .815 | 1.000 | .018 | .004 |
| 305 | 2 | 20 | V2,F15 | .052 | .820 | 1.000 | .017 | .006 |
| 306 | 2 | 20 | V8,F9 | .051 | .822 | 1.000 | -.012 | -.003 |
| 307 | 2 | 20 | V3,F13 | .046 | .830 | 1.000 | .023 | .006 |
| 308 | 2 | 16 | F14,F11 | .043 | .836 | 1.000 | .028 | .013 |
| 309 | 2 | 20 | V15,F15 | .042 | .838 | 1.000 | .023 | .006 |

310 2 20 V19,F13 .042 .838 1.000 -
.018 -.005
311 2 12 V24,F17 .042 .838 1.000 -
.049 -.072
312 2 12 V17,F16 .041 .840
1.000 .041 .029
313 2 20 V29,F14 .041 .840 1.000 -
.018 -.032
314 2 12 V17,F7 .039 .843
1.000 .021 .007
315 2 20 V3,F15 .038 .846
1.000 .022 .006
316 2 20 V24,F14 .032 .858
1.000 .072 .023
317 2 12 V13,F6 .030 .863
1.000 .013 .003
318 2 12 V10,F17 .029 .864 1.000 -
.040 -.047
319 2 20 V13,F13 .029 .865 1.000 -
.014 -.004
320 2 20 V12,F13 .026 .871 1.000 -
.013 -.004
321 2 20 V2,F13 .025 .874
1.000 .011 .004
322 2 20 V22,F12 .025 .874 1.000 -
.056 -.040
323 2 20 V21,F12 .025 .875 1.000 -
.056 -.038
324 2 20 V13,F8 .023 .880 1.000 -
.013 -.003
325 2 12 V8,F6 .019 .890
1.000 .007 .002
326 2 16 F14,F17 .019 .890
1.000 .039 .068
327 2 12 V13,F11 .018 .892
1.000 .029 .010
328 2 12 V13,F7 .018 .893 1.000 -
.013 -.004
329 2 12 V20,F7 .018 .893
1.000 .007 .005
330 2 12 V8,F16 .018 .893 1.000 -
.016 -.011
331 2 12 V16,F16 .017 .897
1.000 .026 .019
332 2 12 V23,F17 .016 .899 1.000 -
.026 -.043
333 2 20 V1,F12 .015 .901 1.000 -
.021 -.014
334 2 12 V7,F17 .013 .910
1.000 .043 .050
335 2 12 V23,F6 .012 .914 1.000 -
.005 -.002
336 2 20 V8,F15 .011 .918 1.000 -
.006 -.002
337 2 12 V19,F7 .010 .921 1.000 -
.011 -.003
338 2 12 V13,F17 .008 .928 1.000 -
.028 -.033

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 339 | 2 | 20 | V3,F14 | .007 | .932 | 1.000 | -.009 | -.002 |
| 340 | 2 | 12 | V15,F16 | .007 | .933 | 1.000 | .019 | .013 |
| 341 | 2 | 16 | F12,F6 | .007 | .934 | 1.000 | .003 | .002 |
| 342 | 2 | 12 | V20,F6 | .006 | .937 | 1.000 | -.003 | -.002 |
| 343 | 2 | 20 | V23,F9 | .005 | .945 | 1.000 | .003 | .001 |
| 344 | 2 | 20 | V5,F8 | .004 | .947 | 1.000 | .010 | .002 |
| 345 | 2 | 20 | V8,F14 | .004 | .949 | 1.000 | -.003 | -.001 |
| 346 | 2 | 12 | V18,F16 | .004 | .950 | 1.000 | -.013 | -.010 |
| 347 | 2 | 20 | V25,F15 | .004 | .952 | 1.000 | -.011 | -.005 |
| 348 | 2 | 20 | V7,F12 | .004 | .953 | 1.000 | .013 | .007 |
| 349 | 2 | 20 | V15,F13 | .003 | .956 | 1.000 | .005 | .001 |
| 350 | 2 | 20 | V4,F13 | .003 | .956 | 1.000 | -.005 | -.001 |
| 351 | 2 | 12 | V17,F11 | .002 | .967 | 1.000 | .006 | .002 |
| 352 | 2 | 20 | V14,F12 | .001 | .975 | 1.000 | .006 | .004 |
| 353 | 2 | 12 | V12,F16 | .001 | .981 | 1.000 | -.004 | -.003 |
| 354 | 2 | 20 | V32,F13 | .000 | .983 | 1.000 | -.001 | -.001 |
| 355 | 2 | 12 | V12,F11 | .000 | .991 | 1.000 | .002 | .001 |
| 356 | 2 | 20 | V7,F13 | .000 | .997 | 1.000 | .000 | .000 |
| 357 | 2 | 12 | V5,F10 | .000 | .998 | 1.000 | .000 | .000 |
| 358 | 2 | 12 | V6,F10 | .000 | .998 | 1.000 | -.001 | .000 |
| 359 | 2 | 20 | V15,F8 | .000 | .999 | 1.000 | .000 | .000 |
| 360 | 2 | 12 | V32,F6 | .000 | 1.000 | 1.000 | .000 | .000 |
| 361 | 2 | 12 | V32,F10 | .000 | 1.000 | 1.000 | .000 | .000 |
| 362 | 2 | 12 | V32,F7 | .000 | 1.000 | 1.000 | .000 | .000 |
| 363 | 2 | 0 | V29,F17 | .000 | 1.000 | 1.000 | .000 | .000 |
| 364 | 2 | 12 | V29,F16 | .000 | 1.000 | 1.000 | .000 | .000 |
| 365 | 2 | 0 | V1,F6 | .000 | 1.000 | 1.000 | .000 | .000 |
| 366 | 2 | 12 | V29,F10 | .000 | 1.000 | 1.000 | .000 | .000 |
| 367 | 2 | 12 | V29,F11 | .000 | 1.000 | 1.000 | .000 | .000 |

```
        368    2   0       F14,F15        .000     1.000
1.000      .000      .000
        369    2  12       V29,F6         .000     1.000
1.000      .000      .000
        370    2  12       V29,F7         .000     1.000
1.000      .000      .000
        371    2  12       V32,F11        .000     1.000
1.000      .000      .000
        372    2   0       V32,F16        .000     1.000
1.000      .000      .000
        373    2   0       V11,F9         .000     1.000
1.000      .000      .000
        374    2   0       V20,F12        .000     1.000
1.000      .000      .000
        375    2   0       V15,F10        .000     1.000
1.000      .000      .000
        376    2   0       V21,F14        .000     1.000
1.000      .000      .000
        377    2  20       V21,F15        .000     1.000
1.000      .000      .000
        378    2   0        V7,F8         .000     1.000
1.000      .000      .000
        379    2  20       V22,F15        .000     1.000
1.000      .000      .000
        380    2   0       V23,F13        .000     1.000
1.000      .000      .000
        381    2  20       V23,F15        .000     1.000
1.000      .000      .000
        382    2  20       V24,F15        .000     1.000
1.000      .000      .000
        383    2  20       V29,F15        .000     1.000
1.000      .000      .000
        384    2   0        V5,F7         .000     1.000
1.000      .000      .000
        385    2  20       V32,F15        .000     1.000
1.000      .000      .000
        386    2  22        F8,F9         .000     1.000
1.000      .000      .000
        387    2  22        F9,F8         .000     1.000
1.000      .000      .000
        388    2   0        F8,F11        .000     1.000
1.000      .000      .000
        389    2  12       V32,F17        .000     1.000
1.000      .000      .000
        390    2  10        D9,D8         .000     1.000
1.000      .000      .000


      24-Jul-17      PAGE : 26  EQS     Licensee:
        TITLE:   master confirmatorio la 5 sobre la 6, 7, 10 y 11 y la 4
sob

        MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


        MULTIVARIATE LAGRANGE MULTIPLIER TEST BY SIMULTANEOUS PROCESS IN
STAGE  1

        PARAMETER SETS (SUBMATRICES) ACTIVE AT THIS STAGE ARE:
```

```
           PVV PFV PFF PDD GVV GVF GFV GFF BVF BFF


              CUMULATIVE MULTIVARIATE STATISTICS      UNIVARIATE
INCREMENT
              ----------------------------------      -------------------
-----------

HANCOCK'S

SEQUENTIAL
       STEP   PARAMETER   CHI-SQUARE  D.F.    PROB.   CHI-SQUARE   PROB.
D.F.   PROB.
       ----  -----------  ----------  ----    -----   ----------   -----
----   -----
          1      V25,F8        9.595     1     .002        9.595    .002
326   1.000
          2       V7,F7       18.582     2     .000        8.987    .003
325   1.000
          3       F9,F12      26.161     3     .000        7.579    .006
324   1.000
          4      V11,F16      33.585     4     .000        7.424    .006
323   1.000
          5      V21,F10      40.922     5     .000        7.337    .007
322   1.000
          6       V3,F9       47.652     6     .000        6.731    .009
321   1.000
          7       V4,F9       54.561     7     .000        6.909    .009
320   1.000
          8      V10,F15      60.952     8     .000        6.391    .011
319   1.000
          9       V9,F7       67.164     9     .000        6.211    .013
318   1.000
         10      V18,F8       72.911    10     .000        5.747    .017
317   1.000
         11      V16,F14      78.368    11     .000        5.457    .019
316   1.000
         12      V15,F6       83.173    12     .000        4.805    .028
315   1.000
         13      V12,F10      87.271    13     .000        4.099    .043
314   1.000


        LAGRANGIAN MULTIPLIER TEST REQUIRED   440271 WORDS OF MEMORY.
        PROGRAM ALLOCATES ******** WORDS.
      1
        Execution begins at 10:58:06
        Execution ends   at 10:58:13
        Elapsed time =       7.00 seconds
```

# ANEXO XVII

# MODELOS DE ECUACIONES ESTRUCTURALES

# TIC-FLEX-RDOS

```
1
   EQS, A STRUCTURAL EQUATION PROGRAM          MULTIVARIATE SOFTWARE, INC.
   COPYRIGHT BY P.M. BENTLER                   VERSION 6.1 (C) 1985 - 2005 (B85).


   PROGRAM CONTROL INFORMATION

/TITLE
 Your EQS 6 Model
/SPECIFICATIONS
VARIABLES= 80 ; CASES= 170 ;
DATA='C:\tesis1\ticflexrdoscontroltotal.ESS';
MATRIX=RAW;METHOD=ML,robust;
/LABELS
V1=P.1.1; V2=P.1.2; V3=P.1.3; V4=P.1.4; V5=P.1.5;
V6=P.1.6; V7=P.1.7; V8=P.1.8; V9=P.1.9; V10=P.1.10;
V11=P.1.11; V12=P.1.12; V13=P.1.13; V14=P.1.14; V15=P.1.15;
V16=P.1.16; V17=P.1.17; V18=P.2.1; V19=P.2.2; V20=P.2.3;
V21=P.2.4; V22=P.2.5; V23=P.2.6; V24=P.2.7; V25=P.2.8;
V26=P.2.9; V27=P.2.10; V28=P.2.11; V29=P.2.12; V30=P.2.13;
V31=P.2.14; V32=P.2.15; V33=P.3.1; V34=P.3.2; V35=P.3.3;
V36=P.4.1; V37=P.4.2; V38=P.4.3; V39=P.4.4; V40=P.4.5;
V41=P.4.6; V42=P.4.7; V43=P.4.8; V44=P.4.9; V45=P.4.10;
V46=P.4.11; V47=P.6.1; V48=P.6.2; V49=P.6.3; V50=P.6.4;
V51=P.6.5; V52=P.6.6; V53=P.6.7; V54=P.6.8; V55=P.6.9;
V56=P.6.10; V57=P.9.1; V58=P.9.2; V59=P.9.3; V60=P.9.4;
V61=P.9.5; V62=P.9.6; V63=P.9.7; V64=P.9.8; V65=P.9.9;
V66=P.9.10; V67=P.9.11; V68=P.9.12; V69=P.9.13; V70=P.9.14;
V71=P.9.15; V72=P.9.16; V73=P.9.17;
V74=P.11.1; V75=ANTIGUED; V76=LOGANTIG; V77=RAIZANTI; V78=P.10.1;
V79=LOGTAMA; V80=RAIZTAMA;

/EQUATIONS
V1 =   1F1 + E1;
V2 =   *F1 + E2;
V3 =   *F1 + E3;
V5 =   F3 + E5;
V6 =   *F3 + E6;
V8 =   *F1 + E8;
V9 =   *F4 + E9;
V10 =   1F2 + E10;
V11 =   *F2 + E11;
V12 =   F4 + E12;
V16 =   *F2 + E16;
V17 =   *F2 + E17;
V19 =   1F6 + E19;
V20 =   *F6 + E20;
V21 =   *F6 + E21;
V23 =   *F6 + E23;
V33 =   1F7 + E33;
V35 =   *F7 + E35;
V36 =   1F8 + E36;
V37 =   *F8 + E37;
```

```
V38 =   *F8 + E38;
V39 =   *F8 + E39;
V42 =   1F9 + E42;
V43 =   *F9 + E43;
V44 =   *F9 + E44;
V45 =   *F9 + E45;

24-Jul-17      PAGE :  2  EQS     Licensee:
  TITLE:   Your EQS 6 Model

V47 =   1F10 + E47;
V48 =   *F10 + E48;
V49 =   *F10 + E49;
V50 =   *F10 + E50;
V51 =   *F10 + E51;
V59 =   *F12 + E59;
V65 =   1F14 + E65;
V66 =   *F14 + E66;
V68 =   1F13 + E68;
V69 =   *F13 + E69;
V70 =   1F12 + E70;
V71 =   *F12 + E71;
V76 =   F17 + E76;
V79 =   F16 + E79;
F1 =   F5 + D1;
F2 =   *F5 + D2;
F3 =   *F5 + D3;
F6 =   *F5 + D6;
F7 =   *F4 + *F5 + D7;
F8 =   1F11 + D8;
F9 =   *F11 + D9;
F10 =   *F4 + D10;
F11 =   *F5 + D11;
F12 =   1F15 + D12;
F13 =   *F15 + D13;
F14 =   *F15 + D14;
F15 =   *F6 + *F7 + *F10 + *F11 + *F16 + *F17 + D15;
/VARIANCES
 F4=*;
F5=*;
F16=*;
F17=*;
E1 = *;
 E2 = *;
 E3 = *;
 E5 = *;
 E6 = *;
 E8 = *;
 E9 = *;
 E10 = *;
 E11 = *;
 E12 = *;
 E16 = *;
 E17 = *;
 E19 = *;
 E20 = *;
 E21 = *;
 E23 = *;
 E33 = *;
```

```
E35 = *;
E36 = *;
E37 = *;
E38 = *;
E39 = *;
E42 = *;
E43 = *;
E44 = *;

24-Jul-17      PAGE :  3  EQS     Licensee:
 TITLE:   Your EQS 6 Model

E45 = *;
E47 = *;
E48 = *;
E49 = *;
E50 = *;
E51 = *;
E59 = *;
E65 = *;
E66 = *;
E68 = *;
E69 = *;
E70 = *;
E71 = *;
E76 = 0;
E79 = 0;
D1 = *;
D2 = *;
D3 = *;
D6 = *;
D7 = *;
D8 = *;
D9 = *;
D10 = *;
D11 = *;
D12 = *;
D13 = *;
D14 = *;
D15 = *;
/COVARIANCES
F4,F5=*;
F16,F4=*;
F16,F5=*;
F17,F4=*;
F17,F5=*;
F16,F17=*;
/PRINT
FIT=ALL;
TABLE=EQUATION;
/END


   148 RECORDS OF INPUT MODEL FILE WERE READ


 DATA IS READ FROM C:\tesis1\ticflexrdoscontroltotal.ESS
 THERE ARE  80 VARIABLES AND   170 CASES
```

IT IS A RAW DATA ESS FILE

24-Jul-17 PAGE : 4 EQS Licensee:
TITLE: Your EQS 6 Model

SAMPLE STATISTICS BASED ON COMPLETE CASES

UNIVARIATE STATISTICS
---------------------

| VARIABLE | P.1.1 | P.1.2 | P.1.3 | P.1.5 | P.1.6 |
|---|---|---|---|---|---|
| | V1 | V2 | V3 | V5 | V6 |
| MEAN | 3.6941 | 4.0059 | 3.4235 | 4.8765 | 4.4000 |
| SKEWNESS (G1) | -.1427 | -.3284 | -.0187 | -.8703 | -.5597 |
| KURTOSIS (G2) | -1.6839 | -1.4951 | -1.5302 | -.8141 | -1.3132 |
| STANDARD DEV. | 2.9694 | 2.7873 | 2.7126 | 2.6540 | 2.7914 |

| VARIABLE | P.1.8 | P.1.9 | P.1.10 | P.1.11 | P.1.12 |
|---|---|---|---|---|---|
| | V8 | V9 | V10 | V11 | V12 |
| MEAN | 2.1353 | 2.3647 | 4.7059 | 3.5059 | 2.3706 |
| SKEWNESS (G1) | .8348 | .6639 | -.7765 | -.0322 | .6738 |
| KURTOSIS (G2) | -.8715 | -1.0669 | -1.1465 | -1.6572 | -1.2320 |
| STANDARD DEV. | 2.5971 | 2.6147 | 2.8939 | 2.9053 | 2.8385 |

| VARIABLE | P.1.16 | P.1.17 | P.2.2 | P.2.3 | P.2.4 |
|---|---|---|---|---|---|
| | V16 | V17 | V19 | V20 | V21 |
| MEAN | 4.6235 | 4.6176 | 1.8765 | 1.4588 | 2.9471 |

```
           SKEWNESS (G1)      -.7038     -.6901     1.2422
1.5942        .4243
           KURTOSIS (G2)     -1.0836    -1.0056      .3913     1.6513    -
1.3650
           STANDARD DEV.      2.7217     2.6110     2.1295     1.8908
2.5309

           VARIABLE         P.2.6      P.3.1      P.3.3      P.4.1
P.4.2
                               V23        V33        V35        V36
V37
           MEAN                2.0882     2.2059     1.9000     2.7294
2.8235
           SKEWNESS (G1)      1.0549      .8539
1.1054        .4621       .2998
           KURTOSIS (G2)      -.2638     -.6331     -.1092    -1.1132    -
1.2121
           STANDARD DEV.      2.3150     2.3856     2.3626     2.4441
2.3818

           VARIABLE         P.4.3      P.4.4      P.4.7      P.4.8
P.4.9
                               V38        V39        V42        V43
V44
           MEAN                2.6882     2.6647     3.4059     4.0471
3.5353
           SKEWNESS (G1)       .4307      .4202      .1232     -.2498     -
.0173
           KURTOSIS (G2)     -1.1559    -1.1980    -1.1944    -1.1031    -
1.3026
           STANDARD DEV.      2.4185     2.4372     2.2624     2.2710
2.3663

           VARIABLE         P.4.10     P.6.1      P.6.2      P.6.3
P.6.4
                               V45        V47        V48        V49
V50
           MEAN                2.7706     2.8294     2.9235     2.5529
2.3765
           SKEWNESS
(G1)         .4803      .3455      .2227      .5477      .4525
```

```
        KURTOSIS (G2)     -1.0218    -1.0645    -1.0536     -.9088     -
.9277
        STANDARD DEV.      2.3180     2.3282     2.2241     2.3077
2.1810

        VARIABLE         P.6.5      P.9.3      P.9.9      P.9.10
P.9.12
                            V51        V59        V65        V66
V68
        MEAN               2.1118     6.1647     4.1824     4.5118
4.8235
        SKEWNESS (G1)        .8085    -1.6316     -.3570     -.5772     -
.5256
        KURTOSIS (G2)      -.5685     2.6761     -.7646     -.3762     -
.2772
        STANDARD DEV.      2.2544     1.0642     1.9901     1.9192
1.6900

        VARIABLE         P.9.13     P.9.14     P.9.15     LOGANTIG
LOGTAMA
                            V69        V70        V71        V76
V79
        MEAN               4.4235     5.8059     5.7588     1.2075
1.2278
        SKEWNESS (G1)      -.4133    -1.4572    -1.3098     -
.7551     .7711
        KURTOSIS (G2)      -.6250     2.0533     1.3013     1.3199
1.2529
        STANDARD DEV.      1.9269     1.4567
1.4618     .3556      .6087

                                MULTIVARIATE KURTOSIS
                                ---------------------

        MARDIA'S COEFFICIENT (G2,P) =    197.6423
        NORMALIZED ESTIMATE =             22.2282

                         ELLIPTICAL THEORY KURTOSIS ESTIMATES
                         ------------------------------------

        MARDIA-BASED KAPPA =       .1176 MEAN SCALED UNIVARIATE KURTOSIS
=     -.1874

        MARDIA-BASED KAPPA IS USED IN COMPUTATION.
KAPPA=            .1176
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        CASE NUMBERS WITH LARGEST CONTRIBUTION TO NORMALIZED
MULTIVARIATE KURTOSIS:
        ---------------------------------------------------------------------------
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        CASE NUMBER        21           61           63           85
150

        ESTIMATE       635.8837     357.6279     444.8294    1364.5695
666.6377


     24-Jul-17      PAGE :  5  EQS     Licensee:
       TITLE:   Your EQS 6 Model

       COVARIANCE  MATRIX TO BE ANALYZED:  40 VARIABLES (SELECTED FROM
80 VARIABLES)
       BASED ON   170 CASES.


                             P.1.1      P.1.2      P.1.3      P.1.5
P.1.6
                                V1         V2         V3         V5
V6
          P.1.1    V1         8.817
          P.1.2    V2         5.617      7.769
          P.1.3    V3         4.781      4.938      7.358
          P.1.5    V5         4.287      3.800      3.810      7.044
          P.1.6    V6         3.147      3.353      2.978      5.417
7.792
          P.1.8    V8         3.917      3.981      4.392      2.242
2.336
          P.1.9    V9         1.757      2.838      1.892       .957
1.717
          P.1.10   V10        3.389      3.451      3.741      3.247
2.006
          P.1.11   V11        3.327      3.399      3.441      3.282
3.004
          P.1.12   V12        3.558      3.838      3.611      2.863
3.040
          P.1.16   V16        3.269      3.576      3.657      3.308
2.595
          P.1.17   V17        2.823      3.061      3.305      3.621
2.822
          P.2.2    V19         .370       .385
1.017      .434       .073
          P.2.3
V20        .520       .725       .941       .453       .472
          P.2.4    V21         .635       .568       .691       .248
-.535
          P.2.6    V23        1.311      1.201      1.128       .484
-.053
          P.3.1    V33        -.682      -.196       .226     -1.199
-1.237
          P.3.3    V35         .111       .385       .214      -.669
-.676
```

P.4.1 V36 .544
1.303 .701 .073 .292
P.4.2 V37 1.295 1.758 1.430 .795
1.195
P.4.3 V38 1.170 1.771 1.074 .772
1.256
P.4.4 V39 1.394 1.653 1.107 .757
1.277
P.4.7 V42 .746 1.441
1.312 .151 .375
P.4.8 V43 1.352 2.183
1.773 .787 .863
P.4.9 V44 .745 1.423
1.275 .611 .560
P.4.10 V45 .977 1.463 1.334 .758
1.288
P.6.1 V47 1.782 1.989 2.161 1.174
1.134
P.6.2 V48 1.332 1.279 1.364 1.251
1.504
P.6.3 V49 2.217 1.932 2.244 2.223
2.269
P.6.4 V50 1.406 1.169 1.508 1.035
1.115
P.6.5 V51 2.188 2.124 2.006 1.606
1.570
P.9.3
V59 .092 .384 .249 .162 .336
P.9.9 V65 1.109 1.301
1.372 .348 .867
P.9.10
V66 .862 .843 .782 .531 .818
P.9.12
V68 .478 .463 .596 .191 .822
P.9.13 V69 .592 .873
1.021 .378 .936
P.9.14
V70 .183 .321 .905 .319 .244
P.9.15
V71 .210 .516 .618 .372 .458
LOGANTIG
V76 .319 .236 .180 .076 .001
LOGTAMA
V79 .772 .630 .512 .438 .409

P.1.8 P.1.9 P.1.10 P.1.11
P.1.12
V8 V9 V10 V11
V12
P.1.8 V8 6.745
P.1.9 V9 2.134 6.837
P.1.10 V10 2.016 1.179 8.375
P.1.11 V11 3.316 2.140 3.724 8.441
P.1.12 V12 3.772 3.704 2.956 3.770
8.057
P.1.16 V16 2.886 1.706 3.528 3.795
3.566

| | | | | | | |
|---|---|---|---|---|---|---|
| P.1.17 | V17 | 2.129 | 1.904 | 3.106 | 3.147 | 3.048 |
| P.2.2 | V19 | .875 | .359 | .301 | .755 | .715 |
| P.2.3 | V20 | 1.299 | 1.086 | .219 | .843 | 1.119 |
| P.2.4 | V21 | .806 | 1.079 | .475 | .145 | 1.428 |
| P.2.6 | V23 | 1.603 | 1.317 | .979 | 1.298 | 1.713 |
| P.3.1 | V33 | -.016 | .711 | -1.756 | -.324 | -.195 |
| P.3.3 | V35 | .203 | .806 | -1.024 | .069 | .173 |
| P.4.1 | V36 | 1.226 | 1.383 | .387 | 1.138 | 1.687 |
| P.4.2 | V37 | 1.793 | 1.538 | .829 | .954 | 2.249 |
| P.4.3 | V38 | 1.853 | 2.026 | .440 | 1.348 | 2.495 |
| P.4.4 | V39 | 1.933 | 2.076 | .422 | 1.543 | 2.232 |
| P.4.7 | V42 | 1.223 | .543 | .233 | 1.285 | 1.257 |
| P.4.8 | V43 | 1.390 | .782 | .493 | 1.739 | 1.456 |
| P.4.9 | V44 | 1.330 | 1.413 | -.155 | 1.325 | 1.493 |
| P.4.10 | V45 | 1.729 | 1.049 | .080 | 1.099 | 1.304 |
| P.6.1 | V47 | 2.059 | 2.145 | 1.056 | 1.998 | 2.614 |
| P.6.2 | V48 | 1.543 | 1.430 | 1.060 | 1.690 | 2.484 |
| P.6.3 | V49 | 2.605 | 2.347 | 1.004 | 2.452 | 3.285 |
| P.6.4 | V50 | 1.576 | 1.891 | .703 | 1.104 | 2.262 |
| P.6.5 | V51 | 1.878 | 1.995 | 1.370 | 1.955 | 2.615 |
| P.9.3 | V59 | .279 | .336 | .173 | .484 | .371 |
| P.9.9 | V65 | 1.585 | 1.631 | .427 | 1.014 | 1.689 |
| P.9.10 | V66 | 1.238 | .996 | .252 | .840 | 1.324 |
| P.9.12 | V68 | .770 | .479 | -.011 | .634 | .480 |
| P.9.13 | V69 | .954 | 1.064 | -.005 | .838 | .966 |
| P.9.14 | V70 | .867 | .077 | .629 | .726 | .321 |
| P.9.15 | V71 | .654 | .301 | -.125 | 1.004 | .605 |
| LOGANTIG | V76 | .015 | .144 | .201 | -.015 | .167 |
| LOGTAMA | V79 | .436 | .586 | .320 | .297 | .807 |

```
                              P.1.16     P.1.17     P.2.2      P.2.3
P.2.4
                                 V16        V17        V19        V20
V21
          P.1.16   V16          7.408
          P.1.17   V17          3.832      6.817
          P.2.2    V19          1.042       .787      4.535
          P.2.3    V20           .771       .833      3.051      3.575
          P.2.4    V21          1.199      1.364      2.804      2.356
6.405
          P.2.6    V23          1.075      1.016      2.561      2.462
3.667
          P.3.1    V33          -.591      -
.447       .375       .461       .573
          P.3.3    V35          -
.245       .068       .088       .395       .279
          P.4.1    V36           .578       .985      1.173      1.113
2.181
          P.4.2    V37           .620      1.021      1.292      1.123
1.979
          P.4.3    V38           .799      1.211      1.056      1.197
2.019
          P.4.4    V39           .636      1.019      1.219      1.285
2.290
          P.4.7    V42           .674       .908      1.210       .777
1.590
          P.4.8    V43           .888      1.503      1.674      1.304
2.221
          P.4.9    V44          1.138      1.466      1.410      1.067
2.573
          P.4.10   V45          1.026      1.498      1.185      1.029
1.402
          P.6.1    V47          2.012      1.627       .210       .546
1.109
          P.6.2    V48          1.805       .858       .848       .941
1.457
          P.6.3    V49          2.363      1.704       .950
1.159       .947
          P.6.4    V50          1.148       .813       .917      1.098
1.866
          P.6.5    V51          2.161      1.570       .754
1.108       .929
          P.9.3
V59         .352       .182       .228       .220       .234
          P.9.9    V65
1.110       .816       .549       .815       .584
          P.9.10
V66         .306       .712       .206       .592       .501
          P.9.12
V68         .359       .595       .724       .584       .707
          P.9.13   V69           .403
1.050       .893       .775       .762
          P.9.14
V70         .418       .245       .579       .397       .493
          P.9.15
V71         .737       .162       .260       .176       .419
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         LOGANTIG
V76       .138       .114       .082       .034       .124
         LOGTAMA
V79       .472       .430       .075       .081       .281


                              P.2.6      P.3.1      P.3.3      P.4.1
P.4.2
                                 V23        V33        V35        V36
V37
         P.2.6    V23          5.359
         P.3.1    V33          -.101      5.691
         P.3.3    V35           .488      2.731      5.582
         P.4.1    V36          1.710      1.802      1.996      5.974
         P.4.2    V37          1.743       .924      1.396      3.952
5.673
         P.4.3    V38          1.750      1.136      1.874      4.033
5.270
         P.4.4    V39          1.882      1.247      1.309      3.678
4.988
         P.4.7    V42          1.514       .815       .869      1.868
2.149
         P.4.8    V43          1.931       .913       .904      2.338
2.653
         P.4.9    V44          1.929      1.155      1.030      2.199
2.574
         P.4.10   V45          1.689       .888      1.220      2.263
2.669
         P.6.1    V47           .707      1.408      1.385      1.764
1.940
         P.6.2    V48          1.634       .590      1.122      1.896
2.022
         P.6.3    V49          1.448       .613      1.346      1.707
2.086
         P.6.4    V50          1.617       .620       .689      1.753
2.357
         P.6.5    V51          1.043       .835      1.141      1.764
1.913
         P.9.3    V59           .252      -
.028      .159      .429       .556
         P.9.9    V65          1.280       .175       .575      1.020
1.506
         P.9.10   V66           .848       .515       .478      1.370
1.523
         P.9.12   V68           .542       .344       .195       .828
1.087
         P.9.13   V69           .661       .468       .125       .819
1.247
         P.9.14   V70           .544       .318      -
.085      .415      .468
         P.9.15
V71       .211       .482       .343       .496       .484
         LOGANTIG V76           .083      -.056      -.105      -.023
-.014
         LOGTAMA
V79       .181       .095       .047       .287       .208
```

| | | P.4.3 V38 | P.4.4 V39 | P.4.7 V42 | P.4.8 V43 | P.4.9 V44 |
|---|---|---|---|---|---|---|
| P.4.3 | V38 | 5.849 | | | | |
| P.4.4 | V39 | 5.226 | 5.940 | | | |
| P.4.7 | V42 | 2.098 | 2.279 | 5.118 | | |
| P.4.8 | V43 | 2.630 | 2.797 | 4.093 | 5.158 | |
| P.4.9 | V44 | 2.718 | 2.968 | 3.545 | 3.768 | 5.599 |
| P.4.10 | V45 | 2.674 | 2.686 | 2.958 | 3.111 | 4.236 |
| P.6.1 | V47 | 2.035 | 2.262 | 1.283 | 1.209 | 1.672 |
| P.6.2 | V48 | 2.023 | 2.004 | 1.262 | 1.021 | 1.384 |
| P.6.3 | V49 | 2.440 | 2.358 | 1.106 | 1.145 | 1.750 |
| P.6.4 | V50 | 2.378 | 2.512 | 1.296 | 1.130 | 1.531 |
| P.6.5 | V51 | 1.840 | 2.008 | 1.641 | 1.397 | 1.662 |
| P.9.3 | V59 | .703 | .777 | .737 | .856 | .692 |
| P.9.9 | V65 | 1.477 | 1.576 | 1.571 | 1.281 | 1.517 |
| P.9.10 | V66 | 1.468 | 1.853 | 1.330 | 1.313 | 1.429 |
| P.9.12 | V68 | .939 | 1.153 | 1.368 | 1.316 | 1.397 |
| P.9.13 | V69 | 1.133 | 1.415 | 1.614 | 1.483 | 1.583 |
| P.9.14 | V70 | .371 | .645 | 1.073 | 1.045 | .998 |
| P.9.15 | V71 | .741 | .759 | 1.246 | 1.077 | 1.083 |
| LOGANTIG | V76 | -.047 | -.041 | -.119 | -.031 | -.082 |
| LOGTAMA | V79 | .212 | .235 | -.055 | .100 | .194 |

| | | P.4.10 V45 | P.6.1 V47 | P.6.2 V48 | P.6.3 V49 | P.6.4 V50 |
|---|---|---|---|---|---|---|
| P.4.10 | V45 | 5.373 | | | | |
| P.6.1 | V47 | 1.215 | 5.420 | | | |
| P.6.2 | V48 | 1.184 | 3.218 | 4.947 | | |
| P.6.3 | V49 | 1.642 | 3.124 | 3.427 | 5.326 | |
| P.6.4 | V50 | 1.111 | 2.976 | 2.609 | 2.731 | 4.757 |
| P.6.5 | V51 | 1.783 | 2.972 | 2.991 | 3.547 | 2.952 |
| P.9.3 | V59 | .541 | .312 | .415 | .488 | .198 |
| P.9.9 | V65 | 1.699 | 1.469 | 1.943 | 1.916 | 1.097 |

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          P.9.10   V66        1.491      1.532      1.797
1.348      .990
          P.9.12   V68
1.444      .804      .910       .962       .540
          P.9.13   V69        1.660      1.173
1.098      .912      .934
          P.9.14
V70        .914      .730       .944       .552       .322
          P.9.15
V71        .885      .734       .881       .803       .476
          LOGANTIG V76        -.105       .006       .003      -.079
-.032
          LOGTAMA
V79        .075      .256       .261       .283       .220


                             P.6.5      P.9.3      P.9.9      P.9.10
P.9.12
                                V51        V59        V65        V66
V68
          P.6.5    V51        5.082
          P.9.3    V59         .337      1.132
          P.9.9    V65        1.772       .905      3.961
          P.9.10   V66        1.303      1.022      2.800      3.683
          P.9.12   V68         .848       .733      1.843      2.049
2.856
          P.9.13   V69        1.083       .735      1.999      2.214
2.625
          P.9.14   V70         .507       .890      1.373      1.561
1.374
          P.9.15   V71         .642       .756      1.352
1.130      .963
          LOGANTIG V76         .002       .004       .010      -.042
-.030
          LOGTAMA  V79         .237      -
.052      .160      .116      .035


                             P.9.13     P.9.14     P.9.15     LOGANTIG
LOGTAMA
                                V69        V70        V71        V76
V79
          P.9.13   V69        3.713
          P.9.14   V70        1.384      2.122
          P.9.15   V71         .984      1.308      2.137
          LOGANTIG V76        -.035      -.008      -.022       .126
          LOGTAMA
V79        .079      .010       .042       .096       .370


       BENTLER-WEEKS STRUCTURAL REPRESENTATION:

             NUMBER OF DEPENDENT VARIABLES = 53
                 DEPENDENT V'S :     1    2    3    5    6    8    9
10   11   12
                 DEPENDENT V'S :    16   17   19   20   21   23   33
35   36   37
```

```
                 DEPENDENT V'S :    38   39   42   43   44   45   47
48   49   50
                 DEPENDENT V'S :    51   59   65   66   68   69   70
71   76   79
                 DEPENDENT F'S :     1    2    3    6    7    8    9
10   11   12
                 DEPENDENT F'S :    13   14   15

             NUMBER OF INDEPENDENT VARIABLES = 57
                 INDEPENDENT F'S :     4    5   16   17
                 INDEPENDENT E'S :     1    2    3    5    6    8    9
10   11   12
                 INDEPENDENT E'S :    16   17   19   20   21   23   33
35   36   37
                 INDEPENDENT E'S :    38   39   42   43   44   45   47
48   49   50
                 INDEPENDENT E'S :    51   59   65   66   68   69   70
71   76   79
                 INDEPENDENT D'S :     1    2    3    6    7    8    9
10   11   12
                 INDEPENDENT D'S :    13   14   15

             NUMBER OF FREE PARAMETERS = 103
             NUMBER OF FIXED NONZERO PARAMETERS =  70

       *** WARNING MESSAGES ABOVE, IF ANY, REFER TO THE MODEL PROVIDED.
           CALCULATIONS FOR INDEPENDENCE MODEL NOW BEGIN.

       *** WARNING MESSAGES ABOVE, IF ANY, REFER TO INDEPENDENCE MODEL.
           CALCULATIONS FOR USER'S MODEL NOW BEGIN.


        3RD STAGE OF COMPUTATION REQUIRED   7730167 WORDS OF MEMORY.
        PROGRAM ALLOCATED 200000000 WORDS

        DETERMINANT OF INPUT MATRIX IS    .23277D+14

       *** NOTE *** RESIDUAL-BASED STATISTICS CANNOT BE
                    CALCULATED BECAUSE OF PIVOTING PROBLEMS.

        PARAMETER ESTIMATES APPEAR IN ORDER,
        NO SPECIAL PROBLEMS WERE ENCOUNTERED DURING OPTIMIZATION.



        RESIDUAL COVARIANCE MATRIX  (S-SIGMA) :


                            P.1.1      P.1.2      P.1.3      P.1.5
P.1.6
                               V1         V2         V3         V5
V6
           P.1.1    V1          .000
           P.1.2    V2          .410       .000
           P.1.3    V3         -.225      -.141       .000
           P.1.5    V5          .675       .135       .287       .000
           P.1.6    V6          .030       .190      -
.063       .000       .000
```

| | | | | | | |
|---|---|---|---|---|---|---|
| | P.1.8 | V8 | -.207 | -.203 | .369 | -.661 |
| -.169 | | | | | | |
| | P.1.9 | V9 | -.729 | .315 | -.534 | -1.254 |
| -.190 | | | | | | |
| | P.1.10 | V10 | .119 | .134 | .551 | .341 |
| -.502 | | | | | | |
| | P.1.11 | V11 | -.198 | - | | |
| .177 | .003 | .148 | .300 | | | |
| | P.1.12 | V12 | -.159 | .067 | -.014 | - |
| .441 | .190 | | | | | |
| | P.1.16 | V16 | -.402 | -.148 | .077 | .046 |
| -.220 | | | | | | |
| | P.1.17 | V17 | -.461 | - | | |
| .270 | .102 | .702 | .304 | | | |
| | P.2.2 | V19 | -.670 | -.670 | .002 | -.491 |
| -.725 | | | | | | |
| | P.2.3 | V20 | -.422 | -.231 | .022 | -.384 |
| -.250 | | | | | | |
| | P.2.4 | V21 | -.301 | -.381 | -.221 | -.584 |
| -1.252 | | | | | | |
| | P.2.6 | V23 | .401 | .277 | .240 | -.325 |
| -.752 | | | | | | |
| | P.3.1 | V33 | -.385 | .105 | .516 | -.935 |
| -1.009 | | | | | | |
| | P.3.3 | V35 | .387 | .665 | .483 | -.424 |
| -.464 | | | | | | |
| | P.4.1 | V36 | -.360 | .386 | -.181 | -.731 |
| -.401 | | | | | | |
| | P.4.2 | V37 | .114 | .560 | .278 | - |
| .255 | .289 | | | | | |
| | P.4.3 | V38 | -.058 | .525 | -.124 | - |
| .320 | .314 | | | | | |
| | P.4.4 | V39 | .225 | .467 | -.033 | - |
| .282 | .380 | | | | | |
| | P.4.7 | V42 | -.577 | .099 | .021 | -1.025 |
| -.640 | | | | | | |
| | P.4.8 | V43 | -.043 | .768 | .412 | -.453 |
| -.207 | | | | | | |
| | P.4.9 | V44 | -.701 | -.044 | -.135 | -.674 |
| -.549 | | | | | | |
| | P.4.10 | V45 | -.305 | .162 | .084 | - |
| .381 | .304 | | | | | |
| | P.6.1 | V47 | -.139 | .040 | .288 | -.533 |
| -.340 | | | | | | |
| | P.6.2 | V48 | -.591 | -.672 | -.511 | - |
| .458 | .030 | | | | | |
| | P.6.3 | V49 | .100 | - | | |
| .217 | .178 | .340 | .644 | | | |
| | P.6.4 | V50 | -.284 | -.545 | -.140 | -.467 |
| -.181 | | | | | | |
| | P.6.5 | V51 | .212 | .119 | .078 | - |
| .151 | .055 | | | | | |
| | P.9.3 | V59 | -.287 | -.001 | -.121 | - |
| .175 | .045 | | | | | |
| | P.9.9 | V65 | .120 | .297 | .407 | - |
| .531 | .109 | | | | | |
| | P.9.10 | V66 | -.179 | -.213 | -.233 | - |
| .394 | .019 | | | | | |

```
          P.9.12   V68        -.356      -.384      -.218      -
.551       .182
          P.9.13   V69        -.305      -.037       .146      -
.419       .248
          P.9.14   V70        -.459      -.331       .279      -.251
-.248
          P.9.15   V71        -.326      -.028       .095      -
.104       .047
          LOGANTIG V76         .168       .083       .033      -.058
-.115
          LOGTAMA  V79         .240       .091      -.007      -
.034       .001


                            P.1.8      P.1.9      P.1.10     P.1.11
P.1.12
                               V8         V9        V10        V11
V12
          P.1.8    V8          .000
          P.1.9    V9          .136       .000
          P.1.10   V10        -.611      -.822       .000
          P.1.11   V11         .483      -.017       .282       .000
          P.1.12   V12         .786       .136      -
.035       .546       .000
          P.1.16   V16        -.064      -.540      -.056      -
.069       .210
          P.1.17   V17        -.510      -.106      -.101      -
.310       .045
          P.2.2    V19         .039      -.278      -.537      -.148
-.237
          P.2.3    V20         .542       .510      -
.539       .026       .257
          P.2.4    V21         .054       .506      -.277      -
.666       .573
          P.2.6
V23         .872       .760       .246       .508       .880
          P.3.1    V33         .223       .282     -1.517      -.066
-.837
          P.3.3    V35         .425       .407      -.802       .308
-.423
          P.4.1    V36         .500       .830      -
.340       .353       .860
          P.4.2    V37         .844       .815      -.121      -.071
1.169
          P.4.3    V38         .866      1.274      -.548       .283
1.372
          P.4.4    V39         .994      1.361      -.519       .530
1.163
          P.4.7    V42         .159      -.266      -
.832       .137       .047
          P.4.8    V43         .269      -.072      -
.629       .529       .180
          P.4.9    V44         .168       .528     -
1.319       .071       .171
          P.4.10   V45         .699       .264      -.951      -
.013       .132
          P.6.1    V47         .515       .301      -.490       .332
-.143
```

| | | | | | | |
|---|---|---|---|---|---|---|
| | P.6.2 | V48 | -.002 | -.415 | -.487 | .022 |
| -.275 | | | | | | |
| | P.6.3 | V49 | .903 | .314 | - | |
| .700 | .615 | .246 | | | | |
| | P.6.4 | V50 | .218 | .270 | -.656 | -.361 |
| -.162 | | | | | | |
| | P.6.5 | V51 | .291 | .097 | -.219 | .241 |
| -.220 | | | | | | |
| | P.9.3 | V59 | -.025 | .057 | -.132 | .155 |
| -.047 | | | | | | |
| | P.9.9 | V65 | .790 | .904 | - | |
| .369 | .156 | .602 | | | | |
| | P.9.10 | V66 | .402 | .230 | -.586 | - |
| .063 | .179 | | | | | |
| | P.9.12 | V68 | .099 | -.135 | -.682 | -.090 |
| -.438 | | | | | | |
| | P.9.13 | V69 | .233 | .404 | -.727 | .060 |
| -.020 | | | | | | |
| | P.9.14 | V70 | .351 | -.395 | .113 | .169 |
| -.385 | | | | | | |
| | P.9.15 | V71 | .223 | -.093 | - | |
| .556 | .539 | .015 | | | | |
| | LOGANTIG | V76 | -.106 | .066 | .079 | - |
| .146 | .051 | | | | | |
| | LOGTAMA | V79 | .009 | .087 | -.108 | - |
| .164 | .062 | | | | | |

| | | | | | | |
|---|---|---|---|---|---|---|
| | | | P.1.16 | P.1.17 | P.2.2 | P.2.3 |
| P.2.4 | | | | | | |
| | | | V16 | V17 | V19 | V20 |
| V21 | | | | | | |
| | P.1.16 | V16 | .000 | | | |
| | P.1.17 | V17 | .232 | .000 | | |
| | P.2.2 | V19 | .102 | -.054 | .000 | |
| | P.2.3 | V20 | -.079 | .072 | .124 | .000 |
| | P.2.4 | V21 | .354 | .608 | -.102 | - |
| .275 | .000 | | | | | |
| | P.2.6 | V23 | .252 | .280 | -.268 | -.099 |
| 1.124 | | | | | | |
| | P.3.1 | V33 | -.322 | - | | |
| .207 | .451 | .530 | .642 | | | |
| | P.3.3 | | | | | |
| V35 | .004 | .291 | .159 | .459 | .342 | |
| | P.4.1 | V36 | -.239 | .254 | .942 | .903 |
| 1.973 | | | | | | |
| | P.4.2 | V37 | -.447 | .066 | .989 | .849 |
| 1.707 | | | | | | |
| | P.4.3 | V38 | -.310 | .219 | .741 | .912 |
| 1.736 | | | | | | |
| | P.4.4 | V39 | -.419 | .075 | .919 | 1.014 |
| 2.021 | | | | | | |
| | P.4.7 | V42 | -.521 | -.162 | .871 | .470 |
| 1.285 | | | | | | |
| | P.4.8 | V43 | -.373 | .376 | 1.317 | .980 |
| 1.900 | | | | | | |
| | P.4.9 | V44 | -.168 | .298 | 1.040 | .731 |
| 2.240 | | | | | | |

P.4.10 V45 -.132 .462 .856 .732
1.107
P.6.1 V47 .277 .074 -
.282 .101 .667
P.6.2 V48 .069 -.695 .356 .495
1.015
P.6.3 V49 .450 -
.008 .408 .668 .459
P.6.4 V50 -.377 -.552 .484 .707
1.477
P.6.5 V51 .376 -
.027 .248 .650 .474
P.9.3 V59 .010 -
.125 .135 .136 .151
P.9.9
V65 .217 .017 .309 .598 .368
P.9.10 V66 -.634 -.130 -
.048 .363 .273
P.9.12 V68 -.395 -
.080 .521 .401 .524
P.9.13 V69 -
.407 .326 .675 .578 .566
P.9.14 V70 -.162 -
.274 .423 .256 .352
P.9.15 V71 .253 -
.272 .130 .058 .302
LOGANTIG V76 .002 -.008 .043 -
.001 .089
LOGTAMA V79 -.008 .000 -.061 -
.042 .158

P.2.6 P.3.1 P.3.3 P.4.1
P.4.2
V23 V33 V35 V36
V37
P.2.6 V23 .000
P.3.1 V33 -.035 .000
P.3.3 V35 .550 -.001 .000
P.4.1 V36 1.508 1.868 2.058 .000
P.4.2 V37 1.479 1.011
1.477 .074 .000
P.4.3 V38 1.474 1.225
1.957 .001 .003
P.4.4 V39 1.620 1.332 1.389 -.160
-.025
P.4.7 V42 1.218 .912 .959 -.006
-.299
P.4.8 V43 1.618
1.015 .999 .362 .073
P.4.9 V44 1.605 1.261 1.128 .152
-.100
P.4.10 V45 1.402 .982
1.307 .448 .298
P.6.1 V47 .277 1.076 1.077 1.337
1.382
P.6.2 V48 1.203 .258 .814 1.469
1.463

P.6.3 V49 .973 .247 1.006 1.235
1.471
P.6.4 V50 1.239 .328 .418 1.377
1.866
P.6.5 V51 .601 .493 .825 1.324
1.339
P.9.3
V59 .171 .006 .190 .088 .110
P.9.9 V65
1.069 .263 .656 .131 .344
P.9.10
V66 .627 .608 .564 .434 .300
P.9.12
V68 .365 .419 .264 .077 .107
P.9.13
V69 .470 .548 .200 .013 .193
P.9.14 V70 .407 .375 -.032 -.163
-.286
P.9.15 V71 .097 .530 .387 .014
-.146
LOGANTIG V76 .049 -.035 -.085 -.057
-.058
LOGTAMA V79 .062 .012 -
.031 .168 .054

P.4.3 P.4.4 P.4.7 P.4.8
P.4.9
V38 V39 V42 V43
V44
P.4.3 V38 .000
P.4.4 V39 .014 .000
P.4.7 V42 -.448 -.143 .000
P.4.8 V43 -.053 .243 .480 .000
P.4.9 V44 -.063 .321 -.199 -
.180 .000
P.4.10 V45 .208 .340 -.362 -
.389 .609
P.6.1 V47 1.455
1.710 .657 .550 .988
P.6.2 V48 1.442
1.451 .636 .361 .700
P.6.3 V49 1.800
1.749 .416 .418 .996
P.6.4 V50 1.868
2.026 .746 .550 .930
P.6.5 V51 1.243
1.440 .997 .719 .959
P.9.3
V59 .239 .336 .238 .330 .147
P.9.9 V65 .269 .427 .269 -
.091 .095
P.9.10 V66 .196 .643 -.041 -.132
-.068
P.9.12 V68 -
.081 .183 .269 .158 .197
P.9.13
V69 .037 .372 .433 .238 .293

| | | | | | | |
|---|---|---|---|---|---|---|
| P.9.14 | V70 | -.413 | -.102 | .228 | .154 | .075 |
| P.9.15 | V71 | .086 | .136 | .541 | .332 | .312 |
| LOGANTIG | V76 | -.093 | -.085 | -.168 | -.083 | -.136 |
| LOGTAMA | V79 | .051 | .082 | -.228 | -.082 | .005 |

| | | P.4.10 | P.6.1 | P.6.2 | P.6.3 | P.6.4 |
|---|---|---|---|---|---|---|
| | | V45 | V47 | V48 | V49 | V50 |
| P.4.10 | V45 | .000 | | | | |
| P.6.1 | V47 | .609 | .000 | | | |
| P.6.2 | V48 | .577 | .181 | .000 | | |
| P.6.3 | V49 | .974 | -.221 | .079 | .000 | |
| P.6.4 | V50 | .578 | .307 | -.062 | -.211 | .000 |
| P.6.5 | V51 | 1.160 | -.149 | -.133 | .106 | .207 |
| P.9.3 | V59 | .057 | -.056 | .046 | .082 | -.126 |
| P.9.9 | V65 | .438 | .509 | .982 | .857 | .252 |
| P.9.10 | V66 | .164 | .520 | .785 | .234 | .100 |
| P.9.12 | V68 | .380 | -.007 | .098 | .068 | -.173 |
| P.9.13 | V69 | .516 | .302 | .226 | -.048 | .168 |
| P.9.14 | V70 | .095 | .107 | .320 | -.136 | -.226 |
| P.9.15 | V71 | .202 | .213 | .360 | .229 | .018 |
| LOGANTIG | V76 | -.153 | -.054 | -.058 | -.145 | -.085 |
| LOGTAMA | V79 | -.093 | -.130 | -.125 | -.142 | -.119 |

| | | P.6.5 | P.9.3 | P.9.9 | P.9.10 | P.9.12 |
|---|---|---|---|---|---|---|
| | | V51 | V59 | V65 | V66 | V68 |
| P.6.5 | V51 | .000 | | | | |
| P.9.3 | V59 | -.043 | .014 | | | |
| P.9.9 | V65 | .784 | .068 | .094 | | |
| P.9.10 | V66 | .263 | .140 | .099 | .104 | |
| P.9.12 | V68 | .014 | .027 | .001 | .111 | .067 |
| P.9.13 | V69 | .186 | -.025 | .020 | .130 | .072 |
| P.9.14 | V70 | -.134 | .005 | -.043 | .071 | .179 |
| P.9.15 | V71 | .107 | .017 | .169 | -.115 | -.035 |

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          LOGANTIG V76        -.060      -.007      -.016      -.070
-.053
          LOGTAMA  V79        -.159      -.101       .034      -.017
-.071


                            P.9.13     P.9.14     P.9.15     LOGANTIG
LOGTAMA
                               V69        V70        V71         V76
V79
          P.9.13   V69         .077
          P.9.14   V70         .100       .039
          P.9.15   V71        -.089       .057       .028
          LOGANTIG V76        -.059      -.025      -.036        .000
          LOGTAMA  V79        -.035      -.071      -
.026       .000       .000


                          AVERAGE ABSOLUTE  COVARIANCE  RESIDUALS
=         .3817
             AVERAGE OFF-DIAGONAL ABSOLUTE  COVARIANCE  RESIDUALS
=         .4008


     24-Jul-17      PAGE :  6  EQS     Licensee:
       TITLE:   Your EQS 6 Model

       MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)



       STANDARDIZED RESIDUAL MATRIX:


                            P.1.1      P.1.2      P.1.3      P.1.5
P.1.6
                               V1         V2         V3         V5
V6
          P.1.1    V1          .000
          P.1.2    V2          .049       .000
          P.1.3    V3         -.028      -.019       .000
          P.1.5    V5          .086       .018       .040        .000
          P.1.6    V6          .004       .024      -
.008       .000       .000
          P.1.8    V8         -.027      -.028       .052       -.096
-.023
          P.1.9    V9         -.094       .043      -.075       -.181
-.026
          P.1.10   V10         .014       .017       .070        .044
-.062
          P.1.11   V11        -.023      -
.022       .000       .019       .037
          P.1.12   V12        -.019       .008      -.002       -
.059       .024
          P.1.16   V16        -.050      -.019       .010        .006
-.029
          P.1.17   V17        -.059      -
.037       .014       .101       .042
```

| | | | | | | |
|---|---|---|---|---|---|---|
| P.2.2 | V19 | -.106 | -.113 | .000 | -.087 | -.122 |
| P.2.3 | V20 | -.075 | -.044 | .004 | -.076 | -.047 |
| P.2.4 | V21 | -.040 | -.054 | -.032 | -.087 | -.177 |
| P.2.6 | V23 | .058 | .043 | .038 | -.053 | -.116 |
| P.3.1 | V33 | -.054 | .016 | .080 | -.148 | -.151 |
| P.3.3 | V35 | .055 | .101 | .075 | -.068 | -.070 |
| P.4.1 | V36 | -.050 | .057 | -.027 | -.113 | -.059 |
| P.4.2 | V37 | .016 | .084 | .043 | -.040 | .044 |
| P.4.3 | V38 | -.008 | .078 | -.019 | -.050 | .046 |
| P.4.4 | V39 | .031 | .069 | -.005 | -.044 | .056 |
| P.4.7 | V42 | -.086 | .016 | .003 | -.171 | -.101 |
| P.4.8 | V43 | -.006 | .121 | .067 | -.075 | -.033 |
| P.4.9 | V44 | -.100 | -.007 | -.021 | -.107 | -.083 |
| P.4.10 | V45 | -.044 | .025 | .013 | -.062 | .047 |
| P.6.1 | V47 | -.020 | .006 | .046 | -.086 | -.052 |
| P.6.2 | V48 | -.089 | -.108 | -.085 | -.078 | .005 |
| P.6.3 | V49 | .015 | -.034 | .028 | .056 | .100 |
| P.6.4 | V50 | -.044 | -.090 | -.024 | -.081 | -.030 |
| P.6.5 | V51 | .032 | .019 | .013 | -.025 | .009 |
| P.9.3 | V59 | -.091 | .000 | -.042 | -.062 | .015 |
| P.9.9 | V65 | .020 | .054 | .075 | -.101 | .020 |
| P.9.10 | V66 | -.031 | -.040 | -.045 | -.077 | .004 |
| P.9.12 | V68 | -.071 | -.082 | -.048 | -.123 | .039 |
| P.9.13 | V69 | -.053 | -.007 | .028 | -.082 | .046 |
| P.9.14 | V70 | -.106 | -.081 | .071 | -.065 | -.061 |
| P.9.15 | V71 | -.075 | -.007 | .024 | -.027 | .011 |
| LOGANTIG | V76 | .159 | .084 | .034 | -.062 | -.116 |
| LOGTAMA | V79 | .133 | .053 | -.004 | -.021 | .000 |

| | | P.1.8 V8 | P.1.9 V9 | P.1.10 V10 | P.1.11 V11 | P.1.12 V12 |
|---|---|---|---|---|---|---|
| P.1.8 | V8 | .000 | | | | |
| P.1.9 | V9 | .020 | .000 | | | |
| P.1.10 | V10 | -.081 | -.109 | .000 | | |
| P.1.11 | V11 | .064 | -.002 | .033 | .000 | |
| P.1.12 | V12 | .107 | .018 | -.004 | .066 | .000 |
| P.1.16 | V16 | -.009 | -.076 | -.007 | -.009 | .027 |
| P.1.17 | V17 | -.075 | -.015 | -.013 | -.041 | .006 |
| P.2.2 | V19 | .007 | -.050 | -.087 | -.024 | -.039 |
| P.2.3 | V20 | .110 | .103 | -.099 | .005 | .048 |
| P.2.4 | V21 | .008 | .076 | -.038 | -.091 | .080 |
| P.2.6 | V23 | .145 | .125 | .037 | .076 | .134 |
| P.3.1 | V33 | .036 | .045 | -.220 | -.010 | -.124 |
| P.3.3 | V35 | .069 | .066 | -.117 | .045 | -.063 |
| P.4.1 | V36 | .079 | .130 | -.048 | .050 | .124 |
| P.4.2 | V37 | .136 | .131 | -.018 | -.010 | .173 |
| P.4.3 | V38 | .138 | .201 | -.078 | .040 | .200 |
| P.4.4 | V39 | .157 | .213 | -.074 | .075 | .168 |
| P.4.7 | V42 | .027 | -.045 | -.127 | .021 | .007 |
| P.4.8 | V43 | .046 | -.012 | -.096 | .080 | .028 |
| P.4.9 | V44 | .027 | .085 | -.193 | .010 | .025 |
| P.4.10 | V45 | .116 | .044 | -.142 | -.002 | .020 |
| P.6.1 | V47 | .085 | .049 | -.073 | .049 | -.022 |
| P.6.2 | V48 | .000 | -.071 | -.076 | .003 | -.044 |
| P.6.3 | V49 | .151 | .052 | -.105 | .092 | .038 |
| P.6.4 | V50 | .039 | .047 | -.104 | -.057 | -.026 |
| P.6.5 | V51 | .050 | .017 | -.034 | .037 | -.034 |
| P.9.3 | V59 | -.009 | .020 | -.043 | .050 | -.015 |
| P.9.9 | V65 | .153 | .174 | -.064 | .027 | .107 |
| P.9.10 | V66 | .081 | .046 | -.105 | -.011 | .033 |

P.9.12 V68 .023 -.031 -.140 -.018
-.091
P.9.13 V69 .047 .080 -.130 .011
-.004
P.9.14 V70 .093 -.104 .027 .040
-.093
P.9.15 V71 .059 -.024 -
.131 .127 .004
LOGANTIG V76 -.115 .071 .077 -
.141 .050
LOGTAMA V79 .006 .055 -.061 -
.093 .036

P.1.16 P.1.17 P.2.2 P.2.3
P.2.4
V16 V17 V19 V20
V21
P.1.16 V16 .000
P.1.17 V17 .033 .000
P.2.2 V19 .018 -.010 .000
P.2.3 V20 -.015 .015 .031 .000
P.2.4 V21 .051 .092 -.019 -
.058 .000
P.2.6 V23 .040 .046 -.054 -
.023 .192
P.3.1 V33 -.050 -
.033 .089 .118 .106
P.3.3
V35 .001 .047 .032 .103 .057
P.4.1 V36 -
.036 .040 .181 .195 .319
P.4.2 V37 -
.069 .011 .195 .189 .283
P.4.3 V38 -
.047 .035 .144 .200 .284
P.4.4 V39 -
.063 .012 .177 .220 .328
P.4.7 V42 -.085 -
.027 .181 .110 .224
P.4.8 V43 -
.060 .063 .272 .228 .331
P.4.9 V44 -
.026 .048 .206 .163 .374
P.4.10 V45 -
.021 .076 .173 .167 .189
P.6.1 V47 .044 .012 -
.057 .023 .113
P.6.2 V48 .011 -
.120 .075 .118 .180
P.6.3 V49 .072 -
.001 .083 .153 .079
P.6.4 V50 -.064 -
.097 .104 .171 .268
P.6.5 V51 .061 -
.005 .052 .153 .083
P.9.3 V59 .003 -
.045 .060 .068 .056

P.9.9
V65 .040 .003 .073 .159 .073
P.9.10 V66 -.121 -.026 -
.012 .100 .056
P.9.12 V68 -.086 -
.018 .145 .125 .123
P.9.13 V69 -
.078 .065 .164 .159 .116
P.9.14 V70 -.041 -
.072 .136 .093 .096
P.9.15 V71 .064 -
.071 .042 .021 .082
LOGANTIG V76 .002 -.008 .057 -
.002 .099
LOGTAMA V79 -.005 .000 -.047 -
.037 .103

P.2.6 P.3.1 P.3.3 P.4.1
P.4.2
V23 V33 V35 V36
V37
P.2.6 V23 .000
P.3.1 V33 -.006 .000
P.3.3 V35 .101 .000 .000
P.4.1 V36 .266 .320 .356 .000
P.4.2
V37 .268 .178 .262 .013 .000
P.4.3
V38 .263 .212 .343 .000 .000
P.4.4 V39 .287 .229 .241 -.027
-.004
P.4.7 V42 .233 .169 .179 -.001
-.055
P.4.8
V43 .308 .187 .186 .065 .013
P.4.9 V44 .293 .223 .202 .026
-.018
P.4.10
V45 .261 .177 .239 .079 .054
P.6.1
V47 .051 .194 .196 .235 .249
P.6.2
V48 .234 .049 .155 .270 .276
P.6.3
V49 .182 .045 .184 .219 .268
P.6.4
V50 .245 .063 .081 .258 .359
P.6.5
V51 .115 .092 .155 .240 .249
P.9.3
V59 .069 .002 .076 .034 .043
P.9.9
V65 .232 .055 .140 .027 .073
P.9.10
V66 .141 .133 .124 .092 .066
P.9.12
V68 .093 .104 .066 .019 .026

P.9.13
V69 .105 .119 .044 .003 .042
P.9.14 V70 .121 .108 -.009 -.046
-.082
P.9.15 V71 .029 .152 .112 .004
-.042
LOGANTIG V76 .059 -.041 -.102 -.066
-.068
LOGTAMA V79 .044 .008 -
.021 .113 .037

P.4.3 P.4.4 P.4.7 P.4.8
P.4.9
V38 V39 V42 V43
V44
P.4.3 V38 .000
P.4.4 V39 .002 .000
P.4.7 V42 -.082 -.026 .000
P.4.8 V43 -.010 .044 .093 .000
P.4.9 V44 -.011 .056 -.037 -
.033 .000
P.4.10 V45 .037 .060 -.069 -
.074 .111
P.6.1
V47 .258 .301 .125 .104 .179
P.6.2
V48 .268 .268 .126 .072 .133
P.6.3
V49 .322 .311 .080 .080 .182
P.6.4
V50 .354 .381 .151 .111 .180
P.6.5
V51 .228 .262 .196 .140 .180
P.9.3
V59 .093 .130 .099 .136 .058
P.9.9 V65 .056 .088 .060 -
.020 .020
P.9.10 V66 .042 .137 -.009 -.030
-.015
P.9.12 V68 -
.020 .044 .070 .041 .049
P.9.13
V69 .008 .079 .099 .054 .064
P.9.14 V70 -.117 -
.029 .069 .047 .022
P.9.15
V71 .024 .038 .163 .100 .090
LOGANTIG V76 -.108 -.098 -.209 -.102
-.162
LOGTAMA V79 .035 .055 -.166 -
.059 .003

P.4.10 P.6.1 P.6.2 P.6.3
P.6.4
V45 V47 V48 V49
V50
P.4.10 V45 .000

```
          P.6.1    V47         .113        .000
          P.6.2    V48         .112        .035        .000
          P.6.3    V49         .182       -.041        .015        .000
          P.6.4    V50         .114        .061       -.013        -
.042       .000
          P.6.5    V51         .222       -.028        -
.026       .020       .042
          P.9.3    V59         .023       -.023        .020        .033
-.054
          P.9.9
V65         .095       .110        .222        .187        .058
          P.9.10
V66         .037       .116        .184        .053        .024
          P.9.12   V68         .097       -.002        .026        .018
-.047
          P.9.13   V69         .116        .067        .053        -
.011       .040
          P.9.14   V70         .028        .031        .099       -.040
-.071
          P.9.15
V71         .059       .063        .111        .068        .006
          LOGANTIG V76        -.186       -.066       -.073       -.177
-.110
          LOGTAMA  V79        -.066       -.091       -.092       -.101
-.089


                              P.6.5       P.9.3       P.9.9       P.9.10
P.9.12
                                 V51         V59         V65         V66
V68
          P.6.5    V51         .000
          P.9.3    V59        -.018        .012
          P.9.9    V65         .175        .032        .024
          P.9.10   V66         .061        .069        .026        .028
          P.9.12
V68         .004       .015        .000        .034        .023
          P.9.13   V69         .043        -
.012       .005       .035        .022
          P.9.14   V70        -.041        .003        -
.015       .025       .073
          P.9.15   V71         .032        .011        .058       -.041
-.014
          LOGANTIG V76        -.075       -.018       -.023       -.102
-.088
          LOGTAMA  V79        -.116       -.156        .028       -.014
-.069


                              P.9.13      P.9.14      P.9.15      LOGANTIG
LOGTAMA
                                 V69         V70         V71         V76
V79
          P.9.13   V69         .021
          P.9.14   V70         .036        .019
          P.9.15   V71        -.031        .027        .013
          LOGANTIG V76        -.087       -.049       -.070        .000
```

```
             LOGTAMA  V79        -.030      -.081      -
.029       .000       .000
```

AVERAGE ABSOLUTE STANDARDIZED RESIDUALS
= .0764

AVERAGE OFF-DIAGONAL ABSOLUTE STANDARDIZED RESIDUALS
= .0801

LARGEST STANDARDIZED RESIDUALS:

| NO. | PARAMETER | ESTIMATE | NO. | PARAMETER | ESTIMATE |
|---|---|---|---|---|---|
| 1 | V50, V39 | .381 | 11 | V36, V21 | .319 |
| 2 | V44, V21 | .374 | 12 | V49, V39 | .311 |
| 3 | V50, V37 | .359 | 13 | V43, V23 | .308 |
| 4 | V36, V35 | .356 | 14 | V47, V39 | .301 |
| 5 | V50, V38 | .354 | 15 | V44, V23 | .293 |
| 6 | V38, V35 | .343 | 16 | V39, V23 | .287 |
| 7 | V43, V21 | .331 | 17 | V38, V21 | .284 |
| 8 | V39, V21 | .328 | 18 | V37, V21 | .283 |
| 9 | V49, V38 | .322 | 19 | V48, V37 | .276 |
| 10 | V36, V33 | .320 | 20 | V43, V19 | .272 |

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MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

DISTRIBUTION OF STANDARDIZED RESIDUALS

```
          ----------------------------------------
          !                                      !
       340-                    *                 -
          !                    *                 !
          !                    *                 !
          !                    *                 !
          !                    *                 !           RANGE
FREQ PERCENT
       255-                 *  *                 -
          !                 *  *                 !    1   -0.5  -  --
0    .00%
          !                 *  *                 !    2   -0.4  -  -0.5
0    .00%
          !                 *  *                 !    3   -0.3  -  -0.4
0    .00%
          !                 *  *                 !    4   -0.2  -  -0.3
2    .24%
       170-                 *  *                 -    5   -0.1  -  -0.2
47   5.73%
          !                 *  *                 !    6    0.0  -  -0.1
258  31.46%
```

```
           !                 *  *                    !    7    0.1  -   0.0
340  41.46%
           !                 *  *  *                 !    8    0.2  -   0.1
116  14.15%
           !                 *  *  *                 !    9    0.3  -   0.2
43   5.24%
         85-                 *  *  *                 -    A    0.4  -   0.3
14   1.71%
           !                 *  *  *                 !    B    0.5  -   0.4
0    .00%
           !              *  *  *  *  *              !    C     ++  -   0.5
0    .00%
           !              *  *  *  *  *              !    -----------------
-------------
           !              *  *  *  *  *  *           !            TOTAL
820 100.00%
           ----------------------------------------
              1  2  3  4  5  6  7  8  9  A  B  C      EACH "*" REPRESENTS
17 RESIDUALS


      24-Jul-17      PAGE :  8  EQS     Licensee:
        TITLE:   Your EQS 6 Model

        MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)



        GOODNESS OF FIT SUMMARY FOR METHOD = ML

        INDEPENDENCE MODEL CHI-SQUARE        =    4873.818 ON   782
DEGREES OF FREEDOM

        INDEPENDENCE AIC =  3309.81820   INDEPENDENCE CAIC =    75.62382
               MODEL AIC =  -240.12048          MODEL CAIC = -3205.48796

        CHI-SQUARE =     1193.880 BASED ON     717 DEGREES OF FREEDOM
        PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00000

        THE NORMAL THEORY RLS CHI-SQUARE FOR THIS ML SOLUTION IS
1126.696.

        FIT INDICES
        -----------
        BENTLER-BONETT     NORMED FIT INDEX =      .755
        BENTLER-BONETT NON-NORMED FIT INDEX =      .873
        COMPARATIVE FIT INDEX (CFI)         =      .883
        BOLLEN   (IFI) FIT INDEX            =      .885
        MCDONALD (MFI) FIT INDEX            =      .246
        LISREL    GFI  FIT INDEX            =      .750
        LISREL   AGFI  FIT INDEX            =      .714
        ROOT MEAN-SQUARE RESIDUAL (RMR)     =      .559
        STANDARDIZED RMR                    =      .105
        ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .063
        90% CONFIDENCE INTERVAL OF RMSEA  (         .056,        .069)

        RELIABILITY COEFFICIENTS
```

```
        ------------------------
        CRONBACH'S ALPHA                    =      .924
        COEFFICIENT ALPHA FOR AN OPTIMAL SHORT SCALE
=      .928
        BASED ON 36 VARIABLES, ALL EXCEPT:
        P.1.10    P.3.1     P.3.3     LOGANTIG
        RELIABILITY COEFFICIENT RHO         =      .956
        GREATEST LOWER BOUND RELIABILITY
=      .984
        GLB RELIABILITY FOR AN OPTIMAL SHORT SCALE
=      .985
        BASED ON 37 VARIABLES, ALL EXCEPT:
        P.1.9     P.3.1     P.3.3
        BENTLER'S DIMENSION-FREE LOWER BOUND RELIABILITY
=      .984
        SHAPIRO'S LOWER BOUND RELIABILITY FOR A WEIGHTED COMPOSITE
=      .706
        WEIGHTS THAT ACHIEVE SHAPIRO'S LOWER BOUND:
        P.1.1     P.1.2     P.1.3     P.1.5     P.1.6     P.1.8
           -.809      .528     -.009     -.061     -.022      .054
        P.1.9     P.1.10    P.1.11    P.1.12    P.1.16    P.1.17
            .063     -.089      .002      .079     -.015     -.008
        P.2.2     P.2.3     P.2.4     P.2.6     P.3.1     P.3.3
            .029      .032      .020      .029     -.032     -.019
        P.4.1     P.4.2     P.4.3     P.4.4     P.4.7     P.4.8
           -.001      .050      .059      .047      .020      .016
        P.4.9     P.4.10    P.6.1     P.6.2     P.6.3     P.6.4
            .022      .020      .059      .063      .081      .058
        P.6.5     P.9.3     P.9.9     P.9.10    P.9.12    P.9.13
            .062      .012      .047      .032      .030      .034
        P.9.14    P.9.15    LOGANTIG  LOGTAMA
            .016      .018     -.001      .021


        GOODNESS OF FIT SUMMARY FOR METHOD = ROBUST

        ROBUST INDEPENDENCE MODEL CHI-SQUARE =    4677.321 ON   782
DEGREES OF FREEDOM

        INDEPENDENCE AIC =  3113.32107   INDEPENDENCE CAIC =  -120.87331
               MODEL AIC =  -422.87494          MODEL CAIC = -3388.24242

        SATORRA-BENTLER SCALED CHI-SQUARE =   1011.1251 ON     717
DEGREES OF FREEDOM
        PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00000

        FIT INDICES
        -----------
        BENTLER-BONETT     NORMED FIT INDEX =      .784
        BENTLER-BONETT NON-NORMED FIT INDEX =      .918
        COMPARATIVE FIT INDEX (CFI)         =      .924
        BOLLEN   (IFI) FIT INDEX            =      .926
        MCDONALD (MFI) FIT INDEX            =      .421
        ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .049
        90% CONFIDENCE INTERVAL OF RMSEA  (        .042,        .056)
```

ITERATIVE SUMMARY

| ITERATION | PARAMETER ABS CHANGE | ALPHA | FUNCTION |
|---|---|---|---|
| 1 | 1.973550 | 1.00000 | 14.96959 |
| 2 | .522124 | 1.00000 | 13.33247 |
| 3 | .391355 | 1.00000 | 11.92318 |
| 4 | .275343 | 1.00000 | 11.27369 |
| 5 | .717443 | .50000 | 10.78326 |
| 6 | .331539 | 1.00000 | 9.26679 |
| 7 | .085607 | 1.00000 | 8.37611 |
| 8 | .083638 | 1.00000 | 7.37842 |
| 9 | .056576 | 1.00000 | 7.11427 |
| 10 | .029139 | 1.00000 | 7.07178 |
| 11 | .018380 | 1.00000 | 7.06770 |
| 12 | .012670 | 1.00000 | 7.06574 |
| 13 | .008786 | 1.00000 | 7.06503 |
| 14 | .006381 | 1.00000 | 7.06467 |
| 15 | .004336 | 1.00000 | 7.06452 |
| 16 | .003167 | 1.00000 | 7.06444 |
| 17 | .002139 | 1.00000 | 7.06441 |
| 18 | .001554 | 1.00000 | 7.06439 |
| 19 | .001052 | 1.00000 | 7.06438 |
| 20 | .000759 | 1.00000 | 7.06438 |

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MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
(ROBUST STATISTICS IN PARENTHESES)

```
P.1.1   =V1  =   1.000 F1    + 1.000 E1



P.1.2   =V2  =   1.015*F1    + 1.000 E2
                  .094
                10.836@
              (   .068)
              ( 14.830@

P.1.3   =V3  =    .975*F1    + 1.000 E3
                  .091
                10.700@
              (   .071)
              ( 13.702@

P.1.5   =V5  =   1.000 F3    + 1.000 E5



P.1.6   =V6  =    .863*F3    + 1.000 E6
                  .090
                 9.600@
              (   .073)
              ( 11.777@

P.1.8   =V8  =    .804*F1    + 1.000 E8
                  .089
                 9.077@
              (   .076)
              ( 10.562@

P.1.9   =V9  =    .669*F4    + 1.000 E9
                  .092
                 7.235@
              (   .079)
              (  8.451@

P.1.10  =V10 =   1.000 F2    + 1.000 E10



P.1.11  =V11 =   1.078*F2    + 1.000 E11
                  .157
                 6.854@
              (   .126)
              (  8.537@

P.1.12  =V12 =   1.000 F4    + 1.000 E12
```

```
P.1.16  =V16 =   1.123*F2    + 1.000 E16
                  .152
                 7.375@
              (   .119)
              (  9.419@

P.1.17  =V17 =   1.004*F2    + 1.000 E17
                  .143
                 7.033@
              (   .125)
              (  8.060@


        MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
(CONTINUED)


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        MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)
        (ROBUST STATISTICS IN PARENTHESES)

P.2.2   =V19 =   1.000 F6    + 1.000 E19




P.2.3   =V20 =    .905*F6    + 1.000 E20
                  .077
                11.795@
              (   .082)
              ( 11.015@

P.2.4   =V21 =    .899*F6    + 1.000 E21
                  .105
                 8.584@
              (   .085)
              ( 10.635@

P.2.6   =V23 =    .875*F6    + 1.000 E23
                  .094
                 9.261@
              (   .086)
              ( 10.142@

P.3.1   =V33 =   1.000 F7    + 1.000 E33




P.3.3   =V35 =    .928*F7    + 1.000 E35
                  .382
```

```
                    2.429@
                 (   .421)
                 (  2.205@

 P.4.1   =V36 =   1.000 F8    + 1.000 E36



 P.4.2   =V37 =   1.306*F8    + 1.000 E37
                   .109
                 11.980@
                 (   .120)
                 ( 10.905@

 P.4.3   =V38 =   1.358*F8    + 1.000 E38
                   .111
                 12.230@
                 (   .127)
                 ( 10.670@

 P.4.4   =V39 =   1.292*F8    + 1.000 E39
                   .111
                 11.599@
                 (   .123)
                 ( 10.495@

 P.4.7   =V42 =   1.000 F9    + 1.000 E42



 P.4.8   =V43 =   1.054*F9    + 1.000 E43
                   .082
                 12.891@
                 (   .073)
                 ( 14.465@


  MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
(CONTINUED)


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  TITLE:   Your EQS 6 Model

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)
  (ROBUST STATISTICS IN PARENTHESES)

 P.4.9   =V44 =   1.092*F9    + 1.000 E44
                   .085
                 12.800@
                 (   .079)
                 ( 13.762@

 P.4.10  =V45 =    .969*F9    + 1.000 E45
```

```
                  .087
                11.195@
              (   .081)
              ( 11.916@

P.6.1   =V47 =   1.000 F10   + 1.000 E47




P.6.2   =V48 =   1.001*F10   + 1.000 E48
                  .099
                10.080@
              (   .089)
              ( 11.223@

P.6.3   =V49 =   1.102*F10   + 1.000 E49
                  .103
                10.722@
              (   .092)
              ( 11.966@

P.6.4   =V50 =    .879*F10   + 1.000 E50
                  .098
                 8.968@
              (   .091)
              (  9.635@

P.6.5   =V51 =   1.029*F10   + 1.000 E51
                  .101
                10.228@
              (   .102)
              ( 10.092@

P.9.3   =V59 =    .591*F12   + 1.000 E59
                  .068
                 8.696@
              (   .086)
              (  6.846@

P.9.9   =V65 =   1.000 F14   + 1.000 E65




P.9.10  =V66 =   1.053*F14   + 1.000 E66
                  .089
                11.784@
              (   .095)
              ( 11.025@

P.9.12  =V68 =   1.000 F13   + 1.000 E68
```

```
 P.9.13  =V69 =   1.075*F13   + 1.000 E69
                   .081
                 13.341@
               (   .089)
               ( 12.109@
```

MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS (CONTINUED)

```
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)
  (ROBUST STATISTICS IN PARENTHESES)

 P.9.14  =V70 =   1.000 F12   + 1.000 E70



 P.9.15  =V71 =    .835*F12   + 1.000 E71
                   .093
                  8.952@
               (   .114)
               (  7.317@

 LOGANTIG=V76 =   1.000 F17   + 1.000 E76



 LOGTAMA =V79 =   1.000 F16   + 1.000 E79



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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  CONSTRUCT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
  (ROBUST STATISTICS IN PARENTHESES)


   F1   =F1   =   1.000 F5    + 1.000 D1
```

```
F2   =F2  =    .805*F5    + 1.000 D2
               .121
              6.659@
           (   .100)
           (  8.059@

F3   =F3  =    .889*F5    + 1.000 D3
               .115
              7.750@
           (   .084)
           ( 10.556@

F6   =F6  =    .256*F5    + 1.000 D6
               .081
              3.174@
           (   .076)
           (  3.362@

F7   =F7  =    .473*F4    -  .505*F5    + 1.000 D7
               .202           .225
              2.341@        -2.245@
           (   .240)     (   .264)
           (  1.969@     ( -1.913)

F8   =F8  =   1.000 F11   + 1.000 D8



F9   =F9  =   1.463*F11   + 1.000 D9
               .306
              4.789@
           (   .281)
           (  5.206@

F10  =F10 =    .517*F4    + 1.000 D10
               .074
              6.984@
           (   .064)
           (  8.092@

F11  =F11 =    .223*F5    + 1.000 D11
               .065
              3.437@
           (   .067)
           (  3.342@

F12  =F12 =   1.000 F15   + 1.000 D12
```

```
F13  =F13 =   1.300*F15   + 1.000 D13
               .162
              8.020@
           (   .164)
           (  7.920@

F14  =F14 =   1.541*F15   + 1.000 D14
               .201
              7.663@
           (   .238)
           (  6.462@
```

CONSTRUCT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS (CONTINUED)

```
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)
  (ROBUST STATISTICS IN PARENTHESES)

    F15  =F15 =   -.003*F6    -  .027*F7    +  .161*F10
+  .403*F11
                   .043          .052          .052          .097
                  -.065         -.516         3.111@        4.130@
               (   .044)     (   .057)     (   .047)     (   .101)
               (  -.063)     (  -.465)     (  3.415@     (  3.984@

                -  .068*F16   +  .002*F17   + 1.000 D15
                   .140          .221
                  -.485          .007
               (   .139)     (   .224)
               (  -.491)     (   .007)
```

```
24-Jul-17      PAGE : 15  EQS     Licensee:
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES
  ----------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                V                                 F
               ---                               ---
                              I F4  -   F4              5.333*I
                              I                          .929 I
                              I                         5.738@I
                              I                      (   .718)I
                              I                      (  7.431@I
                              I                               I
                              I F5  -   F5              4.064*I
                              I                          .838 I
                              I                         4.852@I
```

```
                                     I                       (    .611)I
                                     I                       (   6.649@I
                                     I                                 I
                                     I F16 -   F16                .370*I
                                     I                            .040 I
                                     I                           9.192@I
                                     I                       (    .051)I
                                     I                       (   7.251@I
                                     I                                 I
                                     I F17 -   F17                .126*I
                                     I                            .014 I
                                     I                           9.192@I
                                     I                       (    .018)I
                                     I                       (   7.177@I
                                     I                                 I


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES
  ----------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                 E                                 D
                ---                               ---
 E1  -P.1.1                3.684*I D1   -   F1               1.069*I
                            .486 I                            .354 I
                           7.586@I                           3.017@I
                       (    .585)I                       (    .423)I
                       (   6.296@I                       (   2.527@I
                                 I                                 I
 E2  -P.1.2                2.486*I D2   -   F2                .562*I
                            .370 I                            .263 I
                           6.720@I                           2.133@I
                       (    .418)I                       (    .278)I
                       (   5.945@I                       (   2.021@I
                                 I                                 I
 E3  -P.1.3                2.474*I D3   -   F3               3.066*I
                            .359 I                            .643 I
                           6.898@I                           4.766@I
                       (    .443)I                       (    .656)I
                       (   5.586@I                       (   4.671@I
                                 I                                 I
 E5  -P.1.5                 .767*I D6   -   F6               2.967*I
                            .519 I                            .475 I
                           1.477 I                           6.240@I
                       (    .520)I                       (    .509)I
                       (   1.475)I                       (   5.831@I
                                 I                                 I
 E6  -P.1.6                3.118*I D7   -   F7               2.490*I
                            .510 I                           1.163 I
                           6.107@I                           2.141@I
                       (    .615)I                       (   1.287)I
                       (   5.069@I                       (   1.934)I
                                 I                                 I
```

```
 E8  -P.1.8                3.431*I D8  -   F8                1.689*I
                            .424 I                             .390 I
                           8.087@I                            4.333@I
                        (   .447)I                         (   .371)I
                        (  7.678@I                         (  4.551@I
                                 I                                  I
 E9  -P.1.9                4.449*I D9  -   F9                 .685*I
                            .545 I                             .473 I
                           8.165@I                            1.448 I
                        (   .523)I                         (   .533)I
                        (  8.508@I                         (  1.284)I
                                 I                                  I
 E10 -P.1.10               5.182*I D10 -   F10               1.610*I
                            .636 I                             .336 I
                           8.141@I                            4.792@I
                        (   .647)I                         (   .301)I
                        (  8.006@I                         (  5.347@I
                                 I                                  I
 E11 -P.1.11               4.730*I D11 -   F11               1.079*I
                            .603 I                             .334 I
                           7.844@I                            3.232@I
                        (   .562)I                         (   .332)I
                        (  8.418@I                         (  3.247@I
                                 I                                  I
 E12 -P.1.12               2.724*I D12 -   F12                .578*I
                            .521 I                             .144 I
                           5.231@I                            4.006@I
                        (   .550)I                         (   .172)I
                        (  4.949@I                         (  3.362@I
                                 I                                  I
 E16 -P.1.16               3.385*I D13 -   F13                .822*I
                            .476 I                             .187 I
                           7.112@I                            4.383@I
                        (   .497)I                         (   .223)I
                        (  6.809@I                         (  3.678@I
                                 I                                  I
 E17 -P.1.17               3.597*I D14 -   F14                .384*I
                            .470 I                             .198 I
                           7.646@I                            1.938 I
                        (   .610)I                         (   .304)I
                        (  5.900@I                         (  1.260)I
                                 I                                  I


24-Jul-17      PAGE : 17  EQS     Licensee:
  TITLE:   Your EQS 6 Model

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES (CONTINUED)
  ----------------------------------------------

 E19 -P.2.2                1.302*I D15 -   F15                .591*I
                            .239 I                             .140 I
                           5.449@I                            4.220@I
                        (   .431)I                         (   .169)I
                        (  3.021@I                         (  3.494@I
                                 I                                  I
 E20 -P.2.3                 .926*I                                  I
```

```
                       .186 I                               I
                      4.977@I                               I
                   (   .289)I                               I
                   (  3.206@I                               I
                            I                               I
 E21 -P.2.4           3.793*I                               I
                       .459 I                               I
                      8.255@I                               I
                   (   .517)I                               I
                   (  7.330@I                               I
                            I                               I
 E23 -P.2.6           2.884*I                               I
                       .360 I                               I
                      8.014@I                               I
                   (   .529)I                               I
                   (  5.450@I                               I
                            I                               I
 E33 -P.3.1           2.747*I                               I
                      1.227 I                               I
                      2.238@I                               I
                   (  1.439)I                               I
                   (  1.910)I                               I
                            I                               I
 E35 -P.3.3           3.046*I                               I
                      1.078 I                               I
                      2.827@I                               I
                   (  1.150)I                               I
                   (  2.649@I                               I
                            I                               I
 E36 -P.4.1           3.004*I                               I
                       .338 I                               I
                      8.880@I                               I
                   (   .471)I                               I
                   (  6.381@I                               I
                            I                               I
 E37 -P.4.2            .607*I                               I
                       .100 I                               I
                      6.083@I                               I
                   (   .187)I                               I
                   (  3.253@I                               I
                            I                               I
 E38 -P.4.3            .372*I                               I
                       .089 I                               I
                      4.174@I                               I
                   (   .289)I                               I
                   (  1.286)I                               I
                            I                               I
 E39 -P.4.4            .980*I                               I
                       .131 I                               I
                      7.460@I                               I
                   (   .347)I                               I
                   (  2.824@I                               I
                            I                               I
 E42 -P.4.7           1.691*I                               I
                       .234 I                               I
                      7.219@I                               I
                   (   .274)I                               I
                   (  6.162@I                               I
```

```
                              I                                I
 E43 -P.4.8              1.348*I                                I
                           .210 I                                I
                         6.420@I                                I
                      (   .354)I                                I
                      (  3.805@I                                I
                              I                                I
```

```
24-Jul-17      PAGE : 18  EQS     Licensee:
  TITLE:   Your EQS 6 Model

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES (CONTINUED)
  ----------------------------------------------

 E44 -P.4.9              1.509*I                                I
                           .231 I                                I
                         6.533@I                                I
                      (   .375)I                                I
                      (  4.029@I                                I
                              I                                I
 E45 -P.4.10             2.157*I                                I
                           .278 I                                I
                         7.755@I                                I
                      (   .288)I                                I
                      (  7.504@I                                I
                              I                                I
 E47 -P.6.1              2.386*I                                I
                           .306 I                                I
                         7.792@I                                I
                      (   .436)I                                I
                      (  5.476@I                                I
                              I                                I
 E48 -P.6.2              1.908*I                                I
                           .257 I                                I
                         7.430@I                                I
                      (   .404)I                                I
                      (  4.718@I                                I
                              I                                I
 E49 -P.6.3              1.637*I                                I
                           .245 I                                I
                         6.694@I                                I
                      (   .342)I                                I
                      (  4.791@I                                I
                              I                                I
 E50 -P.6.4              2.410*I                                I
                           .297 I                                I
                         8.125@I                                I
                      (   .343)I                                I
                      (  7.022@I                                I
                              I                                I
 E51 -P.6.5              1.872*I                                I
                           .257 I                                I
                         7.293@I                                I
                      (   .322)I                                I
                      (  5.817@I                                I
                              I                                I
```

```
 E59 -P.9.3                .596*I                                  I
                           .078 I                                  I
                          7.589@I                                  I
                       (   .097)I                                  I
                       (  6.147@I                                  I
                                I                                  I
 E65 -P.9.9               1.301*I                                  I
                           .207 I                                  I
                          6.296@I                                  I
                       (   .367)I                                  I
                       (  3.549@I                                  I
                                I                                  I
 E66 -P.9.10               .736*I                                  I
                           .185 I                                  I
                          3.977@I                                  I
                       (   .199)I                                  I
                       (  3.703@I                                  I
                                I                                  I
 E68 -P.9.12               .414*I                                  I
                           .138 I                                  I
                          3.003@I                                  I
                       (   .191)I                                  I
                       (  2.168@I                                  I
                                I                                  I
 E69 -P.9.13               .891*I                                  I
                           .179 I                                  I
                          4.980@I                                  I
                       (   .318)I                                  I
                       (  2.804@I                                  I
                                I                                  I


24-Jul-17      PAGE : 19  EQS     Licensee:
  TITLE:   Your EQS 6 Model

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES (CONTINUED)
  ----------------------------------------------

 E70 -P.9.14               .585*I                                  I
                           .127 I                                  I
                          4.608@I                                  I
                       (   .200)I                                  I
                       (  2.930@I                                  I
                                I                                  I
 E71 -P.9.15              1.065*I                                  I
                           .144 I                                  I
                          7.382@I                                  I
                       (   .278)I                                  I
                       (  3.830@I                                  I
                                I                                  I
```

```
 24-Jul-17      PAGE : 20  EQS     Licensee:
  TITLE:   Your EQS 6 Model

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  COVARIANCES AMONG INDEPENDENT VARIABLES
  ---------------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                V                                 F
               ---                               ---
                              I F5  -   F5               3.717*I
                              I F4  -   F4                .626 I
                              I                          5.933@I
                              I                       (   .486)I
                              I                       (  7.651@I
                              I                                I
                              I F16 -   F16               .746*I
                              I F4  -   F4                .139 I
                              I                          5.349@I
                              I                       (   .143)I
                              I                       (  5.205@I
                              I                                I
                              I F17 -   F17               .116*I
                              I F4  -   F4                .072 I
                              I                          1.609 I
                              I                       (   .072)I
                              I                       (  1.616)I
                              I                                I
                              I F16 -   F16               .532*I
                              I F5  -   F5                .119 I
                              I                          4.487@I
                              I                       (   .112)I
                              I                       (  4.752@I
                              I                                I
                              I F17 -   F17               .151*I
                              I F5  -   F5                .062 I
                              I                          2.420@I
                              I                       (   .057)I
                              I                       (  2.647@I
                              I                                I
                              I F17 -   F17               .096*I
                              I F16 -   F16               .018 I
                              I                          5.276@I
                              I                       (   .019)I
                              I                       (  5.136@I
                              I                                I


24-Jul-17      PAGE : 21  EQS     Licensee:
  TITLE:   Your EQS 6 Model

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  STANDARDIZED SOLUTION:
R-SQUARED
```

```
        P.1.1   =V1  =   .763 F1    + .646
E1                                       .582
        P.1.2   =V2  =   .825*F1    + .566
E2                                       .680
        P.1.3   =V3  =   .815*F1    + .580
E3                                       .664
        P.1.5   =V5  =   .944 F3    + .330
E5                                       .891
        P.1.6   =V6  =   .775*F3    + .633
E6                                       .600
        P.1.8   =V8  =   .701*F1    + .713
E8                                       .491
        P.1.9   =V9  =   .591*F4    + .807
E9                                       .349
        P.1.10  =V10 =   .617 F2    + .787
E10                                      .381
        P.1.11  =V11 =   .663*F2    + .749
E11                                      .440
        P.1.12  =V12 =   .814 F4    + .581
E12                                      .662
        P.1.16  =V16 =   .737*F2    + .676
E16                                      .543
        P.1.17  =V17 =   .687*F2    + .726
E17                                      .472
        P.2.2   =V19 =   .844 F6    + .536
E19                                      .713
        P.2.3   =V20 =   .861*F6    + .509
E20                                      .741
        P.2.4   =V21 =   .639*F6    + .769
E21                                      .408
        P.2.6   =V23 =   .680*F6    + .734
E23                                      .462
        P.3.1   =V33 =   .719 F7    + .695
E33                                      .517
        P.3.3   =V35 =   .674*F7    + .739
E35                                      .454
        P.4.1   =V36 =   .705 F8    + .709
E36                                      .497
        P.4.2   =V37 =   .945*F8    + .327
E37                                      .893
        P.4.3   =V38 =   .968*F8    + .252
E38                                      .936
        P.4.4   =V39 =   .914*F8    + .406
E39                                      .835
        P.4.7   =V42 =   .818 F9    + .575
E42                                      .670
        P.4.8   =V43 =   .859*F9    + .511
E43                                      .739
        P.4.9   =V44 =   .855*F9    + .519
E44                                      .731
        P.4.10  =V45 =   .774*F9    + .634
E45                                      .598
        P.6.1   =V47 =   .748 F10   + .663
E47                                      .560
        P.6.2   =V48 =   .784*F10   + .621
E48                                      .614
```

```
       P.6.3   =V49 =   .832*F10   + .554
E49                                     .693
       P.6.4   =V50 =   .702*F10   + .712
E50                                     .493
       P.6.5   =V51 =   .795*F10   + .607
E51                                     .632
       P.9.3   =V59 =   .684*F12   + .730
E59                                     .468
       P.9.9   =V65 =   .815 F14   + .580
E65                                     .664
       P.9.10  =V66 =   .891*F14   + .454
E66                                     .794
       P.9.12  =V68 =   .923 F13   + .385
E68                                     .852
       P.9.13  =V69 =   .869*F13   + .495
E69                                     .755
       P.9.14  =V70 =   .848 F12   + .530
E70                                     .719
       P.9.15  =V71 =   .704*F12   + .710
E71                                     .495


        STANDARDIZED SOLUTION:
R-SQUARED


      24-Jul-17      PAGE : 22  EQS     Licensee:
        TITLE:   Your EQS 6 Model

        MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

       LOGANTIG=V76 =  1.000 F17   + .000 E76
1.000
       LOGTAMA =V79 =  1.000 F16   + .000 E79
1.000
          F1   =F1  =   .890 F5    + .456
D1                                      .792
          F2   =F2  =   .908*F5    + .419
D2                                      .824
          F3   =F3  =   .715*F5    + .699
D3                                      .511
          F6   =F6  =   .287*F5    + .958
D6                                      .082
          F7   =F7  =   .636*F4    - .594*F5    + .920
D7                        .154
          F8   =F8  =   .657 F11   + .754
D8                                      .431
          F9   =F9  =   .895*F11   + .447
D9                                      .800
          F10  =F10 =   .685*F4    + .728
D10                                     .470
          F11  =F11 =   .396*F5    + .918
D11                                     .157
          F12  =F12 =   .784 F15   + .621
D12                                     .614
          F13  =F13 =   .809*F15   + .588
D13                                     .654
          F14  =F14 =   .922*F15   + .387
D14                                     .850
```

```
         F15  =F15 =  -.005*F6    - .048*F7    + .292*F10   + .475*F11
                     - .043*F16   + .001*F17   + .802
D15                        .357


      24-Jul-17      PAGE : 23  EQS     Licensee:
        TITLE:   Your EQS 6 Model

        MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

        CORRELATIONS AMONG INDEPENDENT VARIABLES
        ---------------------------------------

                        V                                F
                       ---                              ---
                                      I F5  -   F5              .798*I
                                      I F4  -   F4                   I
                                      I                              I
                                      I F16 -   F16             .530*I
                                      I F4  -   F4                   I
                                      I                              I
                                      I F17 -   F17             .142*I
                                      I F4  -   F4                   I
                                      I                              I
                                      I F16 -   F16             .433*I
                                      I F5  -   F5                   I
                                      I                              I
                                      I F17 -   F17             .211*I
                                      I F5  -   F5                   I
                                      I                              I
                                      I F17 -   F17             .444*I
                                      I F16 -   F16                  I
                                      I                              I


       ------------------------------------------------------------------
-------------
                                E N D   O F   M E T H O D
       ------------------------------------------------------------------
-------------
      1
        Execution begins at 11:12:18
        Execution ends   at 11:12:25
        Elapsed time =       7.00 seconds
```

# ANEXO XVIII

# MODELO EFECTO MEDIADOR DE LA FLEXIBILIDAD EXTERNA DE LA ESTRUCTURA – MODELO A

```
1
  EQS, A STRUCTURAL EQUATION PROGRAM          MULTIVARIATE SOFTWARE, INC.
  COPYRIGHT BY P.M. BENTLER                   VERSION 6.1 (C) 1985 - 2005
(B85).


    PROGRAM CONTROL INFORMATION

        /TITLE
         Your EQS 6 Model
        /SPECIFICATIONS
        VARIABLES= 80 ; CASES= 170 ;
        DATA='C:\tesis1\ticflexrdoscontroltotal.ESS';
        MATRIX=RAW;METHOD=ML,robust;
        /LABELS
        V1=P.1.1; V2=P.1.2; V3=P.1.3; V4=P.1.4; V5=P.1.5;
        V6=P.1.6; V7=P.1.7; V8=P.1.8; V9=P.1.9; V10=P.1.10;
        V11=P.1.11; V12=P.1.12; V13=P.1.13; V14=P.1.14; V15=P.1.15;
        V16=P.1.16; V17=P.1.17; V18=P.2.1; V19=P.2.2; V20=P.2.3;
        V21=P.2.4; V22=P.2.5; V23=P.2.6; V24=P.2.7; V25=P.2.8;
        V26=P.2.9; V27=P.2.10; V28=P.2.11; V29=P.2.12; V30=P.2.13;
        V31=P.2.14; V32=P.2.15; V33=P.3.1; V34=P.3.2; V35=P.3.3;
        V36=P.4.1; V37=P.4.2; V38=P.4.3; V39=P.4.4; V40=P.4.5;
        V41=P.4.6; V42=P.4.7; V43=P.4.8; V44=P.4.9; V45=P.4.10;
        V46=P.4.11; V47=P.6.1; V48=P.6.2; V49=P.6.3; V50=P.6.4;
        V51=P.6.5; V52=P.6.6; V53=P.6.7; V54=P.6.8; V55=P.6.9;
        V56=P.6.10; V57=P.9.1; V58=P.9.2; V59=P.9.3; V60=P.9.4;
        V61=P.9.5; V62=P.9.6; V63=P.9.7; V64=P.9.8; V65=P.9.9;
        V66=P.9.10; V67=P.9.11; V68=P.9.12; V69=P.9.13; V70=P.9.14;
        V71=P.9.15; V72=P.9.16; V73=P.9.17;
        V74=P.11.1; V75=ANTIGUED; V76=LOGANTIG; V77=RAIZANTI; V78=P.10.1;
        V79=LOGTAMA; V80=RAIZTAMA;

        /EQUATIONS
        V9 =   1F4 + E9;
        V12 =   *F4 + E12;
        V59 =   *F12 + E59;
        V65 =   1F14 + E65;
        V66 =   *F14 + E66;
        V68 =   1F13 + E68;
        V69 =   *F13 + E69;
        V70 =   1F12 + E70;
        V71 =   *F12 + E71;
        V76 =   F17 + E76;
        V79 =   F16 + E79;
        F12 =   1F15 + D12;
        F13 =   *F15 + D13;
        F14 =   *F15 + D14;
        F15 =   *F4 + *F16 + *F17 + D15;

        /VARIANCES
         F4=*;
         F16=*;
         F17=*;
```

```
E9 = *;
E12 = *;
E59 = *;
E65 = *;
E66 = *;
E68 = *;
```

```
05-Feb-18      PAGE :  2  EQS     Licensee:
  TITLE:    Your EQS 6 Model
```

```
 E69 = *;
 E70 = *;
 E71 = *;
 E76 = 0;
 E79 = 0;
 D12 = *;
 D13 = *;
 D14 = *;
 D15 = *;
/COVARIANCES
 F4,F16=*;
 F4,F17=*;
 F16,F17=*;
/PRINT
FIT=ALL;
TABLE=EQUATION;
/END
```

```
   69 RECORDS OF INPUT MODEL FILE WERE READ


DATA IS READ FROM C:\tesis1\ticflexrdoscontroltotal.ESS
THERE ARE  80 VARIABLES AND   170 CASES
IT IS A RAW DATA ESS FILE
```

```
05-Feb-18      PAGE :  3  EQS     Licensee:
  TITLE:    Your EQS 6 Model
```

SAMPLE STATISTICS BASED ON COMPLETE CASES

UNIVARIATE STATISTICS
---------------------

| VARIABLE | P.1.9 V9 | P.1.12 V12 | P.9.3 V59 | P.9.9 V65 | P.9.10 V66 |
|---|---|---|---|---|---|
| MEAN | 2.3647 | 2.3706 | 6.1647 | 4.1824 | 4.5118 |
| SKEWNESS (G1) | .6639 | .6738 | -1.6316 | -.3570 | -.5772 |
| KURTOSIS (G2) | -1.0669 | -1.2320 | 2.6761 | -.7646 | -.3762 |
| STANDARD DEV. | 2.6147 | 2.8385 | 1.0642 | 1.9901 | 1.9192 |

| VARIABLE | P.9.12 V68 | P.9.13 V69 | P.9.14 V70 | P.9.15 V71 | LOGANTIG V76 |
|---|---|---|---|---|---|
| MEAN | 4.8235 | 4.4235 | 5.8059 | 5.7588 | 1.2075 |
| SKEWNESS (G1) | -.5256 | -.4133 | -1.4572 | -1.3098 | -.7551 |
| KURTOSIS (G2) | -.2772 | -.6250 | 2.0533 | 1.3013 | 1.3199 |
| STANDARD DEV. | 1.6900 | 1.9269 | 1.4567 | 1.4618 | .3556 |

| VARIABLE | LOGTAMA V79 |
|---|---|
| MEAN | 1.2278 |
| SKEWNESS (G1) | .7711 |
| KURTOSIS (G2) | 1.2529 |
| STANDARD DEV. | .6087 |

MULTIVARIATE KURTOSIS
---------------------

MARDIA'S COEFFICIENT (G2,P) = 41.9466
NORMALIZED ESTIMATE = 16.1699

ELLIPTICAL THEORY KURTOSIS ESTIMATES
------------------------------------

MARDIA-BASED KAPPA = .2933 MEAN SCALED UNIVARIATE KURTOSIS = .1291

MARDIA-BASED KAPPA IS USED IN COMPUTATION. KAPPA= .2933

CASE NUMBERS WITH LARGEST CONTRIBUTION TO NORMALIZED MULTIVARIATE KURTOSIS:
---------------------------------------------------------------------------

| CASE NUMBER | 1 | 22 | 63 | 85 | 169 |
|---|---|---|---|---|---|
| ESTIMATE | 430.1447 | 322.3794 | 306.5681 | 1139.1785 | 552.0069 |

05-Feb-18      PAGE :  4  EQS     Licensee:
TITLE:    Your EQS 6 Model

COVARIANCE  MATRIX TO BE ANALYZED:  11 VARIABLES (SELECTED FROM  80 VARIABLES)
BASED ON   170 CASES.

| | | P.1.9 | P.1.12 | P.9.3 | P.9.9 | P.9.10 |
|---|---|---|---|---|---|---|
| | | V9 | V12 | V59 | V65 | V66 |
| P.1.9 | V9 | 6.837 | | | | |
| P.1.12 | V12 | 3.704 | 8.057 | | | |
| P.9.3 | V59 | .336 | .371 | 1.132 | | |
| P.9.9 | V65 | 1.631 | 1.689 | .905 | 3.961 | |
| P.9.10 | V66 | .996 | 1.324 | 1.022 | 2.800 | 3.683 |
| P.9.12 | V68 | .479 | .480 | .733 | 1.843 | 2.049 |
| P.9.13 | V69 | 1.064 | .966 | .735 | 1.999 | 2.214 |
| P.9.14 | V70 | .077 | .321 | .890 | 1.373 | 1.561 |
| P.9.15 | V71 | .301 | .605 | .756 | 1.352 | 1.130 |
| LOGANTIG | V76 | .144 | .167 | .004 | .010 | -.042 |
| LOGTAMA | V79 | .586 | .807 | -.052 | .160 | .116 |

| | | P.9.12 | P.9.13 | P.9.14 | P.9.15 | LOGANTIG |
|---|---|---|---|---|---|---|
| | | V68 | V69 | V70 | V71 | V76 |
| P.9.12 | V68 | 2.856 | | | | |
| P.9.13 | V69 | 2.625 | 3.713 | | | |
| P.9.14 | V70 | 1.374 | 1.384 | 2.122 | | |
| P.9.15 | V71 | .963 | .984 | 1.308 | 2.137 | |
| LOGANTIG | V76 | -.030 | -.035 | -.008 | -.022 | .126 |
| LOGTAMA | V79 | .035 | .079 | .010 | .042 | .096 |

| | | LOGTAMA |
|---|---|---|
| | | V79 |
| LOGTAMA | V79 | .370 |

BENTLER-WEEKS STRUCTURAL REPRESENTATION:

NUMBER OF DEPENDENT VARIABLES = 15
DEPENDENT V'S :     9   12   59   65   66   68   69   70   71   76
DEPENDENT V'S :    79
DEPENDENT F'S :    12   13   14   15

NUMBER OF INDEPENDENT VARIABLES = 18
INDEPENDENT F'S :     4   16   17

```
            INDEPENDENT E'S :     9   12   59   65   66   68   69   70
71   76
            INDEPENDENT E'S :    79
            INDEPENDENT D'S :    12   13   14   15

        NUMBER OF FREE PARAMETERS =  29
        NUMBER OF FIXED NONZERO PARAMETERS =  22

 *** WARNING MESSAGES ABOVE, IF ANY, REFER TO THE MODEL PROVIDED.
     CALCULATIONS FOR INDEPENDENCE MODEL NOW BEGIN.

 *** WARNING MESSAGES ABOVE, IF ANY, REFER TO INDEPENDENCE MODEL.
     CALCULATIONS FOR USER'S MODEL NOW BEGIN.


  3RD STAGE OF COMPUTATION REQUIRED     64600 WORDS OF MEMORY.
  PROGRAM ALLOCATED 200000000 WORDS

  DETERMINANT OF INPUT MATRIX IS    .13409D+02

  PARAMETER ESTIMATES APPEAR IN ORDER,
  NO SPECIAL PROBLEMS WERE ENCOUNTERED DURING OPTIMIZATION.


  RESIDUAL COVARIANCE MATRIX  (S-SIGMA) :
```

| | | P.1.9 V9 | P.1.12 V12 | P.9.3 V59 | P.9.9 V65 | P.9.10 V66 |
|---|---|---|---|---|---|---|
| P.1.9 | V9 | .000 | | | | |
| P.1.12 | V12 | .000 | .000 | | | |
| P.9.3 | V59 | .018 | -.057 | .000 | | |
| P.9.9 | V65 | .780 | .544 | .044 | .000 | |
| P.9.10 | V66 | .082 | .095 | .098 | .000 | .000 |
| P.9.12 | V68 | -.226 | -.468 | .020 | -.067 | .000 |
| P.9.13 | V69 | .305 | -.054 | -.033 | -.056 | .009 |
| P.9.14 | V70 | -.465 | -.407 | -.021 | -.094 | -.012 |
| P.9.15 | V71 | -.146 | .002 | .003 | .139 | -.171 |
| LOGANTIG | V76 | .014 | -.008 | .013 | .036 | -.014 |
| LOGTAMA | V79 | -.010 | .006 | -.085 | .074 | .024 |

| | | P.9.12 V68 | P.9.13 V69 | P.9.14 V70 | P.9.15 V71 | LOGANTIG V76 |
|---|---|---|---|---|---|---|
| P.9.12 | V68 | .000 | | | | |
| P.9.13 | V69 | .000 | .000 | | | |
| P.9.14 | V70 | .159 | .077 | .000 | | |
| P.9.15 | V71 | -.041 | -.097 | .025 | .000 | |

| | | | | | | |
|---|---|---|---|---|---|---|
| LOGANTIG | V76 | -.009 | -.012 | .008 | -.009 | .000 |
| LOGTAMA | V79 | -.036 | .003 | -.044 | -.003 | .000 |

| | | LOGTAMA V79 |
|---|---|---|
| LOGTAMA | V79 | .000 |

AVERAGE ABSOLUTE COVARIANCE RESIDUALS = .0791

AVERAGE OFF-DIAGONAL ABSOLUTE COVARIANCE RESIDUALS = .0950

STANDARDIZED RESIDUAL MATRIX:

| | | P.1.9 V9 | P.1.12 V12 | P.9.3 V59 | P.9.9 V65 | P.9.10 V66 |
|---|---|---|---|---|---|---|
| P.1.9 | V9 | .000 | | | | |
| P.1.12 | V12 | .000 | .000 | | | |
| P.9.3 | V59 | .006 | -.019 | .000 | | |
| P.9.9 | V65 | .150 | .096 | .021 | .000 | |
| P.9.10 | V66 | .016 | .018 | .048 | .000 | .000 |
| P.9.12 | V68 | -.051 | -.098 | .011 | -.020 | .000 |
| P.9.13 | V69 | .060 | -.010 | -.016 | -.015 | .002 |
| P.9.14 | V70 | -.122 | -.099 | -.013 | -.032 | -.004 |
| P.9.15 | V71 | -.038 | .001 | .002 | .048 | -.061 |
| LOGANTIG | V76 | .015 | -.008 | .035 | .051 | -.021 |
| LOGTAMA | V79 | -.006 | .003 | -.131 | .061 | .021 |

| | | P.9.12 V68 | P.9.13 V69 | P.9.14 V70 | P.9.15 V71 | LOGANTIG V76 |
|---|---|---|---|---|---|---|
| P.9.12 | V68 | .000 | | | | |
| P.9.13 | V69 | .000 | .000 | | | |
| P.9.14 | V70 | .065 | .027 | .000 | | |
| P.9.15 | V71 | -.017 | -.034 | .012 | .000 | |
| LOGANTIG | V76 | -.015 | -.018 | .016 | -.016 | .000 |
| LOGTAMA | V79 | -.035 | .002 | -.050 | -.003 | .000 |

| | | LOGTAMA V79 |
|---|---|---|
| LOGTAMA | V79 | .000 |

```
                    AVERAGE ABSOLUTE STANDARDIZED RESIDUALS     =
.0263
        AVERAGE OFF-DIAGONAL ABSOLUTE STANDARDIZED RESIDUALS     =
.0316


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  LARGEST STANDARDIZED RESIDUALS:

      NO.    PARAMETER   ESTIMATE      NO.    PARAMETER   ESTIMATE
      ---    ---------   --------      ---    ---------   --------
       1     V65, V9        .150       11     V68, V9       -.051
       2     V79, V59      -.131       12     V76, V65       .051
       3     V70, V9       -.122       13     V79, V70      -.050
       4     V70, V12      -.099       14     V66, V59       .048
       5     V68, V12      -.098       15     V71, V65       .048
       6     V65, V12       .096       16     V71, V9       -.038
       7     V70, V68       .065       17     V79, V68      -.035
       8     V79, V65       .061       18     V76, V59       .035
       9     V71, V66      -.061       19     V71, V69      -.034
      10     V69, V9        .060       20     V70, V65      -.032


  DISTRIBUTION OF STANDARDIZED RESIDUALS



     ----------------------------------------
     !                                       !
   40-                                       -
     !                                       !
     !                                       !
     !                    *                  !
     !                    *                  !           RANGE       FREQ
PERCENT
   30-                 *  *                  -
     !                 *  *                  !    1    -0.5  -  --         0
.00%
     !                 *  *                  !    2    -0.4  -  -0.5       0
.00%
     !                 *  *                  !    3    -0.3  -  -0.4       0
.00%
     !                 *  *                  !    4    -0.2  -  -0.3       0
.00%
   20-                 *  *                  -    5    -0.1  -  -0.2       2
3.03%
     !                 *  *                  !    6     0.0  -  -0.1      30
45.45%
     !                 *  *                  !    7     0.1  -   0.0      33
50.00%
```

```
     !                 *  *                !    8    0.2  -   0.1     1
1.52%
     !                 *  *                !    9    0.3  -   0.2     0
.00%
   10-                 *  *                -    A    0.4  -   0.3     0
.00%
     !                 *  *                !    B    0.5  -   0.4     0
.00%
     !                 *  *                !    C     ++  -   0.5     0
.00%
     !                 *  *                !    -----------------------
-------
     !              *  *  *  *             !            TOTAL        66
100.00%
     ----------------------------------------
        1  2  3  4  5  6  7  8  9  A  B  C      EACH "*" REPRESENTS  2
RESIDUALS


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)



  GOODNESS OF FIT SUMMARY FOR METHOD = ML

  INDEPENDENCE MODEL CHI-SQUARE        =     849.987 ON    57 DEGREES OF
FREEDOM

  INDEPENDENCE AIC =   735.98663   INDEPENDENCE CAIC =   500.24612
         MODEL AIC =   -20.49863          MODEL CAIC =  -173.52317

  CHI-SQUARE =       53.501 BASED ON      37 DEGREES OF FREEDOM
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .03877

  THE NORMAL THEORY RLS CHI-SQUARE FOR THIS ML SOLUTION IS
52.687.

  FIT INDICES
  -----------
  BENTLER-BONETT     NORMED FIT INDEX =      .937
  BENTLER-BONETT NON-NORMED FIT INDEX =      .968
  COMPARATIVE FIT INDEX (CFI)         =      .979
  BOLLEN   (IFI) FIT INDEX            =      .980
  MCDONALD (MFI) FIT INDEX            =      .953
  LISREL    GFI  FIT INDEX            =      .946
  LISREL   AGFI  FIT INDEX            =      .904
  ROOT MEAN-SQUARE RESIDUAL (RMR)     =      .167
  STANDARDIZED RMR                    =      .043
  ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .051
  90% CONFIDENCE INTERVAL OF RMSEA  (        .012,        .080)

  RELIABILITY COEFFICIENTS
  ------------------------
  CRONBACH'S ALPHA                    =      .799
  COEFFICIENT ALPHA FOR AN OPTIMAL SHORT SCALE                =      .879
```

```
  BASED ON  7 VARIABLES, ALL EXCEPT:
  P.1.9     P.1.12    LOGANTIG  LOGTAMA
  RELIABILITY COEFFICIENT RHO          =      .900
  GREATEST LOWER BOUND RELIABILITY                            =      .914
  GLB RELIABILITY FOR AN OPTIMAL SHORT SCALE                  =      .941
  BASED ON  9 VARIABLES, ALL EXCEPT:
  P.1.9     P.1.12
  BENTLER'S DIMENSION-FREE LOWER BOUND RELIABILITY            =      .914
  SHAPIRO'S LOWER BOUND RELIABILITY FOR A WEIGHTED COMPOSITE  =      .945
  WEIGHTS THAT ACHIEVE SHAPIRO'S LOWER BOUND:
  P.1.9     P.1.12    P.9.3     P.9.9     P.9.10    P.9.12
      .151      .151      .190      .419      .438      .430
  P.9.13    P.9.14    P.9.15    LOGANTIG  LOGTAMA
      .447      .301      .267      .001      .061


  GOODNESS OF FIT SUMMARY FOR METHOD = ROBUST

  ROBUST INDEPENDENCE MODEL CHI-SQUARE =     699.801 ON    57 DEGREES OF
FREEDOM

  INDEPENDENCE AIC =   585.80147   INDEPENDENCE CAIC =   350.06096
         MODEL AIC =   -28.00884          MODEL CAIC =  -181.03338

  SATORRA-BENTLER SCALED CHI-SQUARE =     45.9912 ON      37 DEGREES OF
FREEDOM
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .14756

  RESIDUAL-BASED TEST STATISTIC                    =    50.776
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .06520

  YUAN-BENTLER RESIDUAL-BASED TEST STATISTIC       =    39.098
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .37576

  YUAN-BENTLER RESIDUAL-BASED F-STATISTIC     =      1.080
  DEGREES OF FREEDOM  =                          37,   133
  PROBABILITY VALUE FOR THE F-STATISTIC IS          .36565

  FIT INDICES
  -----------
  BENTLER-BONETT     NORMED FIT INDEX =      .934
  BENTLER-BONETT NON-NORMED FIT INDEX =      .978
  COMPARATIVE FIT INDEX (CFI)         =      .986
  BOLLEN   (IFI) FIT INDEX            =      .986
  MCDONALD (MFI) FIT INDEX            =      .974
  ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .038
  90% CONFIDENCE INTERVAL OF RMSEA  (        .000,        .070)


                         ITERATIVE SUMMARY

                   PARAMETER
  ITERATION        ABS CHANGE          ALPHA                 FUNCTION
      1             1.318797         1.00000                 1.72791
      2              .440521         1.00000                  .82999
      3              .124905         1.00000                  .45756
```

```
     4                .048707         1.00000                 .32292
     5                .014345         1.00000                 .31666
     6                .002880         1.00000                 .31658
     7                .000740         1.00000                 .31658
```

```
05-Feb-18      PAGE :  7  EQS     Licensee:
  TITLE:    Your EQS 6 Model

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
  (ROBUST STATISTICS IN PARENTHESES)


 P.1.9   =V9  =   1.000 F4    + 1.000 E9




 P.1.12  =V12 =   1.345*F4    + 1.000 E12
                   .232
                  5.795@
               (   .185)
               (  7.266@

 P.9.3   =V59 =    .587*F12   + 1.000 E59
                   .067
                  8.820@
               (   .083)
               (  7.044@

 P.9.9   =V65 =   1.000 F14   + 1.000 E65




 P.9.10  =V66 =   1.073*F14   + 1.000 E66
                   .090
                 11.958@
               (   .091)
               ( 11.758@

 P.9.12  =V68 =   1.000 F13   + 1.000 E68




 P.9.13  =V69 =   1.076*F13   + 1.000 E69
                   .079
                 13.540@
               (   .087)
               ( 12.309@
```

```
 P.9.14  =V70 =   1.000 F12   + 1.000 E70



 P.9.15  =V71 =    .827*F12   + 1.000 E71
                   .091
                  9.049@
               (   .110)
               (  7.526@

 LOGANTIG=V76 =   1.000 F17   + 1.000 E76



 LOGTAMA =V79 =   1.000 F16   + 1.000 E79




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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  CONSTRUCT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
  (ROBUST STATISTICS IN PARENTHESES)


    F12  =F12 =   1.000 F15   + 1.000 D12



    F13  =F13 =   1.302*F15   + 1.000 D13
                   .162
                  8.041@
               (   .155)
               (  8.412@

    F14  =F14 =   1.572*F15   + 1.000 D14
                   .210
                  7.488@
               (   .254)
               (  6.195@

    F15  =F15 =    .249*F4    -  .191*F16   -  .240*F17   + 1.000 D15
```

```
                  .086          .201          .249
                 2.911@        -.954         -.966
              (   .093)     (   .211)     (   .281)
              (  2.678@     (  -.905)     (  -.855)


05-Feb-18      PAGE :  9  EQS     Licensee:
  TITLE:    Your EQS 6 Model

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES
  ----------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                 V                                F
                ---                              ---
                             I F4  -   F4               2.755*I
                             I                           .727 I
                             I                          3.789@I
                             I                       (   .614)I
                             I                       (  4.484@I
                             I                                I
                             I F16 -   F16               .370*I
                             I                           .040 I
                             I                          9.192@I
                             I                       (   .051)I
                             I                       (  7.251@I
                             I                                I
                             I F17 -   F17               .126*I
                             I                           .014 I
                             I                          9.192@I
                             I                       (   .018)I
                             I                       (  7.177@I
                             I                                I


05-Feb-18      PAGE : 10  EQS     Licensee:
  TITLE:    Your EQS 6 Model

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES
  ----------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                 E                                D
                ---                              ---
 E9  -P.1.9               4.082*I D12 -   F12                .619*I
                           .608 I                           .151 I
                          6.710@I                          4.105@I
                       (   .571)I                       (   .181)I
                       (  7.149@I                       (  3.423@I
                                I                                I
 E12 -P.1.12              3.077*I D13 -   F13                .858*I
                           .823 I                           .197 I
                          3.739@I                          4.346@I
                       (   .878)I                       (   .253)I
```

```
                       (   3.504@I                          (   3.390@I
                                 I                                    I
 E59 -P.9.3                 .598*I D14 -   F14                  .303*I
                            .079 I                              .216 I
                           7.593@I                             1.406 I
                       (    .096)I                          (    .327)I
                       (   6.209@I                          (    .927)I
                                 I                                    I
 E65 -P.9.9                1.351*I D15 -   F15                  .805*I
                            .210 I                              .184 I
                           6.445@I                             4.365@I
                       (    .366)I                          (    .236)I
                       (   3.688@I                          (   3.413@I
                                 I                                    I
 E66 -P.9.10                .679*I                                    I
                            .187 I                                    I
                           3.627@I                                    I
                       (    .189)I                                    I
                       (   3.592@I                                    I
                                 I                                    I
 E68 -P.9.12                .417*I                                    I
                            .139 I                                    I
                           2.998@I                                    I
                       (    .194)I                                    I
                       (   2.153@I                                    I
                                 I                                    I
 E69 -P.9.13                .887*I                                    I
                            .180 I                                    I
                           4.923@I                                    I
                       (    .315)I                                    I
                       (   2.814@I                                    I
                                 I                                    I
 E70 -P.9.14                .570*I                                    I
                            .128 I                                    I
                           4.457@I                                    I
                       (    .205)I                                    I
                       (   2.778@I                                    I
                                 I                                    I
 E71 -P.9.15               1.076*I                                    I
                            .145 I                                    I
                           7.412@I                                    I
                       (    .284)I                                    I
                       (   3.786@I                                    I
                                 I                                    I


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  COVARIANCES AMONG INDEPENDENT VARIABLES
  ---------------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                 V                                 F
                ---                               ---
                                 I F16 -   F16                  .596*I
```

```
                                      I F4  -   F4              .127 I
                                      I                        4.706@I
                                      I                     (   .117)I
                                      I                     (  5.085@I
                                      I                              I
                                      I F17 -   F17             .130*I
                                      I F4  -   F4              .058 I
                                      I                        2.263@I
                                      I                     (   .058)I
                                      I                     (  2.229@I
                                      I                              I
                                      I F17 -   F17             .096*I
                                      I F16 -   F16             .018 I
                                      I                        5.276@I
                                      I                     (   .019)I
                                      I                     (  5.136@I
                                      I                              I


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  STANDARDIZED SOLUTION:                                                  R-
SQUARED

 P.1.9   =V9  =   .635 F4    + .773 E9
.403
 P.1.12  =V12 =   .786*F4    + .618 E12
.618
 P.9.3   =V59 =   .687*F12   + .727 E59
.472
 P.9.9   =V65 =   .812 F14   + .584 E65
.659
 P.9.10  =V66 =   .903*F14   + .429 E66
.816
 P.9.12  =V68 =   .924 F13   + .382 E68
.854
 P.9.13  =V69 =   .872*F13   + .489 E69
.761
 P.9.14  =V70 =   .855 F12   + .518 E70
.731
 P.9.15  =V71 =   .705*F12   + .710 E71
.496
 LOGANTIG=V76 =  1.000 F17   + .000 E76
1.000
 LOGTAMA =V79 =  1.000 F16   + .000 E79
1.000
    F12  =F12 =   .775 F15   + .631 D12
.601
    F13  =F13 =   .805*F15   + .593 D13
.648
    F14  =F14 =   .940*F15   + .341 D14
.884
    F15  =F15 =   .429*F4    - .121*F16   - .088*F17   + .929 D15
.138
```

```
05-Feb-18      PAGE : 13  EQS     Licensee:
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  CORRELATIONS AMONG INDEPENDENT VARIABLES
  ---------------------------------------

                 V                                F
                ---                              ---
                              I F16 -   F16              .590*I
                              I F4  -   F4                    I
                              I                               I
                              I F17 -   F17              .221*I
                              I F4  -   F4                    I
                              I                               I
                              I F17 -   F17              .444*I
                              I F16 -   F16                   I
                              I                               I




 -----------------------------------------------------------------------
-------
                           E N D    O F    M E T H O D
 -----------------------------------------------------------------------
-------
1
  Execution begins at 14:18:02
  Execution ends   at 14:18:02
  Elapsed time =        .00 seconds
```

# ANEXO XIX

# MODELO EFECTO MEDIADOR DE LA FLEXIBILIDAD EXTERNA DE LA ESTRUCTURA – MODELO B

```
1
  EQS, A STRUCTURAL EQUATION PROGRAM          MULTIVARIATE SOFTWARE, INC.
  COPYRIGHT BY P.M. BENTLER                   VERSION 6.1 (C) 1985 - 2005
(B85).


    PROGRAM CONTROL INFORMATION

        /TITLE
         Your EQS 6 Model
        /SPECIFICATIONS
        VARIABLES= 80 ; CASES= 170 ;
        DATA='C:\tesis1\ticflexrdoscontroltotal.ESS';
        MATRIX=RAW;METHOD=ML,robust;
        /LABELS
        V1=P.1.1; V2=P.1.2; V3=P.1.3; V4=P.1.4; V5=P.1.5;
        V6=P.1.6; V7=P.1.7; V8=P.1.8; V9=P.1.9; V10=P.1.10;
        V11=P.1.11; V12=P.1.12; V13=P.1.13; V14=P.1.14; V15=P.1.15;
        V16=P.1.16; V17=P.1.17; V18=P.2.1; V19=P.2.2; V20=P.2.3;
        V21=P.2.4; V22=P.2.5; V23=P.2.6; V24=P.2.7; V25=P.2.8;
        V26=P.2.9; V27=P.2.10; V28=P.2.11; V29=P.2.12; V30=P.2.13;
        V31=P.2.14; V32=P.2.15; V33=P.3.1; V34=P.3.2; V35=P.3.3;
        V36=P.4.1; V37=P.4.2; V38=P.4.3; V39=P.4.4; V40=P.4.5;
        V41=P.4.6; V42=P.4.7; V43=P.4.8; V44=P.4.9; V45=P.4.10;
        V46=P.4.11; V47=P.6.1; V48=P.6.2; V49=P.6.3; V50=P.6.4;
        V51=P.6.5; V52=P.6.6; V53=P.6.7; V54=P.6.8; V55=P.6.9;
        V56=P.6.10; V57=P.9.1; V58=P.9.2; V59=P.9.3; V60=P.9.4;
        V61=P.9.5; V62=P.9.6; V63=P.9.7; V64=P.9.8; V65=P.9.9;
        V66=P.9.10; V67=P.9.11; V68=P.9.12; V69=P.9.13; V70=P.9.14;
        V71=P.9.15; V72=P.9.16; V73=P.9.17;
        V74=P.11.1; V75=ANTIGUED; V76=LOGANTIG; V77=RAIZANTI; V78=P.10.1;
        V79=LOGTAMA; V80=RAIZTAMA;

        /EQUATIONS
        V9 =   1F4 + E9;
        V12 =   *F4 + E12;
        V47 =   1F10 + E47;
        V48 =   *F10 + E48;
        V49 =   *F10 + E49;
        V50 =   *F10 + E50;
        V51 =   *F10 + E51;
        V59 =   *F12 + E59;
        V65 =   1F14 + E65;
        V66 =   *F14 + E66;
        V68 =   1F13 + E68;
        V69 =   *F13 + E69;
        V70 =   1F12 + E70;
        V71 =   *F12 + E71;
        V76 =   F17 + E76;
        V79 =   F16 + E79;
        F10 =   *F4 + D10;
        F12 =   1F15 + D12;
        F13 =   *F15 + D13;
        F14 =   *F15 + D14;
```

```
F15 =   *F10 + *F16 + *F17 + D15;
/VARIANCES

 F4 = *;
 E9 = *;
 F16=*;


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 F17=*;
 E47 = *;
 E48 = *;
 E49 = *;
 E50 = *;
 E51 = *;
 E59 = *;
 E65 = *;
 E66 = *;
 E68 = *;
 E69 = *;
 E70 = *;
 E71 = *;
 E76 = 0;
 E79 = 0;
 D10 = *;
 D12 = *;
 D13 = *;
 D14 = *;
 D15 = *;
/COVARIANCES
 F4,F16 = *;
 F4,F17 = *;
 F16,F17 = *;
/PRINT
FIT=ALL;
TABLE=EQUATION;
/END


       80 RECORDS OF INPUT MODEL FILE WERE READ


    DATA IS READ FROM C:\tesis1\ticflexrdoscontroltotal.ESS
    THERE ARE  80 VARIABLES AND   170 CASES
    IT IS A RAW DATA ESS FILE


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  SAMPLE STATISTICS BASED ON COMPLETE CASES


                           UNIVARIATE STATISTICS
                           ---------------------
```

| VARIABLE | P.1.9<br>V9 | P.1.12<br>V12 | P.6.1<br>V47 | P.6.2<br>V48 | P.6.3<br>V49 |
|---|---|---|---|---|---|
| MEAN | 2.3647 | 2.3706 | 2.8294 | 2.9235 | 2.5529 |
| SKEWNESS (G1) | .6639 | .6738 | .3455 | .2227 | .5477 |
| KURTOSIS (G2) | -1.0669 | -1.2320 | -1.0645 | -1.0536 | -.9088 |
| STANDARD DEV. | 2.6147 | 2.8385 | 2.3282 | 2.2241 | 2.3077 |

| VARIABLE | P.6.4<br>V50 | P.6.5<br>V51 | P.9.3<br>V59 | P.9.9<br>V65 | P.9.10<br>V66 |
|---|---|---|---|---|---|
| MEAN | 2.3765 | 2.1118 | 6.1647 | 4.1824 | 4.5118 |
| SKEWNESS (G1) | .4525 | .8085 | -1.6316 | -.3570 | -.5772 |
| KURTOSIS (G2) | -.9277 | -.5685 | 2.6761 | -.7646 | -.3762 |
| STANDARD DEV. | 2.1810 | 2.2544 | 1.0642 | 1.9901 | 1.9192 |

| VARIABLE | P.9.12<br>V68 | P.9.13<br>V69 | P.9.14<br>V70 | P.9.15<br>V71 | LOGANTIG<br>V76 |
|---|---|---|---|---|---|
| MEAN | 4.8235 | 4.4235 | 5.8059 | 5.7588 | 1.2075 |
| SKEWNESS (G1) | -.5256 | -.4133 | -1.4572 | -1.3098 | -.7551 |
| KURTOSIS (G2) | -.2772 | -.6250 | 2.0533 | 1.3013 | 1.3199 |
| STANDARD DEV. | 1.6900 | 1.9269 | 1.4567 | 1.4618 | .3556 |

| VARIABLE | LOGTAMA<br>V79 |
|---|---|
| MEAN | 1.2278 |
| SKEWNESS (G1) | .7711 |
| KURTOSIS (G2) | 1.2529 |
| STANDARD DEV. | .6087 |

MULTIVARIATE KURTOSIS
---------------------

MARDIA'S COEFFICIENT (G2,P) = 54.1238
NORMALIZED ESTIMATE = 14.7018

ELLIPTICAL THEORY KURTOSIS ESTIMATES
------------------------------------

MARDIA-BASED KAPPA = .1879 MEAN SCALED UNIVARIATE KURTOSIS = -.0054

MARDIA-BASED KAPPA IS USED IN COMPUTATION. KAPPA= .1879

CASE NUMBERS WITH LARGEST CONTRIBUTION TO NORMALIZED MULTIVARIATE KURTOSIS:

---

| | | | | | |
|---|---|---|---|---|---|
| CASE NUMBER | 1 | 85 | 125 | 150 | 169 |
| ESTIMATE | 356.5668 | 1212.0287 | 368.1973 | 349.1001 | 383.1531 |

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COVARIANCE MATRIX TO BE ANALYZED: 16 VARIABLES (SELECTED FROM 80 VARIABLES)
BASED ON 170 CASES.

| | | P.1.9 V9 | P.1.12 V12 | P.6.1 V47 | P.6.2 V48 | P.6.3 V49 |
|---|---|---|---|---|---|---|
| P.1.9 | V9 | 6.837 | | | | |
| P.1.12 | V12 | 3.704 | 8.057 | | | |
| P.6.1 | V47 | 2.145 | 2.614 | 5.420 | | |
| P.6.2 | V48 | 1.430 | 2.484 | 3.218 | 4.947 | |
| P.6.3 | V49 | 2.347 | 3.285 | 3.124 | 3.427 | 5.326 |
| P.6.4 | V50 | 1.891 | 2.262 | 2.976 | 2.609 | 2.731 |
| P.6.5 | V51 | 1.995 | 2.615 | 2.972 | 2.991 | 3.547 |
| P.9.3 | V59 | .336 | .371 | .312 | .415 | .488 |
| P.9.9 | V65 | 1.631 | 1.689 | 1.469 | 1.943 | 1.916 |
| P.9.10 | V66 | .996 | 1.324 | 1.532 | 1.797 | 1.348 |
| P.9.12 | V68 | .479 | .480 | .804 | .910 | .962 |
| P.9.13 | V69 | 1.064 | .966 | 1.173 | 1.098 | .912 |
| P.9.14 | V70 | .077 | .321 | .730 | .944 | .552 |
| P.9.15 | V71 | .301 | .605 | .734 | .881 | .803 |
| LOGANTIG | V76 | .144 | .167 | .006 | .003 | -.079 |
| LOGTAMA | V79 | .586 | .807 | .256 | .261 | .283 |

| | | P.6.4 V50 | P.6.5 V51 | P.9.3 V59 | P.9.9 V65 | P.9.10 V66 |
|---|---|---|---|---|---|---|
| P.6.4 | V50 | 4.757 | | | | |
| P.6.5 | V51 | 2.952 | 5.082 | | | |
| P.9.3 | V59 | .198 | .337 | 1.132 | | |
| P.9.9 | V65 | 1.097 | 1.772 | .905 | 3.961 | |
| P.9.10 | V66 | .990 | 1.303 | 1.022 | 2.800 | 3.683 |
| P.9.12 | V68 | .540 | .848 | .733 | 1.843 | 2.049 |
| P.9.13 | V69 | .934 | 1.083 | .735 | 1.999 | 2.214 |
| P.9.14 | V70 | .322 | .507 | .890 | 1.373 | 1.561 |
| P.9.15 | V71 | .476 | .642 | .756 | 1.352 | 1.130 |
| LOGANTIG | V76 | -.032 | .002 | .004 | .010 | -.042 |
| LOGTAMA | V79 | .220 | .237 | -.052 | .160 | .116 |

| | | P.9.12 V68 | P.9.13 V69 | P.9.14 V70 | P.9.15 V71 | LOGANTIG V76 |
|---|---|---|---|---|---|---|
| P.9.12 | V68 | 2.856 | | | | |
| P.9.13 | V69 | 2.625 | 3.713 | | | |
| P.9.14 | V70 | 1.374 | 1.384 | 2.122 | | |
| P.9.15 | V71 | .963 | .984 | 1.308 | 2.137 | |
| LOGANTIG | V76 | -.030 | -.035 | -.008 | -.022 | .126 |
| LOGTAMA | V79 | .035 | .079 | .010 | .042 | .096 |

| | | LOGTAMA V79 |
|---|---|---|
| LOGTAMA | V79 | .370 |

BENTLER-WEEKS STRUCTURAL REPRESENTATION:

NUMBER OF DEPENDENT VARIABLES = 21
DEPENDENT V'S : 9 12 47 48 49 50 51 59 65 66
DEPENDENT V'S : 68 69 70 71 76 79
DEPENDENT F'S : 10 12 13 14 15

NUMBER OF INDEPENDENT VARIABLES = 24
INDEPENDENT F'S : 4 16 17
INDEPENDENT E'S : 9 12 47 48 49 50 51 59 65 66
INDEPENDENT E'S : 68 69 70 71 76 79
INDEPENDENT D'S : 10 12 13 14 15

NUMBER OF FREE PARAMETERS = 40
NUMBER OF FIXED NONZERO PARAMETERS = 29

*** WARNING MESSAGES ABOVE, IF ANY, REFER TO THE MODEL PROVIDED.
CALCULATIONS FOR INDEPENDENCE MODEL NOW BEGIN.

*** WARNING MESSAGES ABOVE, IF ANY, REFER TO INDEPENDENCE MODEL.
CALCULATIONS FOR USER'S MODEL NOW BEGIN.

3RD STAGE OF COMPUTATION REQUIRED 237396 WORDS OF MEMORY.
PROGRAM ALLOCATED 200000000 WORDS

DETERMINANT OF INPUT MATRIX IS .15810D+04

PARAMETER ESTIMATES APPEAR IN ORDER,
NO SPECIAL PROBLEMS WERE ENCOUNTERED DURING OPTIMIZATION.

RESIDUAL COVARIANCE MATRIX (S-SIGMA) :

| | | P.1.9<br>V9 | P.1.12<br>V12 | P.6.1<br>V47 | P.6.2<br>V48 | P.6.3<br>V49 |
|---|---|---|---|---|---|---|
| P.1.9 | V9 | .000 | | | | |
| P.1.12 | V12 | -.149 | .000 | | | |
| P.6.1 | V47 | .361 | -.011 | .000 | | |
| P.6.2 | V48 | -.372 | -.167 | .154 | .000 | |
| P.6.3 | V49 | .393 | .411 | -.197 | .072 | .000 |
| P.6.4 | V50 | .316 | -.055 | .298 | -.096 | -.201 |
| P.6.5 | V51 | .166 | -.074 | -.137 | -.149 | .144 |
| P.9.3 | V59 | .068 | -.024 | -.154 | -.056 | -.023 |
| P.9.9 | V65 | .884 | .590 | .169 | .630 | .493 |
| P.9.10 | V66 | .206 | .163 | .159 | .410 | -.155 |
| P.9.12 | V68 | -.112 | -.389 | -.224 | -.129 | -.164 |
| P.9.13 | V69 | .429 | .032 | .069 | -.018 | -.297 |
| P.9.14 | V70 | -.379 | -.350 | -.063 | .143 | -.317 |
| P.9.15 | V71 | -.078 | .046 | .074 | .214 | .080 |
| LOGANTIG | V76 | .048 | .026 | -.060 | -.063 | -.150 |
| LOGTAMA | V79 | .059 | .032 | -.103 | -.102 | -.111 |

| | | P.6.4<br>V50 | P.6.5<br>V51 | P.9.3<br>V59 | P.9.9<br>V65 | P.9.10<br>V66 |
|---|---|---|---|---|---|---|
| P.6.4 | V50 | .000 | | | | |
| P.6.5 | V51 | .208 | .000 | | | |
| P.9.3 | V59 | -.214 | -.141 | .002 | | |
| P.9.9 | V65 | -.051 | .440 | .033 | .012 | |

```
     P.9.10   V66          -.222      -.103       .101       .013
.013
     P.9.12   V68          -.367      -.205       .044      -.078
.021
     P.9.13   V69          -.041      -.049      -.006      -.064
.035
     P.9.14   V70          -.378      -.306      -.015      -.109      -
.003
     P.9.15   V71          -.107      -.034       .002       .118      -
.173
     LOGANTIG V76          -.090      -.066       .001       .004      -
.048
     LOGTAMA  V79          -.097      -.131      -.100       .028      -
.023


                       P.9.12     P.9.13     P.9.14     P.9.15
LOGANTIG
                          V68        V69        V70        V71        V76
     P.9.12   V68           .007
     P.9.13   V69           .008       .009
     P.9.14   V70           .202       .126       .004
     P.9.15   V71          -.012      -.064       .026       .003
     LOGANTIG V76          -.035      -.041      -.012      -.025
.000
     LOGTAMA  V79          -.069      -.032      -.070      -.025
.000


                       LOGTAMA
                          V79
     LOGTAMA  V79           .000


                     AVERAGE ABSOLUTE  COVARIANCE  RESIDUALS     =
.1289
        AVERAGE OFF-DIAGONAL ABSOLUTE  COVARIANCE  RESIDUALS     =
.1457


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  STANDARDIZED RESIDUAL MATRIX:


                       P.1.9      P.1.12     P.6.1      P.6.2      P.6.3
                          V9         V12        V47        V48        V49
     P.1.9    V9            .000
     P.1.12   V12          -.020       .000
     P.6.1    V47           .059      -.002       .000
     P.6.2    V48          -.064      -.026       .030       .000
     P.6.3    V49           .065       .063      -.037       .014
.000
```

| | | | | | | |
|---|---|---|---|---|---|---|
| P.6.4 | V50 | .055 | -.009 | .059 | -.020 | -.040 |
| P.6.5 | V51 | .028 | -.012 | -.026 | -.030 | .028 |
| P.9.3 | V59 | .024 | -.008 | -.062 | -.024 | -.009 |
| P.9.9 | V65 | .170 | .104 | .036 | .142 | .107 |
| P.9.10 | V66 | .041 | .030 | .036 | .096 | -.035 |
| P.9.12 | V68 | -.025 | -.081 | -.057 | -.034 | -.042 |
| P.9.13 | V69 | .085 | .006 | .015 | -.004 | -.067 |
| P.9.14 | V70 | -.099 | -.085 | -.019 | .044 | -.094 |
| P.9.15 | V71 | -.020 | .011 | .022 | .066 | .024 |
| LOGANTIG | V76 | .052 | .026 | -.072 | -.080 | -.183 |
| LOGTAMA | V79 | .037 | .018 | -.073 | -.075 | -.079 |

| | | P.6.4 V50 | P.6.5 V51 | P.9.3 V59 | P.9.9 V65 | P.9.10 V66 |
|---|---|---|---|---|---|---|
| P.6.4 | V50 | .000 | | | | |
| P.6.5 | V51 | .042 | .000 | | | |
| P.9.3 | V59 | -.092 | -.059 | .001 | | |
| P.9.9 | V65 | -.012 | .098 | .016 | .003 | |
| P.9.10 | V66 | -.053 | -.024 | .050 | .003 | .004 |
| P.9.12 | V68 | -.100 | -.054 | .025 | -.023 | .006 |
| P.9.13 | V69 | -.010 | -.011 | -.003 | -.017 | .009 |
| P.9.14 | V70 | -.119 | -.093 | -.010 | -.038 | -.001 |
| P.9.15 | V71 | -.034 | -.010 | .001 | .041 | -.062 |
| LOGANTIG | V76 | -.116 | -.082 | .003 | .006 | -.071 |
| LOGTAMA | V79 | -.073 | -.096 | -.154 | .023 | -.019 |

| | | P.9.12 V68 | P.9.13 V69 | P.9.14 V70 | P.9.15 V71 | LOGANTIG V76 |
|---|---|---|---|---|---|---|
| P.9.12 | V68 | .003 | | | | |
| P.9.13 | V69 | .002 | .002 | | | |
| P.9.14 | V70 | .082 | .045 | .002 | | |
| P.9.15 | V71 | -.005 | -.023 | .012 | .001 | |
| LOGANTIG | V76 | -.058 | -.059 | -.023 | -.049 | .000 |
| LOGTAMA | V79 | -.067 | -.028 | -.079 | -.028 | .000 |

```
                       LOGTAMA
                          V79
     LOGTAMA   V79         .000


                     AVERAGE ABSOLUTE STANDARDIZED RESIDUALS     =
.0407
        AVERAGE OFF-DIAGONAL ABSOLUTE STANDARDIZED RESIDUALS     =
.0460


  LARGEST STANDARDIZED RESIDUALS:

      NO.     PARAMETER   ESTIMATE      NO.     PARAMETER   ESTIMATE
      ---     ---------   --------      ---     ---------   --------
       1      V76, V49       -.183      11      V65, V51        .098
       2      V65, V9         .170      12      V66, V48        .096
       3      V79, V59       -.154      13      V79, V51       -.096
       4      V65, V48        .142      14      V70, V49       -.094
       5      V70, V50       -.119      15      V70, V51       -.093
       6      V76, V50       -.116      16      V59, V50       -.092
       7      V65, V49        .107      17      V69, V9         .085
       8      V65, V12        .104      18      V70, V12       -.085
       9      V68, V50       -.100      19      V70, V68        .082
      10      V70, V9        -.099      20      V76, V51       -.082

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  DISTRIBUTION OF STANDARDIZED RESIDUALS



     ----------------------------------------
     !                                      !
   80-                                      -
     !                                      !
     !                 *                    !
     !                 *                    !
     !                 *                    !           RANGE      FREQ
PERCENT
   60-                 *                    -
     !                 *  *                 !    1    -0.5  -  --        0
.00%
     !                 *  *                 !    2    -0.4  -  -0.5      0
.00%
     !                 *  *                 !    3    -0.3  -  -0.4      0
.00%
     !                 *  *                 !    4    -0.2  -  -0.3      0
.00%
   40-                 *  *                 -    5    -0.1  -  -0.2      4
2.94%
```

```
     !                 *  *                !    6    0.0  -  -0.1    72
52.94%
     !                 *  *                !    7    0.1  -   0.0    56
41.18%
     !                 *  *                !    8    0.2  -   0.1     4
2.94%
     !                 *  *                !    9    0.3  -   0.2     0
.00%
   20-                 *  *                -    A    0.4  -   0.3     0
.00%
     !                 *  *                !    B    0.5  -   0.4     0
.00%
     !                 *  *                !    C     ++  -   0.5     0
.00%
     !                 *  *                !    ------------------------
-------
     !              *  *  *  *             !            TOTAL       136
100.00%
     ----------------------------------------
        1  2  3  4  5  6  7  8  9  A  B  C      EACH "*" REPRESENTS  4
RESIDUALS


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)



  GOODNESS OF FIT SUMMARY FOR METHOD = ML

  INDEPENDENCE MODEL CHI-SQUARE        =    1420.676 ON   122 DEGREES OF
FREEDOM

  INDEPENDENCE AIC =  1176.67640   INDEPENDENCE CAIC =   672.10899
         MODEL AIC =   -54.82229          MODEL CAIC =  -451.85894

  CHI-SQUARE =      137.178 BASED ON      96 DEGREES OF FREEDOM
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00373

  THE NORMAL THEORY RLS CHI-SQUARE FOR THIS ML SOLUTION IS
128.260.

  FIT INDICES
  -----------
  BENTLER-BONETT     NORMED FIT INDEX =      .903
  BENTLER-BONETT NON-NORMED FIT INDEX =      .960
  COMPARATIVE FIT INDEX (CFI)        =      .968
  BOLLEN   (IFI) FIT INDEX           =      .969
  MCDONALD (MFI) FIT INDEX           =      .886
  LISREL    GFI  FIT INDEX           =      .913
  LISREL   AGFI  FIT INDEX           =      .877
  ROOT MEAN-SQUARE RESIDUAL (RMR)    =      .196
  STANDARDIZED RMR                   =      .056
  ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .050
  90% CONFIDENCE INTERVAL OF RMSEA  (        .029,        .068)
```

```
  RELIABILITY COEFFICIENTS
  ------------------------
  CRONBACH'S ALPHA                   =      .870
  COEFFICIENT ALPHA FOR AN OPTIMAL SHORT SCALE               =      .882
  BASED ON THE FOLLOWING  5 VARIABLES
  P.6.1     P.6.2     P.6.3     P.6.4     P.6.5
  RELIABILITY COEFFICIENT RHO        =      .932
  GREATEST LOWER BOUND RELIABILITY                           =      .949
  GLB RELIABILITY FOR AN OPTIMAL SHORT SCALE                 =      .952
  BASED ON 14 VARIABLES, ALL EXCEPT:
  P.1.9     P.1.12
  BENTLER'S DIMENSION-FREE LOWER BOUND RELIABILITY           =      .949
  SHAPIRO'S LOWER BOUND RELIABILITY FOR A WEIGHTED COMPOSITE  =      .962
  WEIGHTS THAT ACHIEVE SHAPIRO'S LOWER BOUND:
  P.1.9     P.1.12    P.6.1     P.6.2     P.6.3     P.6.4
      .150      .187      .231      .269      .317      .176
  P.6.5     P.9.3     P.9.9     P.9.10    P.9.12    P.9.13
      .232      .169      .347      .374      .351      .349
  P.9.14    P.9.15    LOGANTIG  LOGTAMA
      .234      .198     -.051      .021



  GOODNESS OF FIT SUMMARY FOR METHOD = ROBUST

  ROBUST INDEPENDENCE MODEL CHI-SQUARE =    1270.598 ON   122 DEGREES OF
FREEDOM

  INDEPENDENCE AIC =  1026.59816   INDEPENDENCE CAIC =   522.03075
         MODEL AIC =   -74.09386          MODEL CAIC =  -471.13051

  SATORRA-BENTLER SCALED CHI-SQUARE =    117.9061 ON      96 DEGREES OF
FREEDOM
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .06403

  RESIDUAL-BASED TEST STATISTIC                      =   297.874
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00000

  YUAN-BENTLER RESIDUAL-BASED TEST STATISTIC         =   108.231
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .18528

  YUAN-BENTLER RESIDUAL-BASED F-STATISTIC     =      1.359
  DEGREES OF FREEDOM  =                         96,    74
  PROBABILITY VALUE FOR THE F-STATISTIC IS         .08447

  FIT INDICES
  -----------
  BENTLER-BONETT     NORMED FIT INDEX =      .907
  BENTLER-BONETT NON-NORMED FIT INDEX =      .976
  COMPARATIVE FIT INDEX (CFI)         =      .981
  BOLLEN   (IFI) FIT INDEX            =      .981
  MCDONALD (MFI) FIT INDEX            =      .938
  ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .037
  90% CONFIDENCE INTERVAL OF RMSEA  (        .000,        .057)


                       ITERATIVE SUMMARY
```

| ITERATION | PARAMETER ABS CHANGE | ALPHA | FUNCTION |
|---|---|---|---|
| 1 | 1.278209 | 1.00000 | 2.07583 |
| 2 | .226445 | 1.00000 | 1.19665 |
| 3 | .087625 | 1.00000 | .89992 |
| 4 | .033162 | 1.00000 | .81389 |
| 5 | .006602 | 1.00000 | .81174 |
| 6 | .001558 | 1.00000 | .81171 |
| 7 | .000424 | 1.00000 | .81170 |

```
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
  (ROBUST STATISTICS IN PARENTHESES)


 P.1.9   =V9  =   1.000 F4    + 1.000 E9


 P.1.12  =V12 =   1.471*F4    + 1.000 E12
                    .224
                   6.564@
               (    .193)
               (   7.605@

 P.6.1   =V47 =   1.000 F10   + 1.000 E47


 P.6.2   =V48 =   1.010*F10   + 1.000 E48
                    .099
                  10.168@
               (    .087)
               (  11.648@

 P.6.3   =V49 =   1.095*F10   + 1.000 E49
                    .103
                  10.637@
               (    .092)
               (  11.887@

 P.6.4   =V50 =    .883*F10   + 1.000 E50
                    .098
                   8.997@
               (    .091)
               (   9.676@
```

```
 P.6.5   =V51 =   1.025*F10   + 1.000 E51
                   .101
                 10.177@
               (   .102)
               ( 10.068@

 P.9.3   =V59 =    .588*F12   + 1.000 E59
                   .067
                  8.781@
               (   .084)
               (  6.982@

 P.9.9   =V65 =   1.000 F14   + 1.000 E65




 P.9.10  =V66 =   1.056*F14   + 1.000 E66
                   .087
                 12.204@
               (   .089)
               ( 11.926@

 P.9.12  =V68 =   1.000 F13   + 1.000 E68




 P.9.13  =V69 =   1.074*F13   + 1.000 E69
                   .080
                 13.421@
               (   .088)
               ( 12.208@


  MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
(CONTINUED)


05-Feb-18      PAGE :  9  EQS     Licensee:
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)
  (ROBUST STATISTICS IN PARENTHESES)

 P.9.14  =V70 =   1.000 F12   + 1.000 E70




 P.9.15  =V71 =    .832*F12   + 1.000 E71
                   .092
                  9.051@
```

```
               (    .111)
               (  7.524@

 LOGANTIG=V76 =   1.000 F17   + 1.000 E76



 LOGTAMA =V79 =   1.000 F16   + 1.000 E79
```



```
  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  CONSTRUCT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
  (ROBUST STATISTICS IN PARENTHESES)


    F10  =F10 =    .681*F4    + 1.000 D10
                   .122
                  5.583@
               (    .115)
               (  5.938@

    F12  =F12 =   1.000 F15   + 1.000 D12



    F13  =F13 =   1.296*F15   + 1.000 D13
                   .163
                  7.939@
               (    .153)
               (  8.456@

    F14  =F14 =   1.639*F15   + 1.000 D14
                   .215
                  7.620@
               (    .243)
               (  6.753@

    F15  =F15 =    .265*F10   -  .016*F16   -  .095*F17   + 1.000 D15
                   .056          .140          .226
                  4.703@        -.114         -.420
               (    .055)     (   .151)     (   .226)
               (  4.853@      (  -.106)     (  -.381)
```

```
05-Feb-18      PAGE : 11  EQS     Licensee:
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES
  ----------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                V                                 F
               ---                               ---
                              I F4  -   F4              2.620*I
                              I                          .674 I
                              I                         3.889@I
                              I                      (   .599)I
                              I                      (  4.372@I
                              I                               I
                              I F16 -   F16              .370*I
                              I                          .040 I
                              I                         9.192@I
                              I                      (   .051)I
                              I                      (  7.251@I
                              I                               I
                              I F17 -   F17              .126*I
                              I                          .014 I
                              I                         9.192@I
                              I                      (   .018)I
                              I                      (  7.177@I
                              I                               I


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES
  ----------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                E                                 D
               ---                               ---
 E9  -P.1.9              4.217*I D10 -   F10             1.818*I
                          .567 I                          .378 I
                         7.436@I                         4.804@I
                      (   .570)I                      (   .343)I
                      (  7.392@I                      (  5.301@I
                               I                               I
 E12 -P.1.12             2.390*I D12 -   F12              .636*I
                          .707 I                          .150 I
                         3.381@I                         4.226@I
                      (   .777)I                      (   .177)I
                      (  3.078@I                      (  3.592@I
                               I                               I
 E47 -P.6.1              2.387*I D13 -   F13              .918*I
                          .307 I                          .197 I
                         7.785@I                         4.664@I
                      (   .431)I                      (   .251)I
```

```
                      (  5.531@I                       (  3.652@I
                               I                                I
E48 -P.6.2               1.852*I D14 -   F14               .210*I
                          .253 I                           .211 I
                         7.333@I                           .997 I
                      (   .395)I                       (   .278)I
                      (  4.685@I                       (   .757)I
                               I                                I
E49 -P.6.3               1.689*I D15 -   F15               .695*I
                          .249 I                           .159 I
                         6.791@I                          4.385@I
                      (   .357)I                       (   .189)I
                      (  4.728@I                       (  3.686@I
                               I                                I
E50 -P.6.4               2.393*I                                I
                          .295 I                                I
                         8.103@I                                I
                      (   .339)I                                I
                      (  7.050@I                                I
                               I                                I
E51 -P.6.5               1.897*I                                I
                          .259 I                                I
                         7.323@I                                I
                      (   .327)I                                I
                      (  5.794@I                                I
                               I                                I
E59 -P.9.3                .598*I                                I
                          .079 I                                I
                         7.589@I                                I
                      (   .097)I                                I
                      (  6.176@I                                I
                               I                                I
E65 -P.9.9               1.310*I                                I
                          .204 I                                I
                         6.430@I                                I
                      (   .356)I                                I
                      (  3.679@I                                I
                               I                                I
E66 -P.9.10               .727*I                                I
                          .181 I                                I
                         4.025@I                                I
                      (   .187)I                                I
                      (  3.888@I                                I
                               I                                I
E68 -P.9.12               .412*I                                I
                          .141 I                                I
                         2.933@I                                I
                      (   .194)I                                I
                      (  2.125@I                                I
                               I                                I
E69 -P.9.13               .893*I                                I
                          .182 I                                I
                         4.908@I                                I
                      (   .318)I                                I
                      (  2.808@I                                I
                               I                                I
```

```
 05-Feb-18      PAGE : 13  EQS     Licensee:
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES (CONTINUED)
  ----------------------------------------------

 E70 -P.9.14              .578*I                                I
                          .128 I                                I
                         4.509@I                                I
                      (   .205)I                                I
                      (  2.821@I                                I
                               I                                I
 E71 -P.9.15             1.067*I                                I
                          .145 I                                I
                         7.370@I                                I
                      (   .280)I                                I
                      (  3.804@I                                I
                               I                                I


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  COVARIANCES AMONG INDEPENDENT VARIABLES
  ---------------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                V                                 F
               ---                               ---
                               I F16 -   F16                .527*I
                               I F4  -   F4                 .113 I
                               I                           4.652@I
                               I                        (   .111)I
                               I                        (  4.747@I
                               I                                 I
                               I F17 -   F17                .096*I
                               I F4  -   F4                 .052 I
                               I                           1.853 I
                               I                        (   .054)I
                               I                        (  1.792)I
                               I                                 I
                               I F17 -   F17                .096*I
                               I F16 -   F16                .018 I
                               I                           5.276@I
                               I                        (   .019)I
                               I                        (  5.136@I
                               I                                 I


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)
```

```
  STANDARDIZED SOLUTION:                                                       R-
SQUARED



 P.1.9   =V9  =   .619 F4    + .785 E9
.383
 P.1.12  =V12 =   .839*F4    + .545 E12
.703
 P.6.1   =V47 =   .748 F10   + .664 E47
.560
 P.6.2   =V48 =   .791*F10   + .612 E48
.626
 P.6.3   =V49 =   .826*F10   + .563 E49
.683
 P.6.4   =V50 =   .705*F10   + .709 E50
.497
 P.6.5   =V51 =   .792*F10   + .611 E51
.627
 P.9.3   =V59 =   .686*F12   + .727 E59
.471
 P.9.9   =V65 =   .818 F14   + .576 E65
.668
 P.9.10  =V66 =   .896*F14   + .445 E66
.802
 P.9.12  =V68 =   .925 F13   + .380 E68
.855
 P.9.13  =V69 =   .871*F13   + .491 E69
.759
 P.9.14  =V70 =   .853 F12   + .522 E70
.727
 P.9.15  =V71 =   .707*F12   + .707 E71
.500
 LOGANTIG=V76 =  1.000 F17   + .000 E76
1.000
 LOGTAMA =V79 =  1.000 F16   + .000 E79
1.000
    F10  =F10 =   .633*F4    + .774 D10
.401
    F12  =F12 =   .766 F15   + .642 D12
.587
    F13  =F13 =   .790*F15   + .614 D13
.623
    F14  =F14 =   .959*F15   + .282 D14
.920
    F15  =F15 =   .486*F10   - .010*F16   - .035*F17   + .877 D15
.231


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  CORRELATIONS AMONG INDEPENDENT VARIABLES
  ---------------------------------------

                  V                                F
```

```
                 ---                                ---
                              I F16 -   F16              .535*I
                              I F4  -   F4                    I
                              I                               I
                              I F17 -   F17              .167*I
                              I F4  -   F4                    I
                              I                               I
                              I F17 -   F17              .444*I
                              I F16 -   F16                   I
                              I                               I
```

```
 -------------------------------------------------------------------------
-------
                           E N D    O F    M E T H O D
 -------------------------------------------------------------------------
-------
1
  Execution begins at 16:29:02
  Execution ends   at 16:29:03
  Elapsed time =       1.00 seconds
```

# ANEXO XX

## MODELO EFECTO MEDIADOR DE LA FLEXIBILIDAD EXTERNA DE LA ESTRUCTURA – MODELO C

```
1
  EQS, A STRUCTURAL EQUATION PROGRAM          MULTIVARIATE SOFTWARE, INC.
  COPYRIGHT BY P.M. BENTLER                   VERSION 6.1 (C) 1985 - 2005
(B85).


    PROGRAM CONTROL INFORMATION

    /TITLE
     Your EQS 6 Model
    /SPECIFICATIONS
    VARIABLES= 80 ; CASES= 170 ;
    DATA='C:\tesis1\ticflexrdoscontroltotal.ESS';
    MATRIX=RAW;METHOD=ML,robust;
    /LABELS
    V1=P.1.1; V2=P.1.2; V3=P.1.3; V4=P.1.4; V5=P.1.5;
    V6=P.1.6; V7=P.1.7; V8=P.1.8; V9=P.1.9; V10=P.1.10;
    V11=P.1.11; V12=P.1.12; V13=P.1.13; V14=P.1.14; V15=P.1.15;
    V16=P.1.16; V17=P.1.17; V18=P.2.1; V19=P.2.2; V20=P.2.3;
    V21=P.2.4; V22=P.2.5; V23=P.2.6; V24=P.2.7; V25=P.2.8;
    V26=P.2.9; V27=P.2.10; V28=P.2.11; V29=P.2.12; V30=P.2.13;
    V31=P.2.14; V32=P.2.15; V33=P.3.1; V34=P.3.2; V35=P.3.3;
    V36=P.4.1; V37=P.4.2; V38=P.4.3; V39=P.4.4; V40=P.4.5;
    V41=P.4.6; V42=P.4.7; V43=P.4.8; V44=P.4.9; V45=P.4.10;
    V46=P.4.11; V47=P.6.1; V48=P.6.2; V49=P.6.3; V50=P.6.4;
    V51=P.6.5; V52=P.6.6; V53=P.6.7; V54=P.6.8; V55=P.6.9;
    V56=P.6.10; V57=P.9.1; V58=P.9.2; V59=P.9.3; V60=P.9.4;
    V61=P.9.5; V62=P.9.6; V63=P.9.7; V64=P.9.8; V65=P.9.9;
    V66=P.9.10; V67=P.9.11; V68=P.9.12; V69=P.9.13; V70=P.9.14;
    V71=P.9.15; V72=P.9.16; V73=P.9.17;
    V74=P.11.1; V75=ANTIGUED; V76=LOGANTIG; V77=RAIZANTI; V78=P.10.1;
    V79=LOGTAMA; V80=RAIZTAMA;

    /EQUATIONS
    V9 =   1F4 + E9;
    V12 =   *F4 + E12;
    V47 =   1F10 + E47;
    V48 =   *F10 + E48;
    V49 =   *F10 + E49;
    V50 =   *F10 + E50;
    V51 =   *F10 + E51;
    V59 =   *F12 + E59;
    V65 =   1F14 + E65;
    V66 =   *F14 + E66;
    V68 =   1F13 + E68;
    V69 =   *F13 + E69;
    V70 =   1F12 + E70;
    V71 =   *F12 + E71;
    V76 =   F17 + E76;
    V79 =   F16 + E79;
    F10 =   *F4 + D10;
    F12 =   1F15 + D12;
    F13 =   *F15 + D13;
    F14 =   *F15 + D14;
```

```
F15 =   *F4 + *F10 + *F16 + *F17 + D15;
/VARIANCES

 F4 = *;
 E9 = *;
 F16=*;


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 F17=*;
 E47 = *;
 E48 = *;
 E49 = *;
 E50 = *;
 E51 = *;
 E59 = *;
 E65 = *;
 E66 = *;
 E68 = *;
 E69 = *;
 E70 = *;
 E71 = *;
 E76 = 0;
 E79 = 0;
 D10 = *;
 D12 = *;
 D13 = *;
 D14 = *;
 D15 = *;
/COVARIANCES
 F4,F16 = *;
 F4,F17 = *;
 F16,F17 = *;
/PRINT
FIT=ALL;
TABLE=EQUATION;
/END


   80 RECORDS OF INPUT MODEL FILE WERE READ


DATA IS READ FROM C:\tesis1\ticflexrdoscontroltotal.ESS
THERE ARE  80 VARIABLES AND   170 CASES
IT IS A RAW DATA ESS FILE


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  SAMPLE STATISTICS BASED ON COMPLETE CASES


                          UNIVARIATE STATISTICS
                          ---------------------
```

| VARIABLE | P.1.9 V9 | P.1.12 V12 | P.6.1 V47 | P.6.2 V48 | P.6.3 V49 |
|---|---|---|---|---|---|
| MEAN | 2.3647 | 2.3706 | 2.8294 | 2.9235 | 2.5529 |
| SKEWNESS (G1) | .6639 | .6738 | .3455 | .2227 | .5477 |
| KURTOSIS (G2) | -1.0669 | -1.2320 | -1.0645 | -1.0536 | -.9088 |
| STANDARD DEV. | 2.6147 | 2.8385 | 2.3282 | 2.2241 | 2.3077 |

| VARIABLE | P.6.4 V50 | P.6.5 V51 | P.9.3 V59 | P.9.9 V65 | P.9.10 V66 |
|---|---|---|---|---|---|
| MEAN | 2.3765 | 2.1118 | 6.1647 | 4.1824 | 4.5118 |
| SKEWNESS (G1) | .4525 | .8085 | -1.6316 | -.3570 | -.5772 |
| KURTOSIS (G2) | -.9277 | -.5685 | 2.6761 | -.7646 | -.3762 |
| STANDARD DEV. | 2.1810 | 2.2544 | 1.0642 | 1.9901 | 1.9192 |

| VARIABLE | P.9.12 V68 | P.9.13 V69 | P.9.14 V70 | P.9.15 V71 | LOGANTIG V76 |
|---|---|---|---|---|---|
| MEAN | 4.8235 | 4.4235 | 5.8059 | 5.7588 | 1.2075 |
| SKEWNESS (G1) | -.5256 | -.4133 | -1.4572 | -1.3098 | -.7551 |
| KURTOSIS (G2) | -.2772 | -.6250 | 2.0533 | 1.3013 | 1.3199 |
| STANDARD DEV. | 1.6900 | 1.9269 | 1.4567 | 1.4618 | .3556 |

| VARIABLE | LOGTAMA V79 |
|---|---|
| MEAN | 1.2278 |
| SKEWNESS (G1) | .7711 |
| KURTOSIS (G2) | 1.2529 |
| STANDARD DEV. | .6087 |

MULTIVARIATE KURTOSIS
---------------------

MARDIA'S COEFFICIENT (G2,P) = 54.1238
NORMALIZED ESTIMATE = 14.7018

ELLIPTICAL THEORY KURTOSIS ESTIMATES
------------------------------------

MARDIA-BASED KAPPA = .1879 MEAN SCALED UNIVARIATE KURTOSIS = -.0054

MARDIA-BASED KAPPA IS USED IN COMPUTATION. KAPPA= .1879

CASE NUMBERS WITH LARGEST CONTRIBUTION TO NORMALIZED MULTIVARIATE KURTOSIS:

---------------------------------------------------------------------------

| CASE NUMBER | 1 | 85 | 125 | 150 | 169 |
|---|---|---|---|---|---|
| ESTIMATE | 356.5668 | 1212.0287 | 368.1973 | 349.1001 | 383.1531 |



COVARIANCE MATRIX TO BE ANALYZED: 16 VARIABLES (SELECTED FROM 80 VARIABLES)
BASED ON 170 CASES.

| | | P.1.9 V9 | P.1.12 V12 | P.6.1 V47 | P.6.2 V48 | P.6.3 V49 |
|---|---|---|---|---|---|---|
| P.1.9 | V9 | 6.837 | | | | |
| P.1.12 | V12 | 3.704 | 8.057 | | | |
| P.6.1 | V47 | 2.145 | 2.614 | 5.420 | | |
| P.6.2 | V48 | 1.430 | 2.484 | 3.218 | 4.947 | |
| P.6.3 | V49 | 2.347 | 3.285 | 3.124 | 3.427 | 5.326 |
| P.6.4 | V50 | 1.891 | 2.262 | 2.976 | 2.609 | 2.731 |
| P.6.5 | V51 | 1.995 | 2.615 | 2.972 | 2.991 | 3.547 |
| P.9.3 | V59 | .336 | .371 | .312 | .415 | .488 |
| P.9.9 | V65 | 1.631 | 1.689 | 1.469 | 1.943 | 1.916 |
| P.9.10 | V66 | .996 | 1.324 | 1.532 | 1.797 | 1.348 |
| P.9.12 | V68 | .479 | .480 | .804 | .910 | .962 |
| P.9.13 | V69 | 1.064 | .966 | 1.173 | 1.098 | .912 |
| P.9.14 | V70 | .077 | .321 | .730 | .944 | .552 |
| P.9.15 | V71 | .301 | .605 | .734 | .881 | .803 |
| LOGANTIG | V76 | .144 | .167 | .006 | .003 | -.079 |
| LOGTAMA | V79 | .586 | .807 | .256 | .261 | .283 |

| | | P.6.4 V50 | P.6.5 V51 | P.9.3 V59 | P.9.9 V65 | P.9.10 V66 |
|---|---|---|---|---|---|---|
| P.6.4 | V50 | 4.757 | | | | |
| P.6.5 | V51 | 2.952 | 5.082 | | | |
| P.9.3 | V59 | .198 | .337 | 1.132 | | |
| P.9.9 | V65 | 1.097 | 1.772 | .905 | 3.961 | |
| P.9.10 | V66 | .990 | 1.303 | 1.022 | 2.800 | 3.683 |
| P.9.12 | V68 | .540 | .848 | .733 | 1.843 | 2.049 |
| P.9.13 | V69 | .934 | 1.083 | .735 | 1.999 | 2.214 |
| P.9.14 | V70 | .322 | .507 | .890 | 1.373 | 1.561 |
| P.9.15 | V71 | .476 | .642 | .756 | 1.352 | 1.130 |
| LOGANTIG | V76 | -.032 | .002 | .004 | .010 | -.042 |
| LOGTAMA | V79 | .220 | .237 | -.052 | .160 | .116 |

| | | P.9.12 V68 | P.9.13 V69 | P.9.14 V70 | P.9.15 V71 | LOGANTIG V76 |
|---|---|---|---|---|---|---|
| P.9.12 | V68 | 2.856 | | | | |
| P.9.13 | V69 | 2.625 | 3.713 | | | |
| P.9.14 | V70 | 1.374 | 1.384 | 2.122 | | |
| P.9.15 | V71 | .963 | .984 | 1.308 | 2.137 | |
| LOGANTIG | V76 | -.030 | -.035 | -.008 | -.022 | .126 |
| LOGTAMA | V79 | .035 | .079 | .010 | .042 | .096 |

| | | LOGTAMA V79 |
|---|---|---|
| LOGTAMA | V79 | .370 |

BENTLER-WEEKS STRUCTURAL REPRESENTATION:

```
    NUMBER OF DEPENDENT VARIABLES = 21
        DEPENDENT V'S :     9   12   47   48   49   50   51   59   65   66
        DEPENDENT V'S :    68   69   70   71   76   79
        DEPENDENT F'S :    10   12   13   14   15

    NUMBER OF INDEPENDENT VARIABLES = 24
        INDEPENDENT F'S :     4   16   17
        INDEPENDENT E'S :     9   12   47   48   49   50   51   59   65   66
        INDEPENDENT E'S :    68   69   70   71   76   79
        INDEPENDENT D'S :    10   12   13   14   15

    NUMBER OF FREE PARAMETERS =  41
    NUMBER OF FIXED NONZERO PARAMETERS =  29
```

```
*** WARNING MESSAGES ABOVE, IF ANY, REFER TO THE MODEL PROVIDED.
    CALCULATIONS FOR INDEPENDENCE MODEL NOW BEGIN.

*** WARNING MESSAGES ABOVE, IF ANY, REFER TO INDEPENDENCE MODEL.
    CALCULATIONS FOR USER'S MODEL NOW BEGIN.


 3RD STAGE OF COMPUTATION REQUIRED    238374 WORDS OF MEMORY.
 PROGRAM ALLOCATED 200000000 WORDS

 DETERMINANT OF INPUT MATRIX IS    .15810D+04

 PARAMETER ESTIMATES APPEAR IN ORDER,
 NO SPECIAL PROBLEMS WERE ENCOUNTERED DURING OPTIMIZATION.
```

RESIDUAL COVARIANCE MATRIX (S-SIGMA) :

| | | P.1.9 V9 | P.1.12 V12 | P.6.1 V47 | P.6.2 V48 | P.6.3 V49 |
|---|---|---|---|---|---|---|
| P.1.9 | V9 | .000 | | | | |
| P.1.12 | V12 | -.149 | .000 | | | |
| P.6.1 | V47 | .359 | .000 | .000 | | |
| P.6.2 | V48 | -.373 | -.156 | .153 | .000 | |
| P.6.3 | V49 | .392 | .423 | -.197 | .073 | .000 |
| P.6.4 | V50 | .314 | -.047 | .296 | -.098 | -.203 |
| P.6.5 | V51 | .164 | -.064 | -.138 | -.150 | .142 |
| P.9.3 | V59 | .040 | -.062 | -.149 | -.051 | -.017 |
| P.9.9 | V65 | .804 | .479 | .178 | .639 | .503 |
| P.9.10 | V66 | .123 | .047 | .169 | .421 | -.143 |
| P.9.12 | V68 | -.172 | -.472 | -.212 | -.116 | -.150 |
| P.9.13 | V69 | .364 | -.058 | .080 | -.006 | -.284 |
| P.9.14 | V70 | -.425 | -.414 | -.054 | .152 | -.306 |
| P.9.15 | V71 | -.117 | -.007 | .081 | .221 | .088 |
| LOGANTIG | V76 | .048 | .026 | -.060 | -.063 | -.150 |
| LOGTAMA | V79 | .057 | .033 | -.103 | -.102 | -.110 |

| | | P.6.4 V50 | P.6.5 V51 | P.9.3 V59 | P.9.9 V65 | P.9.10 V66 |
|---|---|---|---|---|---|---|
| P.6.4 | V50 | .000 | | | | |
| P.6.5 | V51 | .205 | .000 | | | |
| P.9.3 | V59 | -.210 | -.137 | .002 | | |
| P.9.9 | V65 | -.044 | .449 | .033 | .016 | |

```
    P.9.10   V66         -.214      -.093       .102       .017
.018
    P.9.12   V68         -.357      -.193       .047      -.076
.025
    P.9.13   V69         -.031      -.038      -.003      -.065
.037
    P.9.14   V70         -.370      -.296      -.015      -.107
.000
    P.9.15   V71         -.101      -.027       .002       .118      -
.171
    LOGANTIG V76         -.090      -.066       .002       .006      -
.046
    LOGTAMA  V79         -.097      -.131      -.099       .031      -
.020


                       P.9.12     P.9.13     P.9.14     P.9.15
LOGANTIG
                          V68        V69        V70        V71        V76
    P.9.12   V68          .010
    P.9.13   V69          .011       .011
    P.9.14   V70          .209       .132       .006
    P.9.15   V71         -.007      -.059       .028       .004
    LOGANTIG V76         -.033      -.039      -.010      -.024
.000
    LOGTAMA  V79         -.066      -.030      -.068      -.023
.000


                       LOGTAMA
                          V79
    LOGTAMA  V79          .000


                     AVERAGE ABSOLUTE  COVARIANCE  RESIDUALS    =
.1267
        AVERAGE OFF-DIAGONAL ABSOLUTE  COVARIANCE  RESIDUALS    =
.1430


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  STANDARDIZED RESIDUAL MATRIX:


                       P.1.9      P.1.12     P.6.1      P.6.2      P.6.3
                          V9         V12        V47        V48        V49
    P.1.9    V9           .000
    P.1.12   V12         -.020       .000
    P.6.1    V47          .059       .000       .000
    P.6.2    V48         -.064      -.025       .030       .000
    P.6.3    V49          .065       .065      -.037       .014
.000
```

| | | | | | | |
|---|---|---|---|---|---|---|
| P.6.4 | V50 | .055 | -.008 | .058 | -.020 | -.040 |
| P.6.5 | V51 | .028 | -.010 | -.026 | -.030 | .027 |
| P.9.3 | V59 | .014 | -.021 | -.060 | -.022 | -.007 |
| P.9.9 | V65 | .155 | .085 | .038 | .144 | .109 |
| P.9.10 | V66 | .025 | .009 | .038 | .099 | -.032 |
| P.9.12 | V68 | -.039 | -.098 | -.054 | -.031 | -.039 |
| P.9.13 | V69 | .072 | -.011 | .018 | -.001 | -.064 |
| P.9.14 | V70 | -.112 | -.100 | -.016 | .047 | -.091 |
| P.9.15 | V71 | -.031 | -.002 | .024 | .068 | .026 |
| LOGANTIG | V76 | .051 | .026 | -.072 | -.080 | -.183 |
| LOGTAMA | V79 | .036 | .019 | -.073 | -.075 | -.079 |

| | | P.6.4 V50 | P.6.5 V51 | P.9.3 V59 | P.9.9 V65 | P.9.10 V66 |
|---|---|---|---|---|---|---|
| P.6.4 | V50 | .000 | | | | |
| P.6.5 | V51 | .042 | .000 | | | |
| P.9.3 | V59 | -.090 | -.057 | .002 | | |
| P.9.9 | V65 | -.010 | .100 | .015 | .004 | |
| P.9.10 | V66 | -.051 | -.021 | .050 | .004 | .005 |
| P.9.12 | V68 | -.097 | -.051 | .026 | -.023 | .008 |
| P.9.13 | V69 | -.007 | -.009 | -.002 | -.017 | .010 |
| P.9.14 | V70 | -.117 | -.090 | -.009 | -.037 | .000 |
| P.9.15 | V71 | -.032 | -.008 | .001 | .041 | -.061 |
| LOGANTIG | V76 | -.116 | -.082 | .006 | .009 | -.067 |
| LOGTAMA | V79 | -.073 | -.096 | -.152 | .025 | -.017 |

| | | P.9.12 V68 | P.9.13 V69 | P.9.14 V70 | P.9.15 V71 | LOGANTIG V76 |
|---|---|---|---|---|---|---|
| P.9.12 | V68 | .003 | | | | |
| P.9.13 | V69 | .003 | .003 | | | |
| P.9.14 | V70 | .085 | .047 | .003 | | |
| P.9.15 | V71 | -.003 | -.021 | .013 | .002 | |
| LOGANTIG | V76 | -.055 | -.056 | -.020 | -.046 | .000 |
| LOGTAMA | V79 | -.065 | -.026 | -.077 | -.026 | .000 |

```
                       LOGTAMA
                          V79
     LOGTAMA  V79          .000


                    AVERAGE ABSOLUTE STANDARDIZED RESIDUALS     =
.0402
       AVERAGE OFF-DIAGONAL ABSOLUTE STANDARDIZED RESIDUALS     =
.0454


  LARGEST STANDARDIZED RESIDUALS:

      NO.    PARAMETER   ESTIMATE      NO.    PARAMETER   ESTIMATE
      ---    ---------   --------      ---    ---------   --------
       1     V76, V49      -.183       11     V66, V48       .099
       2     V65, V9        .155       12     V68, V12      -.098
       3     V79, V59      -.152       13     V68, V50      -.097
       4     V65, V48       .144       14     V79, V51      -.096
       5     V70, V50      -.117       15     V70, V49      -.091
       6     V76, V50      -.116       16     V59, V50      -.090
       7     V70, V9       -.112       17     V70, V51      -.090
       8     V65, V49       .109       18     V70, V68       .085
       9     V70, V12      -.100       19     V65, V12       .085
      10     V65, V51       .100       20     V76, V51      -.082

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  DISTRIBUTION OF STANDARDIZED RESIDUALS



     ----------------------------------------
     !                                      !
   80-                                      -
     !                                      !
     !                                      !
     !                 *                    !
     !                 *                    !            RANGE      FREQ
PERCENT
   60-                 *  *                 -
     !                 *  *                 !     1   -0.5  -  --        0
.00%
     !                 *  *                 !     2   -0.4  -  -0.5      0
.00%
     !                 *  *                 !     3   -0.3  -  -0.4      0
.00%
     !                 *  *                 !     4   -0.2  -  -0.3      0
.00%
   40-                 *  *                 -     5   -0.1  -  -0.2      6
4.41%
```

```
     !                 *  *                 !    6    0.0  -  -0.1    66
48.53%
     !                 *  *                 !    7    0.1  -   0.0    60
44.12%
     !                 *  *                 !    8    0.2  -   0.1     4
2.94%
     !                 *  *                 !    9    0.3  -   0.2     0
.00%
   20-                 *  *                 -    A    0.4  -   0.3     0
.00%
     !                 *  *                 !    B    0.5  -   0.4     0
.00%
     !                 *  *                 !    C     ++  -   0.5     0
.00%
     !              *  *  *                 !    -----------------------
-------
     !              *  *  *  *              !          TOTAL        136
100.00%
     ----------------------------------------
        1  2  3  4  5  6  7  8  9  A  B  C       EACH "*" REPRESENTS  4
RESIDUALS


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)



  GOODNESS OF FIT SUMMARY FOR METHOD = ML

  INDEPENDENCE MODEL CHI-SQUARE        =    1420.676 ON   122 DEGREES OF
FREEDOM

  INDEPENDENCE AIC =  1176.67640   INDEPENDENCE CAIC =   672.10899
         MODEL AIC =   -53.02518          MODEL CAIC =  -445.92603

  CHI-SQUARE =      136.975 BASED ON      95 DEGREES OF FREEDOM
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00314

  THE NORMAL THEORY RLS CHI-SQUARE FOR THIS ML SOLUTION IS
128.594.

  FIT INDICES
  -----------
  BENTLER-BONETT     NORMED FIT INDEX =      .904
  BENTLER-BONETT NON-NORMED FIT INDEX =      .958
  COMPARATIVE FIT INDEX (CFI)         =      .968
  BOLLEN   (IFI) FIT INDEX            =      .968
  MCDONALD (MFI) FIT INDEX            =      .884
  LISREL    GFI  FIT INDEX            =      .913
  LISREL   AGFI  FIT INDEX            =      .876
  ROOT MEAN-SQUARE RESIDUAL (RMR)     =      .193
  STANDARDIZED RMR                    =      .055
  ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .051
  90% CONFIDENCE INTERVAL OF RMSEA  (        .030,        .069)
```

```
  RELIABILITY COEFFICIENTS
  ------------------------
  CRONBACH'S ALPHA                    =      .870
  COEFFICIENT ALPHA FOR AN OPTIMAL SHORT SCALE               =      .882
  BASED ON THE FOLLOWING  5 VARIABLES
  P.6.1    P.6.2    P.6.3    P.6.4    P.6.5
  RELIABILITY COEFFICIENT RHO         =      .932
  GREATEST LOWER BOUND RELIABILITY                           =      .949
  GLB RELIABILITY FOR AN OPTIMAL SHORT SCALE                 =      .952
  BASED ON 14 VARIABLES, ALL EXCEPT:
  P.1.9    P.1.12
  BENTLER'S DIMENSION-FREE LOWER BOUND RELIABILITY           =      .949
  SHAPIRO'S LOWER BOUND RELIABILITY FOR A WEIGHTED COMPOSITE  =      .962
  WEIGHTS THAT ACHIEVE SHAPIRO'S LOWER BOUND:
  P.1.9    P.1.12   P.6.1    P.6.2    P.6.3    P.6.4
      .150     .187     .231     .269     .317     .176
  P.6.5    P.9.3    P.9.9    P.9.10   P.9.12   P.9.13
      .232     .169     .347     .374     .351     .349
  P.9.14   P.9.15   LOGANTIG  LOGTAMA
      .234     .198    -.051     .021



  GOODNESS OF FIT SUMMARY FOR METHOD = ROBUST

  ROBUST INDEPENDENCE MODEL CHI-SQUARE =    1270.598 ON   122 DEGREES OF
FREEDOM

  INDEPENDENCE AIC =  1026.59816   INDEPENDENCE CAIC =   522.03075
         MODEL AIC =   -72.53473          MODEL CAIC =  -465.43558

  SATORRA-BENTLER SCALED CHI-SQUARE =    117.4653 ON      95 DEGREES OF
FREEDOM
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .05890

  RESIDUAL-BASED TEST STATISTIC                     =   259.377
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00000

  YUAN-BENTLER RESIDUAL-BASED TEST STATISTIC        =   102.693
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .27699

  YUAN-BENTLER RESIDUAL-BASED F-STATISTIC     =      1.212
  DEGREES OF FREEDOM  =                        95,    75
  PROBABILITY VALUE FOR THE F-STATISTIC IS         .19385

  FIT INDICES
  -----------
  BENTLER-BONETT     NORMED FIT INDEX =      .908
  BENTLER-BONETT NON-NORMED FIT INDEX =      .975
  COMPARATIVE FIT INDEX (CFI)         =      .980
  BOLLEN   (IFI) FIT INDEX            =      .981
  MCDONALD (MFI) FIT INDEX            =      .936
  ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .037
  90% CONFIDENCE INTERVAL OF RMSEA  (        .000,        .058)


                         ITERATIVE SUMMARY
```

| ITERATION | PARAMETER ABS CHANGE | ALPHA | FUNCTION |
|---|---|---|---|
| 1 | 1.546912 | 1.00000 | 3.62715 |
| 2 | .368191 | 1.00000 | 2.72851 |
| 3 | .360987 | 1.00000 | 1.30010 |
| 4 | .080901 | 1.00000 | .96303 |
| 5 | .038846 | 1.00000 | .81721 |
| 6 | .010041 | 1.00000 | .81066 |
| 7 | .002953 | 1.00000 | .81052 |
| 8 | .000816 | 1.00000 | .81050 |


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MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
(ROBUST STATISTICS IN PARENTHESES)

```
P.1.9   =V9  =   1.000 F4    + 1.000 E9



P.1.12  =V12 =   1.463*F4    + 1.000 E12
                   .222
                  6.584@
              (    .190)
              (   7.695@

P.6.1   =V47 =   1.000 F10   + 1.000 E47



P.6.2   =V48 =   1.010*F10   + 1.000 E48
                   .099
                 10.165@
              (    .087)
              (  11.622@

P.6.3   =V49 =   1.095*F10   + 1.000 E49
                   .103
                 10.634@
              (    .092)
              (  11.863@

P.6.4   =V50 =    .883*F10   + 1.000 E50
                   .098
                  9.003@
              (    .091)
```

```
              (   9.674@

 P.6.5   =V51 =   1.025*F10   + 1.000 E51
                   .101
                 10.180@
              (    .102)
              (  10.064@

 P.9.3   =V59 =    .589*F12   + 1.000 E59
                   .067
                  8.775@
              (    .084)
              (   6.984@

 P.9.9   =V65 =   1.000 F14   + 1.000 E65




 P.9.10  =V66 =   1.055*F14   + 1.000 E66
                   .086
                 12.210@
              (    .088)
              (  11.940@

 P.9.12  =V68 =   1.000 F13   + 1.000 E68




 P.9.13  =V69 =   1.076*F13   + 1.000 E69
                   .080
                 13.404@
              (    .088)
              (  12.185@


  MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
(CONTINUED)


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  (ROBUST STATISTICS IN PARENTHESES)

 P.9.14  =V70 =   1.000 F12   + 1.000 E70




 P.9.15  =V71 =    .833*F12   + 1.000 E71
                   .092
```

```
                 9.042@
              (   .111)
              (  7.533@

 LOGANTIG=V76 =   1.000 F17   + 1.000 E76



 LOGTAMA =V79 =   1.000 F16   + 1.000 E79
```



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MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

CONSTRUCT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
(ROBUST STATISTICS IN PARENTHESES)

```
   F10  =F10 =    .678*F4    + 1.000 D10
                  .122
                 5.575@
              (   .114)
              (  5.926@

   F12  =F12 =   1.000 F15   + 1.000 D12



   F13  =F13 =   1.296*F15   + 1.000 D13
                  .164
                 7.911@
              (   .153)
              (  8.446@

   F14  =F14 =   1.648*F15   + 1.000 D14
                  .217
                 7.606@
              (   .245)
              (  6.725@

   F15  =F15 =    .243*F10   +  .041*F4    -  .058*F16   -  .094*F17
                  .070          .085          .164          .226
                 3.478@         .479         -.352         -.417
              (   .072)     (   .089)     (   .167)     (   .245)
              (  3.383@     (   .458)     (  -.345)     (  -.385)
```

```
                + 1.000 D15




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   MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

   VARIANCES OF INDEPENDENT VARIABLES
   ----------------------------------
   STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                  V                                F
                 ---                              ---
                               I F4  -   F4              2.633*I
                               I                          .675 I
                               I                         3.901@I
                               I                      (   .598)I
                               I                      (  4.402@I
                               I                               I
                               I F16 -   F16              .370*I
                               I                          .040 I
                               I                         9.192@I
                               I                      (   .051)I
                               I                      (  7.251@I
                               I                               I
                               I F17 -   F17              .126*I
                               I                          .014 I
                               I                         9.192@I
                               I                      (   .018)I
                               I                      (  7.177@I
                               I                               I

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   MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

   VARIANCES OF INDEPENDENT VARIABLES
   ----------------------------------
   STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                  E                                D
                 ---                              ---
  E9  -P.1.9             4.203*I D10 -   F10             1.823*I
                          .566 I                          .379 I
                         7.423@I                         4.803@I
                      (   .565)I                      (   .345)I
                      (  7.437@I                      (  5.285@I
                               I                               I
  E12 -P.1.12            2.417*I D12 -   F12              .638*I
```

```
                          .704 I                           .151 I
                         3.434@I                          4.236@I
                      (   .772)I                       (   .177)I
                      (  3.132@I                       (  3.607@I
                               I                                I
E47 -P.6.1               2.386*I D13 -   F13               .922*I
                          .307 I                           .197 I
                         7.780@I                          4.684@I
                      (   .432)I                       (   .251)I
                      (  5.518@I                       (  3.677@I
                               I                                I
E48 -P.6.2               1.853*I D14 -   F14               .199*I
                          .253 I                           .211 I
                         7.328@I                           .943 I
                      (   .396)I                       (   .278)I
                      (  4.675@I                       (   .716)I
                               I                                I
E49 -P.6.3               1.689*I D15 -   F15               .692*I
                          .249 I                           .158 I
                         6.784@I                          4.377@I
                      (   .359)I                       (   .189)I
                      (  4.703@I                       (  3.661@I
                               I                                I
E50 -P.6.4               2.389*I                                I
                          .295 I                                I
                         8.097@I                                I
                      (   .340)I                                I
                      (  7.033@I                                I
                               I                                I
E51 -P.6.5               1.894*I                                I
                          .259 I                                I
                         7.313@I                                I
                      (   .327)I                                I
                      (  5.786@I                                I
                               I                                I
E59 -P.9.3                .598*I                                I
                          .079 I                                I
                         7.581@I                                I
                      (   .097)I                                I
                      (  6.181@I                                I
                               I                                I
E65 -P.9.9               1.307*I                                I
                          .203 I                                I
                         6.427@I                                I
                      (   .355)I                                I
                      (  3.681@I                                I
                               I                                I
E66 -P.9.10               .730*I                                I
                          .180 I                                I
                         4.052@I                                I
                      (   .187)I                                I
                      (  3.902@I                                I
                               I                                I
E68 -P.9.12               .415*I                                I
                          .141 I                                I
                         2.952@I                                I
                      (   .194)I                                I
                      (  2.137@I                                I
                               I                                I
```

```
 E69 -P.9.13               .889*I                               I
                           .182 I                               I
                          4.886@I                               I
                       (   .318)I                               I
                       (  2.800@I                               I
                                I                               I


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES (CONTINUED)
  ----------------------------------------------

 E70 -P.9.14               .580*I                               I
                           .128 I                               I
                          4.522@I                               I
                       (   .206)I                               I
                       (  2.814@I                               I
                                I                               I
 E71 -P.9.15              1.066*I                               I
                           .145 I                               I
                          7.364@I                               I
                       (   .280)I                               I
                       (  3.805@I                               I
                                I                               I


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  TITLE:    Your EQS 6 Model

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  COVARIANCES AMONG INDEPENDENT VARIABLES
  ---------------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                 V                                F
                ---                              ---
                                I F16 -   F16              .529*I
                                I F4  -   F4               .114 I
                                I                         4.663@I
                                I                      (   .111)I
                                I                      (  4.750@I
                                I                               I
                                I F17 -   F17              .097*I
                                I F4  -   F4               .052 I
                                I                         1.854 I
                                I                      (   .054)I
                                I                      (  1.792)I
                                I                               I
                                I F17 -   F17              .096*I
                                I F16 -   F16              .018 I
                                I                         5.276@I
                                I                      (   .019)I
                                I                      (  5.136@I
```

```
                                I                                I


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  TITLE:    Your EQS 6 Model

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  STANDARDIZED SOLUTION:                                              R-
SQUARED



 P.1.9   =V9  =   .621 F4    + .784 E9
.385
 P.1.12  =V12 =   .837*F4    + .548 E12
.700
 P.6.1   =V47 =   .748 F10   + .663 E47
.560
 P.6.2   =V48 =   .791*F10   + .612 E48
.625
 P.6.3   =V49 =   .826*F10   + .563 E49
.683
 P.6.4   =V50 =   .705*F10   + .709 E50
.498
 P.6.5   =V51 =   .792*F10   + .611 E51
.627
 P.9.3   =V59 =   .687*F12   + .727 E59
.471
 P.9.9   =V65 =   .818 F14   + .576 E65
.669
 P.9.10  =V66 =   .895*F14   + .446 E66
.801
 P.9.12  =V68 =   .924 F13   + .382 E68
.854
 P.9.13  =V69 =   .872*F13   + .490 E69
.760
 P.9.14  =V70 =   .852 F12   + .524 E70
.726
 P.9.15  =V71 =   .707*F12   + .707 E71
.500
 LOGANTIG=V76 =  1.000 F17   + .000 E76
1.000
 LOGTAMA =V79 =  1.000 F16   + .000 E79
1.000
    F10  =F10 =   .632*F4    + .775 D10
.399
    F12  =F12 =   .765 F15   + .644 D12
.585
    F13  =F13 =   .788*F15   + .616 D13
.621
    F14  =F14 =   .961*F15   + .275 D14
.924
    F15  =F15 =   .447*F10   + .070*F4    - .037*F16   - .035*F17
                + .878 D15
.230
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```

```
  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  CORRELATIONS AMONG INDEPENDENT VARIABLES
  ---------------------------------------

                 V                                F
                ---                              ---
                               I F16 -   F16                .536*I
                               I F4  -   F4                      I
                               I                                 I
                               I F17 -   F17                .167*I
                               I F4  -   F4                      I
                               I                                 I
                               I F17 -   F17                .444*I
                               I F16 -   F16                     I
                               I                                 I

 ------------------------------------------------------------------------
-------
                          E N D   O F   M E T H O D
 ------------------------------------------------------------------------
-------
1
  Execution begins at 14:23:27
  Execution ends   at 14:23:27
  Elapsed time =        .00 seconds
```

# ANEXO XXI

# MODELO EFECTO MEDIADOR DE LA FLEXIBILIDAD INTERNA DE LA ESTRUCTURA – MODELO A

```
1
  EQS, A STRUCTURAL EQUATION PROGRAM          MULTIVARIATE SOFTWARE, INC.
  COPYRIGHT BY P.M. BENTLER                   VERSION 6.1 (C) 1985 - 2005
(B85).


    PROGRAM CONTROL INFORMATION

        /TITLE
          Your EQS 6 Model
        /SPECIFICATIONS
        VARIABLES= 80 ; CASES= 170 ;
        DATA='C:\tesis1\ticflexrdoscontroltotal.ESS';
        MATRIX=RAW;METHOD=ML,robust;
        /LABELS
        V1=P.1.1; V2=P.1.2; V3=P.1.3; V4=P.1.4; V5=P.1.5;
        V6=P.1.6; V7=P.1.7; V8=P.1.8; V9=P.1.9; V10=P.1.10;
        V11=P.1.11; V12=P.1.12; V13=P.1.13; V14=P.1.14; V15=P.1.15;
        V16=P.1.16; V17=P.1.17; V18=P.2.1; V19=P.2.2; V20=P.2.3;
        V21=P.2.4; V22=P.2.5; V23=P.2.6; V24=P.2.7; V25=P.2.8;
        V26=P.2.9; V27=P.2.10; V28=P.2.11; V29=P.2.12; V30=P.2.13;
        V31=P.2.14; V32=P.2.15; V33=P.3.1; V34=P.3.2; V35=P.3.3;
        V36=P.4.1; V37=P.4.2; V38=P.4.3; V39=P.4.4; V40=P.4.5;
        V41=P.4.6; V42=P.4.7; V43=P.4.8; V44=P.4.9; V45=P.4.10;
        V46=P.4.11; V47=P.6.1; V48=P.6.2; V49=P.6.3; V50=P.6.4;
        V51=P.6.5; V52=P.6.6; V53=P.6.7; V54=P.6.8; V55=P.6.9;
        V56=P.6.10; V57=P.9.1; V58=P.9.2; V59=P.9.3; V60=P.9.4;
        V61=P.9.5; V62=P.9.6; V63=P.9.7; V64=P.9.8; V65=P.9.9;
        V66=P.9.10; V67=P.9.11; V68=P.9.12; V69=P.9.13; V70=P.9.14;
        V71=P.9.15; V72=P.9.16; V73=P.9.17;
        V74=P.11.1; V75=ANTIGUED; V76=LOGANTIG; V77=RAIZANTI; V78=P.10.1;
        V79=LOGTAMA; V80=RAIZTAMA;

        /EQUATIONS
        V1 =   1F1 + E1;
        V2 =   *F1 + E2;
        V3 =   *F1 + E3;
        V5 =   F3 + E5;
        V6 =   *F3 + E6;
        V8 =   *F1 + E8;
        V10 =   1F2 + E10;
        V11 =   *F2 + E11;
        V16 =   *F2 + E16;
        V17 =   *F2 + E17;
        V59 =   *F12 + E59;
        V65 =   1F14 + E65;
        V66 =   *F14 + E66;
        V68 =   1F13 + E68;
        V69 =   *F13 + E69;
        V70 =   1F12 + E70;
        V71 =   *F12 + E71;
        V76 =   F17 + E76;
        V79 =   F16 + E79;
        F1 =   1F5 + D1;
```

```
F2 =   *F5 + D2;
F3 =   *F5 + D3;
F12 =   1F15 + D12;
F13 =   *F15 + D13;
F14 =   *F15 + D14;
F15 =   *F5 + *F16 + *F17 + D15;
```

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```
/VARIANCES
 F5 = *;
 F16=*;
 F17=*;
 E1 = *;
 E2 = *;
 E3 = *;
 E5 = *;
 E6 = *;
 E8 = *;
 E10 = *;
 E11 = *;
 E16 = *;
 E17 = *;
 E59 = *;
 E65 = *;
 E66 = *;
 E68 = *;
 E69 = *;
 E70 = *;
 E71 = *;
 E76 = 0;
 E79 = 0;
 D1 = *;
 D2 = *;
 D3 = *;
 D12 = *;
 D13 = *;
 D14 = *;
 D15 = *;
/COVARIANCES

 F5,F16 = *;
 F5,F17 = *;
 F16,F17 = *;

/PRINT
FIT=ALL;
TABLE=EQUATION;
/END
```

92 RECORDS OF INPUT MODEL FILE WERE READ

DATA IS READ FROM C:\tesis1\ticflexrdoscontroltotal.ESS
THERE ARE 80 VARIABLES AND 170 CASES
IT IS A RAW DATA ESS FILE

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SAMPLE STATISTICS BASED ON COMPLETE CASES

UNIVARIATE STATISTICS
---------------------

| VARIABLE | P.1.1 V1 | P.1.2 V2 | P.1.3 V3 | P.1.5 V5 | P.1.6 V6 |
|---|---|---|---|---|---|
| MEAN | 3.6941 | 4.0059 | 3.4235 | 4.8765 | 4.4000 |
| SKEWNESS (G1) | -.1427 | -.3284 | -.0187 | -.8703 | -.5597 |
| KURTOSIS (G2) | -1.6839 | -1.4951 | -1.5302 | -.8141 | -1.3132 |
| STANDARD DEV. | 2.9694 | 2.7873 | 2.7126 | 2.6540 | 2.7914 |

| VARIABLE | P.1.8 V8 | P.1.10 V10 | P.1.11 V11 | P.1.16 V16 | P.1.17 V17 |
|---|---|---|---|---|---|
| MEAN | 2.1353 | 4.7059 | 3.5059 | 4.6235 | 4.6176 |
| SKEWNESS (G1) | .8348 | -.7765 | -.0322 | -.7038 | -.6901 |
| KURTOSIS (G2) | -.8715 | -1.1465 | -1.6572 | -1.0836 | -1.0056 |
| STANDARD DEV. | 2.5971 | 2.8939 | 2.9053 | 2.7217 | 2.6110 |

| VARIABLE | P.9.3 V59 | P.9.9 V65 | P.9.10 V66 | P.9.12 V68 | P.9.13 V69 |
|---|---|---|---|---|---|
| MEAN | 6.1647 | 4.1824 | 4.5118 | 4.8235 | 4.4235 |
| SKEWNESS (G1) | -1.6316 | -.3570 | -.5772 | -.5256 | -.4133 |
| KURTOSIS (G2) | 2.6761 | -.7646 | -.3762 | -.2772 | -.6250 |
| STANDARD DEV. | 1.0642 | 1.9901 | 1.9192 | 1.6900 | 1.9269 |

| VARIABLE | P.9.14 V70 | P.9.15 V71 | LOGANTIG V76 | LOGTAMA V79 |
|---|---|---|---|---|
| MEAN | 5.8059 | 5.7588 | 1.2075 | 1.2278 |
| SKEWNESS (G1) | -1.4572 | -1.3098 | -.7551 | .7711 |
| KURTOSIS (G2) | 2.0533 | 1.3013 | 1.3199 | 1.2529 |

```
   STANDARD DEV.      1.4567     1.4618      .3556      .6087


                         MULTIVARIATE KURTOSIS
                         ---------------------

   MARDIA'S COEFFICIENT (G2,P) =     63.9585
   NORMALIZED ESTIMATE =             14.7602


                  ELLIPTICAL THEORY KURTOSIS ESTIMATES
                  ------------------------------------

   MARDIA-BASED KAPPA =       .1603 MEAN SCALED UNIVARIATE KURTOSIS =
-.1060

   MARDIA-BASED KAPPA IS USED IN COMPUTATION. KAPPA=           .1603


   CASE NUMBERS WITH LARGEST CONTRIBUTION TO NORMALIZED MULTIVARIATE
KURTOSIS:
   ----------------------------------------------------------------------
-----

   CASE NUMBER        63           81           85          158
169

   ESTIMATE       426.5459     463.7923     771.4209     374.8516
448.1090


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  COVARIANCE  MATRIX TO BE ANALYZED:  19 VARIABLES (SELECTED FROM  80
VARIABLES)
  BASED ON   170 CASES.
```

| | | P.1.1 V1 | P.1.2 V2 | P.1.3 V3 | P.1.5 V5 | P.1.6 V6 |
|---|---|---|---|---|---|---|
| P.1.1 | V1 | 8.817 | | | | |
| P.1.2 | V2 | 5.617 | 7.769 | | | |
| P.1.3 | V3 | 4.781 | 4.938 | 7.358 | | |
| P.1.5 | V5 | 4.287 | 3.800 | 3.810 | 7.044 | |
| P.1.6 | V6 | 3.147 | 3.353 | 2.978 | 5.417 | 7.792 |
| P.1.8 | V8 | 3.917 | 3.981 | 4.392 | 2.242 | 2.336 |
| P.1.10 | V10 | 3.389 | 3.451 | 3.741 | 3.247 | 2.006 |
| P.1.11 | V11 | 3.327 | 3.399 | 3.441 | 3.282 | 3.004 |
| P.1.16 | V16 | 3.269 | 3.576 | 3.657 | 3.308 | 2.595 |
| P.1.17 | V17 | 2.823 | 3.061 | 3.305 | 3.621 | 2.822 |
| P.9.3 | V59 | .092 | .384 | .249 | .162 | .336 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.9.9 | V65 | 1.109 | 1.301 | 1.372 | .348 | .867 |
| P.9.10 | V66 | .862 | .843 | .782 | .531 | .818 |
| P.9.12 | V68 | .478 | .463 | .596 | .191 | .822 |
| P.9.13 | V69 | .592 | .873 | 1.021 | .378 | .936 |
| P.9.14 | V70 | .183 | .321 | .905 | .319 | .244 |
| P.9.15 | V71 | .210 | .516 | .618 | .372 | .458 |
| LOGANTIG | V76 | .319 | .236 | .180 | .076 | .001 |
| LOGTAMA | V79 | .772 | .630 | .512 | .438 | .409 |

| | | P.1.8 V8 | P.1.10 V10 | P.1.11 V11 | P.1.16 V16 | P.1.17 V17 |
|---|---|---|---|---|---|---|
| P.1.8 | V8 | 6.745 | | | | |
| P.1.10 | V10 | 2.016 | 8.375 | | | |
| P.1.11 | V11 | 3.316 | 3.724 | 8.441 | | |
| P.1.16 | V16 | 2.886 | 3.528 | 3.795 | 7.408 | |
| P.1.17 | V17 | 2.129 | 3.106 | 3.147 | 3.832 | 6.817 |
| P.9.3 | V59 | .279 | .173 | .484 | .352 | .182 |
| P.9.9 | V65 | 1.585 | .427 | 1.014 | 1.110 | .816 |
| P.9.10 | V66 | 1.238 | .252 | .840 | .306 | .712 |
| P.9.12 | V68 | .770 | -.011 | .634 | .359 | .595 |
| P.9.13 | V69 | .954 | -.005 | .838 | .403 | 1.050 |
| P.9.14 | V70 | .867 | .629 | .726 | .418 | .245 |
| P.9.15 | V71 | .654 | -.125 | 1.004 | .737 | .162 |
| LOGANTIG | V76 | .015 | .201 | -.015 | .138 | .114 |
| LOGTAMA | V79 | .436 | .320 | .297 | .472 | .430 |

| | | P.9.3 V59 | P.9.9 V65 | P.9.10 V66 | P.9.12 V68 | P.9.13 V69 |
|---|---|---|---|---|---|---|
| P.9.3 | V59 | 1.132 | | | | |
| P.9.9 | V65 | .905 | 3.961 | | | |
| P.9.10 | V66 | 1.022 | 2.800 | 3.683 | | |
| P.9.12 | V68 | .733 | 1.843 | 2.049 | 2.856 | |
| P.9.13 | V69 | .735 | 1.999 | 2.214 | 2.625 | 3.713 |
| P.9.14 | V70 | .890 | 1.373 | 1.561 | 1.374 | 1.384 |
| P.9.15 | V71 | .756 | 1.352 | 1.130 | .963 | .984 |

```
    LOGANTIG V76         .004       .010      -.042      -.030      -
.035
    LOGTAMA  V79        -.052       .160       .116       .035
.079


                       P.9.14     P.9.15     LOGANTIG   LOGTAMA
                          V70        V71        V76        V79
    P.9.14   V70        2.122
    P.9.15   V71        1.308      2.137
    LOGANTIG V76        -.008      -.022       .126
    LOGTAMA  V79         .010       .042       .096       .370


   BENTLER-WEEKS STRUCTURAL REPRESENTATION:

         NUMBER OF DEPENDENT VARIABLES = 26
             DEPENDENT V'S :     1    2    3    5    6    8   10   11   16
17
             DEPENDENT V'S :    59   65   66   68   69   70   71   76   79
             DEPENDENT F'S :     1    2    3   12   13   14   15

         NUMBER OF INDEPENDENT VARIABLES = 29
             INDEPENDENT F'S :     5   16   17
             INDEPENDENT E'S :     1    2    3    5    6    8   10   11
16   17
             INDEPENDENT E'S :    59   65   66   68   69   70   71   76
79
             INDEPENDENT D'S :     1    2    3   12   13   14   15

         NUMBER OF FREE PARAMETERS =  48
         NUMBER OF FIXED NONZERO PARAMETERS =  36

  *** WARNING MESSAGES ABOVE, IF ANY, REFER TO THE MODEL PROVIDED.
      CALCULATIONS FOR INDEPENDENCE MODEL NOW BEGIN.

  *** WARNING MESSAGES ABOVE, IF ANY, REFER TO INDEPENDENCE MODEL.
      CALCULATIONS FOR USER'S MODEL NOW BEGIN.


   3RD STAGE OF COMPUTATION REQUIRED    448452 WORDS OF MEMORY.
   PROGRAM ALLOCATED 200000000 WORDS

   DETERMINANT OF INPUT MATRIX IS    .92235D+06

  *** NOTE *** RESIDUAL-BASED STATISTICS CANNOT BE
               CALCULATED BECAUSE OF PIVOTING PROBLEMS.

   PARAMETER ESTIMATES APPEAR IN ORDER,
   NO SPECIAL PROBLEMS WERE ENCOUNTERED DURING OPTIMIZATION.


   RESIDUAL COVARIANCE MATRIX  (S-SIGMA) :


                       P.1.1      P.1.2      P.1.3      P.1.5      P.1.6
                          V1         V2         V3         V5         V6
```

| | | | | | | |
|---|---|---|---|---|---|---|
| P.1.1 | V1 | .000 | | | | |
| P.1.2 | V2 | .331 | .000 | | | |
| P.1.3 | V3 | -.316 | -.151 | .000 | | |
| P.1.5 | V5 | .366 | -.116 | .034 | .000 | |
| P.1.6 | V6 | -.075 | .136 | -.125 | .000 | .000 |
| P.1.8 | V8 | -.162 | -.091 | .465 | -.780 | -.146 |
| P.1.10 | V10 | .046 | .114 | .522 | .213 | -.487 |
| P.1.11 | V11 | -.157 | -.080 | .086 | .119 | .405 |
| P.1.16 | V16 | -.418 | -.104 | .108 | -.038 | -.154 |
| P.1.17 | V17 | -.494 | -.251 | .111 | .610 | .348 |
| P.9.3 | V59 | -.212 | .080 | -.043 | -.113 | .109 |
| P.9.9 | V65 | .333 | .526 | .625 | -.356 | .289 |
| P.9.10 | V66 | .021 | .003 | -.028 | -.232 | .191 |
| P.9.12 | V68 | -.203 | -.218 | -.060 | -.428 | .314 |
| P.9.13 | V69 | -.135 | .147 | .321 | -.282 | .394 |
| P.9.14 | V70 | -.343 | -.204 | .399 | -.158 | -.148 |
| P.9.15 | V71 | -.219 | .088 | .204 | -.017 | .138 |
| LOGANTIG | V76 | .158 | .076 | .025 | -.070 | -.119 |
| LOGTAMA | V79 | .218 | .077 | -.022 | -.065 | -.005 |

| | | P.1.8 V8 | P.1.10 V10 | P.1.11 V11 | P.1.16 V16 | P.1.17 V17 |
|---|---|---|---|---|---|---|
| P.1.8 | V8 | .000 | | | | |
| P.1.10 | V10 | -.559 | .000 | | | |
| P.1.11 | V11 | .631 | .285 | .000 | | |
| P.1.16 | V16 | .045 | -.111 | .003 | .000 | |
| P.1.17 | V17 | -.427 | -.168 | -.266 | .221 | .000 |
| P.9.3 | V59 | .045 | -.062 | .239 | .093 | -.052 |
| P.9.9 | V65 | .987 | -.174 | .388 | .448 | .220 |
| P.9.10 | V66 | .590 | -.399 | .162 | -.411 | .066 |
| P.9.12 | V68 | .244 | -.538 | .084 | -.223 | .071 |
| P.9.13 | V69 | .394 | -.567 | .251 | -.217 | .492 |
| P.9.14 | V70 | .462 | .222 | .302 | -.031 | -.159 |
| P.9.15 | V71 | .323 | -.457 | .658 | .371 | -.168 |

| | | | | | | |
|---|---|---|---|---|---|---|
| LOGANTIG | V76 | -.109 | .076 | -.144 | .001 | -.009 |
| LOGTAMA | V79 | .009 | -.109 | -.150 | -.001 | .004 |

| | | P.9.3<br>V59 | P.9.9<br>V65 | P.9.10<br>V66 | P.9.12<br>V68 | P.9.13<br>V69 |
|---|---|---|---|---|---|---|
| P.9.3 | V59 | .000 | | | | |
| P.9.9 | V65 | .063 | .000 | | | |
| P.9.10 | V66 | .110 | .000 | .000 | | |
| P.9.12 | V68 | -.006 | -.045 | .004 | .000 | |
| P.9.13 | V69 | -.054 | -.014 | .032 | .000 | .000 |
| P.9.14 | V70 | -.021 | -.083 | -.016 | .095 | .021 |
| P.9.15 | V71 | .012 | .163 | -.158 | -.081 | -.129 |
| LOGANTIG | V76 | .013 | .036 | -.014 | -.008 | -.011 |
| LOGTAMA | V79 | -.083 | .083 | .032 | -.033 | .007 |

| | | P.9.14<br>V70 | P.9.15<br>V71 | LOGANTIG<br>V76 | LOGTAMA<br>V79 |
|---|---|---|---|---|---|
| P.9.14 | V70 | .000 | | | |
| P.9.15 | V71 | .021 | .000 | | |
| LOGANTIG | V76 | .009 | -.008 | .000 | |
| LOGTAMA | V79 | -.042 | -.001 | .000 | .000 |

AVERAGE ABSOLUTE COVARIANCE RESIDUALS = .1683

AVERAGE OFF-DIAGONAL ABSOLUTE COVARIANCE RESIDUALS = .1870

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TITLE: Your EQS 6 Model

MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

STANDARDIZED RESIDUAL MATRIX:

| | | P.1.1<br>V1 | P.1.2<br>V2 | P.1.3<br>V3 | P.1.5<br>V5 | P.1.6<br>V6 |
|---|---|---|---|---|---|---|
| P.1.1 | V1 | .000 | | | | |
| P.1.2 | V2 | .040 | .000 | | | |
| P.1.3 | V3 | -.039 | -.020 | .000 | | |
| P.1.5 | V5 | .046 | -.016 | .005 | .000 | |
| P.1.6 | V6 | -.009 | .017 | -.016 | .000 | .000 |
| P.1.8 | V8 | -.021 | -.013 | .066 | -.113 | -.020 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.1.10 | V10 | .005 | .014 | .066 | .028 | -.060 |
| P.1.11 | V11 | -.018 | -.010 | .011 | .015 | .050 |
| P.1.16 | V16 | -.052 | -.014 | .015 | -.005 | -.020 |
| P.1.17 | V17 | -.064 | -.034 | .016 | .088 | .048 |
| P.9.3 | V59 | -.067 | .027 | -.015 | -.040 | .037 |
| P.9.9 | V65 | .056 | .095 | .116 | -.067 | .052 |
| P.9.10 | V66 | .004 | .001 | -.005 | -.046 | .036 |
| P.9.12 | V68 | -.041 | -.046 | -.013 | -.095 | .067 |
| P.9.13 | V69 | -.024 | .027 | .061 | -.055 | .073 |
| P.9.14 | V70 | -.079 | -.050 | .101 | -.041 | -.036 |
| P.9.15 | V71 | -.051 | .022 | .052 | -.004 | .034 |
| LOGANTIG | V76 | .150 | .076 | .026 | -.074 | -.120 |
| LOGTAMA | V79 | .121 | .045 | -.013 | -.040 | -.003 |

| | | P.1.8 V8 | P.1.10 V10 | P.1.11 V11 | P.1.16 V16 | P.1.17 V17 |
|---|---|---|---|---|---|---|
| P.1.8 | V8 | .000 | | | | |
| P.1.10 | V10 | -.074 | .000 | | | |
| P.1.11 | V11 | .084 | .034 | .000 | | |
| P.1.16 | V16 | .006 | -.014 | .000 | .000 | |
| P.1.17 | V17 | -.063 | -.022 | -.035 | .031 | .000 |
| P.9.3 | V59 | .016 | -.020 | .077 | .032 | -.019 |
| P.9.9 | V65 | .191 | -.030 | .067 | .083 | .042 |
| P.9.10 | V66 | .118 | -.072 | .029 | -.079 | .013 |
| P.9.12 | V68 | .056 | -.110 | .017 | -.048 | .016 |
| P.9.13 | V69 | .079 | -.102 | .045 | -.041 | .098 |
| P.9.14 | V70 | .122 | .053 | .071 | -.008 | -.042 |
| P.9.15 | V71 | .085 | -.108 | .155 | .093 | -.044 |
| LOGANTIG | V76 | -.118 | .074 | -.140 | .001 | -.010 |
| LOGTAMA | V79 | .006 | -.062 | -.085 | .000 | .003 |

| | | P.9.3 V59 | P.9.9 V65 | P.9.10 V66 | P.9.12 V68 | P.9.13 V69 |
|---|---|---|---|---|---|---|

```
     P.9.3    V59         .000
     P.9.9    V65         .030       .000
     P.9.10   V66         .054       .000       .000
     P.9.12   V68        -.003      -.013       .001       .000
     P.9.13   V69        -.026      -.004       .009       .000
.000
     P.9.14   V70        -.014      -.029      -.006       .039
.007
     P.9.15   V71         .008       .056      -.056      -.033      -
.046
     LOGANTIG V76         .036       .051      -.020      -.013      -
.017
     LOGTAMA  V79        -.128       .068       .028      -.032
.006


                       P.9.14     P.9.15     LOGANTIG   LOGTAMA
                          V70        V71        V76        V79
     P.9.14   V70         .000
     P.9.15   V71         .010       .000
     LOGANTIG V76         .018      -.015       .000
     LOGTAMA  V79        -.047      -.001       .000       .000


                    AVERAGE ABSOLUTE STANDARDIZED RESIDUALS     =
.0392
       AVERAGE OFF-DIAGONAL ABSOLUTE STANDARDIZED RESIDUALS     =
.0435


  LARGEST STANDARDIZED RESIDUALS:

      NO.    PARAMETER   ESTIMATE      NO.    PARAMETER   ESTIMATE
      ---    ---------   --------      ---    ---------   --------
       1     V65, V8         .191      11     V65, V3         .116
       2     V71, V11        .155      12     V8,  V5        -.113
       3     V76, V1         .150      13     V68, V10       -.110
       4     V76, V11       -.140      14     V71, V10       -.108
       5     V79, V59       -.128      15     V69, V10       -.102
       6     V70, V8         .122      16     V70, V3         .101
       7     V79, V1         .121      17     V69, V17        .098
       8     V76, V6        -.120      18     V68, V5        -.095
       9     V66, V8         .118      19     V65, V2         .095
      10     V76, V8        -.118      20     V71, V16        .093


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)



  DISTRIBUTION OF STANDARDIZED RESIDUALS



     ----------------------------------------
     !                                      !
```

```
  100-                                        -
      !                   *                   !
      !                   *                   !
      !                   *                   !
      !                   *                   !            RANGE       FREQ
PERCENT
   75-                 *  *                   -
      !                *  *                   !    1    -0.5  -  --         0
.00%
      !                *  *                   !    2    -0.4  -  -0.5       0
.00%
      !                *  *                   !    3    -0.3  -  -0.4       0
.00%
      !                *  *                   !    4    -0.2  -  -0.3       0
.00%
   50-                 *  *                   -    5    -0.1  -  -0.2       8
4.21%
      !                *  *                   !    6     0.0  -  -0.1      77
40.53%
      !                *  *                   !    7     0.1  -   0.0      97
51.05%
      !                *  *                   !    8     0.2  -   0.1       8
4.21%
      !                *  *                   !    9     0.3  -   0.2       0
.00%
   25-                 *  *                   -    A     0.4  -   0.3       0
.00%
      !                *  *                   !    B     0.5  -   0.4       0
.00%
      !                *  *                   !    C      ++  -   0.5       0
.00%
      !             *  *  *  *                !    ------------------------
-------
      !             *  *  *  *                !            TOTAL       190
100.00%
     ----------------------------------------
        1  2  3  4  5  6  7  8  9  A  B  C      EACH "*" REPRESENTS   5
RESIDUALS


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)



  GOODNESS OF FIT SUMMARY FOR METHOD = ML

  INDEPENDENCE MODEL CHI-SQUARE        =    1723.600 ON   173 DEGREES OF
FREEDOM

  INDEPENDENCE AIC =  1377.59963   INDEPENDENCE CAIC =    662.10650
         MODEL AIC =   -64.49400          MODEL CAIC =  -651.77738

  CHI-SQUARE =       219.506 BASED ON     142 DEGREES OF FREEDOM
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00003
```

```
  THE NORMAL THEORY RLS CHI-SQUARE FOR THIS ML SOLUTION IS
211.969.

  FIT INDICES
  -----------
  BENTLER-BONETT     NORMED FIT INDEX =      .873
  BENTLER-BONETT NON-NORMED FIT INDEX =      .939
  COMPARATIVE FIT INDEX (CFI)         =      .950
  BOLLEN   (IFI) FIT INDEX            =      .951
  MCDONALD (MFI) FIT INDEX            =      .796
  LISREL    GFI  FIT INDEX            =      .883
  LISREL   AGFI  FIT INDEX            =      .844
  ROOT MEAN-SQUARE RESIDUAL (RMR)     =      .248
  STANDARDIZED RMR                    =      .054
  ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .057
  90% CONFIDENCE INTERVAL OF RMSEA  (        .041,        .071)

  RELIABILITY COEFFICIENTS
  ------------------------
  CRONBACH'S ALPHA                    =      .874
  COEFFICIENT ALPHA FOR AN OPTIMAL SHORT SCALE               =      .891
  BASED ON 10 VARIABLES, ALL EXCEPT:
  P.9.3     P.9.9     P.9.10    P.9.12    P.9.13    P.9.14
  P.9.15    LOGANTIG  LOGTAMA
  RELIABILITY COEFFICIENT RHO         =      .931
  GREATEST LOWER BOUND RELIABILITY                           =      .958
  GLB RELIABILITY FOR AN OPTIMAL SHORT SCALE                 =      .958
  BASED ON ALL VARIABLES
  BENTLER'S DIMENSION-FREE LOWER BOUND RELIABILITY           =      .958
  SHAPIRO'S LOWER BOUND RELIABILITY FOR A WEIGHTED COMPOSITE  =      .964
  WEIGHTS THAT ACHIEVE SHAPIRO'S LOWER BOUND:
  P.1.1     P.1.2     P.1.3     P.1.5     P.1.6     P.1.8
      .262      .272      .265      .271      .279      .247
  P.1.10    P.1.11    P.1.16    P.1.17    P.9.3     P.9.9
      .151      .211      .203      .186      .134      .286
  P.9.10    P.9.12    P.9.13    P.9.14    P.9.15    LOGANTIG
      .305      .272      .274      .223      .186      .019
  LOGTAMA
      .066



  GOODNESS OF FIT SUMMARY FOR METHOD = ROBUST

  ROBUST INDEPENDENCE MODEL CHI-SQUARE =    1661.575 ON   173 DEGREES OF
FREEDOM

  INDEPENDENCE AIC =  1315.57520   INDEPENDENCE CAIC =   600.08207
         MODEL AIC =   -90.41970          MODEL CAIC =  -677.70307

  SATORRA-BENTLER SCALED CHI-SQUARE =    193.5803 ON     142 DEGREES OF
FREEDOM
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00262

  FIT INDICES
  -----------
  BENTLER-BONETT     NORMED FIT INDEX =      .883
  BENTLER-BONETT NON-NORMED FIT INDEX =      .958
```

```
COMPARATIVE FIT INDEX (CFI)          =      .965
BOLLEN   (IFI) FIT INDEX             =      .966
MCDONALD (MFI) FIT INDEX             =      .859
ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .046
90% CONFIDENCE INTERVAL OF RMSEA  (        .028,        .062)


                       ITERATIVE SUMMARY

                   PARAMETER
ITERATION          ABS CHANGE          ALPHA              FUNCTION
    1               1.624992          1.00000             5.41896
    2                .679655          1.00000             3.50584
    3                .604552          1.00000             1.43740
    4                .046960          1.00000             1.30520
    5                .014748          1.00000             1.29891
    6                .002707          1.00000             1.29886
    7                .000859          1.00000             1.29885

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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
  (ROBUST STATISTICS IN PARENTHESES)


 P.1.1   =V1  =   1.000 F1    + 1.000 E1



 P.1.2   =V2  =    .998*F1    + 1.000 E2
                   .091
                 11.016@
               (   .071)
               ( 14.114@

 P.1.3   =V3  =    .963*F1    + 1.000 E3
                   .088
                 10.910@
               (   .070)
               ( 13.835@

 P.1.5   =V5  =   1.000 F3    + 1.000 E5



 P.1.6   =V6  =    .822*F3    + 1.000 E6
```

```
                     .086
                    9.501@
                 (   .075)
                 ( 10.992@

 P.1.8   =V8  =     .770*F1    + 1.000 E8
                     .086
                    8.917@
                 (   .076)
                 ( 10.201@

 P.1.10  =V10 =    1.000 F2    + 1.000 E10



 P.1.11  =V11 =    1.042*F2    + 1.000 E11
                     .154
                    6.786@
                 (   .122)
                 (  8.569@

 P.1.16  =V16 =    1.103*F2    + 1.000 E16
                     .149
                    7.391@
                 (   .117)
                 (  9.445@

 P.1.17  =V17 =     .992*F2    + 1.000 E17
                     .140
                    7.077@
                 (   .127)
                 (  7.799@

 P.9.3   =V59 =     .578*F12   + 1.000 E59
                     .066
                    8.822@
                 (   .083)
                 (  6.957@

 P.9.9   =V65 =    1.000 F14   + 1.000 E65
```

MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS (CONTINUED)

```
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)
  (ROBUST STATISTICS IN PARENTHESES)


 P.9.10  =V66 =   1.084*F14   + 1.000 E66
                   .093
                 11.712@
               (   .093)
               ( 11.621@

 P.9.12  =V68 =   1.000 F13   + 1.000 E68



 P.9.13  =V69 =   1.066*F13   + 1.000 E69
                   .078
                 13.587@
               (   .087)
               ( 12.231@

 P.9.14  =V70 =   1.000 F12   + 1.000 E70



 P.9.15  =V71 =    .817*F12   + 1.000 E71
                   .090
                  9.084@
               (   .110)
               (  7.403@

 LOGANTIG=V76 =   1.000 F17   + 1.000 E76



 LOGTAMA =V79 =   1.000 F16   + 1.000 E79



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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  CONSTRUCT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
```

```
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
  (ROBUST STATISTICS IN PARENTHESES)


    F1   =F1  =   1.000 F5    + 1.000 D1




    F2   =F2  =    .774*F5    + 1.000 D2
                   .120
                  6.460@
               (   .106)
               (  7.268@

    F3   =F3  =    .908*F5    + 1.000 D3
                   .115
                  7.865@
               (   .088)
               ( 10.328@

    F12  =F12 =   1.000 F15   + 1.000 D12




    F13  =F13 =   1.297*F15   + 1.000 D13
                   .157
                  8.242@
               (   .153)
               (  8.458@

    F14  =F14 =   1.476*F15   + 1.000 D14
                   .196
                  7.541@
               (   .233)
               (  6.330@

    F15  =F15 =    .130*F5    +  .032*F16   -  .325*F17   + 1.000 D15
                   .051          .165          .257
                  2.537@         .193        -1.268
               (   .050)     (   .168)     (   .301)
               (  2.591@     (   .189)     ( -1.080)


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES
  ----------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                V                                 F
```

```
                 ---                               ---
                              I F5   -   F5                  4.320*I
                              I                                .888 I
                              I                              4.865@I
                              I                           (    .666)I
                              I                           (  6.489@I
                              I                                     I
                              I F16 -   F16                    .370*I
                              I                                .040 I
                              I                              9.192@I
                              I                           (    .051)I
                              I                           (  7.251@I
                              I                                     I
                              I F17 -   F17                    .126*I
                              I                                .014 I
                              I                              9.192@I
                              I                           (    .018)I
                              I                           (  7.177@I
                              I                                     I


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES
  ----------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                  E                                 D
                 ---                               ---
 E1  -P.1.1              3.523*I D1  -   F1                    .974*I
                           .475 I                                .408 I
                         7.423@I                               2.390@I
                      (    .588)I                           (    .497)I
                      (  5.989@I                           (  1.961@I
                                I                                     I
 E2  -P.1.2              2.492*I D2  -   F2                    .713*I
                           .373 I                                .311 I
                         6.681@I                               2.294@I
                      (    .457)I                           (    .334)I
                      (  5.446@I                           (  2.132@I
                                I                                     I
 E3  -P.1.3              2.450*I D3  -   F3                  3.033*I
                           .359 I                                .680 I
                         6.818@I                               4.459@I
                      (    .442)I                           (    .702)I
                      (  5.543@I                           (  4.319@I
                                I                                     I
 E5  -P.1.5               .451*I D12 -   F12                   .590*I
                           .535 I                                .150 I
                           .843 I                              3.947@I
                      (    .535)I                           (    .183)I
                      (    .844)I                           (  3.222@I
                                I                                     I
 E6  -P.1.6              3.341*I D13 -   F13                   .804*I
                           .511 I                                .197 I
```

```
                           6.534@I                          4.075@I
                        (   .632)I                       (   .248)I
                        (  5.283@I                       (  3.235@I
                                 I                                I
 E8  -P.1.8                3.602*I D14 -   F14                .434*I
                            .440 I                            .211 I
                           8.178@I                          2.061@I
                        (   .465)I                       (   .341)I
                        (  7.745@I                       (  1.275)I
                                 I                                I
 E10 -P.1.10               5.075*I D15 -   F15                .911*I
                            .635 I                            .197 I
                           7.995@I                          4.617@I
                        (   .671)I                       (   .234)I
                        (  7.563@I                       (  3.888@I
                                 I                                I
 E11 -P.1.11               4.856*I                                I
                            .620 I                                I
                           7.828@I                                I
                        (   .569)I                                I
                        (  8.539@I                                I
                                 I                                I
 E16 -P.1.16               3.395*I                                I
                            .487 I                                I
                           6.976@I                                I
                        (   .511)I                                I
                        (  6.646@I                                I
                                 I                                I
 E17 -P.1.17               3.568*I                                I
                            .476 I                                I
                           7.499@I                                I
                        (   .618)I                                I
                        (  5.769@I                                I
                                 I                                I
 E59 -P.9.3                 .606*I                                I
                            .079 I                                I
                           7.675@I                                I
                        (   .098)I                                I
                        (  6.175@I                                I
                                 I                                I
 E65 -P.9.9                1.377*I                                I
                            .215 I                                I
                           6.414@I                                I
                        (   .369)I                                I
                        (  3.733@I                                I
                                 I                                I
```



```
  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES (CONTINUED)
  ----------------------------------------------

 E66 -P.9.10                .650*I                                I
                            .194 I                                I
                           3.349@I                                I
```

```
                      (    .190)I                              I
                      (  3.416@I                               I
                               I                               I
 E68 -P.9.12                .394*I                             I
                            .138 I                             I
                           2.853@I                             I
                      (    .194)I                              I
                      (  2.038@I                               I
                               I                               I
 E69 -P.9.13                .913*I                             I
                            .179 I                             I
                           5.088@I                             I
                      (    .323)I                              I
                      (  2.829@I                               I
                               I                               I
 E70 -P.9.14                .545*I                             I
                            .127 I                             I
                           4.305@I                             I
                      (    .194)I                              I
                      (  2.808@I                               I
                               I                               I
 E71 -P.9.15               1.086*I                             I
                            .145 I                             I
                           7.484@I                             I
                      (    .287)I                              I
                      (  3.784@I                               I
                               I                               I


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  COVARIANCES AMONG INDEPENDENT VARIABLES
  ---------------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                 V                                 F
                ---                               ---
                               I F16 -   F16               .554*I
                               I F5  -   F5                .122 I
                               I                          4.526@I
                               I                       (    .113)I
                               I                       (  4.904@I
                               I                                I
                               I F17 -   F17               .161*I
                               I F5  -   F5                .065 I
                               I                          2.484@I
                               I                       (    .056)I
                               I                       (  2.860@I
                               I                                I
                               I F17 -   F17               .096*I
                               I F16 -   F16               .018 I
                               I                          5.276@I
                               I                       (    .019)I
                               I                       (  5.136@I
                               I                                I
```

```
  TITLE:    Your EQS 6 Model

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  STANDARDIZED SOLUTION:                                                  R-
SQUARED



 P.1.1   =V1  =   .775 F1    + .632 E1
.600
 P.1.2   =V2  =   .824*F1    + .566 E2
.679
 P.1.3   =V3  =   .817*F1    + .577 E3
.667
 P.1.5   =V5  =   .967 F3    + .253 E5
.936
 P.1.6   =V6  =   .756*F3    + .655 E6
.571
 P.1.8   =V8  =   .683*F1    + .731 E8
.466
 P.1.10  =V10 =   .628 F2    + .778 E10
.394
 P.1.11  =V11 =   .652*F2    + .759 E11
.425
 P.1.16  =V16 =   .736*F2    + .677 E16
.542
 P.1.17  =V17 =   .690*F2    + .723 E17
.477
 P.9.3   =V59 =   .682*F12   + .731 E59
.465
 P.9.9   =V65 =   .808 F14   + .590 E65
.652
 P.9.10  =V66 =   .908*F14   + .420 E66
.824
 P.9.12  =V68 =   .928 F13   + .372 E68
.862
 P.9.13  =V69 =   .868*F13   + .496 E69
.754
 P.9.14  =V70 =   .862 F12   + .507 E70
.743
 P.9.15  =V71 =   .701*F12   + .713 E71
.492
 LOGANTIG=V76 =  1.000 F17   + .000 E76
1.000
 LOGTAMA =V79 =  1.000 F16   + .000 E79
1.000
    F1   =F1  =   .903 F5    + .429 D1
.816
    F2   =F2  =   .885*F5    + .465 D2
.784
    F3   =F3  =   .735*F5    + .678 D3
.540
    F12  =F12 =   .791 F15   + .612 D12
.626
    F13  =F13 =   .821*F15   + .571 D13
.674
```

```
    F14  =F14 =   .912*F15   + .410 D14
.832
    F15  =F15 =   .272*F5    + .019*F16   - .117*F17   + .961 D15
.077

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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  CORRELATIONS AMONG INDEPENDENT VARIABLES
  ---------------------------------------

                 V                                F
                ---                              ---
                               I F16 -   F16              .438*I
                               I F5  -   F5                    I
                               I                               I
                               I F17 -   F17              .217*I
                               I F5  -   F5                    I
                               I                               I
                               I F17 -   F17              .444*I
                               I F16 -   F16                   I
                               I                               I



 ------------------------------------------------------------------------
-------
                          E N D    O F    M E T H O D
 ------------------------------------------------------------------------
-------
1
  Execution begins at 17:17:47
  Execution ends   at 17:17:48
  Elapsed time =       1.00 seconds
```

# ANEXO XXII

# MODELO EFECTO MEDIADOR DE LA FLEXIBILIDAD INTERNA DE LA ESTRUCTURA – MODELO B

```
1
  EQS, A STRUCTURAL EQUATION PROGRAM          MULTIVARIATE SOFTWARE, INC.
  COPYRIGHT BY P.M. BENTLER                   VERSION 6.1 (C) 1985 - 2005
(B85).


    PROGRAM CONTROL INFORMATION

        /TITLE
         Your EQS 6 Model
        /SPECIFICATIONS
        VARIABLES= 80 ; CASES= 170 ;
        DATA='C:\tesis1\ticflexrdoscontroltotal.ESS';
        MATRIX=RAW;METHOD=ML,robust;
        /LABELS
        V1=P.1.1; V2=P.1.2; V3=P.1.3; V4=P.1.4; V5=P.1.5;
        V6=P.1.6; V7=P.1.7; V8=P.1.8; V9=P.1.9; V10=P.1.10;
        V11=P.1.11; V12=P.1.12; V13=P.1.13; V14=P.1.14; V15=P.1.15;
        V16=P.1.16; V17=P.1.17; V18=P.2.1; V19=P.2.2; V20=P.2.3;
        V21=P.2.4; V22=P.2.5; V23=P.2.6; V24=P.2.7; V25=P.2.8;
        V26=P.2.9; V27=P.2.10; V28=P.2.11; V29=P.2.12; V30=P.2.13;
        V31=P.2.14; V32=P.2.15; V33=P.3.1; V34=P.3.2; V35=P.3.3;
        V36=P.4.1; V37=P.4.2; V38=P.4.3; V39=P.4.4; V40=P.4.5;
        V41=P.4.6; V42=P.4.7; V43=P.4.8; V44=P.4.9; V45=P.4.10;
        V46=P.4.11; V47=P.6.1; V48=P.6.2; V49=P.6.3; V50=P.6.4;
        V51=P.6.5; V52=P.6.6; V53=P.6.7; V54=P.6.8; V55=P.6.9;
        V56=P.6.10; V57=P.9.1; V58=P.9.2; V59=P.9.3; V60=P.9.4;
        V61=P.9.5; V62=P.9.6; V63=P.9.7; V64=P.9.8; V65=P.9.9;
        V66=P.9.10; V67=P.9.11; V68=P.9.12; V69=P.9.13; V70=P.9.14;
        V71=P.9.15; V72=P.9.16; V73=P.9.17;
        V74=P.11.1; V75=ANTIGUED; V76=LOGANTIG; V77=RAIZANTI; V78=P.10.1;
        V79=LOGTAMA; V80=RAIZTAMA;

        /EQUATIONS
        V1 =   1F1 + E1;
        V2 =   *F1 + E2;
        V3 =   *F1 + E3;
        V5 =    F3 + E5;
        V6 =   *F3 + E6;
        V8 =   *F1 + E8;
        V10 =   1F2 + E10;
        V11 =   *F2 + E11;
        V16 =   *F2 + E16;
        V17 =   *F2 + E17;
        V36 =   1F8 + E36;
        V37 =   *F8 + E37;
        V38 =   *F8 + E38;
        V39 =   *F8 + E39;
        V42 =   1F9 + E42;
        V43 =   *F9 + E43;
        V44 =   *F9 + E44;
        V45 =   *F9 + E45;
        V59 =   *F12 + E59;
        V65 =   1F14 + E65;
```

```
V66 =   *F14 + E66;
V68 =   1F13 + E68;
V69 =   *F13 + E69;
V70 =   1F12 + E70;
V71 =   *F12 + E71;
V76 =   F17 + E76;


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  TITLE:    Your EQS 6 Model

V79 =   F16 + E79;
F1 =   1F5 + D1;
F2 =   *F5 + D2;
F3 =   *F5 + D3;
F8 =   1F11 + D8;
F9 =   *F11 + D9;
F11 =   *F5 + D11;
F12 =   1F15 + D12;
F13 =   *F15 + D13;
F14 =   *F15 + D14;
F15 =   *F11 + *F16 + *F17 + D15;
/VARIANCES
 F5 = *;
 F16=*;
 F17=*;
 E1 = *;
 E2 = *;
 E3 = *;
 E5 = *;
 E8 = *;
 E11 = *;
 E16 = *;
 E17 = *;
 E36 = *;
 E37 = *;
 E38 = *;
 E39 = *;
 E42 = *;
 E43 = *;
 E44 = *;
 E45 = *;
 E59 = *;
 E65 = *;
 E66 = *;
 E68 = *;
 E69 = *;
 E70 = *;
 E71 = *;
 E76 = 0;
 E79 = 0;
 D1 = *;
 D2 = *;
 D3 = *;
 D8 = *;
 D9 = *;
 D11 = *;
 D12 = *;
 D13 = *;
```

```
 D14 = *;
 D15 = *;
/COVARIANCES

 F5,F16 = *;
 F5,F17 = *;
 F16,F17 = *;

/PRINT
```

```
05-Feb-18      PAGE :  3  EQS     Licensee:
  TITLE:    Your EQS 6 Model
```

```
FIT=ALL;
TABLE=EQUATION;
/END
```

```
      112 RECORDS OF INPUT MODEL FILE WERE READ


    DATA IS READ FROM C:\tesis1\ticflexrdoscontroltotal.ESS
    THERE ARE  80 VARIABLES AND   170 CASES
    IT IS A RAW DATA ESS FILE


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  TITLE:    Your EQS 6 Model


  SAMPLE STATISTICS BASED ON COMPLETE CASES


                            UNIVARIATE STATISTICS
                            ---------------------
```

| VARIABLE | P.1.1 V1 | P.1.2 V2 | P.1.3 V3 | P.1.5 V5 | P.1.6 V6 |
|---|---|---|---|---|---|
| MEAN | 3.6941 | 4.0059 | 3.4235 | 4.8765 | 4.4000 |
| SKEWNESS (G1) | -.1427 | -.3284 | -.0187 | -.8703 | -.5597 |
| KURTOSIS (G2) | -1.6839 | -1.4951 | -1.5302 | -.8141 | -1.3132 |
| STANDARD DEV. | 2.9694 | 2.7873 | 2.7126 | 2.6540 | 2.7914 |

| VARIABLE | P.1.8 V8 | P.1.10 V10 | P.1.11 V11 | P.1.16 V16 | P.1.17 V17 |
|---|---|---|---|---|---|
| MEAN | 2.1353 | 4.7059 | 3.5059 | 4.6235 | 4.6176 |
| SKEWNESS (G1) | .8348 | -.7765 | -.0322 | -.7038 | -.6901 |
| KURTOSIS (G2) | -.8715 | -1.1465 | -1.6572 | -1.0836 | -1.0056 |

| | | | | | |
|---|---|---|---|---|---|
| STANDARD DEV. | 2.5971 | 2.8939 | 2.9053 | 2.7217 | 2.6110 |

| VARIABLE | P.4.1 V36 | P.4.2 V37 | P.4.3 V38 | P.4.4 V39 | P.4.7 V42 |
|---|---|---|---|---|---|
| MEAN | 2.7294 | 2.8235 | 2.6882 | 2.6647 | 3.4059 |
| SKEWNESS (G1) | .4621 | .2998 | .4307 | .4202 | .1232 |
| KURTOSIS (G2) | -1.1132 | -1.2121 | -1.1559 | -1.1980 | -1.1944 |
| STANDARD DEV. | 2.4441 | 2.3818 | 2.4185 | 2.4372 | 2.2624 |

| VARIABLE | P.4.8 V43 | P.4.9 V44 | P.4.10 V45 | P.9.3 V59 | P.9.9 V65 |
|---|---|---|---|---|---|
| MEAN | 4.0471 | 3.5353 | 2.7706 | 6.1647 | 4.1824 |
| SKEWNESS (G1) | -.2498 | -.0173 | .4803 | -1.6316 | -.3570 |
| KURTOSIS (G2) | -1.1031 | -1.3026 | -1.0218 | 2.6761 | -.7646 |
| STANDARD DEV. | 2.2710 | 2.3663 | 2.3180 | 1.0642 | 1.9901 |

| VARIABLE | P.9.10 V66 | P.9.12 V68 | P.9.13 V69 | P.9.14 V70 | P.9.15 V71 |
|---|---|---|---|---|---|
| MEAN | 4.5118 | 4.8235 | 4.4235 | 5.8059 | 5.7588 |
| SKEWNESS (G1) | -.5772 | -.5256 | -.4133 | -1.4572 | -1.3098 |
| KURTOSIS (G2) | -.3762 | -.2772 | -.6250 | 2.0533 | 1.3013 |
| STANDARD DEV. | 1.9192 | 1.6900 | 1.9269 | 1.4567 | 1.4618 |

| VARIABLE | LOGANTIG V76 | LOGTAMA V79 |
|---|---|---|
| MEAN | 1.2075 | 1.2278 |
| SKEWNESS (G1) | -.7551 | .7711 |
| KURTOSIS (G2) | 1.3199 | 1.2529 |
| STANDARD DEV. | .3556 | .6087 |

MULTIVARIATE KURTOSIS
---------------------

MARDIA'S COEFFICIENT (G2,P) = 137.1023
NORMALIZED ESTIMATE = 22.5862

ELLIPTICAL THEORY KURTOSIS ESTIMATES
------------------------------------

MARDIA-BASED KAPPA = .1751 MEAN SCALED UNIVARIATE KURTOSIS = -.1894

MARDIA-BASED KAPPA IS USED IN COMPUTATION. KAPPA= .1751

CASE NUMBERS WITH LARGEST CONTRIBUTION TO NORMALIZED MULTIVARIATE KURTOSIS:
---------------------------------------------------------------------------

| | | | | | |
|---|---|---|---|---|---|
| CASE NUMBER | 21 | 56 | 85 | 150 | 158 |
| ESTIMATE | 458.8245 | 417.9891 | 1646.2718 | 806.4739 | 438.5976 |

05-Feb-18 PAGE : 5 EQS Licensee:
TITLE: Your EQS 6 Model

COVARIANCE MATRIX TO BE ANALYZED: 27 VARIABLES (SELECTED FROM 80 VARIABLES)
BASED ON 170 CASES.

| | | P.1.1 V1 | P.1.2 V2 | P.1.3 V3 | P.1.5 V5 | P.1.6 V6 |
|---|---|---|---|---|---|---|
| P.1.1 | V1 | 8.817 | | | | |
| P.1.2 | V2 | 5.617 | 7.769 | | | |
| P.1.3 | V3 | 4.781 | 4.938 | 7.358 | | |
| P.1.5 | V5 | 4.287 | 3.800 | 3.810 | 7.044 | |
| P.1.6 | V6 | 3.147 | 3.353 | 2.978 | 5.417 | 7.792 |
| P.1.8 | V8 | 3.917 | 3.981 | 4.392 | 2.242 | 2.336 |
| P.1.10 | V10 | 3.389 | 3.451 | 3.741 | 3.247 | 2.006 |
| P.1.11 | V11 | 3.327 | 3.399 | 3.441 | 3.282 | 3.004 |
| P.1.16 | V16 | 3.269 | 3.576 | 3.657 | 3.308 | 2.595 |
| P.1.17 | V17 | 2.823 | 3.061 | 3.305 | 3.621 | 2.822 |
| P.4.1 | V36 | .544 | 1.303 | .701 | .073 | .292 |
| P.4.2 | V37 | 1.295 | 1.758 | 1.430 | .795 | 1.195 |
| P.4.3 | V38 | 1.170 | 1.771 | 1.074 | .772 | 1.256 |
| P.4.4 | V39 | 1.394 | 1.653 | 1.107 | .757 | 1.277 |
| P.4.7 | V42 | .746 | 1.441 | 1.312 | .151 | .375 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.4.8 | V43 | 1.352 | 2.183 | 1.773 | .787 | .863 |
| P.4.9 | V44 | .745 | 1.423 | 1.275 | .611 | .560 |
| P.4.10 | V45 | .977 | 1.463 | 1.334 | .758 | 1.288 |
| P.9.3 | V59 | .092 | .384 | .249 | .162 | .336 |
| P.9.9 | V65 | 1.109 | 1.301 | 1.372 | .348 | .867 |
| P.9.10 | V66 | .862 | .843 | .782 | .531 | .818 |
| P.9.12 | V68 | .478 | .463 | .596 | .191 | .822 |
| P.9.13 | V69 | .592 | .873 | 1.021 | .378 | .936 |
| P.9.14 | V70 | .183 | .321 | .905 | .319 | .244 |
| P.9.15 | V71 | .210 | .516 | .618 | .372 | .458 |
| LOGANTIG | V76 | .319 | .236 | .180 | .076 | .001 |
| LOGTAMA | V79 | .772 | .630 | .512 | .438 | .409 |

| | | P.1.8 | P.1.10 | P.1.11 | P.1.16 | P.1.17 |
|---|---|---|---|---|---|---|
| | | V8 | V10 | V11 | V16 | V17 |
| P.1.8 | V8 | 6.745 | | | | |
| P.1.10 | V10 | 2.016 | 8.375 | | | |
| P.1.11 | V11 | 3.316 | 3.724 | 8.441 | | |
| P.1.16 | V16 | 2.886 | 3.528 | 3.795 | 7.408 | |
| P.1.17 | V17 | 2.129 | 3.106 | 3.147 | 3.832 | 6.817 |
| P.4.1 | V36 | 1.226 | .387 | 1.138 | .578 | .985 |
| P.4.2 | V37 | 1.793 | .829 | .954 | .620 | 1.021 |
| P.4.3 | V38 | 1.853 | .440 | 1.348 | .799 | 1.211 |
| P.4.4 | V39 | 1.933 | .422 | 1.543 | .636 | 1.019 |
| P.4.7 | V42 | 1.223 | .233 | 1.285 | .674 | .908 |
| P.4.8 | V43 | 1.390 | .493 | 1.739 | .888 | 1.503 |
| P.4.9 | V44 | 1.330 | -.155 | 1.325 | 1.138 | 1.466 |
| P.4.10 | V45 | 1.729 | .080 | 1.099 | 1.026 | 1.498 |
| P.9.3 | V59 | .279 | .173 | .484 | .352 | .182 |
| P.9.9 | V65 | 1.585 | .427 | 1.014 | 1.110 | .816 |
| P.9.10 | V66 | 1.238 | .252 | .840 | .306 | .712 |
| P.9.12 | V68 | .770 | -.011 | .634 | .359 | .595 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.9.13 | V69 | .954 | -.005 | .838 | .403 | 1.050 |
| P.9.14 | V70 | .867 | .629 | .726 | .418 | .245 |
| P.9.15 | V71 | .654 | -.125 | 1.004 | .737 | .162 |
| LOGANTIG | V76 | .015 | .201 | -.015 | .138 | .114 |
| LOGTAMA | V79 | .436 | .320 | .297 | .472 | .430 |

| | | P.4.1 V36 | P.4.2 V37 | P.4.3 V38 | P.4.4 V39 | P.4.7 V42 |
|---|---|---|---|---|---|---|
| P.4.1 | V36 | 5.974 | | | | |
| P.4.2 | V37 | 3.952 | 5.673 | | | |
| P.4.3 | V38 | 4.033 | 5.270 | 5.849 | | |
| P.4.4 | V39 | 3.678 | 4.988 | 5.226 | 5.940 | |
| P.4.7 | V42 | 1.868 | 2.149 | 2.098 | 2.279 | 5.118 |
| P.4.8 | V43 | 2.338 | 2.653 | 2.630 | 2.797 | 4.093 |
| P.4.9 | V44 | 2.199 | 2.574 | 2.718 | 2.968 | 3.545 |
| P.4.10 | V45 | 2.263 | 2.669 | 2.674 | 2.686 | 2.958 |
| P.9.3 | V59 | .429 | .556 | .703 | .777 | .737 |
| P.9.9 | V65 | 1.020 | 1.506 | 1.477 | 1.576 | 1.571 |
| P.9.10 | V66 | 1.370 | 1.523 | 1.468 | 1.853 | 1.330 |
| P.9.12 | V68 | .828 | 1.087 | .939 | 1.153 | 1.368 |
| P.9.13 | V69 | .819 | 1.247 | 1.133 | 1.415 | 1.614 |
| P.9.14 | V70 | .415 | .468 | .371 | .645 | 1.073 |
| P.9.15 | V71 | .496 | .484 | .741 | .759 | 1.246 |
| LOGANTIG | V76 | -.023 | -.014 | -.047 | -.041 | -.119 |
| LOGTAMA | V79 | .287 | .208 | .212 | .235 | -.055 |

| | | P.4.8 V43 | P.4.9 V44 | P.4.10 V45 | P.9.3 V59 | P.9.9 V65 |
|---|---|---|---|---|---|---|
| P.4.8 | V43 | 5.158 | | | | |
| P.4.9 | V44 | 3.768 | 5.599 | | | |
| P.4.10 | V45 | 3.111 | 4.236 | 5.373 | | |
| P.9.3 | V59 | .856 | .692 | .541 | 1.132 | |
| P.9.9 | V65 | 1.281 | 1.517 | 1.699 | .905 | 3.961 |
| P.9.10 | V66 | 1.313 | 1.429 | 1.491 | 1.022 | 2.800 |
| P.9.12 | V68 | 1.316 | 1.397 | 1.444 | .733 | 1.843 |

```
    P.9.13   V69         1.483      1.583      1.660       .735
1.999
    P.9.14   V70         1.045       .998       .914       .890
1.373
    P.9.15   V71         1.077      1.083       .885       .756
1.352
    LOGANTIG V76         -.031      -.082      -.105       .004
.010
    LOGTAMA  V79          .100       .194       .075      -.052
.160


                       P.9.10     P.9.12     P.9.13     P.9.14     P.9.15
                          V66        V68        V69        V70        V71
    P.9.10   V66         3.683
    P.9.12   V68         2.049      2.856
    P.9.13   V69         2.214      2.625      3.713
    P.9.14   V70         1.561      1.374      1.384      2.122
    P.9.15   V71         1.130       .963       .984      1.308
2.137
    LOGANTIG V76         -.042      -.030      -.035      -.008      -
.022
    LOGTAMA  V79          .116       .035       .079       .010
.042


                       LOGANTIG   LOGTAMA
                          V76        V79
    LOGANTIG V76          .126
    LOGTAMA  V79          .096       .370



   BENTLER-WEEKS STRUCTURAL REPRESENTATION:

         NUMBER OF DEPENDENT VARIABLES = 37
             DEPENDENT V'S :     1    2    3    5    6    8   10   11   16
17
             DEPENDENT V'S :    36   37   38   39   42   43   44   45   59
65
             DEPENDENT V'S :    66   68   69   70   71   76   79
             DEPENDENT F'S :     1    2    3    8    9   11   12   13   14
15

         NUMBER OF INDEPENDENT VARIABLES = 40
             INDEPENDENT F'S :     5   16   17
             INDEPENDENT E'S :     1    2    3    5    6    8   10   11
16   17
             INDEPENDENT E'S :    36   37   38   39   42   43   44   45
59   65
             INDEPENDENT E'S :    66   68   69   70   71   76   79
             INDEPENDENT D'S :     1    2    3    8    9   11   12   13
14   15

         NUMBER OF FREE PARAMETERS =  67
         NUMBER OF FIXED NONZERO PARAMETERS =  50

 *** WARNING MESSAGES ABOVE, IF ANY, REFER TO THE MODEL PROVIDED.
    CALCULATIONS FOR INDEPENDENCE MODEL NOW BEGIN.
```

*** WARNING MESSAGES ABOVE, IF ANY, REFER TO INDEPENDENCE MODEL.
CALCULATIONS FOR USER'S MODEL NOW BEGIN.

3RD STAGE OF COMPUTATION REQUIRED 1687672 WORDS OF MEMORY.
PROGRAM ALLOCATED 200000000 WORDS

DETERMINANT OF INPUT MATRIX IS .13966D+09

*** NOTE *** RESIDUAL-BASED STATISTICS CANNOT BE
CALCULATED BECAUSE OF PIVOTING PROBLEMS.

PARAMETER ESTIMATES APPEAR IN ORDER,
NO SPECIAL PROBLEMS WERE ENCOUNTERED DURING OPTIMIZATION.

RESIDUAL COVARIANCE MATRIX (S-SIGMA) :

| | | P.1.1 V1 | P.1.2 V2 | P.1.3 V3 | P.1.5 V5 | P.1.6 V6 |
|---|---|---|---|---|---|---|
| P.1.1 | V1 | .000 | | | | |
| P.1.2 | V2 | .330 | .000 | | | |
| P.1.3 | V3 | -.298 | -.160 | .000 | | |
| P.1.5 | V5 | .378 | -.125 | .040 | .000 | |
| P.1.6 | V6 | -.077 | .116 | -.132 | .000 | .000 |
| P.1.8 | V8 | -.155 | -.106 | .465 | -.781 | -.157 |
| P.1.10 | V10 | .056 | .106 | .526 | .280 | -.441 |
| P.1.11 | V11 | -.177 | -.118 | .062 | .162 | .430 |
| P.1.16 | V16 | -.425 | -.131 | .096 | .020 | -.117 |
| P.1.17 | V17 | -.508 | -.283 | .093 | .655 | .377 |
| P.4.1 | V36 | -.360 | .396 | -.170 | -.732 | -.371 |
| P.4.2 | V37 | .115 | .574 | .292 | -.256 | .329 |
| P.4.3 | V38 | -.056 | .540 | -.109 | -.320 | .355 |
| P.4.4 | V39 | .226 | .480 | -.019 | -.283 | .419 |
| P.4.7 | V42 | -.519 | .172 | .093 | -.975 | -.554 |
| P.4.8 | V43 | .021 | .848 | .490 | -.398 | -.114 |
| P.4.9 | V44 | -.639 | .034 | -.059 | -.621 | -.456 |
| P.4.10 | V45 | -.251 | .231 | .151 | -.334 | .386 |
| P.9.3 | V59 | -.184 | .107 | -.017 | -.083 | .134 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.9.9 | V65 | .421 | .610 | .708 | -.265 | .362 |
| P.9.10 | V66 | .124 | .102 | .070 | -.126 | .276 |
| P.9.12 | V68 | -.137 | -.155 | .003 | -.357 | .371 |
| P.9.13 | V69 | -.066 | .213 | .387 | -.208 | .453 |
| P.9.14 | V70 | -.286 | -.150 | .453 | -.099 | -.101 |
| P.9.15 | V71 | -.179 | .126 | .242 | .026 | .172 |
| LOGANTIG | V76 | .164 | .080 | .031 | -.062 | -.113 |
| LOGTAMA | V79 | .214 | .070 | -.026 | -.059 | -.001 |

| | | P.1.8 V8 | P.1.10 V10 | P.1.11 V11 | P.1.16 V16 | P.1.17 V17 |
|---|---|---|---|---|---|---|
| P.1.8 | V8 | .000 | | | | |
| P.1.10 | V10 | -.561 | .000 | | | |
| P.1.11 | V11 | .606 | .291 | .000 | | |
| P.1.16 | V16 | .030 | -.090 | -.008 | .000 | |
| P.1.17 | V17 | -.447 | -.157 | -.283 | .216 | .000 |
| P.4.1 | V36 | .528 | -.298 | .417 | -.182 | .299 |
| P.4.2 | V37 | .881 | -.066 | .012 | -.373 | .126 |
| P.4.3 | V38 | .905 | -.491 | .369 | -.233 | .281 |
| P.4.4 | V39 | 1.030 | -.465 | .611 | -.346 | .133 |
| P.4.7 | V42 | .245 | -.728 | .275 | -.389 | -.052 |
| P.4.8 | V43 | .361 | -.517 | .678 | -.231 | .494 |
| P.4.9 | V44 | .260 | -1.205 | .221 | -.026 | .417 |
| P.4.10 | V45 | .780 | -.852 | .119 | -.007 | .566 |
| P.9.3 | V59 | .066 | -.036 | .264 | .120 | -.028 |
| P.9.9 | V65 | 1.053 | -.096 | .465 | .532 | .294 |
| P.9.10 | V66 | .667 | -.308 | .251 | -.314 | .152 |
| P.9.12 | V68 | .294 | -.478 | .143 | -.158 | .128 |
| P.9.13 | V69 | .446 | -.504 | .313 | -.150 | .552 |
| P.9.14 | V70 | .504 | .273 | .351 | .023 | -.111 |
| P.9.15 | V71 | .353 | -.420 | .694 | .410 | -.133 |
| LOGANTIG | V76 | -.105 | .083 | -.138 | .008 | -.003 |

| | | | | | | |
|---|---|---|---|---|---|---|
| LOGTAMA | V79 | .005 | -.104 | -.148 | .003 | .006 |

| | | P.4.1<br>V36 | P.4.2<br>V37 | P.4.3<br>V38 | P.4.4<br>V39 | P.4.7<br>V42 |
|---|---|---|---|---|---|---|
| P.4.1 | V36 | .000 | | | | |
| P.4.2 | V37 | .073 | .000 | | | |
| P.4.3 | V38 | .002 | .003 | .000 | | |
| P.4.4 | V39 | -.161 | -.027 | .014 | .000 | |
| P.4.7 | V42 | .010 | -.278 | -.425 | -.123 | .000 |
| P.4.8 | V43 | .384 | .100 | -.024 | .271 | .488 |
| P.4.9 | V44 | .167 | -.080 | -.041 | .341 | -.204 |
| P.4.10 | V45 | .460 | .314 | .225 | .355 | -.368 |
| P.9.3 | V59 | .026 | .029 | .154 | .256 | .172 |
| P.9.9 | V65 | .013 | .191 | .110 | .275 | .161 |
| P.9.10 | V66 | .290 | .112 | .002 | .457 | -.182 |
| P.9.12 | V68 | -.072 | -.089 | -.283 | -.010 | .108 |
| P.9.13 | V69 | -.143 | -.010 | -.174 | .171 | .267 |
| P.9.14 | V70 | -.272 | -.429 | -.561 | -.243 | .112 |
| P.9.15 | V71 | -.073 | -.260 | -.032 | .023 | .449 |
| LOGANTIG | V76 | -.055 | -.056 | -.091 | -.083 | -.164 |
| LOGTAMA | V79 | .172 | .058 | .056 | .086 | -.216 |

| | | P.4.8<br>V43 | P.4.9<br>V44 | P.4.10<br>V45 | P.9.3<br>V59 | P.9.9<br>V65 |
|---|---|---|---|---|---|---|
| P.4.8 | V43 | .000 | | | | |
| P.4.9 | V44 | -.175 | .000 | | | |
| P.4.10 | V45 | -.387 | .598 | .000 | | |
| P.9.3 | V59 | .262 | .074 | -.007 | .001 | |
| P.9.9 | V65 | -.201 | -.024 | .331 | .057 | .005 |
| P.9.10 | V66 | -.277 | -.225 | .024 | .113 | .006 |
| P.9.12 | V68 | -.009 | .019 | .222 | -.024 | -.047 |
| P.9.13 | V69 | .066 | .109 | .352 | -.076 | -.022 |
| P.9.14 | V70 | .033 | -.053 | -.019 | -.019 | -.069 |
| P.9.15 | V71 | .238 | .211 | .112 | .003 | .157 |
| LOGANTIG | V76 | -.078 | -.131 | -.149 | -.004 | -.008 |

| | | | | | | |
|---|---|---|---|---|---|---|
| LOGTAMA | V79 | -.069 | .018 | -.081 | -.088 | .070 |

| | | P.9.10 V66 | P.9.12 V68 | P.9.13 V69 | P.9.14 V70 | P.9.15 V71 |
|---|---|---|---|---|---|---|
| P.9.10 | V66 | .006 | | | | |
| P.9.12 | V68 | .023 | .004 | | | |
| P.9.13 | V69 | .047 | .004 | .005 | | |
| P.9.14 | V70 | .015 | .085 | .006 | .002 | |
| P.9.15 | V71 | -.152 | -.105 | -.158 | .027 | .002 |
| LOGANTIG | V76 | -.061 | -.046 | -.052 | -.020 | -.032 |
| LOGTAMA | V79 | .020 | -.045 | -.006 | -.051 | -.008 |

| | | LOGANTIG V76 | LOGTAMA V79 |
|---|---|---|---|
| LOGANTIG | V76 | .000 | |
| LOGTAMA | V79 | .000 | .000 |

AVERAGE ABSOLUTE COVARIANCE RESIDUALS = .2118

AVERAGE OFF-DIAGONAL ABSOLUTE COVARIANCE RESIDUALS = .2280

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MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

STANDARDIZED RESIDUAL MATRIX:

| | | P.1.1 V1 | P.1.2 V2 | P.1.3 V3 | P.1.5 V5 | P.1.6 V6 |
|---|---|---|---|---|---|---|
| P.1.1 | V1 | .000 | | | | |
| P.1.2 | V2 | .040 | .000 | | | |
| P.1.3 | V3 | -.037 | -.021 | .000 | | |
| P.1.5 | V5 | .048 | -.017 | .006 | .000 | |
| P.1.6 | V6 | -.009 | .015 | -.017 | .000 | .000 |
| P.1.8 | V8 | -.020 | -.015 | .066 | -.113 | -.022 |
| P.1.10 | V10 | .006 | .013 | .067 | .036 | -.055 |
| P.1.11 | V11 | -.021 | -.015 | .008 | .021 | .053 |
| P.1.16 | V16 | -.053 | -.017 | .013 | .003 | -.015 |
| P.1.17 | V17 | -.066 | -.039 | .013 | .095 | .052 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.4.1 | V36 | -.050 | .058 | -.026 | -.113 | -.054 |
| P.4.2 | V37 | .016 | .086 | .045 | -.041 | .049 |
| P.4.3 | V38 | -.008 | .080 | -.017 | -.050 | .053 |
| P.4.4 | V39 | .031 | .071 | -.003 | -.044 | .062 |
| P.4.7 | V42 | -.077 | .027 | .015 | -.162 | -.088 |
| P.4.8 | V43 | .003 | .134 | .080 | -.066 | -.018 |
| P.4.9 | V44 | -.091 | .005 | -.009 | -.099 | -.069 |
| P.4.10 | V45 | -.036 | .036 | .024 | -.054 | .060 |
| P.9.3 | V59 | -.058 | .036 | -.006 | -.029 | .045 |
| P.9.9 | V65 | .071 | .110 | .131 | -.050 | .065 |
| P.9.10 | V66 | .022 | .019 | .014 | -.025 | .052 |
| P.9.12 | V68 | -.027 | -.033 | .001 | -.079 | .079 |
| P.9.13 | V69 | -.012 | .040 | .074 | -.041 | .084 |
| P.9.14 | V70 | -.066 | -.037 | .115 | -.026 | -.025 |
| P.9.15 | V71 | -.041 | .031 | .061 | .007 | .042 |
| LOGANTIG | V76 | .155 | .081 | .032 | -.066 | -.114 |
| LOGTAMA | V79 | .118 | .041 | -.016 | -.036 | -.001 |

| | | P.1.8 V8 | P.1.10 V10 | P.1.11 V11 | P.1.16 V16 | P.1.17 V17 |
|---|---|---|---|---|---|---|
| P.1.8 | V8 | .000 | | | | |
| P.1.10 | V10 | -.075 | .000 | | | |
| P.1.11 | V11 | .080 | .035 | .000 | | |
| P.1.16 | V16 | .004 | -.011 | -.001 | .000 | |
| P.1.17 | V17 | -.066 | -.021 | -.037 | .030 | .000 |
| P.4.1 | V36 | .083 | -.042 | .059 | -.027 | .047 |
| P.4.2 | V37 | .142 | -.010 | .002 | -.058 | .020 |
| P.4.3 | V38 | .144 | -.070 | .053 | -.035 | .044 |
| P.4.4 | V39 | .163 | -.066 | .086 | -.052 | .021 |
| P.4.7 | V42 | .042 | -.111 | .042 | -.063 | -.009 |
| P.4.8 | V43 | .061 | -.079 | .103 | -.037 | .083 |
| P.4.9 | V44 | .042 | -.176 | .032 | -.004 | .067 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.4.10 | V45 | .130 | -.127 | .018 | -.001 | .094 |
| P.9.3 | V59 | .024 | -.012 | .085 | .042 | -.010 |
| P.9.9 | V65 | .204 | -.017 | .080 | .098 | .057 |
| P.9.10 | V66 | .134 | -.055 | .045 | -.060 | .030 |
| P.9.12 | V68 | .067 | -.098 | .029 | -.034 | .029 |
| P.9.13 | V69 | .089 | -.090 | .056 | -.029 | .110 |
| P.9.14 | V70 | .133 | .065 | .083 | .006 | -.029 |
| P.9.15 | V71 | .093 | -.099 | .163 | .103 | -.035 |
| LOGANTIG | V76 | -.114 | .081 | -.134 | .008 | -.004 |
| LOGTAMA | V79 | .003 | -.059 | -.084 | .002 | .004 |

| | | P.4.1 V36 | P.4.2 V37 | P.4.3 V38 | P.4.4 V39 | P.4.7 V42 |
|---|---|---|---|---|---|---|
| P.4.1 | V36 | .000 | | | | |
| P.4.2 | V37 | .013 | .000 | | | |
| P.4.3 | V38 | .000 | .001 | .000 | | |
| P.4.4 | V39 | -.027 | -.005 | .002 | .000 | |
| P.4.7 | V42 | .002 | -.052 | -.078 | -.022 | .000 |
| P.4.8 | V43 | .069 | .019 | -.004 | .049 | .095 |
| P.4.9 | V44 | .029 | -.014 | -.007 | .059 | -.038 |
| P.4.10 | V45 | .081 | .057 | .040 | .063 | -.070 |
| P.9.3 | V59 | .010 | .011 | .060 | .099 | .072 |
| P.9.9 | V65 | .003 | .040 | .023 | .057 | .036 |
| P.9.10 | V66 | .062 | .025 | .000 | .098 | -.042 |
| P.9.12 | V68 | -.017 | -.022 | -.069 | -.002 | .028 |
| P.9.13 | V69 | -.030 | -.002 | -.037 | .036 | .061 |
| P.9.14 | V70 | -.076 | -.124 | -.159 | -.069 | .034 |
| P.9.15 | V71 | -.020 | -.075 | -.009 | .006 | .136 |
| LOGANTIG | V76 | -.064 | -.066 | -.105 | -.095 | -.204 |
| LOGTAMA | V79 | .116 | .040 | .038 | .058 | -.157 |

| | | P.4.8 V43 | P.4.9 V44 | P.4.10 V45 | P.9.3 V59 | P.9.9 V65 |
|---|---|---|---|---|---|---|
| P.4.8 | V43 | .000 | | | | |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.4.9 | V44 | -.033 | .000 | | | |
| P.4.10 | V45 | -.074 | .109 | .000 | | |
| P.9.3 | V59 | .108 | .030 | -.003 | .001 | |
| P.9.9 | V65 | -.045 | -.005 | .072 | .027 | .001 |
| P.9.10 | V66 | -.064 | -.049 | .005 | .055 | .001 |
| P.9.12 | V68 | -.002 | .005 | .057 | -.013 | -.014 |
| P.9.13 | V69 | .015 | .024 | .079 | -.037 | -.006 |
| P.9.14 | V70 | .010 | -.016 | -.006 | -.012 | -.024 |
| P.9.15 | V71 | .072 | .061 | .033 | .002 | .054 |
| LOGANTIG | V76 | -.096 | -.156 | -.180 | -.010 | -.011 |
| LOGTAMA | V79 | -.050 | .013 | -.057 | -.136 | .058 |

| | | P.9.10 V66 | P.9.12 V68 | P.9.13 V69 | P.9.14 V70 | P.9.15 V71 |
|---|---|---|---|---|---|---|
| P.9.10 | V66 | .002 | | | | |
| P.9.12 | V68 | .007 | .001 | | | |
| P.9.13 | V69 | .013 | .001 | .001 | | |
| P.9.14 | V70 | .005 | .034 | .002 | .001 | |
| P.9.15 | V71 | -.054 | -.043 | -.056 | .012 | .001 |
| LOGANTIG | V76 | -.089 | -.077 | -.076 | -.039 | -.062 |
| LOGTAMA | V79 | .017 | -.044 | -.005 | -.057 | -.009 |

| | | LOGANTIG V76 | LOGTAMA V79 |
|---|---|---|---|
| LOGANTIG | V76 | .000 | |
| LOGTAMA | V79 | .000 | .000 |

AVERAGE ABSOLUTE STANDARDIZED RESIDUALS = .0463

AVERAGE OFF-DIAGONAL ABSOLUTE STANDARDIZED RESIDUALS = .0499

LARGEST STANDARDIZED RESIDUALS:

| NO. | PARAMETER | ESTIMATE | NO. | PARAMETER | ESTIMATE |
|---|---|---|---|---|---|
| 1 | V76, V42 | -.204 | 11 | V76, V1 | .155 |
| 2 | V65, V8 | .204 | 12 | V38, V8 | .144 |
| 3 | V76, V45 | -.180 | 13 | V37, V8 | .142 |
| 4 | V44, V10 | -.176 | 14 | V79, V59 | -.136 |
| 5 | V71, V11 | .163 | 15 | V71, V42 | .136 |
| 6 | V39, V8 | .163 | 16 | V76, V11 | -.134 |
| 7 | V42, V5 | -.162 | 17 | V66, V8 | .134 |

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       8      V70, V38       -.159      18      V43, V2          .134
       9      V79, V42       -.157      19      V70, V8          .133
      10      V76, V44       -.156      20      V65, V3          .131


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  DISTRIBUTION OF STANDARDIZED RESIDUALS


     ----------------------------------------
     !                                      !
  200-                                      -
     !                    *                 !
     !                    *                 !
     !                    *                 !
     !                    *                 !          RANGE      FREQ
PERCENT
  150-                 *  *                 -
     !                 *  *                 !   1   -0.5  -  --        0
.00%
     !                 *  *                 !   2   -0.4  -  -0.5      0
.00%
     !                 *  *                 !   3   -0.3  -  -0.4      0
.00%
     !                 *  *                 !   4   -0.2  -  -0.3      1
.26%
  100-                 *  *                 -   5   -0.1  -  -0.2     16
4.23%
     !                 *  *                 !   6    0.0  -  -0.1    154
40.74%
     !                 *  *                 !   7    0.1  -   0.0    186
49.21%
     !                 *  *                 !   8    0.2  -   0.1     20
5.29%
     !                 *  *                 !   9    0.3  -   0.2      1
.26%
   50-                 *  *                 -   A    0.4  -   0.3      0
.00%
     !                 *  *                 !   B    0.5  -   0.4      0
.00%
     !                 *  *                 !   C     ++  -   0.5      0
.00%
     !              *  *  *  *              !   ------------------------
-------
     !              *  *  *  *              !          TOTAL      378
100.00%
     ----------------------------------------
        1  2  3  4  5  6  7  8  9  A  B  C      EACH "*" REPRESENTS 10
RESIDUALS
```

```
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)



  GOODNESS OF FIT SUMMARY FOR METHOD = ML

  INDEPENDENCE MODEL CHI-SQUARE        =    3198.690 ON   353 DEGREES OF
FREEDOM

  INDEPENDENCE AIC =  2492.69008   INDEPENDENCE CAIC =  1032.75324
         MODEL AIC =  -124.44760          MODEL CAIC = -1410.68091

  CHI-SQUARE =      497.552 BASED ON     311 DEGREES OF FREEDOM
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00000

  THE NORMAL THEORY RLS CHI-SQUARE FOR THIS ML SOLUTION IS
479.664.

  FIT INDICES
  -----------
  BENTLER-BONETT     NORMED FIT INDEX =      .844
  BENTLER-BONETT NON-NORMED FIT INDEX =      .926
  COMPARATIVE FIT INDEX (CFI)         =      .934
  BOLLEN   (IFI) FIT INDEX            =      .935
  MCDONALD (MFI) FIT INDEX            =      .578
  LISREL    GFI  FIT INDEX            =      .826
  LISREL   AGFI  FIT INDEX            =      .789
  ROOT MEAN-SQUARE RESIDUAL (RMR)     =      .301
  STANDARDIZED RMR                    =      .062
  ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .060
  90% CONFIDENCE INTERVAL OF RMSEA  (        .050,        .069)

  RELIABILITY COEFFICIENTS
  ------------------------
  CRONBACH'S ALPHA                    =      .902
  COEFFICIENT ALPHA FOR AN OPTIMAL SHORT SCALE               =      .909
  BASED ON 15 VARIABLES, ALL EXCEPT:
  P.1.1     P.1.2     P.1.3     P.1.5     P.1.6     P.1.8
  P.1.10    P.1.11    P.1.16    P.1.17    LOGANTIG  LOGTAMA
  RELIABILITY COEFFICIENT RHO         =      .953
  GREATEST LOWER BOUND RELIABILITY                           =      .977
  GLB RELIABILITY FOR AN OPTIMAL SHORT SCALE                 =      .978
  BASED ON 24 VARIABLES, ALL EXCEPT:
  P.1.16    P.1.17    LOGANTIG
  BENTLER'S DIMENSION-FREE LOWER BOUND RELIABILITY           =      .977
  SHAPIRO'S LOWER BOUND RELIABILITY FOR A WEIGHTED COMPOSITE  =      .984
  WEIGHTS THAT ACHIEVE SHAPIRO'S LOWER BOUND:
  P.1.1     P.1.2     P.1.3     P.1.5     P.1.6     P.1.8
      .137      .166      .142      .117      .153      .179
  P.1.10    P.1.11    P.1.16    P.1.17    P.4.1     P.4.2
      .062      .124      .097      .120      .241      .354
  P.4.3     P.4.4     P.4.7     P.4.8     P.4.9     P.4.10
      .382      .343      .206      .241      .255      .237
  P.9.3     P.9.9     P.9.10    P.9.12    P.9.13    P.9.14
```

```
      .092      .173      .183      .159      .176      .104
  P.9.15    LOGANTIG  LOGTAMA
      .110     -.001      .043


  GOODNESS OF FIT SUMMARY FOR METHOD = ROBUST

  ROBUST INDEPENDENCE MODEL CHI-SQUARE =    3108.659 ON   353 DEGREES OF
FREEDOM

  INDEPENDENCE AIC =  2402.65943   INDEPENDENCE CAIC =   942.72258
        MODEL AIC =  -205.42219          MODEL CAIC = -1491.65551

  SATORRA-BENTLER SCALED CHI-SQUARE =    416.5778 ON     311 DEGREES OF
FREEDOM
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00006

  FIT INDICES
  -----------
  BENTLER-BONETT     NORMED FIT INDEX =      .866
  BENTLER-BONETT NON-NORMED FIT INDEX =      .957
  COMPARATIVE FIT INDEX (CFI)         =      .962
  BOLLEN   (IFI) FIT INDEX            =      .962
  MCDONALD (MFI) FIT INDEX            =      .733
  ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .045
  90% CONFIDENCE INTERVAL OF RMSEA  (        .033,        .055)


                       ITERATIVE SUMMARY

                   PARAMETER
  ITERATION        ABS CHANGE         ALPHA              FUNCTION
      1             1.677435        1.00000             7.10719
      2              .519654        1.00000             5.10176
      3              .325661        1.00000             3.53620
      4              .076721        1.00000             2.96994
      5              .024839        1.00000             2.94457
      6              .004630        1.00000             2.94414
      7              .001241        1.00000             2.94411
      8              .000465        1.00000             2.94410


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
  (ROBUST STATISTICS IN PARENTHESES)


 P.1.1   =V1  =   1.000 F1    + 1.000 E1
```

```
P.1.2   =V2  =   1.004*F1    + 1.000 E2
                  .091
                11.031@
              (   .071)
              ( 14.165@

P.1.3   =V3  =    .964*F1    + 1.000 E3
                  .089
                10.880@
              (   .070)
              ( 13.728@

P.1.5   =V5  =   1.000 F3    + 1.000 E5



P.1.6   =V6  =    .825*F3    + 1.000 E6
                  .087
                 9.468@
              (   .075)
              ( 10.963@

P.1.8   =V8  =    .773*F1    + 1.000 E8
                  .087
                 8.916@
              (   .076)
              ( 10.220@

P.1.10  =V10 =   1.000 F2    + 1.000 E10



P.1.11  =V11 =   1.051*F2    + 1.000 E11
                  .155
                 6.772@
              (   .124)
              (  8.458@

P.1.16  =V16 =   1.108*F2    + 1.000 E16
                  .151
                 7.350@
              (   .119)
              (  9.282@

P.1.17  =V17 =    .999*F2    + 1.000 E17
                  .142
                 7.052@
              (   .127)
              (  7.877@

P.4.1   =V36 =   1.000 F8    + 1.000 E36
```

```
 P.4.2   =V37 =   1.306*F8    + 1.000 E37
                   .109
                 11.980@
               (   .120)
               ( 10.901@
```

```
  MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
(CONTINUED)
```



```
  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)
  (ROBUST STATISTICS IN PARENTHESES)

 P.4.3   =V38 =   1.358*F8    + 1.000 E38
                   .111
                 12.226@
               (   .127)
               ( 10.659@

 P.4.4   =V39 =   1.293*F8    + 1.000 E39
                   .111
                 11.601@
               (   .123)
               ( 10.492@

 P.4.7   =V42 =   1.000 F9    + 1.000 E42




 P.4.8   =V43 =   1.052*F9    + 1.000 E43
                   .082
                 12.855@
               (   .072)
               ( 14.514@

 P.4.9   =V44 =   1.094*F9    + 1.000 E44
                   .085
                 12.820@
               (   .079)
               ( 13.860@

 P.4.10  =V45 =    .970*F9    + 1.000 E45
                   .086
                 11.224@
               (   .081)
               ( 11.985@
```

```
 P.9.3   =V59 =    .588*F12   + 1.000 E59
                   .066
                  8.868@
               (   .083)
               (  7.076@

 P.9.9   =V65 =   1.000 F14   + 1.000 E65




 P.9.10  =V66 =   1.072*F14   + 1.000 E66
                   .091
                 11.799@
               (   .095)
               ( 11.277@

 P.9.12  =V68 =   1.000 F13   + 1.000 E68




 P.9.13  =V69 =   1.069*F13   + 1.000 E69
                   .078
                 13.767@
               (   .084)
               ( 12.785@

 P.9.14  =V70 =   1.000 F12   + 1.000 E70





  MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
(CONTINUED)


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)
  (ROBUST STATISTICS IN PARENTHESES)

 P.9.15  =V71 =    .829*F12   + 1.000 E71
                   .091
                  9.116@
               (   .111)
               (  7.498@

 LOGANTIG=V76 =   1.000 F17   + 1.000 E76
```

```
 LOGTAMA =V79 =   1.000 F16   + 1.000 E79
```



```
  TITLE:    Your EQS 6 Model

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  CONSTRUCT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
  (ROBUST STATISTICS IN PARENTHESES)


    F1   =F1  =   1.000 F5    + 1.000 D1



    F2   =F2  =    .759*F5    + 1.000 D2
                   .118
                  6.451@
               (   .104)
               (  7.293@

    F3   =F3  =    .890*F5    + 1.000 D3
                   .114
                  7.843@
               (   .086)
               ( 10.399@

    F8   =F8  =   1.000 F11   + 1.000 D8



    F9   =F9  =   1.400*F11   + 1.000 D9
                   .270
                  5.178@
               (   .249)
               (  5.613@

    F11  =F11 =    .206*F5    + 1.000 D11
                   .061
                  3.378@
               (   .063)
               (  3.265@

    F12  =F12 =   1.000 F15   + 1.000 D12
```

```
 F13  =F13 =   1.310*F15   + 1.000 D13
                .157
               8.355@
            (   .160)
            (  8.204@

 F14  =F14 =   1.466*F15   + 1.000 D14
                .189
               7.749@
            (   .225)
            (  6.518@

 F15  =F15 =    .517*F11   +  .017*F16   -  .046*F17   + 1.000 D15
                .109          .137          .230
               4.724@         .121         -.201
            (   .117)     (   .139)     (   .245)
            (  4.408@     (   .120)     (  -.189)


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  TITLE:    Your EQS 6 Model

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES
  ----------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                V                                F
               ---                              ---
                              I F5  -   F5              4.391*I
                              I                          .895 I
                              I                         4.909@I
                              I                      (   .665)I
                              I                      (  6.606@I
                              I                               I
                              I F16 -   F16              .370*I
                              I                          .040 I
                              I                         9.192@I
                              I                      (   .051)I
                              I                      (  7.251@I
                              I                               I
                              I F17 -   F17              .126*I
                              I                          .014 I
                              I                         9.192@I
                              I                      (   .018)I
                              I                      (  7.177@I
                              I                               I
```

```
 TITLE:    Your EQS 6 Model

 MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

 VARIANCES OF INDEPENDENT VARIABLES
 ----------------------------------
 STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                E                                D
               ---                              ---
E1  -P.1.1               3.550*I D1  -   F1              .876*I
                          .476 I                         .399 I
                         7.464@I                        2.197@I
                      (   .592)I                     (   .472)I
                      (  5.997@I                     (  1.854)I
                               I                              I
E2  -P.1.2               2.462*I D2  -   F2              .734*I
                          .369 I                         .309 I
                         6.663@I                        2.374@I
                      (   .451)I                     (   .326)I
                      (  5.455@I                     (  2.252@I
                               I                              I
E3  -P.1.3               2.460*I D3  -   F3             3.087*I
                          .359 I                         .682 I
                         6.858@I                        4.528@I
                      (   .442)I                     (   .708)I
                      (  5.561@I                     (  4.358@I
                               I                              I
E5  -P.1.5                .476*I D8  -   F8             1.642*I
                          .538 I                         .373 I
                          .884 I                        4.397@I
                      (   .541)I                     (   .360)I
                      (   .879)I                     (  4.562@I
                               I                              I
E6  -P.1.6               3.325*I D9  -   F9              .826*I
                          .513 I                         .411 I
                         6.479@I                        2.013@I
                      (   .632)I                     (   .477)I
                      (  5.261@I                     (  1.732)I
                               I                              I
E8  -P.1.8               3.596*I D11 -   F11            1.141*I
                          .439 I                         .342 I
                         8.185@I                        3.333@I
                      (   .463)I                     (   .340)I
                      (  7.774@I                     (  3.352@I
                               I                              I
E10 -P.1.10              5.110*I D12 -   F12             .562*I
                          .638 I                         .144 I
                         8.016@I                        3.918@I
                      (   .672)I                     (   .174)I
                      (  7.609@I                     (  3.225@I
                               I                              I
E11 -P.1.11              4.832*I D13 -   F13             .762*I
                          .619 I                         .186 I
                         7.811@I                        4.092@I
                      (   .570)I                     (   .220)I
                      (  8.480@I                     (  3.467@I
                               I                              I
```

```
 E16 -P.1.16              3.399*I D14 -   F14             .491*I
                           .487 I                          .198 I
                          6.980@I                         2.481@I
                       (   .513)I                      (   .320)I
                       (  6.627@I                      (  1.537)I
                                I                               I
 E17 -P.1.17              3.557*I D15 -   F15             .628*I
                           .475 I                          .149 I
                          7.487@I                         4.207@I
                       (   .611)I                      (   .180)I
                       (  5.826@I                      (  3.481@I
                                I                               I
 E36 -P.4.1               3.004*I                               I
                           .338 I                               I
                          8.880@I                               I
                       (   .471)I                               I
                       (  6.378@I                               I
                                I                               I
 E37 -P.4.2                .606*I                               I
                           .100 I                               I
                          6.075@I                               I
                       (   .187)I                               I
                       (  3.243@I                               I
                                I                               I


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES (CONTINUED)
  ----------------------------------------------

 E38 -P.4.3                .374*I                               I
                           .089 I                               I
                          4.199@I                               I
                       (   .292)I                               I
                       (  1.282)I                               I
                                I                               I
 E39 -P.4.4                .978*I                               I
                           .131 I                               I
                          7.454@I                               I
                       (   .347)I                               I
                       (  2.819@I                               I
                                I                               I
 E42 -P.4.7               1.691*I                               I
                           .234 I                               I
                          7.221@I                               I
                       (   .273)I                               I
                       (  6.204@I                               I
                                I                               I
 E43 -P.4.8               1.365*I                               I
                           .211 I                               I
                          6.472@I                               I
                       (   .353)I                               I
                       (  3.865@I                               I
                                I                               I
```

```
 E44 -P.4.9                 1.500*I                                I
                             .230 I                                I
                            6.515@I                                I
                         (   .373)I                                I
                         (  4.024@I                                I
                                  I                                I
 E45 -P.4.10                2.145*I                                I
                             .277 I                                I
                            7.743@I                                I
                         (   .286)I                                I
                         (  7.498@I                                I
                                  I                                I
 E59 -P.9.3                  .598*I                                I
                             .078 I                                I
                            7.624@I                                I
                         (   .097)I                                I
                         (  6.147@I                                I
                                  I                                I
 E65 -P.9.9                 1.350*I                                I
                             .212 I                                I
                            6.356@I                                I
                         (   .376)I                                I
                         (  3.587@I                                I
                                  I                                I
 E66 -P.9.10                 .681*I                                I
                             .191 I                                I
                            3.557@I                                I
                         (   .200)I                                I
                         (  3.412@I                                I
                                  I                                I
 E68 -P.9.12                 .401*I                                I
                             .135 I                                I
                            2.975@I                                I
                         (   .186)I                                I
                         (  2.161@I                                I
                                  I                                I
 E69 -P.9.13                 .905*I                                I
                             .176 I                                I
                            5.144@I                                I
                         (   .315)I                                I
                         (  2.877@I                                I
                                  I                                I
 E70 -P.9.14                 .574*I                                I
                             .126 I                                I
                            4.554@I                                I
                         (   .195)I                                I
                         (  2.941@I                                I
                                  I                                I


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES (CONTINUED)
  ----------------------------------------------

 E71 -P.9.15                1.073*I                                I
```

```
                          .144 I                                I
                         7.438@I                                I
                      (   .281)I                                I
                      (  3.819@I                                I
                               I                                I


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  COVARIANCES AMONG INDEPENDENT VARIABLES
  ---------------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                 V                                F
                ---                              ---
                               I F16 -   F16              .558*I
                               I F5  -   F5               .123 I
                               I                         4.542@I
                               I                      (   .115)I
                               I                      (  4.858@I
                               I                               I
                               I F17 -   F17              .155*I
                               I F5  -   F5               .065 I
                               I                         2.395@I
                               I                      (   .058)I
                               I                      (  2.689@I
                               I                               I
                               I F17 -   F17              .096*I
                               I F16 -   F16              .018 I
                               I                         5.276@I
                               I                      (   .019)I
                               I                      (  5.136@I
                               I                               I


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  STANDARDIZED SOLUTION:                                             R-
SQUARED



 P.1.1   =V1  =   .773 F1    + .635 E1
.597
 P.1.2   =V2  =   .826*F1    + .563 E2
.683
 P.1.3   =V3  =   .816*F1    + .578 E3
.666
 P.1.5   =V5  =   .966 F3    + .260 E5
.932
```

```
 P.1.6   =V6  =   .757*F3    + .653 E6
.573
 P.1.8   =V8  =   .683*F1    + .730 E8
.467
 P.1.10  =V10 =   .624 F2    + .781 E10
.390
 P.1.11  =V11 =   .654*F2    + .757 E11
.428
 P.1.16  =V16 =   .736*F2    + .677 E16
.541
 P.1.17  =V17 =   .692*F2    + .722 E17
.478
 P.4.1   =V36 =   .705 F8    + .709 E36
.497
 P.4.2   =V37 =   .945*F8    + .327 E37
.893
 P.4.3   =V38 =   .967*F8    + .253 E38
.936
 P.4.4   =V39 =   .914*F8    + .406 E39
.835
 P.4.7   =V42 =   .818 F9    + .575 E42
.670
 P.4.8   =V43 =   .857*F9    + .515 E43
.735
 P.4.9   =V44 =   .856*F9    + .518 E44
.732
 P.4.10  =V45 =   .775*F9    + .632 E45
.601
 P.9.3   =V59 =   .687*F12   + .727 E59
.472
 P.9.9   =V65 =   .812 F14   + .584 E65
.659
 P.9.10  =V66 =   .903*F14   + .430 E66
.815
 P.9.12  =V68 =   .927 F13   + .375 E68
.859
 P.9.13  =V69 =   .869*F13   + .494 E69
.756
 P.9.14  =V70 =   .854 F12   + .520 E70
.729
 P.9.15  =V71 =   .705*F12   + .709 E71
.497
 LOGANTIG=V76 =  1.000 F17   + .000 E76
1.000
 LOGTAMA =V79 =  1.000 F16   + .000 E79
1.000
    F1   =F1  =   .913 F5    + .408 D1
.834
    F2   =F2  =   .880*F5    + .474 D2
.775
    F3   =F3  =   .728*F5    + .686 D3
.530
    F8   =F8  =   .669 F11   + .744 D8
.447
    F9   =F9  =   .871*F11   + .491 D9
.759
    F11  =F11 =   .374*F5    + .927 D11
.140
```

```
    F12  =F12 =   .798 F15   + .603 D12
.636
    F13  =F13 =   .830*F15   + .558 D13
.689
    F14  =F14 =   .901*F15   + .434 D14
.811
    F15  =F15 =   .601*F11   + .010*F16   - .017*F17   + .799 D15
.362


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  CORRELATIONS AMONG INDEPENDENT VARIABLES
  ---------------------------------------

                 V                                F
                ---                              ---
                              I F16 -   F16               .438*I
                              I F5  -   F5                     I
                              I                                I
                              I F17 -   F17               .208*I
                              I F5  -   F5                     I
                              I                                I
                              I F17 -   F17               .444*I
                              I F16 -   F16                    I
                              I                                I



 ------------------------------------------------------------------------
-------
                           E N D   O F   M E T H O D
 ------------------------------------------------------------------------
-------
1
  Execution begins at 18:13:35
  Execution ends   at 18:13:37
  Elapsed time =       2.00 seconds
```

# ANEXO XIII

# MODELO EFECTO MEDIADOR DE LA FLEXIBILIDAD INTERNA DE LA ESTRUCTURA – MODELO C

```
1
  EQS, A STRUCTURAL EQUATION PROGRAM          MULTIVARIATE SOFTWARE, INC.
  COPYRIGHT BY P.M. BENTLER                   VERSION 6.1 (C) 1985 - 2005
(B85).


    PROGRAM CONTROL INFORMATION

     /TITLE
      Your EQS 6 Model
     /SPECIFICATIONS
     VARIABLES= 80 ; CASES= 170 ;
     DATA='C:\tesis1\ticflexrdoscontroltotal.ESS';
     MATRIX=RAW;METHOD=ML,robust;
     /LABELS
     V1=P.1.1; V2=P.1.2; V3=P.1.3; V4=P.1.4; V5=P.1.5;
     V6=P.1.6; V7=P.1.7; V8=P.1.8; V9=P.1.9; V10=P.1.10;
     V11=P.1.11; V12=P.1.12; V13=P.1.13; V14=P.1.14; V15=P.1.15;
     V16=P.1.16; V17=P.1.17; V18=P.2.1; V19=P.2.2; V20=P.2.3;
     V21=P.2.4; V22=P.2.5; V23=P.2.6; V24=P.2.7; V25=P.2.8;
     V26=P.2.9; V27=P.2.10; V28=P.2.11; V29=P.2.12; V30=P.2.13;
     V31=P.2.14; V32=P.2.15; V33=P.3.1; V34=P.3.2; V35=P.3.3;
     V36=P.4.1; V37=P.4.2; V38=P.4.3; V39=P.4.4; V40=P.4.5;
     V41=P.4.6; V42=P.4.7; V43=P.4.8; V44=P.4.9; V45=P.4.10;
     V46=P.4.11; V47=P.6.1; V48=P.6.2; V49=P.6.3; V50=P.6.4;
     V51=P.6.5; V52=P.6.6; V53=P.6.7; V54=P.6.8; V55=P.6.9;
     V56=P.6.10; V57=P.9.1; V58=P.9.2; V59=P.9.3; V60=P.9.4;
     V61=P.9.5; V62=P.9.6; V63=P.9.7; V64=P.9.8; V65=P.9.9;
     V66=P.9.10; V67=P.9.11; V68=P.9.12; V69=P.9.13; V70=P.9.14;
     V71=P.9.15; V72=P.9.16; V73=P.9.17;
     V74=P.11.1; V75=ANTIGUED; V76=LOGANTIG; V77=RAIZANTI; V78=P.10.1;
     V79=LOGTAMA; V80=RAIZTAMA;

     /EQUATIONS
     V1 =   1F1 + E1;
     V2 =   *F1 + E2;
     V3 =   *F1 + E3;
     V5 =    F3 + E5;
     V6 =   *F3 + E6;
     V8 =   *F1 + E8;
     V10 =   1F2 + E10;
     V11 =   *F2 + E11;
     V16 =   *F2 + E16;
     V17 =   *F2 + E17;
     V36 =   1F8 + E36;
     V37 =   *F8 + E37;
     V38 =   *F8 + E38;
     V39 =   *F8 + E39;
     V42 =   1F9 + E42;
     V43 =   *F9 + E43;
     V44 =   *F9 + E44;
     V45 =   *F9 + E45;
     V59 =   *F12 + E59;
     V65 =   1F14 + E65;
```

```
V66 =   *F14 + E66;
V68 =   1F13 + E68;
V69 =   *F13 + E69;
V70 =   1F12 + E70;
V71 =   *F12 + E71;
V76 =   F17 + E76;


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V79 =   F16 + E79;
F1 =   1F5 + D1;
F2 =   *F5 + D2;
F3 =   *F5 + D3;
F8 =   1F11 + D8;
F9 =   *F11 + D9;
F11 =   *F5 + D11;
F12 =   1F15 + D12;
F13 =   *F15 + D13;
F14 =   *F15 + D14;
F15 =   *F5 + *F11 + *F16 + *F17 + D15;
/VARIANCES
 F5 = *;
 F16=*;
 F17=*;
 E1 = *;
 E2 = *;
 E3 = *;
 E5 = *;
 E8 = *;
 E11 = *;
 E16 = *;
 E17 = *;
 E36 = *;
 E37 = *;
 E38 = *;
 E39 = *;
 E42 = *;
 E43 = *;
 E44 = *;
 E45 = *;
 E59 = *;
 E65 = *;
 E66 = *;
 E68 = *;
 E69 = *;
 E70 = *;
 E71 = *;
 E76 = 0;
 E79 = 0;
 D1 = *;
 D2 = *;
 D3 = *;
 D8 = *;
 D9 = *;
 D11 = *;
 D12 = *;
 D13 = *;
```

```
  D14 = *;
  D15 = *;
/COVARIANCES

  F5,F16 = *;
  F5,F17 = *;
  F16,F17 = *;

/PRINT
```

```
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```

```
FIT=ALL;
TABLE=EQUATION;
/END
```

```
      112 RECORDS OF INPUT MODEL FILE WERE READ


    DATA IS READ FROM C:\tesis1\ticflexrdoscontroltotal.ESS
    THERE ARE  80 VARIABLES AND   170 CASES
    IT IS A RAW DATA ESS FILE


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  TITLE:    Your EQS 6 Model


  SAMPLE STATISTICS BASED ON COMPLETE CASES
```

UNIVARIATE STATISTICS

---------------------

| VARIABLE | P.1.1 V1 | P.1.2 V2 | P.1.3 V3 | P.1.5 V5 | P.1.6 V6 |
|---|---|---|---|---|---|
| MEAN | 3.6941 | 4.0059 | 3.4235 | 4.8765 | 4.4000 |
| SKEWNESS (G1) | -.1427 | -.3284 | -.0187 | -.8703 | -.5597 |
| KURTOSIS (G2) | -1.6839 | -1.4951 | -1.5302 | -.8141 | -1.3132 |
| STANDARD DEV. | 2.9694 | 2.7873 | 2.7126 | 2.6540 | 2.7914 |

| VARIABLE | P.1.8 V8 | P.1.10 V10 | P.1.11 V11 | P.1.16 V16 | P.1.17 V17 |
|---|---|---|---|---|---|
| MEAN | 2.1353 | 4.7059 | 3.5059 | 4.6235 | 4.6176 |
| SKEWNESS (G1) | .8348 | -.7765 | -.0322 | -.7038 | -.6901 |
| KURTOSIS (G2) | -.8715 | -1.1465 | -1.6572 | -1.0836 | -1.0056 |

| | | | | | |
|---|---|---|---|---|---|
| STANDARD DEV. | 2.5971 | 2.8939 | 2.9053 | 2.7217 | 2.6110 |

| VARIABLE | P.4.1 V36 | P.4.2 V37 | P.4.3 V38 | P.4.4 V39 | P.4.7 V42 |
|---|---|---|---|---|---|
| MEAN | 2.7294 | 2.8235 | 2.6882 | 2.6647 | 3.4059 |
| SKEWNESS (G1) | .4621 | .2998 | .4307 | .4202 | .1232 |
| KURTOSIS (G2) | -1.1132 | -1.2121 | -1.1559 | -1.1980 | -1.1944 |
| STANDARD DEV. | 2.4441 | 2.3818 | 2.4185 | 2.4372 | 2.2624 |

| VARIABLE | P.4.8 V43 | P.4.9 V44 | P.4.10 V45 | P.9.3 V59 | P.9.9 V65 |
|---|---|---|---|---|---|
| MEAN | 4.0471 | 3.5353 | 2.7706 | 6.1647 | 4.1824 |
| SKEWNESS (G1) | -.2498 | -.0173 | .4803 | -1.6316 | -.3570 |
| KURTOSIS (G2) | -1.1031 | -1.3026 | -1.0218 | 2.6761 | -.7646 |
| STANDARD DEV. | 2.2710 | 2.3663 | 2.3180 | 1.0642 | 1.9901 |

| VARIABLE | P.9.10 V66 | P.9.12 V68 | P.9.13 V69 | P.9.14 V70 | P.9.15 V71 |
|---|---|---|---|---|---|
| MEAN | 4.5118 | 4.8235 | 4.4235 | 5.8059 | 5.7588 |
| SKEWNESS (G1) | -.5772 | -.5256 | -.4133 | -1.4572 | -1.3098 |
| KURTOSIS (G2) | -.3762 | -.2772 | -.6250 | 2.0533 | 1.3013 |
| STANDARD DEV. | 1.9192 | 1.6900 | 1.9269 | 1.4567 | 1.4618 |

| VARIABLE | LOGANTIG V76 | LOGTAMA V79 |
|---|---|---|
| MEAN | 1.2075 | 1.2278 |
| SKEWNESS (G1) | -.7551 | .7711 |
| KURTOSIS (G2) | 1.3199 | 1.2529 |
| STANDARD DEV. | .3556 | .6087 |

MULTIVARIATE KURTOSIS
---------------------

MARDIA'S COEFFICIENT (G2,P) = 137.1023
NORMALIZED ESTIMATE = 22.5862

```
                     ELLIPTICAL THEORY KURTOSIS ESTIMATES
                     ------------------------------------

   MARDIA-BASED KAPPA =       .1751 MEAN SCALED UNIVARIATE KURTOSIS =
-.1894

   MARDIA-BASED KAPPA IS USED IN COMPUTATION. KAPPA=            .1751


   CASE NUMBERS WITH LARGEST CONTRIBUTION TO NORMALIZED MULTIVARIATE
KURTOSIS:
   -------------------------------------------------------------------------
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   CASE NUMBER        21          56          85          150
158

   ESTIMATE       458.8245     417.9891    1646.2718     806.4739
438.5976


05-Feb-18      PAGE :  5  EQS     Licensee:
  TITLE:    Your EQS 6 Model

  COVARIANCE  MATRIX TO BE ANALYZED:  27 VARIABLES (SELECTED FROM  80
VARIABLES)
  BASED ON   170 CASES.


                        P.1.1      P.1.2      P.1.3      P.1.5      P.1.6
                          V1         V2         V3         V5         V6
    P.1.1    V1         8.817
    P.1.2    V2         5.617      7.769
    P.1.3    V3         4.781      4.938      7.358
    P.1.5    V5         4.287      3.800      3.810      7.044
    P.1.6    V6         3.147      3.353      2.978      5.417
7.792
    P.1.8    V8         3.917      3.981      4.392      2.242
2.336
    P.1.10   V10        3.389      3.451      3.741      3.247
2.006
    P.1.11   V11        3.327      3.399      3.441      3.282
3.004
    P.1.16   V16        3.269      3.576      3.657      3.308
2.595
    P.1.17   V17        2.823      3.061      3.305      3.621
2.822
    P.4.1    V36         .544      1.303       .701       .073
.292
    P.4.2    V37        1.295      1.758      1.430       .795
1.195
    P.4.3    V38        1.170      1.771      1.074       .772
1.256
    P.4.4    V39        1.394      1.653      1.107       .757
1.277
    P.4.7    V42         .746      1.441      1.312       .151
.375
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| | | | | | | |
|---|---|---|---|---|---|---|
| P.4.8 | V43 | 1.352 | 2.183 | 1.773 | .787 | .863 |
| P.4.9 | V44 | .745 | 1.423 | 1.275 | .611 | .560 |
| P.4.10 | V45 | .977 | 1.463 | 1.334 | .758 | 1.288 |
| P.9.3 | V59 | .092 | .384 | .249 | .162 | .336 |
| P.9.9 | V65 | 1.109 | 1.301 | 1.372 | .348 | .867 |
| P.9.10 | V66 | .862 | .843 | .782 | .531 | .818 |
| P.9.12 | V68 | .478 | .463 | .596 | .191 | .822 |
| P.9.13 | V69 | .592 | .873 | 1.021 | .378 | .936 |
| P.9.14 | V70 | .183 | .321 | .905 | .319 | .244 |
| P.9.15 | V71 | .210 | .516 | .618 | .372 | .458 |
| LOGANTIG | V76 | .319 | .236 | .180 | .076 | .001 |
| LOGTAMA | V79 | .772 | .630 | .512 | .438 | .409 |

| | | P.1.8<br>V8 | P.1.10<br>V10 | P.1.11<br>V11 | P.1.16<br>V16 | P.1.17<br>V17 |
|---|---|---|---|---|---|---|
| P.1.8 | V8 | 6.745 | | | | |
| P.1.10 | V10 | 2.016 | 8.375 | | | |
| P.1.11 | V11 | 3.316 | 3.724 | 8.441 | | |
| P.1.16 | V16 | 2.886 | 3.528 | 3.795 | 7.408 | |
| P.1.17 | V17 | 2.129 | 3.106 | 3.147 | 3.832 | 6.817 |
| P.4.1 | V36 | 1.226 | .387 | 1.138 | .578 | .985 |
| P.4.2 | V37 | 1.793 | .829 | .954 | .620 | 1.021 |
| P.4.3 | V38 | 1.853 | .440 | 1.348 | .799 | 1.211 |
| P.4.4 | V39 | 1.933 | .422 | 1.543 | .636 | 1.019 |
| P.4.7 | V42 | 1.223 | .233 | 1.285 | .674 | .908 |
| P.4.8 | V43 | 1.390 | .493 | 1.739 | .888 | 1.503 |
| P.4.9 | V44 | 1.330 | -.155 | 1.325 | 1.138 | 1.466 |
| P.4.10 | V45 | 1.729 | .080 | 1.099 | 1.026 | 1.498 |
| P.9.3 | V59 | .279 | .173 | .484 | .352 | .182 |
| P.9.9 | V65 | 1.585 | .427 | 1.014 | 1.110 | .816 |
| P.9.10 | V66 | 1.238 | .252 | .840 | .306 | .712 |
| P.9.12 | V68 | .770 | -.011 | .634 | .359 | .595 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.9.13 | V69 | .954 | -.005 | .838 | .403 | 1.050 |
| P.9.14 | V70 | .867 | .629 | .726 | .418 | .245 |
| P.9.15 | V71 | .654 | -.125 | 1.004 | .737 | .162 |
| LOGANTIG | V76 | .015 | .201 | -.015 | .138 | .114 |
| LOGTAMA | V79 | .436 | .320 | .297 | .472 | .430 |

| | | P.4.1 V36 | P.4.2 V37 | P.4.3 V38 | P.4.4 V39 | P.4.7 V42 |
|---|---|---|---|---|---|---|
| P.4.1 | V36 | 5.974 | | | | |
| P.4.2 | V37 | 3.952 | 5.673 | | | |
| P.4.3 | V38 | 4.033 | 5.270 | 5.849 | | |
| P.4.4 | V39 | 3.678 | 4.988 | 5.226 | 5.940 | |
| P.4.7 | V42 | 1.868 | 2.149 | 2.098 | 2.279 | 5.118 |
| P.4.8 | V43 | 2.338 | 2.653 | 2.630 | 2.797 | 4.093 |
| P.4.9 | V44 | 2.199 | 2.574 | 2.718 | 2.968 | 3.545 |
| P.4.10 | V45 | 2.263 | 2.669 | 2.674 | 2.686 | 2.958 |
| P.9.3 | V59 | .429 | .556 | .703 | .777 | .737 |
| P.9.9 | V65 | 1.020 | 1.506 | 1.477 | 1.576 | 1.571 |
| P.9.10 | V66 | 1.370 | 1.523 | 1.468 | 1.853 | 1.330 |
| P.9.12 | V68 | .828 | 1.087 | .939 | 1.153 | 1.368 |
| P.9.13 | V69 | .819 | 1.247 | 1.133 | 1.415 | 1.614 |
| P.9.14 | V70 | .415 | .468 | .371 | .645 | 1.073 |
| P.9.15 | V71 | .496 | .484 | .741 | .759 | 1.246 |
| LOGANTIG | V76 | -.023 | -.014 | -.047 | -.041 | -.119 |
| LOGTAMA | V79 | .287 | .208 | .212 | .235 | -.055 |

| | | P.4.8 V43 | P.4.9 V44 | P.4.10 V45 | P.9.3 V59 | P.9.9 V65 |
|---|---|---|---|---|---|---|
| P.4.8 | V43 | 5.158 | | | | |
| P.4.9 | V44 | 3.768 | 5.599 | | | |
| P.4.10 | V45 | 3.111 | 4.236 | 5.373 | | |
| P.9.3 | V59 | .856 | .692 | .541 | 1.132 | |
| P.9.9 | V65 | 1.281 | 1.517 | 1.699 | .905 | 3.961 |
| P.9.10 | V66 | 1.313 | 1.429 | 1.491 | 1.022 | 2.800 |
| P.9.12 | V68 | 1.316 | 1.397 | 1.444 | .733 | 1.843 |

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     P.9.13   V69         1.483      1.583      1.660       .735
1.999
     P.9.14   V70         1.045       .998       .914       .890
1.373
     P.9.15   V71         1.077      1.083       .885       .756
1.352
     LOGANTIG V76         -.031      -.082      -.105       .004
.010
     LOGTAMA  V79          .100       .194       .075      -.052
.160


                       P.9.10     P.9.12     P.9.13     P.9.14     P.9.15
                          V66        V68        V69        V70        V71
     P.9.10   V66         3.683
     P.9.12   V68         2.049      2.856
     P.9.13   V69         2.214      2.625      3.713
     P.9.14   V70         1.561      1.374      1.384      2.122
     P.9.15   V71         1.130       .963       .984      1.308
2.137
     LOGANTIG V76         -.042      -.030      -.035      -.008      -
.022
     LOGTAMA  V79          .116       .035       .079       .010
.042


                       LOGANTIG   LOGTAMA
                          V76        V79
     LOGANTIG V76          .126
     LOGTAMA  V79          .096       .370



  BENTLER-WEEKS STRUCTURAL REPRESENTATION:

        NUMBER OF DEPENDENT VARIABLES = 37
            DEPENDENT V'S :     1    2    3    5    6    8   10   11   16
17
            DEPENDENT V'S :    36   37   38   39   42   43   44   45   59
65
            DEPENDENT V'S :    66   68   69   70   71   76   79
            DEPENDENT F'S :     1    2    3    8    9   11   12   13   14
15

        NUMBER OF INDEPENDENT VARIABLES = 40
            INDEPENDENT F'S :     5   16   17
            INDEPENDENT E'S :     1    2    3    5    6    8   10   11
16   17
            INDEPENDENT E'S :    36   37   38   39   42   43   44   45
59   65
            INDEPENDENT E'S :    66   68   69   70   71   76   79
            INDEPENDENT D'S :     1    2    3    8    9   11   12   13
14   15

        NUMBER OF FREE PARAMETERS =  68
        NUMBER OF FIXED NONZERO PARAMETERS =  50

 *** WARNING MESSAGES ABOVE, IF ANY, REFER TO THE MODEL PROVIDED.
     CALCULATIONS FOR INDEPENDENCE MODEL NOW BEGIN.
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 *** WARNING MESSAGES ABOVE, IF ANY, REFER TO INDEPENDENCE MODEL.
     CALCULATIONS FOR USER'S MODEL NOW BEGIN.


  3RD STAGE OF COMPUTATION REQUIRED   1690188 WORDS OF MEMORY.
  PROGRAM ALLOCATED 200000000 WORDS

  DETERMINANT OF INPUT MATRIX IS    .13966D+09

 *** NOTE *** RESIDUAL-BASED STATISTICS CANNOT BE
              CALCULATED BECAUSE OF PIVOTING PROBLEMS.

  PARAMETER ESTIMATES APPEAR IN ORDER,
  NO SPECIAL PROBLEMS WERE ENCOUNTERED DURING OPTIMIZATION.


  RESIDUAL COVARIANCE MATRIX  (S-SIGMA) :
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| | | P.1.1 V1 | P.1.2 V2 | P.1.3 V3 | P.1.5 V5 | P.1.6 V6 |
|---|---|---|---|---|---|---|
| P.1.1 | V1 | .000 | | | | |
| P.1.2 | V2 | .334 | .000 | | | |
| P.1.3 | V3 | -.299 | -.159 | .000 | | |
| P.1.5 | V5 | .379 | -.122 | .039 | .000 | |
| P.1.6 | V6 | -.081 | .114 | -.136 | .000 | .000 |
| P.1.8 | V8 | -.157 | -.107 | .461 | -.783 | -.161 |
| P.1.10 | V10 | .056 | .107 | .525 | .282 | -.443 |
| P.1.11 | V11 | -.178 | -.118 | .059 | .163 | .428 |
| P.1.16 | V16 | -.425 | -.130 | .094 | .022 | -.119 |
| P.1.17 | V17 | -.507 | -.281 | .092 | .658 | .375 |
| P.4.1 | V36 | -.334 | .423 | -.146 | -.708 | -.353 |
| P.4.2 | V37 | .148 | .608 | .324 | -.226 | .353 |
| P.4.3 | V38 | -.022 | .575 | -.076 | -.289 | .380 |
| P.4.4 | V39 | .259 | .514 | .013 | -.252 | .443 |
| P.4.7 | V42 | -.496 | .195 | .114 | -.954 | -.537 |
| P.4.8 | V43 | .045 | .872 | .512 | -.376 | -.098 |
| P.4.9 | V44 | -.614 | .059 | -.036 | -.598 | -.439 |
| P.4.10 | V45 | -.229 | .253 | .171 | -.314 | .402 |
| P.9.3 | V59 | -.221 | .070 | -.053 | -.116 | .106 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.9.9 | V65 | .328 | .517 | .619 | -.347 | .294 |
| P.9.10 | V66 | .025 | .004 | -.025 | -.213 | .203 |
| P.9.12 | V68 | -.219 | -.237 | -.076 | -.429 | .311 |
| P.9.13 | V69 | -.154 | .125 | .301 | -.285 | .388 |
| P.9.14 | V70 | -.350 | -.214 | .391 | -.155 | -.148 |
| P.9.15 | V71 | -.232 | .073 | .192 | -.020 | .134 |
| LOGANTIG | V76 | .164 | .080 | .030 | -.062 | -.113 |
| LOGTAMA | V79 | .214 | .070 | -.027 | -.058 | -.002 |

| | | P.1.8<br>V8 | P.1.10<br>V10 | P.1.11<br>V11 | P.1.16<br>V16 | P.1.17<br>V17 |
|---|---|---|---|---|---|---|
| P.1.8 | V8 | .000 | | | | |
| P.1.10 | V10 | -.563 | .000 | | | |
| P.1.11 | V11 | .603 | .291 | .000 | | |
| P.1.16 | V16 | .027 | -.090 | -.009 | .000 | |
| P.1.17 | V17 | -.448 | -.156 | -.283 | .217 | .000 |
| P.4.1 | V36 | .547 | -.279 | .437 | -.160 | .319 |
| P.4.2 | V37 | .906 | -.041 | .039 | -.345 | .151 |
| P.4.3 | V38 | .931 | -.464 | .397 | -.203 | .308 |
| P.4.4 | V39 | 1.055 | -.439 | .638 | -.318 | .159 |
| P.4.7 | V42 | .262 | -.710 | .293 | -.370 | -.034 |
| P.4.8 | V43 | .379 | -.498 | .696 | -.211 | .512 |
| P.4.9 | V44 | .278 | -1.186 | .241 | -.005 | .436 |
| P.4.10 | V45 | .797 | -.835 | .137 | .012 | .583 |
| P.9.3 | V59 | .037 | -.064 | .234 | .089 | -.056 |
| P.9.9 | V65 | .980 | -.166 | .391 | .454 | .224 |
| P.9.10 | V66 | .591 | -.383 | .173 | -.397 | .078 |
| P.9.12 | V68 | .230 | -.539 | .078 | -.227 | .067 |
| P.9.13 | V69 | .377 | -.571 | .243 | -.224 | .485 |
| P.9.14 | V70 | .454 | .225 | .301 | -.030 | -.159 |
| P.9.15 | V71 | .313 | -.460 | .652 | .366 | -.173 |
| LOGANTIG | V76 | -.105 | .083 | -.139 | .008 | -.003 |

| | | | | | | |
|---|---|---|---|---|---|---|
| LOGTAMA | V79 | .004 | -.104 | -.148 | .003 | .006 |

| | | P.4.1 V36 | P.4.2 V37 | P.4.3 V38 | P.4.4 V39 | P.4.7 V42 |
|---|---|---|---|---|---|---|
| P.4.1 | V36 | .000 | | | | |
| P.4.2 | V37 | .073 | .000 | | | |
| P.4.3 | V38 | .001 | .003 | .000 | | |
| P.4.4 | V39 | -.161 | -.026 | .014 | .000 | |
| P.4.7 | V42 | .002 | -.288 | -.435 | -.132 | .000 |
| P.4.8 | V43 | .375 | .089 | -.035 | .260 | .489 |
| P.4.9 | V44 | .158 | -.092 | -.053 | .329 | -.203 |
| P.4.10 | V45 | .452 | .304 | .215 | .345 | -.367 |
| P.9.3 | V59 | .032 | .036 | .162 | .263 | .175 |
| P.9.9 | V65 | .027 | .209 | .129 | .293 | .166 |
| P.9.10 | V66 | .307 | .134 | .025 | .479 | -.175 |
| P.9.12 | V68 | -.058 | -.070 | -.264 | .009 | .115 |
| P.9.13 | V69 | -.128 | .009 | -.154 | .190 | .273 |
| P.9.14 | V70 | -.262 | -.416 | -.548 | -.231 | .115 |
| P.9.15 | V71 | -.065 | -.249 | -.021 | .034 | .452 |
| LOGANTIG | V76 | -.055 | -.054 | -.089 | -.081 | -.163 |
| LOGTAMA | V79 | .175 | .063 | .061 | .091 | -.213 |

| | | P.4.8 V43 | P.4.9 V44 | P.4.10 V45 | P.9.3 V59 | P.9.9 V65 |
|---|---|---|---|---|---|---|
| P.4.8 | V43 | .000 | | | | |
| P.4.9 | V44 | -.176 | .000 | | | |
| P.4.10 | V45 | -.387 | .598 | .000 | | |
| P.9.3 | V59 | .264 | .076 | -.005 | .001 | |
| P.9.9 | V65 | -.197 | -.020 | .336 | .057 | .007 |
| P.9.10 | V66 | -.270 | -.217 | .031 | .113 | .008 |
| P.9.12 | V68 | -.003 | .026 | .228 | -.023 | -.045 |
| P.9.13 | V69 | .072 | .115 | .358 | -.075 | -.021 |
| P.9.14 | V70 | .037 | -.050 | -.016 | -.018 | -.071 |
| P.9.15 | V71 | .241 | .214 | .115 | .003 | .156 |
| LOGANTIG | V76 | -.077 | -.130 | -.148 | -.003 | -.006 |

| | | | | | | |
|---|---|---|---|---|---|---|
| LOGTAMA | V79 | -.066 | .021 | -.078 | -.088 | .071 |

| | | P.9.10 V66 | P.9.12 V68 | P.9.13 V69 | P.9.14 V70 | P.9.15 V71 |
|---|---|---|---|---|---|---|
| P.9.10 | V66 | .008 | | | | |
| P.9.12 | V68 | .028 | .006 | | | |
| P.9.13 | V69 | .050 | .006 | .007 | | |
| P.9.14 | V70 | .016 | .086 | .006 | .003 | |
| P.9.15 | V71 | -.151 | -.104 | -.158 | .027 | .002 |
| LOGANTIG | V76 | -.059 | -.045 | -.051 | -.019 | -.031 |
| LOGTAMA | V79 | .021 | -.044 | -.005 | -.050 | -.008 |

| | | LOGANTIG V76 | LOGTAMA V79 |
|---|---|---|---|
| LOGANTIG | V76 | .000 | |
| LOGTAMA | V79 | .000 | .000 |

AVERAGE ABSOLUTE COVARIANCE RESIDUALS = .2103

AVERAGE OFF-DIAGONAL ABSOLUTE COVARIANCE RESIDUALS = .2264



TITLE: Your EQS 6 Model

MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

STANDARDIZED RESIDUAL MATRIX:

| | | P.1.1 V1 | P.1.2 V2 | P.1.3 V3 | P.1.5 V5 | P.1.6 V6 |
|---|---|---|---|---|---|---|
| P.1.1 | V1 | .000 | | | | |
| P.1.2 | V2 | .040 | .000 | | | |
| P.1.3 | V3 | -.037 | -.021 | .000 | | |
| P.1.5 | V5 | .048 | -.017 | .005 | .000 | |
| P.1.6 | V6 | -.010 | .015 | -.018 | .000 | .000 |
| P.1.8 | V8 | -.020 | -.015 | .066 | -.114 | -.022 |
| P.1.10 | V10 | .006 | .013 | .067 | .037 | -.055 |
| P.1.11 | V11 | -.021 | -.015 | .008 | .021 | .053 |
| P.1.16 | V16 | -.053 | -.017 | .013 | .003 | -.016 |
| P.1.17 | V17 | -.065 | -.039 | .013 | .095 | .052 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.4.1 | V36 | -.046 | .062 | -.022 | -.109 | -.052 |
| P.4.2 | V37 | .021 | .092 | .050 | -.036 | .053 |
| P.4.3 | V38 | -.003 | .085 | -.012 | -.045 | .056 |
| P.4.4 | V39 | .036 | .076 | .002 | -.039 | .065 |
| P.4.7 | V42 | -.074 | .031 | .019 | -.159 | -.085 |
| P.4.8 | V43 | .007 | .138 | .083 | -.062 | -.015 |
| P.4.9 | V44 | -.087 | .009 | -.006 | -.095 | -.066 |
| P.4.10 | V45 | -.033 | .039 | .027 | -.051 | .062 |
| P.9.3 | V59 | -.070 | .023 | -.018 | -.041 | .036 |
| P.9.9 | V65 | .056 | .093 | .115 | -.066 | .053 |
| P.9.10 | V66 | .004 | .001 | -.005 | -.042 | .038 |
| P.9.12 | V68 | -.044 | -.050 | -.017 | -.096 | .066 |
| P.9.13 | V69 | -.027 | .023 | .058 | -.056 | .072 |
| P.9.14 | V70 | -.081 | -.053 | .099 | -.040 | -.036 |
| P.9.15 | V71 | -.053 | .018 | .048 | -.005 | .033 |
| LOGANTIG | V76 | .155 | .081 | .031 | -.066 | -.114 |
| LOGTAMA | V79 | .118 | .041 | -.016 | -.036 | -.001 |

| | | P.1.8 V8 | P.1.10 V10 | P.1.11 V11 | P.1.16 V16 | P.1.17 V17 |
|---|---|---|---|---|---|---|
| P.1.8 | V8 | .000 | | | | |
| P.1.10 | V10 | -.075 | .000 | | | |
| P.1.11 | V11 | .080 | .035 | .000 | | |
| P.1.16 | V16 | .004 | -.011 | -.001 | .000 | |
| P.1.17 | V17 | -.066 | -.021 | -.037 | .031 | .000 |
| P.4.1 | V36 | .086 | -.039 | .062 | -.024 | .050 |
| P.4.2 | V37 | .146 | -.006 | .006 | -.053 | .024 |
| P.4.3 | V38 | .148 | -.066 | .056 | -.031 | .049 |
| P.4.4 | V39 | .167 | -.062 | .090 | -.048 | .025 |
| P.4.7 | V42 | .045 | -.108 | .045 | -.060 | -.006 |
| P.4.8 | V43 | .064 | -.076 | .106 | -.034 | .086 |
| P.4.9 | V44 | .045 | -.173 | .035 | -.001 | .071 |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.4.10 | V45 | .132 | -.124 | .020 | .002 | .096 |
| P.9.3 | V59 | .013 | -.021 | .076 | .031 | -.020 |
| P.9.9 | V65 | .190 | -.029 | .068 | .084 | .043 |
| P.9.10 | V66 | .119 | -.069 | .031 | -.076 | .015 |
| P.9.12 | V68 | .053 | -.110 | .016 | -.049 | .015 |
| P.9.13 | V69 | .075 | -.102 | .043 | -.043 | .096 |
| P.9.14 | V70 | .120 | .053 | .071 | -.008 | -.042 |
| P.9.15 | V71 | .082 | -.109 | .154 | .092 | -.045 |
| LOGANTIG | V76 | -.114 | .080 | -.134 | .008 | -.004 |
| LOGTAMA | V79 | .003 | -.059 | -.084 | .002 | .004 |

| | | P.4.1 V36 | P.4.2 V37 | P.4.3 V38 | P.4.4 V39 | P.4.7 V42 |
|---|---|---|---|---|---|---|
| P.4.1 | V36 | .000 | | | | |
| P.4.2 | V37 | .013 | .000 | | | |
| P.4.3 | V38 | .000 | .001 | .000 | | |
| P.4.4 | V39 | -.027 | -.005 | .002 | .000 | |
| P.4.7 | V42 | .000 | -.053 | -.080 | -.024 | .000 |
| P.4.8 | V43 | .068 | .017 | -.006 | .047 | .095 |
| P.4.9 | V44 | .027 | -.016 | -.009 | .057 | -.038 |
| P.4.10 | V45 | .080 | .055 | .038 | .061 | -.070 |
| P.9.3 | V59 | .012 | .014 | .063 | .101 | .073 |
| P.9.9 | V65 | .006 | .044 | .027 | .060 | .037 |
| P.9.10 | V66 | .065 | .029 | .005 | .102 | -.040 |
| P.9.12 | V68 | -.014 | -.017 | -.065 | .002 | .030 |
| P.9.13 | V69 | -.027 | .002 | -.033 | .040 | .063 |
| P.9.14 | V70 | -.074 | -.120 | -.156 | -.065 | .035 |
| P.9.15 | V71 | -.018 | -.072 | -.006 | .009 | .137 |
| LOGANTIG | V76 | -.063 | -.064 | -.104 | -.094 | -.203 |
| LOGTAMA | V79 | .118 | .043 | .041 | .061 | -.155 |

| | | P.4.8 V43 | P.4.9 V44 | P.4.10 V45 | P.9.3 V59 | P.9.9 V65 |
|---|---|---|---|---|---|---|
| P.4.8 | V43 | .000 | | | | |

| | | | | | | |
|---|---|---|---|---|---|---|
| P.4.9 | V44 | -.033 | .000 | | | |
| P.4.10 | V45 | -.074 | .109 | .000 | | |
| P.9.3 | V59 | .109 | .030 | -.002 | .001 | |
| P.9.9 | V65 | -.044 | -.004 | .073 | .027 | .002 |
| P.9.10 | V66 | -.062 | -.048 | .007 | .056 | .002 |
| P.9.12 | V68 | -.001 | .006 | .058 | -.013 | -.013 |
| P.9.13 | V69 | .016 | .025 | .080 | -.037 | -.005 |
| P.9.14 | V70 | .011 | -.015 | -.005 | -.012 | -.024 |
| P.9.15 | V71 | .073 | .062 | .034 | .002 | .054 |
| LOGANTIG | V76 | -.095 | -.155 | -.179 | -.008 | -.009 |
| LOGTAMA | V79 | -.047 | .015 | -.055 | -.136 | .059 |

| | | P.9.10 V66 | P.9.12 V68 | P.9.13 V69 | P.9.14 V70 | P.9.15 V71 |
|---|---|---|---|---|---|---|
| P.9.10 | V66 | .002 | | | | |
| P.9.12 | V68 | .009 | .002 | | | |
| P.9.13 | V69 | .014 | .002 | .002 | | |
| P.9.14 | V70 | .006 | .035 | .002 | .002 | |
| P.9.15 | V71 | -.054 | -.042 | -.056 | .013 | .001 |
| LOGANTIG | V76 | -.087 | -.074 | -.074 | -.037 | -.060 |
| LOGTAMA | V79 | .018 | -.043 | -.004 | -.056 | -.009 |

| | | LOGANTIG V76 | LOGTAMA V79 |
|---|---|---|---|
| LOGANTIG | V76 | .000 | |
| LOGTAMA | V79 | .000 | .000 |

AVERAGE ABSOLUTE STANDARDIZED RESIDUALS = .0460

AVERAGE OFF-DIAGONAL ABSOLUTE STANDARDIZED RESIDUALS = .0495

LARGEST STANDARDIZED RESIDUALS:

| NO. | PARAMETER | ESTIMATE | NO. | PARAMETER | ESTIMATE |
|---|---|---|---|---|---|
| 1 | V76, V42 | -.203 | 11 | V71, V11 | .154 |
| 2 | V65, V8 | .190 | 12 | V38, V8 | .148 |
| 3 | V76, V45 | -.179 | 13 | V37, V8 | .146 |
| 4 | V44, V10 | -.173 | 14 | V43, V2 | .138 |
| 5 | V39, V8 | .167 | 15 | V71, V42 | .137 |
| 6 | V42, V5 | -.159 | 16 | V79, V59 | -.136 |
| 7 | V70, V38 | -.156 | 17 | V76, V11 | -.134 |

```
       8      V76, V1         .155      18      V45, V8          .132
       9      V76, V44       -.155      19      V45, V10        -.124
      10      V79, V42       -.155      20      V70, V8          .120


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)



  DISTRIBUTION OF STANDARDIZED RESIDUALS



     ----------------------------------------
     !                                      !
  200-                                      -
     !                    *                 !
     !                    *                 !
     !                    *                 !
     !                    *                 !          RANGE      FREQ
PERCENT
  150-                 *  *                 -
     !                 *  *                 !    1   -0.5  -   --        0
.00%
     !                 *  *                 !    2   -0.4  -  -0.5       0
.00%
     !                 *  *                 !    3   -0.3  -  -0.4       0
.00%
     !                 *  *                 !    4   -0.2  -  -0.3       1
.26%
  100-                 *  *                 -    5   -0.1  -  -0.2      19
5.03%
     !                 *  *                 !    6    0.0  -  -0.1     147
38.89%
     !                 *  *                 !    7    0.1  -   0.0     192
50.79%
     !                 *  *                 !    8    0.2  -   0.1      19
5.03%
     !                 *  *                 !    9    0.3  -   0.2       0
.00%
   50-                 *  *                 -    A    0.4  -   0.3       0
.00%
     !                 *  *                 !    B    0.5  -   0.4       0
.00%
     !                 *  *                 !    C     ++  -   0.5       0
.00%
     !              *  *  *  *              !    ------------------------
-------
     !              *  *  *  *              !          TOTAL      378
100.00%
     ----------------------------------------
        1  2  3  4  5  6  7  8  9  A  B  C      EACH "*" REPRESENTS 10
RESIDUALS
```

```
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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)



  GOODNESS OF FIT SUMMARY FOR METHOD = ML

  INDEPENDENCE MODEL CHI-SQUARE        =    3198.690 ON   353 DEGREES OF
FREEDOM

  INDEPENDENCE AIC =  2492.69008   INDEPENDENCE CAIC =  1032.75324
         MODEL AIC =  -122.69484          MODEL CAIC = -1404.79235

  CHI-SQUARE =      497.305 BASED ON     310 DEGREES OF FREEDOM
  PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS       .00000

  THE NORMAL THEORY RLS CHI-SQUARE FOR THIS ML SOLUTION IS
479.643.

  FIT INDICES
  -----------
  BENTLER-BONETT     NORMED FIT INDEX =      .845
  BENTLER-BONETT NON-NORMED FIT INDEX =      .925
  COMPARATIVE FIT INDEX (CFI)         =      .934
  BOLLEN   (IFI) FIT INDEX            =      .935
  MCDONALD (MFI) FIT INDEX            =      .576
  LISREL    GFI  FIT INDEX            =      .826
  LISREL   AGFI  FIT INDEX            =      .788
  ROOT MEAN-SQUARE RESIDUAL (RMR)     =      .298
  STANDARDIZED RMR                    =      .061
  ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .060
  90% CONFIDENCE INTERVAL OF RMSEA  (        .050,        .069)

  RELIABILITY COEFFICIENTS
  ------------------------
  CRONBACH'S ALPHA                    =      .902
  COEFFICIENT ALPHA FOR AN OPTIMAL SHORT SCALE                =      .909
  BASED ON 15 VARIABLES, ALL EXCEPT:
  P.1.1     P.1.2     P.1.3     P.1.5     P.1.6     P.1.8
  P.1.10    P.1.11    P.1.16    P.1.17    LOGANTIG  LOGTAMA
  RELIABILITY COEFFICIENT RHO         =      .953
  GREATEST LOWER BOUND RELIABILITY                            =      .977
  GLB RELIABILITY FOR AN OPTIMAL SHORT SCALE                  =      .978
  BASED ON 24 VARIABLES, ALL EXCEPT:
  P.1.16    P.1.17    LOGANTIG
  BENTLER'S DIMENSION-FREE LOWER BOUND RELIABILITY            =      .977
  SHAPIRO'S LOWER BOUND RELIABILITY FOR A WEIGHTED COMPOSITE  =      .984
  WEIGHTS THAT ACHIEVE SHAPIRO'S LOWER BOUND:
  P.1.1     P.1.2     P.1.3     P.1.5     P.1.6     P.1.8
      .137      .166      .142      .117      .153      .179
  P.1.10    P.1.11    P.1.16    P.1.17    P.4.1     P.4.2
      .062      .124      .097      .120      .241      .354
  P.4.3     P.4.4     P.4.7     P.4.8     P.4.9     P.4.10
      .382      .343      .206      .241      .255      .237
  P.9.3     P.9.9     P.9.10    P.9.12    P.9.13    P.9.14
```

```
    .092      .173      .183      .159      .176      .104
P.9.15    LOGANTIG  LOGTAMA
    .110     -.001      .043
```

GOODNESS OF FIT SUMMARY FOR METHOD = ROBUST

ROBUST INDEPENDENCE MODEL CHI-SQUARE = 3108.659 ON 353 DEGREES OF FREEDOM

INDEPENDENCE AIC = 2402.65943   INDEPENDENCE CAIC = 942.72258
MODEL AIC = -204.22236   MODEL CAIC = -1486.31988

SATORRA-BENTLER SCALED CHI-SQUARE = 415.7776 ON 310 DEGREES OF FREEDOM
PROBABILITY VALUE FOR THE CHI-SQUARE STATISTIC IS .00005

FIT INDICES
-----------

```
BENTLER-BONETT     NORMED FIT INDEX =      .866
BENTLER-BONETT NON-NORMED FIT INDEX =      .956
COMPARATIVE FIT INDEX (CFI)         =      .962
BOLLEN   (IFI) FIT INDEX            =      .962
MCDONALD (MFI) FIT INDEX            =      .733
ROOT MEAN-SQUARE ERROR OF APPROXIMATION (RMSEA)    =      .045
90% CONFIDENCE INTERVAL OF RMSEA  (        .033,        .056)
```

ITERATIVE SUMMARY

| ITERATION | PARAMETER ABS CHANGE | ALPHA | FUNCTION |
|---|---|---|---|
| 1 | 1.819615 | 1.00000 | 10.22562 |
| 2 | 1.839883 | .50000 | 8.86299 |
| 3 | 1.429651 | 1.00000 | 7.47440 |
| 4 | 1.403097 | 1.00000 | 5.89649 |
| 5 | .530076 | 1.00000 | 4.04444 |
| 6 | .097591 | 1.00000 | 3.15189 |
| 7 | .030631 | 1.00000 | 2.95604 |
| 8 | .009342 | 1.00000 | 2.94270 |
| 9 | .001675 | 1.00000 | 2.94264 |
| 10 | .000590 | 1.00000 | 2.94263 |

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MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
(ROBUST STATISTICS IN PARENTHESES)

```
P.1.1   =V1  =   1.000 F1    + 1.000 E1
```

```
P.1.2   =V2  =   1.003*F1    + 1.000 E2
                  .091
                11.023@
              (   .071)
              ( 14.153@

P.1.3   =V3  =    .965*F1    + 1.000 E3
                  .089
                10.882@
              (   .070)
              ( 13.743@

P.1.5   =V5  =   1.000 F3    + 1.000 E5



P.1.6   =V6  =    .826*F3    + 1.000 E6
                  .087
                 9.476@
              (   .075)
              ( 10.988@

P.1.8   =V8  =    .774*F1    + 1.000 E8
                  .087
                 8.921@
              (   .076)
              ( 10.225@

P.1.10  =V10 =   1.000 F2    + 1.000 E10



P.1.11  =V11 =   1.052*F2    + 1.000 E11
                  .155
                 6.774@
              (   .124)
              (  8.462@

P.1.16  =V16 =   1.108*F2    + 1.000 E16
                  .151
                 7.350@
              (   .119)
              (  9.289@

P.1.17  =V17 =    .999*F2    + 1.000 E17
                  .142
                 7.051@
              (   .127)
              (  7.866@
```

```
 P.4.1   =V36 =   1.000 F8    + 1.000 E36




 P.4.2   =V37 =   1.306*F8    + 1.000 E37
                   .109
                 11.981@
               (   .120)
               ( 10.903@


  MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
(CONTINUED)


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)
  (ROBUST STATISTICS IN PARENTHESES)

 P.4.3   =V38 =   1.358*F8    + 1.000 E38
                   .111
                 12.228@
               (   .127)
               ( 10.662@

 P.4.4   =V39 =   1.293*F8    + 1.000 E39
                   .111
                 11.601@
               (   .123)
               ( 10.494@

 P.4.7   =V42 =   1.000 F9    + 1.000 E42




 P.4.8   =V43 =   1.052*F9    + 1.000 E43
                   .082
                 12.852@
               (   .073)
               ( 14.497@

 P.4.9   =V44 =   1.094*F9    + 1.000 E44
                   .085
                 12.818@
               (   .079)
               ( 13.865@

 P.4.10  =V45 =    .971*F9    + 1.000 E45
                   .087
                 11.220@
               (   .081)
```

```
              ( 11.979@

 P.9.3   =V59 =    .588*F12   + 1.000 E59
                   .066
                  8.866@
              (    .083)
              (   7.073@

 P.9.9   =V65 =   1.000 F14   + 1.000 E65




 P.9.10  =V66 =   1.071*F14   + 1.000 E66
                   .091
                 11.798@
              (    .095)
              ( 11.322@

 P.9.12  =V68 =   1.000 F13   + 1.000 E68




 P.9.13  =V69 =   1.070*F13   + 1.000 E69
                   .078
                 13.755@
              (    .084)
              ( 12.750@

 P.9.14  =V70 =   1.000 F12   + 1.000 E70





  MEASUREMENT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
(CONTINUED)


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)
  (ROBUST STATISTICS IN PARENTHESES)

 P.9.15  =V71 =    .829*F12   + 1.000 E71
                   .091
                  9.115@
              (    .110)
              (   7.505@

 LOGANTIG=V76 =   1.000 F17   + 1.000 E76
```

```
 LOGTAMA =V79 =   1.000 F16   + 1.000 E79
```



```
  TITLE:    Your EQS 6 Model

  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  CONSTRUCT EQUATIONS WITH STANDARD ERRORS AND TEST STATISTICS
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.
  (ROBUST STATISTICS IN PARENTHESES)


    F1   =F1  =   1.000 F5    + 1.000 D1


    F2   =F2  =    .759*F5    + 1.000 D2
                   .118
                  6.452@
              (    .104)
              (   7.291@

    F3   =F3  =    .890*F5    + 1.000 D3
                   .113
                  7.842@
              (    .086)
              (  10.386@

    F8   =F8  =   1.000 F11   + 1.000 D8


    F9   =F9  =   1.415*F11   + 1.000 D9
                   .280
                  5.061@
              (    .255)
              (   5.556@

    F11  =F11 =    .200*F5    + 1.000 D11
                   .061
                  3.249@
              (    .064)
              (   3.134@
```

```
    F12  =F12 =   1.000 F15   + 1.000 D12




    F13  =F13 =   1.308*F15   + 1.000 D13
                   .157
                  8.353@
               (   .159)
               (  8.223@

    F14  =F14 =   1.466*F15   + 1.000 D14
                   .189
                  7.757@
               (   .224)
               (  6.535@

    F15  =F15 =    .499*F11   +  .025*F5    -  .010*F16   -  .057*F17
                   .113          .049          .149          .230
                  4.428@         .504         -.066         -.248
               (   .124)     (   .046)     (   .147)     (   .244)
               (  4.032@     (   .537)     (  -.067)     (  -.234)

                + 1.000 D15




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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES
  ----------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                V                                F
               ---                              ---
                              I F5  -   F5              4.393*I
                              I                          .895 I
                              I                         4.910@I
                              I                      (   .665)I
                              I                      (  6.607@I
                              I                               I
                              I F16 -   F16              .370*I
                              I                          .040 I
                              I                         9.192@I
                              I                      (   .051)I
                              I                      (  7.251@I
                              I                               I
                              I F17 -   F17              .126*I
                              I                          .014 I
```

```
                               I                          9.192@I
                               I                       (   .018)I
                               I                       (  7.177@I
                               I                                I

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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES
  ----------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                 E                                D
                ---                              ---
 E1  -P.1.1               3.552*I D1  -   F1                .872*I
                           .476 I                           .398 I
                          7.466@I                          2.192@I
                       (   .592)I                       (   .473)I
                       (  6.002@I                       (  1.844)I
                                I                                I
 E2  -P.1.2               2.468*I D2  -   F2                .735*I
                           .370 I                           .309 I
                          6.672@I                          2.377@I
                       (   .452)I                       (   .326)I
                       (  5.462@I                       (  2.255@I
                                I                                I
 E3  -P.1.3               2.457*I D3  -   F3               3.082*I
                           .359 I                           .680 I
                          6.854@I                          4.530@I
                       (   .442)I                       (   .706)I
                       (  5.560@I                       (  4.363@I
                                I                                I
 E5  -P.1.5                .484*I D8  -   F8               1.651*I
                           .537 I                           .377 I
                           .902 I                          4.377@I
                       (   .541)I                       (   .362)I
                       (   .896)I                       (  4.557@I
                                I                                I
 E6  -P.1.6               3.319*I D9  -   F9                .786*I
                           .513 I                           .431 I
                          6.471@I                          1.824 I
                       (   .632)I                       (   .495)I
                       (  5.255@I                       (  1.590)I
                                I                                I
 E8  -P.1.8               3.593*I D11 -   F11              1.143*I
                           .439 I                           .345 I
                          8.183@I                          3.314@I
                       (   .462)I                       (   .341)I
                       (  7.771@I                       (  3.352@I
                                I                                I
 E10 -P.1.10              5.111*I D12 -   F12               .561*I
                           .638 I                           .143 I
                          8.016@I                          3.912@I
                       (   .672)I                       (   .174)I
                       (  7.610@I                       (  3.216@I
                                I                                I
```

```
 E11 -P.1.11              4.830*I D13 -   F13              .763*I
                           .618 I                          .186 I
                          7.810@I                         4.102@I
                       (   .569)I                      (   .218)I
                       (  8.484@I                      (  3.500@I
                                I                               I
 E16 -P.1.16              3.399*I D14 -   F14              .491*I
                           .487 I                          .198 I
                          6.980@I                         2.477@I
                       (   .512)I                      (   .323)I
                       (  6.634@I                      (  1.522)I
                                I                               I
 E17 -P.1.17              3.558*I D15 -   F15              .635*I
                           .475 I                          .150 I
                          7.488@I                         4.224@I
                       (   .612)I                      (   .182)I
                       (  5.819@I                      (  3.481@I
                                I                               I
 E36 -P.4.1               3.004*I                               I
                           .338 I                               I
                          8.880@I                               I
                       (   .471)I                               I
                       (  6.378@I                               I
                                I                               I
 E37 -P.4.2                .606*I                               I
                           .100 I                               I
                          6.077@I                               I
                       (   .187)I                               I
                       (  3.244@I                               I
                                I                               I
```

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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES (CONTINUED)
  ----------------------------------------------

 E38 -P.4.3                .374*I                               I
                           .089 I                               I
                          4.196@I                               I
                       (   .292)I                               I
                       (  1.282)I                               I
                                I                               I
 E39 -P.4.4                .978*I                               I
                           .131 I                               I
                          7.455@I                               I
                       (   .347)I                               I
                       (  2.821@I                               I
                                I                               I
 E42 -P.4.7               1.693*I                               I
                           .234 I                               I
                          7.224@I                               I
                       (   .273)I                               I
                       (  6.210@I                               I
                                I                               I
```

```
E43 -P.4.8                  1.365*I                                I
                             .211 I                                I
                            6.470@I                                I
                       (     .354)I                                I
                       (    3.854@I                                I
                                  I                                I
E44 -P.4.9                  1.498*I                                I
                             .230 I                                I
                            6.511@I                                I
                       (     .372)I                                I
                       (    4.026@I                                I
                                  I                                I
E45 -P.4.10                 2.146*I                                I
                             .277 I                                I
                            7.743@I                                I
                       (     .286)I                                I
                       (    7.502@I                                I
                                  I                                I
E59 -P.9.3                   .598*I                                I
                             .078 I                                I
                            7.627@I                                I
                       (     .097)I                                I
                       (    6.149@I                                I
                                  I                                I
E65 -P.9.9                  1.346*I                                I
                             .212 I                                I
                            6.343@I                                I
                       (     .375)I                                I
                       (    3.593@I                                I
                                  I                                I
E66 -P.9.10                  .685*I                                I
                             .191 I                                I
                            3.582@I                                I
                       (     .199)I                                I
                       (    3.441@I                                I
                                  I                                I
E68 -P.9.12                  .403*I                                I
                             .135 I                                I
                            2.984@I                                I
                       (     .186)I                                I
                       (    2.165@I                                I
                                  I                                I
E69 -P.9.13                  .904*I                                I
                             .176 I                                I
                            5.131@I                                I
                       (     .316)I                                I
                       (    2.864@I                                I
                                  I                                I
E70 -P.9.14                  .573*I                                I
                             .126 I                                I
                            4.552@I                                I
                       (     .195)I                                I
                       (    2.937@I                                I
                                  I                                I
```

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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  VARIANCES OF INDEPENDENT VARIABLES (CONTINUED)
  ----------------------------------------------

 E71 -P.9.15             1.073*I                                I
                          .144 I                                I
                         7.440@I                                I
                      (   .281)I                                I
                      (  3.822@I                                I
                               I                                I


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  COVARIANCES AMONG INDEPENDENT VARIABLES
  ---------------------------------------
  STATISTICS SIGNIFICANT AT THE 5% LEVEL ARE MARKED WITH @.

                V                                F
               ---                              ---
                               I F16 -   F16              .558*I
                               I F5  -   F5               .123 I
                               I                         4.543@I
                               I                      (   .115)I
                               I                      (  4.859@I
                               I                               I
                               I F17 -   F17              .155*I
                               I F5  -   F5               .065 I
                               I                         2.397@I
                               I                      (   .058)I
                               I                      (  2.692@I
                               I                               I
                               I F17 -   F17              .096*I
                               I F16 -   F16              .018 I
                               I                         5.276@I
                               I                      (   .019)I
                               I                      (  5.136@I
                               I                               I


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)


  STANDARDIZED SOLUTION:                                                  R-
SQUARED
```

```
 P.1.1   =V1  =   .773 F1    + .635 E1
.597
 P.1.2   =V2  =   .826*F1    + .564 E2
.682
 P.1.3   =V3  =   .816*F1    + .578 E3
.666
 P.1.5   =V5  =   .965 F3    + .262 E5
.931
 P.1.6   =V6  =   .758*F3    + .653 E6
.574
 P.1.8   =V8  =   .684*F1    + .730 E8
.467
 P.1.10  =V10 =   .624 F2    + .781 E10
.390
 P.1.11  =V11 =   .654*F2    + .756 E11
.428
 P.1.16  =V16 =   .736*F2    + .677 E16
.541
 P.1.17  =V17 =   .691*F2    + .722 E17
.478
 P.4.1   =V36 =   .705 F8    + .709 E36
.497
 P.4.2   =V37 =   .945*F8    + .327 E37
.893
 P.4.3   =V38 =   .968*F8    + .253 E38
.936
 P.4.4   =V39 =   .914*F8    + .406 E39
.835
 P.4.7   =V42 =   .818 F9    + .575 E42
.669
 P.4.8   =V43 =   .858*F9    + .514 E43
.735
 P.4.9   =V44 =   .856*F9    + .517 E44
.732
 P.4.10  =V45 =   .775*F9    + .632 E45
.601
 P.9.3   =V59 =   .687*F12   + .727 E59
.472
 P.9.9   =V65 =   .812 F14   + .584 E65
.659
 P.9.10  =V66 =   .902*F14   + .432 E66
.814
 P.9.12  =V68 =   .927 F13   + .376 E68
.859
 P.9.13  =V69 =   .870*F13   + .494 E69
.756
 P.9.14  =V70 =   .854 F12   + .520 E70
.730
 P.9.15  =V71 =   .705*F12   + .709 E71
.497
 LOGANTIG=V76 =  1.000 F17   + .000 E76
1.000
 LOGTAMA =V79 =  1.000 F16   + .000 E79
1.000
    F1   =F1  =   .913 F5    + .407 D1
.834
    F2   =F2  =   .880*F5    + .475 D2
.775
```

```
    F3   =F3  =   .728*F5    + .685 D3
.530
    F8   =F8  =   .666 F11   + .746 D8
.444
    F9   =F9  =   .878*F11   + .479 D9
.770
    F11  =F11 =   .365*F5    + .931 D11
.133
    F12  =F12 =   .798 F15   + .602 D12
.637
    F13  =F13 =   .830*F15   + .558 D13
.688
    F14  =F14 =   .901*F15   + .434 D14
.812
    F15  =F15 =   .578*F11   + .052*F5    - .006*F16   - .020*F17
                + .803 D15
.356


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  MAXIMUM LIKELIHOOD SOLUTION (NORMAL DISTRIBUTION THEORY)

  CORRELATIONS AMONG INDEPENDENT VARIABLES
  ---------------------------------------

                 V                                F
                ---                              ---
                               I F16 -   F16               .438*I
                               I F5  -   F5                     I
                               I                                I
                               I F17 -   F17               .208*I
                               I F5  -   F5                     I
                               I                                I
                               I F17 -   F17               .444*I
                               I F16 -   F16                    I
                               I                                I


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                           E N D    O F    M E T H O D
 -------------------------------------------------------------------------
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1
  Execution begins at 17:43:08
  Execution ends   at 17:43:10
  Elapsed time =       2.00 seconds
```